

Analysis of the interaction between liquid tin and austenitic steels, nickel-based alloys as well as protective surface layers at high temperature

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Liquid tin



- Application as a heat transfer medium
 - □ Large liquid temperature range 232 2620 °C
 - □ High heat flux
 - Not volatile or toxic
- □ Corrosion of metallic materials
 - Solution of alloying elements
 - Formation of intermetallic phases with Sn (stannides)
- Compatible materials
 - Rhenium, tungsten, quartz-glass, ceramics, graphite
- □ Alternative
 - Protective surface layers on steels or Ni-based alloys

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Experimental Furnace chamber Gas cavity Sample Tube Door Thermocouple Crucible 52 mm Γ5 TЗ Gas cavity 80 mm Plugs Liquid tin ٢6 Tin filled tubular samples Ø20 mm Ø25 mm □ Austenitic steels (1.4301, 1.4571) at 500 and 700 °C 36 mm Ni-based alloys (2,4642, 2.4650, 2.4663) at 700 and 1000 °C 38 mm Procedure Testing at 500, 700 and 1000 °C for 25, 50 und 100 h Formation of surface layers by gas-phase processes and PVD Post-test analysis Measurement of material loss OM, REM, EDX and XRD Analysis of the interaction between liquid tin and austenitic steels, nickel-based alloys Institute for Applied Materials-3 as well as protective surface layers at high temperature Applied Materials Physics (IAM-AWP) Lausanne, 11.07.2016

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Corrosion by liquid tin





1.4571 at 700 °C for 25 h



2.4663 at 700 °C for 25 h

Steels and Ni-based alloys

- Solution of alloying elements, especially Ni
- Penetration by Sn
- \Box Cr, Fe and Mo form α -, σ or similar phases
- Steels formation of stannide layers
- Stannides allow solutes to re-precipitate in case of local saturation of the melt

Material losses

- □ Steels at 500 °C: 40 µm after 100 h
- □ Steels at 700 °C: 150 µm after 100 h
- □ Ni-based alloys at 700 °C: 1100 µm after 50 h
- Ni-based alloys at 1000 °C: 2500 µm after 25 h

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Surface layers





1.4571 at 700 °C for 100 h

Low pressure carburisation

- □ At 1000 °C in propane
- Internal carbides instead of layer
- □ No significant reduction of corrosion at 700 °C



1.4571 at 700 °C for 100 h

- □ High temperature gas oxidation
 - □ At 800 °C in flowing Ar
 - Continuous oxide layers
 - Oxide layers partially dissolved
 - □ Local protection of alloy at 700 °C

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Surface layers





1.4571 at 700 °C for 100 h



2.4642 at 700 °C for 100 h

□ High temperature gas nitration

- □ At 800 °C in flowing N₂
- Continuous Cr-nitride layers
- □ 1.4571 sample mainly protected (700 °C,100 h)
- Local penetration by Sn through defects
- Cr-nitride layers on 2.4642 were transformed into (AI, Ti)-nitrides

Surface layers





2.4663 at 700 °C for 50 h

Physical vapor deposition

- □ 5 µm thick layers of TiC and TiN on 2.4663
- Layer defects formed, likely due to different
 - thermal expansion than substrate
- Penetration by Sn through defects
- No transformation of TiC and TiN observed

Conclusions



Corrosion

- Dense protective surface layers necessary to prevent solution of alloying elements, especially leaching of Ni
- □ Short grace periods, especially at 1000 °C
- Precise corrosion monitoring necessary

Oxides

- Thick layers necessary for longer durability
- Stabilisation by oxygen content in melt

Nitrides

- □ Improvement of process to ensure layer continuity
- Alloys with higher alloying content of AI or Ti than Cr

PVD

Multi-layer, or gradually structured layers to compensate thermal expansion difference



Thank you for your attention!

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