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# Criteria and geological setting for the generic geothermal underground research laboratory, GEOLAB

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## Abstract

High flow rate injection and related hydromechanical interaction are the most important factors in reservoir development of Enhanced Geothermal Systems (EGS). GeoLaB, a new generic geothermal underground research laboratory (URL), is proposed for controlled high flow rate experiments (CHFE) to address limited comprehension of coupled processes connected to EGS reservoir flow conditions. As analogue for typical EGS development, CHFE require specific hydromechanical conditions including a connected fracture network in crystalline basement rock, sufficient hydraulic fracture transmissivities, a strike-slip to normal faulting tectonic regime, controllable hydraulic boundary conditions, and hydrothermal alteration fracture fillings that improve conditions for hydromechanical interaction. With the aim to identify most appropriate areas for future site selection, four criteria have been established based on the EGS reference site of Soultz. Two URLs in crystalline basement worldwide approximate the requirements of a new generic GeoLaB and may be used for accompanying experimentation. Besides favourable geological, hydraulic, and stress conditions, the vicinity to long-term EGS production favours the southern Black Forest as potential region for GeoLaB. Therefore, an exemplary site assessment has been carried out at “Wilhelminenstollen” in the southern Black Forest (Germany). New remote sensing, hydrochemical, and geophysical analyses as well as reactivation potential, and stress modelling were added to complement existing geological and hydrogeological information. At this site, reactivation potential analysis reveals two local maxima prone for shear reactivation as strike-slip faults. The highest lineament density is observed for the N110°E strike direction that is associated with both slip and dilation tendency maxima. Clay minerals occur in fractures and the matrix. Local, partly water-bearing fractures, when partly filled with ore minerals, were connected to veins in the tunnel using shallow geophysical methods. Hydrochemical data reveal infiltration of the tunnel water from at least 500 m above the tunnel. The results suggest a crystalline basement with a fracture network that is regionally connected and water-conducting. Hydraulic conductivity in the southern Black Forest granite is estimated to amount to about  $4.5 \cdot 10^{-8} \text{ m s}^{-1}$  at 500 m depth. The hydraulic boundary conditions exclude unknown drainage. Analyses of the influence of topography on orientation and magnitude of the maximum stress indicate a minimum overburden of about 500 m for regional reactivation to be valid. In conclusion, the southern Black Forest and in particular “Wilhelminenstollen” offers favourable condition for CHFE. Final decision on the GeoLaB site is to be drawn from forthcoming exploration wells.

**Keywords:** Geothermal underground research laboratory, Fractured crystalline basement, Black forest, GeoLaB

## Background

Most geothermal resources worldwide are found in fractured crystalline basement and may be approached using enhanced geothermal systems (EGS) technology (e.g. MIT 2006). This technology dates back to the 1970s, when first hot dry rock (HDR) projects led to the design of artificial sub-surface heat exchangers in crystalline basement rock. The outcome of the Fenton Hill HDR experiment (1970–1995, Los Alamos National Laboratory, USA) was the identification of the hydraulic challenges related to reservoir creation (Brown 2009). Reservoir testing and development revealed that the characteristics of the crystalline basement appear to be highly variable. Some of the related questions have been addressed along the EGS learning curve, particularly at the Soultz-sous-Forêts EGS site and during its follow-up projects. With regard to productivity enhancement of fractured granitic basement, different injection schemes and operation modes have been tested and validated with respect to their efficiency (Nami et al. 2008; Schill et al. 2015). Cyclic injection along with production from a second well has been found to be most effective for reservoir development (Schindler et al. 2010; Schill et al. 2015). Due to perceptible induced seismicity, however, the deep reservoir at Soultz has mainly been treated chemically in the late stage of the development phase. During operation of the Soultz power plant, occurrence of induced seismicity was reduced in frequency and magnitude by distributing the injected volume over different injection points and limiting the overall flow rate (Cuenot et al. 2011). Still, high flowrate injection is a crucial issue for large-scale industrial development and economic viability of EGS.

As such, current EGS development for controlled enhancement of the reservoir is hindered by fundamental understanding of processes occurring at high volumes and rates of flow in fractured reservoir rocks. Additional complexity results among others from high differential stresses, the related mechanical behaviour, and the chemical response of the fluid. Although experimental progress has been made, fundamental constitutive laws of flow and thermo-hydraulic-mechanical-chemical (THMC) coupling presently are not being considered adequately in reservoir engineering and plant operation in fractured environments. It is, therefore, most important to carry out large-scale in situ tests under hydrogeological conditions and comprehensively study these aspects (Freeze and Javandel 2008).

## Necessity for real-scale experiments

Brady and Brown (2006) detail five inherent complexities in rock mechanical investigation: (1) fracture mechanics, (2) scale effects, (3) tensile strength, (4) fluid interaction, and (5) alteration. Although being established already 20 years ago these are still most important mechanics topics and remain key aspects in characterising the mechanical influence in a reservoir. They involve especially the bias in evaluation of laboratory and field data in terms of the natural complexity of heterogeneity of the host rock but also of the complexity flow pathways. Out of a large assessment, two aspects may be picked out to describe the need for research in a reservoir simulator.

Scale effects are a well-known limitation in describing mechanical processes in subsurface rock since they may exhibit tremendous changes in strength when varying the sample sizes under laboratory conditions. Peak strength of rock, a key parameter separating the linear from the failure regime (i.e. involving possible seismicity), is highly dependent

of rock sample size. Barton et al. (1985) have identified variabilities by more than 50 % by direct shear test with smaller sample sizes involving considerably higher peak strength than larger samples.

The origin of wing-crack mechanisms and their evolution within a shear zone during a stimulation as proposed by Jung (2013) addresses another challenge in reservoir simulation rarely performed in rock mechanics due to not existent opportunities. It involves the creation of new void spaces by the injection of large fluid volumes. Identical mechanisms to wing-cracks in structural geology are proposed when injecting large amounts of fluid in host rock. Under a given stress regime, wing-cracks within a shear zone could connect consecutively in a shear zone until forming tensile fractures.

Besides mechanical interaction, hydraulic effects from high reservoir flow rates need to be studied more in detail to investigate the range of validity for the typically assumed Darcy flow and fluid dynamics need to be carefully evaluated. Zimmerman and Yeo (2000) have shown that the Stokes equations for laminar flow leave their range of validity from  $Re > 10$  and new Navier–Stokes solvers need to be applied. In a heterogeneous network with tube-like structures at the interface of fractures (Wennberg et al. 2016) these conditions are easily met and apparent transmissivity decreases with higher flowrate. Until now, there are ample theoretical and numerical considerations of the flow behaviour in fractured rock; however, little was done to quantify these effects in laboratories or under real field conditions (Kohl et al. 1997).

The implications on hydraulic field and rupture mechanisms are obvious and can be easily extended to thermal and chemical impacts. Therewith, injection in fractured reservoirs can include a high variety of interactions induced from hydraulic fields (Gaucher et al. 2015), known as THMC for thermal, hydraulic, mechanical, and chemical interaction (Kolditz et al. 2012). It is most important to address these questions during large-scale observation to calibrate coupled mechanical models also from real experimental testing under reservoir condition. Providing the specific experimental background going beyond the expertise from nuclear research and applying new probabilistic based approaches are important perspectives for reservoir engineering. Careful analyses of probabilistic response spectra together with geological structural analysis resulting in new hydraulic calibration parameters of fracture network models under variable flow rate can only be performed in a 3D environment where processes are monitored in space and time. In this context, underground research laboratories (URLs) are best suited to monitor and quantify the interrelated processes during large volume injection in fractured rock by large-scale in situ observational methods to complement present-day laboratory-scale experiments. Such experimental facilities for application and monitoring of experiments should address key aspects of a safe and economically efficient use of geothermal energy.

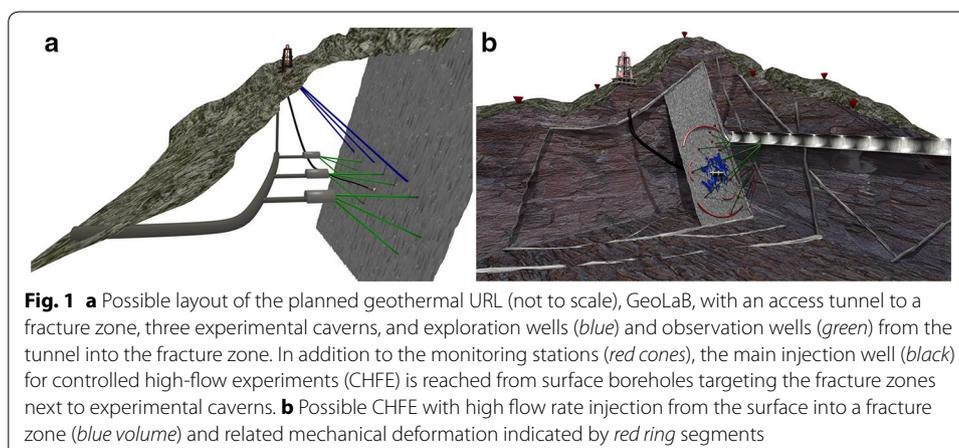
#### **Experiments in a geothermal URL**

In-line with related geo-disciplines, such as nuclear waste disposal research, we propose a specific URL for geothermal purposes, which is to be located in a typical EGS environment to conduct fundamental experiments in space and time (i.e. 4D). As pointed out by NEA (2013) for nuclear waste disposal research, URLs offer an excellent opportunity to integrate multiple disciplines (e.g. geology, hydrology, and engineering), build

technical teams, and gain practical experience that will be invaluable for the next generation of researchers. Decision-making requires practical demonstrations of key technical elements to prove the robustness of the proposed concept as well as to establish confidence in the technology. URLs play an important and multi-faceted role in these scientific assessments and demonstrations, since they provide a realistic environment for characterising and testing the selected technical approaches and materials. In areas of operational safety, acquiring geological information on the repository scale, and constructional and operational feasibility, only URLs can provide reliable in situ data. URLs can also provide tangible benefits in enhancing participation by the general scientific community and confidence of both technical and non-technical stakeholders. The many successful URLs operated for other research purposes reflect their high value.

The 4D controlled high flow rate experiments (CHFEE) in a geothermal URL may address the validity of fundamental flow and hydro-mechanical laws in fractured rock, i.e. on surfaces of variable roughness and tortuosity, and shall provide new insights into the relevant petrophysical, hydrogeological, and mechanical processes in space and time. A typical experiment may include fluid injection into an appropriate fracture zone underneath the URL (Fig. 1). Measurement devices in observation wells and on the surface enable full 3D process monitoring and can be adapted to different experiments and scientific purposes. Furthermore, the URL may provide access to a modified surface for further investigation. A schematic setting of the planned geothermal URL, GeoLaB, is shown in Fig. 1. Our concept of such an infrastructure facility includes a 1–2 km long tunnel with 3–4 side caverns, from which the CHFEEs and other key experiments can be performed (Fig. 1b).

In order to prepare the site selection for GeoLaB, in this study, we establish criteria for a generic geothermal URL for CHFEE. Applying these criteria to existing URLs, we demonstrate the necessity for a new generic URL. Based on these results, the Southern Black Forest appears to reveal appropriate conditions and is selected for further investigation. Furthermore, the study includes a review of suitable existing mines in the Black Forest. Since it is crucial to install the GeoLaB in an environment close to hydraulic reservoir conditions, the detailed planning concept needs to follow the tectonic setting in the adjacent rock. Especially, the structure of the target fault zone imposes boundary



conditions on URL construction and the installation of tools to achieve the scientific targets. In this study, we describe an exploration procedure aiming at the characterisation of a fault zone in a target rock that is predestined for geothermal production in central Europe. In this respect, a case exploration study is carried out at “Wilhelminenstollen” in the southern Black Forest, assuming an extension of existing mining structures for construction of a geothermal URL. Based on the results the necessary exploration steps towards a test site in the Variscan crystalline rock are detailed.

### **Criteria for a generic geothermal URL**

In analogy to the procedure chosen in nuclear waste disposal research, it is distinguished between “generic” scientific investigations in analogue URLs and “site-specific” geothermal URLs linked to a real operation (NEA 2013). In geothermal research, site-specific investigations are to be conducted under real conditions in the deep subsurface using tomographic approaches between geothermal wells (e.g. DOE FORGE project, <http://www.energy.gov/eere/forge>). Complementary, GeoLaB is intended to be developed as generic URL to gain general experience with respect to geological, physical, and chemical processes under high flow rate conditions, including model testing and verification of investigation and measurement techniques and to identify process interactions by means of experiments. Generic URLs are to be installed in the host rock type, but not in the particular geological formation. Although closely mimicking hydraulic or geological reservoir conditions, generic geothermal URLs are not able to reproduce parameters, such as temperature, stress magnitude, and geochemistry in a specifically selected host rock formation.

A geothermal URL designed for CHFE is associated with specific requirements on hydraulic and geological properties of typical EGS reservoirs and, hence, on the GeoLaB site. EGS technology is best studied in the Upper Rhine Graben (URG). This accounts for the Soultz project, the unique proto-type of EGS, in particular, since nowhere else worldwide so many hydromechanical stimulation experiments of different type have been accomplished. Lithologic, hydraulic, and stress conditions in a geothermal URL should thus be comparable to conditions encountered there, but also be transferrable to the crystalline basement of Central Europe and worldwide. Note that URG’s host rocks are exposed in the adjacent low mountain ranges. Against this background, we aim at installing GeoLaB at a site approximating Soultz condition to reduce the number of degrees of freedom when comparing results of CHFE to reservoir experiments. Furthermore, since only few developed EGS sites exist worldwide, the definition of a typical EGS environment is based on the theoretical considerations of Garnish (2002) and the Soultz-sous-Forêts EGS project.

### **EGS reference Soultz-sous-Forêts**

The Soultz site is located in the southern part of the URG’s thermal anomalies (Baillieux et al. 2013). The reservoir in Soultz comprises two different granite varieties:

- a porphyritic K-feldspar monzogranite (from 1420 to 4700 m) with a highly altered and fractured intermediate section (between about 2700 and 3900 m) having a fracture densities of up to  $2.86 \text{ m}^{-1}$  for fractures with an acoustic aperture of  $>1\text{--}2 \text{ mm}$  is

observed in the upper part (Genter and Castaing 1997; Dezayes et al. 2005). A correlation between alteration zones and permeable fractures as well as an increased tendency to shear during stimulation was found for this section (e.g. Evans et al. 2005).

- In the lower part (from 4700 to 5000 m) a two-mica granite with fracture densities of up to  $1.97 \text{ m}^{-1}$  is observed (Dezayes et al. 2005).

In the granitic basement at the Soultz site, three reservoir levels have been developed at about 2000, 3500, and 5000 m depth. The different reservoirs fulfil most of the EGS criteria (Table 1) as defined by Garnish (2002). The upper reservoir extending from the top of the basement at 1420 m depth down to about 2000 m includes an approximately 100 m thick alteration zone at its top. This zone is mainly characterised by precipitated hematite, low magnetic susceptibility (Rummel and König 1991), high electric conductivity (Geiermann and Schill 2010), and high values of heat production of up to  $7 \mu\text{W m}^{-3}$  (Pribnow 2000). As regards reservoir engineering, at the Soultz site, about 35 major injection and production experiments have been carried out, during which different types of hydraulic and chemical stimulations were tested and evaluated for their effectiveness (Schill et al. 2015). Thus, Soultz can be considered a reference EGS site.

The production temperatures are higher than  $140 \text{ }^\circ\text{C}$ , the stimulated rock volume is larger than  $2 \cdot 10^8 \text{ m}^3$ , hydraulic impedance is lower than  $0.1 \text{ MPa kg}^{-1} \text{ s}^{-1}$  (in the wells GPK1 and GPK2), and the produced fluid can be re-injected to the complete extent. The effective heat exchange area has not been estimated. The crucial flow rate of  $50\text{--}100 \text{ L s}^{-1}$  was not reached in Soultz. On the contrary, it had to be reduced to about  $15 \text{ L s}^{-1}$  in 2013 (Schill et al. 2015). Overall hydraulic conductivity in the non-stimulated reservoirs ranges from  $1.2 \cdot 10^{-9} \text{ m s}^{-1}$  in the upper to  $2 \cdot 10^{-8} \text{ m s}^{-1}$  in the intermediate to  $<2 \cdot 10^{-9} \text{ m s}^{-1}$  in the deep reservoir. Separating the most permeable fracture at 3490 m depth from the test section reduces the hydraulic conductivity by one order of magnitude to about  $1 \cdot 10^{-9} \text{ m s}^{-1}$  in the intermediate reservoir (Jung et al. 1995). Hydraulic conductivities in the fractured zone between 2850 and 3100 m were determined to be

**Table 1 Requirements to be met by EGS according to Garnish (2002) and reservoir parameters of the Soultz-sous-Forêts EGS**

	EGS requirement	Soultz 3.5 km reservoir	Soultz 5 km reservoir
Flow rate ( $\text{L s}^{-1}$ )	50–100	24	23
Mean wellhead fluid temperature ( $^\circ\text{C}$ )	150–200	140	157.5
Effective heat exchange area	$>2 \cdot 10^6 \text{ m}^2$	N/A	N/A
Rock volume ( $\text{m}^3$ )	$>2 \cdot 10^8$	About $7 \cdot 10^8$	About $2.7 \cdot 10^9$
Hydraulic impedance	$<0.1 \text{ MPa L}^{-1} \text{ s}^{-1}$	$0.06 \text{ MPa L}^{-1} \text{ s}^{-1}$ (GPK1, injection) $0.06 \text{ MPa L}^{-1} \text{ s}^{-1}$ (GPK2, production)	$0.1 \text{ MPa L}^{-1} \text{ s}^{-1}$ (GPK1, injection) $0.05 \text{ MPa L}^{-1} \text{ s}^{-1}$ (GPK2, production) $0.25 \text{ MPa L}^{-1} \text{ s}^{-1}$ (GPK3, injection) $0.25 \text{ MPa L}^{-1} \text{ s}^{-1}$ (GPK4, production)
Water loss at the surface	$<10 \%$	0 % (Total reinjection)	0 % (Total reinjection)

Data from the 3500 and 5000 m reservoirs were obtained in 1997 and 2011, respectively (modified after Schill et al. 2015)

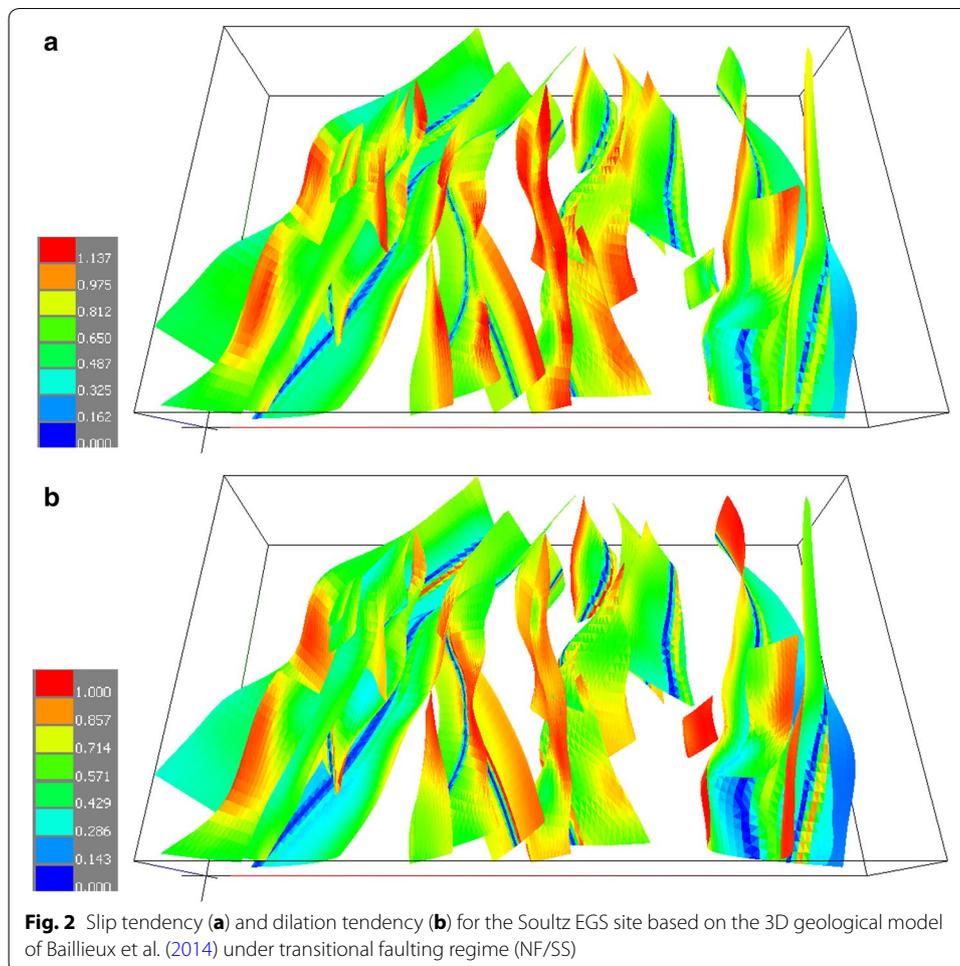
up to  $6 \cdot 10^{-8} \text{ m s}^{-1}$  (Sausse et al. 2006). The lower limit of hydraulic conductivity of the matrix is  $>10^{-11} \text{ m s}^{-1}$  (Rummel and König 1991).

During reservoir development, the factors determining the effectiveness of hydraulic stimulation are the injection volume, downhole pressure, flow rate, injection scheme, and the ambient stress field. The stress field at the Soultz site was determined using drilling-induced tensile fractures and borehole breakouts (Valley and Evans 2007) as well as additional seismic information (Cornet et al. 2007). Mean orientations of the maximum principal stress component ( $S_{H_{\max}}$ ) of  $169 \pm 14^\circ$  and  $175 \pm 10$  obtained by means of the respective methods. The stress field at Soultz is characterised by a transition from normal faulting (NF) to the strike slip regime (SS) at a depth of about 3200 m. In the NF regime of the upper and intermediate reservoirs, maximum slip tendency coincides with the orientation of  $S_{H_{\max}}$ , while maxima are forecast at conjugated angles of  $30^\circ$  to  $S_{H_{\max}}$  in the SS regime of the intermediate and deep reservoirs. With respect to the reactivation potential, these structural trends are most favourably oriented in the ambient state of stress (Fig. 2). Hence, they are supposed to control subsurface fluid flow and associated reservoir processes in Soultz.

The significance of such regional forecast for reservoir processes was verified by observations made during different hydraulic stimulation experiments. For example, the 00JUN30 stimulation of GPK2 well below the NF/SS transition zone (open hole section: 4402–5026 m) in June/July 2000 caused an overall seismic cloud comprising about 7200 single events. Maximum orientation of this cloud is oriented parallel to  $S_{H_{\max}}$  (Hettkamp et al. 2004). Although stress re-orientation close to fault zones is not taken into account, the distribution of the failure plane orientations (Fig. 3) follows the distribution expected on the basis of slip and dilation tendency analyses.

The geothermal reservoir at the Soultz site has experienced significant fracturing and complex alteration since Variscan times. The resulting distinct fracture networks provided pathways for hydrothermal fluids, thus enabling fluid-rock interactions between geothermal brines and reservoir rocks. Pervasive and localised vein alterations can be distinguished in the reservoir rocks. An early propylitic, weak iso-chemical alteration of the matrix without a change of the granite texture incorporates partial transformation of biotite and hornblende into chlorite, the replacement of plagioclase by illite, and the formation of hydrogarnet and epidote within the granite (Genter et al. 2000). A second alteration includes strong chemical and textural changes mainly within and in the immediate vicinity of fractures (Fig. 4). Alteration ranges from moderate to extreme grades (e.g. Meller et al. 2014). Typically, a brecciated and cataclased zone is observed between the protolith and a central, often-sealed quartz vein. Here, primary silicates, such as feldspar and biotite, were transformed into clay minerals, with the original texture of the granite being destroyed by shearing. The precipitation in veins contains secondary quartz, barite, illite, carbonates, iron oxides, and, locally, mixed-layers of illite–smectite and chlorite-smectite (Genter et al. 2000; Schleicher et al. 2006). In some altered zones, quartz, biotite, plagioclase, and hornblende are dissolved completely (Ledésert et al. 2010).

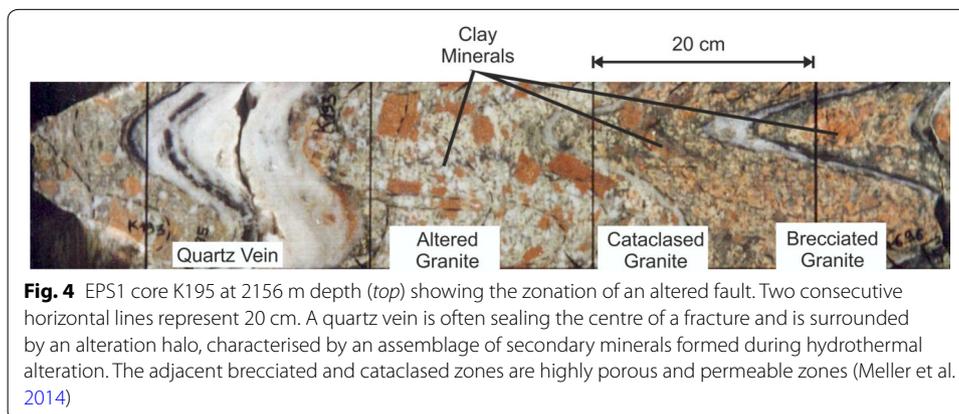
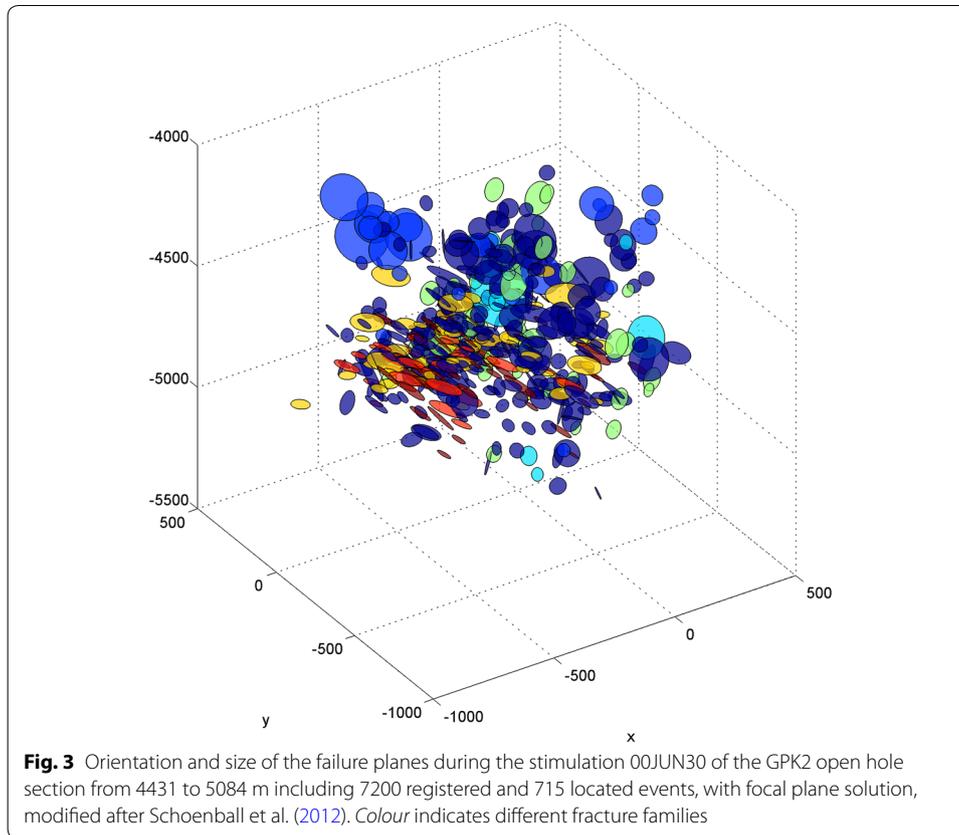
The average porosity of the fresh granite is  $<1\%$  (Genter et al. 2000). For hydrothermally altered samples, they determined porosities of 1.7–25 % (often higher than those of breccia and microbreccia) using mercury porosity measurements. The porosity of



altered plagioclase, which makes up to 40 % of the rock volume (Ledésert et al. 1999), is between 20 and 27 %.

Fracture apertures were determined using different techniques. Electric apertures obtained from azimuthal resistivity images range from about 1  $\mu\text{m}$  to 1 mm (Sausse and Genter 2005). Apertures for the upper reservoir were determined from three different core samples (Sausse 2002). Strongly altered granite with chlorite sealing (from 1557.8 m depth) revealed a mean aperture of  $0.448 \pm 0.101$  mm. Weakly altered granite with hematite sealing (from 1789.6 m depth) was found to have a mean aperture of  $0.518 \pm 0.257$  mm and unaltered granite with drilling-induced fractures (from 2075.46 m depth) had a mean aperture of  $0.748 \pm 0.101$  mm. An upper limit of apertures is given by the width of the fault-related damage and alteration zones (Massart et al. 2010). For the largest group of fractures with a mean lateral extension of about 2700 m, a mean width of damage/alteration zone of about 6 m of (with a maximum width of 13 m) was determined by analysing UBI logs. With decreasing fault size, the relation between extension and width follows a power-law distribution.

Mechanical weakening of rock in hydrothermal alteration zones and the influence of hydrothermally altered fluid pathways are significant for hydro-mechanical processes (e.g. Meller and Kohl 2014; Sausse 2002; Zoback et al. 2012). E-moduli of hydrothermally



altered granite samples, for example, are reduced from about 55 to 40 GPa compared to fresh rock samples (Valley and Evans 2007). Furthermore, a correlation between the occurrence of aseismic creep on fractures and the clay content (alteration grade) of fractures and between the cumulative occurrence of borehole breakouts and a high density of clay-filled fractures was observed. Moreover, the maximum magnitude of seismic events was observed to decrease with increasing clay content inside fractures. Evans et al. (2005) demonstrated that hydrothermally altered fractures can be enhanced best during stimulation. Thus, target candidates for geothermal exploration are fractures and

faults, which are (1) optimally oriented in the ambient stress state, (2) critically stressed for shear reactivation, and (3) show increased fluid conductivities due to alteration processes.

#### **Selection criteria for a geothermal URL**

Considering the relevant observations at Soultz and the controllable and specific boundary conditions required for the planned CHFES, a geothermal URL focusing on EGS should fulfil the following four selection criteria:

1. Complex geological boundary conditions are to be avoided. A rather homogenous crystalline matrix with a high density of connected and highly permeable natural fractures, i.e. a fracture network, provides optimal conditions for CHFES. In the engineered volume of Soultz with a vertical reservoir extension of about 3500 m, maximum mean fracture length and damage zone size are of about 2700 and 60 m, respectively (Massart et al. 2010). A realistic rock volume developed by an URL is  $\ll 2 \cdot 10^8 \text{ m}^3$  (Table 1), which is much smaller than the defined EGS reservoir size suggested by Garnish (2002). Hence, we may consider fracture densities on the order of  $2\text{--}3 \text{ m}^{-1}$  with major fault and fracture zone lengths on the order of  $<400\text{--}500 \text{ m}$  (Sausse et al. 2010). The width of these zones (including damage and alteration zones) is estimated to be on the order of up to  $<1\text{--}2 \text{ m}$  (Massart et al. 2010). The lower limit of the overall hydraulic conductivity is set by the initial hydraulic conductivities of the Soultz reservoirs, which range from about  $10^{-9}\text{--}10^{-8} \text{ m s}^{-1}$  and the lower bound of matrix conductivity of about  $>10^{-11} \text{ m s}^{-1}$ . Considering enhancement by stimulation (factor 10), we set this criterion to a hydraulic conductivity of  $>10^{-7}\text{--}10^{-6} \text{ m s}^{-1}$ . This is in agreement with the permeability estimated by Kohl et al. (2000) for the fracture zones at Soultz.
2. Controllable hydraulic boundary conditions cause CHFES to act on natural fractures or matrix, only. This is a pre-requisite for the validity of the CHFES and the follow-up numerical models. Extensive drainage to surrounding known or unknown adits that may occur in areas of historic mining activities must be excluded.
3. Hydrothermal alteration products in the matrix and along the faults are to cover the illite to smectite range. Clay minerals are known to reduce the mechanical/frictional strength of fractures, i.e. the pressure required to cause shear during hydraulic stimulation. The contribution of mechanically induced rock alteration should be small, because the profound disintegration of large volumes of rock (e.g. *grus*) results in hydraulic conditions, which are no longer controllable (e.g. in terms of discrete hydraulic pathways, discrimination between matrix and fault, often no symmetry of the fault structure).
4. In order to carry out CHFES, fractures that are favourably oriented for reactivation in the ambient stress field are an intrinsic pre-requisite of a geothermal URL. Since the stress field orientation across the European crystalline basement is highly variable, no specific stress field can be chosen, but a favourable reactivation potential has to be considered instead. Since the geothermal resources occur in normal or strike-slip regimes rather than thrust fault regimes, we may consider the latter as less favourable. Non-representative, atypical stress perturbation resulting from, e.g. the

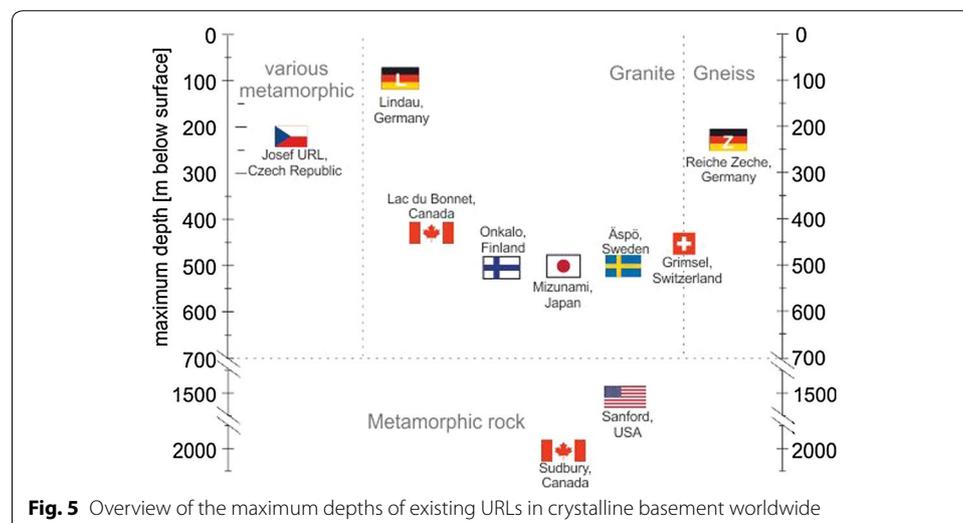
glacial rebound should be avoided. In mountain regions, significant perturbations of the regional stress field pattern by local topography need to be taken into account. To avoid such additional variation in the stress field that biases CHFES with respect to reservoir condition, for the URL design, it is strived for a maximum variation in magnitude of the principal stress of <10 %. Depending on the topography of a potential URL site, a minimum depth below terrain level has to be considered.

### URLs existing in the crystalline basement

A number of URLs worldwide have been installed in crystalline basement rock (Fig. 5; Table 2). Except for the Josef URL, which comprises a number of different lithologies also of sedimentary origin, the host rocks exhibit only few lithological changes across the individual URLs. Host rocks range from gneissic (e.g. in the Mine Reiche Zeche) to granitic basement. The fractures at the Lindau Test Site and the Mine Reiche Zeche are commonly filled with ore minerals (Himmelsbach et al. 1998; Bayer 1998).

In the following section, suitability of the existing URLs for CHFES will be discussed using the above four selection criteria. A compilation of the criteria for the URLs is given in Table 3. It should be noted that (1) the URL Lac du Bonnet is dismantled, (2) Onkalo is a site-specific URL for nuclear waste disposal and (3) the two URLs Sudbury and Sanford are not suitable for CHFES due to their sensitive instrumentation. All four URLs are, therefore, excluded from further consideration.

Criterion 1 is the crystalline lithology, including a well-connected fracture network and a high fracture transmissivity. Based on the minimum hydraulic conductivity range and the expected fracture apertures given above, for CHFES, URLs with fracture transmissivities in the range of  $>10^{-4} \text{ m}^2 \text{ s}^{-1}$  may be take into account. In Europe, such conditions are found in the Lindau Test Site and the Äspö Hard Rock Laboratory (HRL) and partly in the Mine Reiche Zeche (Table 2). Hydraulic testing revealed well-connected fracture networks at Äspö HRL and the Black Forest, in which the Lindau Test site is situated (Stanfors et al. 1999; Stober and Bucher 2014). At Grimsel, for instance, alpine tension fractures may have larger apertures and, hence, transmissivity, but are typically



**Table 2 Overview of general hydraulic conditions and secondary fracture fillings in selected URLs in the crystalline basement worldwide (e.g. Himmelsbach et al. 2003; Stanfors et al. 1999; Himmelsbach et al. 1998; Komulainen et al. 2014; Davison 1984; Kumazaki et al. 2003)**

Name	Hydraulic properties	Secondary minerals in fractures
Grimsel Test Site, Switzerland	MHC: $10^{-12}$ – $10^{-11}$ m s <sup>-1</sup>	Albite, epidote, muscovite, mica, chlorite, calcite
Äspö Hard Rock Laboratory, Sweden	FT: up to $10^{-10}$ – $10^{-5}$ m <sup>2</sup> s <sup>-1</sup>	CM: <10 % mainly illite
	MHC: $>10^{-12}$ m s <sup>-1</sup>	Chlorite, epidote, zoisite, albite, calcite, fluoride, sericite, and zeolites, hematite
	FT: up to $>10^{-4}$ m <sup>2</sup> s <sup>-1</sup>	CM: illite, mixed-layer clay
Onkalo, Finland	Overall pumping rate: about 20 L s <sup>-1</sup>	
	FT (depth <85 m): up to $>10^{-6}$ m <sup>2</sup> s <sup>-1</sup>	Fe-sulphides, pyrrhotite, pyrite, and calcite
AECL URL, Lac du Bonnet, Canada	FT (depth >85 m): up to $>10^{-7}$ m <sup>2</sup> s <sup>-1</sup>	CM: illite, smectite-group, kaolinite
	MHC: $<10^{-11}$ m s <sup>-1</sup>	Chlorite, iron oxides, carbonates, epidote
Mizunami URL, Japan	FT: up to $>10^{-3}$ m <sup>2</sup> s <sup>-1</sup>	CM: present (type N/A)
	HC (fresh Toki granite): $>10^{-7}$ m s <sup>-1</sup>	Quartz, plagioclase, K-feldspar and biotite, iron oxides, chlorite, calcite
Josef URL, Czech Republic	HC (altered Toki granite): $>10^{-8}$ m s <sup>-1</sup>	CM: kaolinite, montmorillonite
	HC (overall): $2$ – $5 \cdot 10^{-9}$ m s <sup>-1</sup>	Ore (gold,...), quartz, calcite, barite CM: n/a
Mine Reiche Zeche, Freiberg, Germany	MHC: $<10^{-12}$ m s <sup>-1</sup>	Ore: sulphides, quartz, fluorite, sulphates, barite, feldspars, pyrite CM: n/a
	FT: up to $10^{-8}$ – $10^{-4}$ m <sup>2</sup> s <sup>-1</sup>	
Lindau test site, Black Forest, Germany	HC (fractured ore dike): $5 \cdot 10^{-6}$ – $10^{-4}$ m s <sup>-1</sup>	Quartz, fluorite, barite, ore
	HC (fractured granite): $5 \cdot 10^{-10}$ – $10^{-8}$ m s <sup>-1</sup>	CM: kaolinite
	FT: up to $>10^{-6}$ – $5 \cdot 10^{-4}$ m <sup>2</sup> s <sup>-1</sup>	

HC hydraulic conductivity, MHC matrix HC, FT fracture transmissivity, CM clay minerals

**Table 3 Criteria match of existing URLs in the crystalline basement worldwide**

Name	Criterion 1:		Criterion 2:	Criterion 3:	Criterion 4:	
	Fractured and rather homogeneous crystalline matrix	Fracture transmissivity $> 10^{-4}$ m <sup>2</sup> s <sup>-1</sup>			Controllable hydraulic boundary condition	Comparable alteration (clay minerals)
Grimsel Test Site	Yes	No	Partly	No	No	Yes
Äspö Hard Rock Laboratory	Yes	Yes	Yes	Yes	Limit	Yes
Mizunami URL	Yes	Limit	Yes	No	No	Yes
Josef URL	No	No	Yes	No	Yes	Limit
Mine Reiche Zeche	Yes	Limit	No	Yes	Yes	Limit
Lindau Test Site	Yes	Yes	Yes	N/A (No)	Yes	No

*Limit* at the limit of the criteria. *Partly* the hydraulic boundary conditions are generally controllable, but due to storage lakes above the URL, special equipment may be needed

short or poorly connected (Himmelsbach et al. 2003). Geothermal energy development activities at Josef URL and Grimsel Test Site focus on HDR or multi-frac technology aiming at engineering naturally impermeable crystalline rock. These approaches represent the opposite end-member of EGS technology are complementary to CHFE.

Criterion 2, controllable hydraulic boundary conditions, further reduces the number of URLs suitable for CHFEs. At the Mine Reiche Zeche, 800 years of continuous mining activities resulted in a dense network of adits causing complex and non-controllable boundary conditions for CHFEs. It should be mentioned that topography-driven fluid circulation at the Lindau Test Site and influence from the Baltic Sea at the Äspö HRL lead to a certain complexity of natural boundary conditions. In the latter case, this mainly concerns the chemical composition of the fluid.

Criterion 3, hydrothermal alteration in the illite–smectite range, is fulfilled at the Äspö HRL. At the Lindau Test Site, only kaolinite is found as clay mineral. Interestingly, clay minerals occur preferably in NW–SE striking fractures (Himmelsbach, pers. comm.). However, hydrothermal alteration has not been studied in detail at the Lindau Test Site. In the Black Forest, alteration often resembles clay mineral assemblage at the Soultz site. For example, 60–90 wt% of illite, smectite, and chlorite are observed in altered granitic rocks of the southern Black Forest batholith (Brockamp et al. 2015).

Criterion 4 refers to suitable regional and homogenous stress conditions across the URL. Near the Äspö HRL, various stress measurements were made in the tunnel and nearby wells using different measurement techniques. The results are summarised, e.g. by Hakami (2003). Large scattering of  $S_{Hmax}$  orientation and principal stress magnitudes is observed. The scattering occurs across the entire depth range down to 800 m and appears to be independent of the measurement technique. Thus, regional and in situ stress states are not fully constrained. However, a mean  $S_{Hmax}$  orientation of N119°E–N138°E is observed in the SE Sweden area (Stephansson et al. 1991) and linear stress–depth relations predict a transitional stress state between thrust and strike-slip faulting with  $S_v \approx S_{hmin} \ll S_{Hmax}$  (Hakami and Min 2009; Klee and Rummel 2002). Hence, fault and fracture reactivation may occur on three differently oriented failure planes. If  $S_{hmin}$  is the smallest principal stress magnitude, a strike-slip faulting regime is supposed to reactivate vertical structures at two conjugated 30° angles around  $S_{Hmax}$ . If  $S_v$  is smallest, a thrust faulting regime is expected to reactivate sub-horizontal structures with a dip of about 30°. All three fracture orientations are predominantly observed at Äspö (Rehn et al. 1997). Favourably oriented and critically stressed structures additionally show increased fracture conductivities. In the borehole KAS06, for example, water-conducting fractures strike around 132° and are aligned almost parallel to  $S_{Hmax}$  (Sehlstedt and Strahle 1991).

At the Lindau Test Site, application of a slip- and dilation tendency analysis on the resulting fault pattern reveals the high reactivation potentials for the N–S striking ore dike as strike-slip fault and for NW–SE striking structures as normal faults within the ambient stress field (see below). However, strong perturbation of the stress field inside the existing is expected due to a steep slope topography in combination with a low overburden of only 90 m. This is considered insufficient for providing rather topography-independent stress conditions in the tunnel.

It can be concluded that the Äspö HRL and Lindau Test Site approximate best criteria for CHFES. While at the Lindau Test Site insufficient overburden represents a criteria of exclusion for the existing design of the tunnel, at Äspö HRL the general stress situation is unsatisfactorily described and furthermore includes most likely thrust faulting. Both URLs may be used in a qualified sense for complementary experiments. In agreement with these findings and the criteria for GeoLaB, we have carried out further studies in the southern Black Forest for the following reasons:

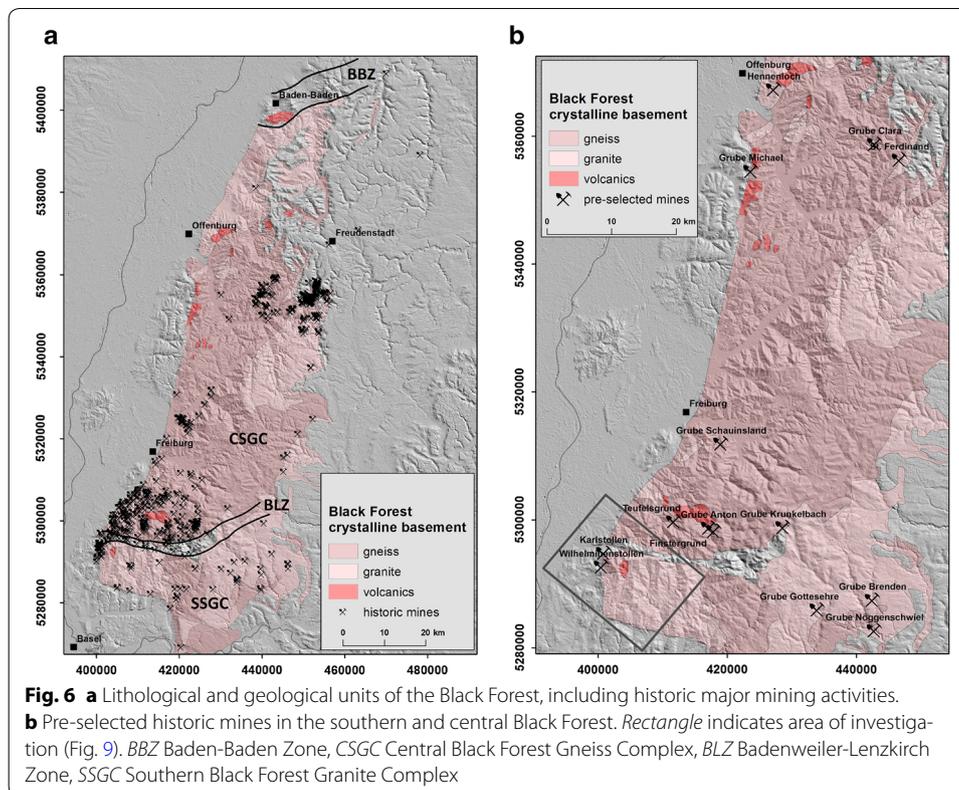
- 1) The basement outcropping in the Black Forest represents to a large extent the lithology of the geothermal host rock in the URG.
- 2) Appropriate hydrothermal alteration is widely observed in the Black Forest (Brockamp et al. 2015).
- 3) Extended fracture networks are indicated (Stober and Bucher 2014).
- 4) Apart from overburden the Lindau Test Site indicates the general suitability of the southern Black Forest. Hydraulic condition fixed in criterion 1 are achieved (Himmelsbach et al. 1998) and the regional stress field represents or at least approximates conditions of major EGS projects in the URG.

## **Geology and hydrogeology of the black forest**

### **Geology of the Black Forest**

From N to S, the Black Forest is subdivided into four zones: the Baden-Baden Zone (BBZ), Central Black Forest Gneiss (CSGC), and Southern Black Forest Granite Complexes (SSGC) that are separated by the Badenweiler-Lenzkirch Zone (BLZ) (Fig. 6). The low-grade metamorphic rocks of BBZ comprise schists, meta-greywackes, and marbles and are separated from the medium to high-grade metamorphic rocks of the CSGC by a major NE–SW striking dextral-transpressive ductile shear zone. Shearing occurred between 335 Ma and the intrusion of an about 325 Ma old biotite-muscovite granite that was cataclastically deformed during sinistral brittle reactivation (Eisbacher et al. 1989; Hess et al. 2000; Kober et al. 2004; Wickert et al. 1990). The CSGC essentially consists of migmatitic and, locally, mylonitic biotite-plagioclase-gneisses hosting irregularly shaped and sized bodies of amphibolites and eclogites, serpentinitised peridotites, and granulites (Kalt and Altherr 1996; Marschall et al. 2003). It was intruded at about 330–325 Ma by batholiths of different size and numerous granitic to porphyritic dykes (Hess et al. 2000). The BLZ is an about 5–10 km wide metasedimentary-metavolanic succession that includes low-grade to non-metamorphic Ordovician to late Carboniferous sedimentary and volcanic rocks (e.g. Krecher and Behrmann 2007). It was overthrust by the CSGC along the dextral transpressive N- to NW-dipping, mylonitic-cataclastic Todtnau thrust (Krohe and Eisbacher 1988; Eisbacher et al. 1989). The southern boundary of BLZ is a WNW-trending shear zone (e.g. Krecher and Behrmann 2007). The SSGC was intruded by the large South Black Forest Batholith between 334 and 328 Ma (Schaltegger 2000; Todt 1976).

Major brittle, commonly mineralised fault zones are observed in abandoned mines (e.g. Werner and Dennert 2004) and quarries and—on a regional scale—at the basement-cover interfaces. During late Variscan times, i.e. from about 310 to 330 Ma, deep and high-level crystalline basement rocks cooled to below 300 °C in the Moldanubian



zone of the Black Forest and, hence, reached upper crustal brittle levels, with retrograde mylonitic shear zones being transformed into cataclastic fault zones (e.g. Eisbacher et al. 1989; Grimmer et al. 2016).

The crystalline basement rocks of the Black Forest display important late- to post-Variscan alteration and mineralisation features (e.g. Simon 1990; Zuther and Brockamp 1988). The Southern Black Forest batholith has significantly reduced  $\delta^{18}\text{O}$ -values compared to its magmatic equilibrium values and to the 325 Ma old granites of the Northern Black Forest Batholith (Hess et al. 2000; Schaltegger 2000; Simon 1990; Hoefs and Emmermann 1983). On the regional scale, the directions, timing, and relative proportions of descending low  $\delta^{18}\text{O}$  meteoric paleofluids versus ascending or recycled and internally buffered high  $\delta^{18}\text{O}$  paleofluids are largely unknown. On the local scale, detailed geochemical studies of post-Variscan mineralised veins indicate a mixture of ascending and descending fluids during mineral formation in fault zones (e.g. Bons et al. 2014). Radiometric dating of minerals originating from hydrothermal alteration of crystalline basement rocks and Permo-Triassic cover rock successions as well as of minerals originating from fault-related, mineralised veins reveal multiple and complex post-Variscan phases of pervasive and localised fluid-rock interactions (Brockamp et al. 2015; Zuther and Brockamp 1988; Glodny and Grauert 2009).

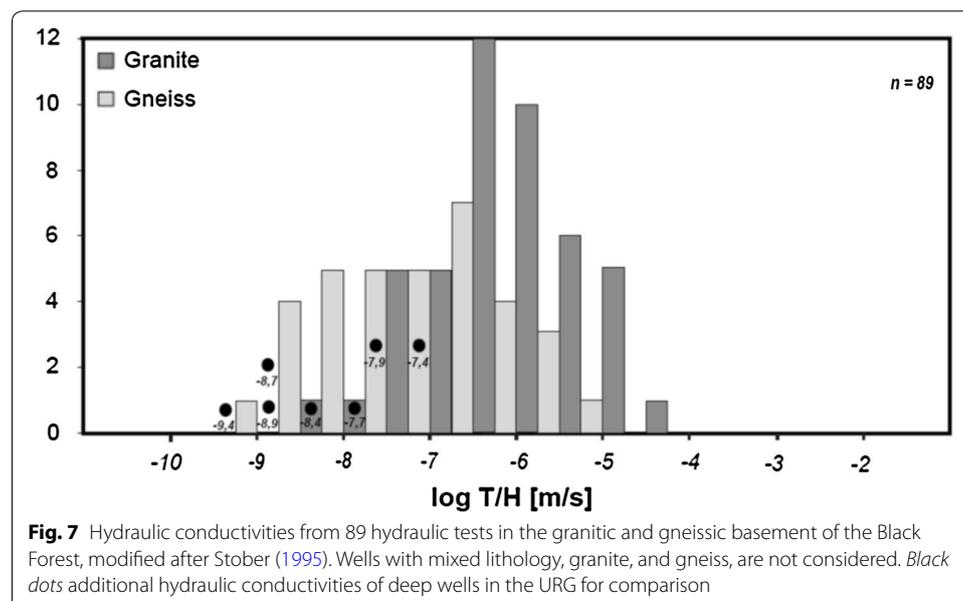
### Hydrogeology of the Black Forest

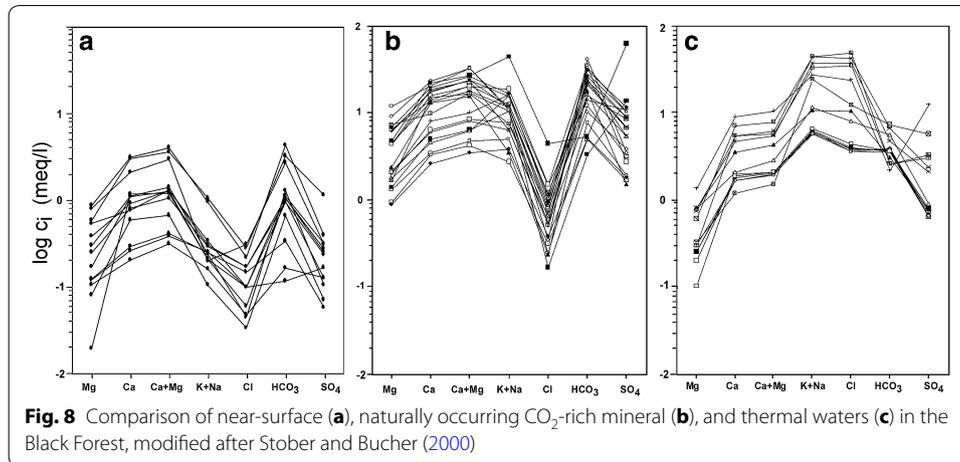
Features of brittle deformation, such as faults and joints, are the principal fluid-conducting structures in crystalline basement rock. In the Black Forest and URG area, hydraulic

tests in boreholes down to 5 km depth revealed hydraulic conductivity values that range over nine orders of magnitude from  $10^{-13}$  to  $10^{-4}$  m s<sup>-1</sup> with a log mean of  $7 \cdot 10^{-6}$  m s<sup>-1</sup> over 175 tests (Stober and Bucher 2007). The large variance observed at shallow depth decreases rapidly to a range between  $10^{-8}$  and  $10^{-6}$  m s<sup>-1</sup> at about 1 km depth. A characteristic value of  $10^{-8}$  m s<sup>-1</sup> is observed at 4 km depth. This decrease appears to be pronounced in gneissic basement (Stober 1995). Thus, mean hydraulic conductivities of  $1 \cdot 10^{-6}$  m s<sup>-1</sup> in fractured granite are generally higher than in fractured gneiss ( $5 \cdot 10^{-8}$  m s<sup>-1</sup>; Fig. 7).

Several hydraulic test data indicated the influence of faults or fault zones acting as distant hydraulic boundaries. Hydraulic conductivities were lower than the values of the undisturbed crystalline basement, retrieved from the radial flow period (Stober and Bucher 2014). This permeability contrast was attributed to low permeabilities within the core of the fault. Investigation of water table fluctuations due to earth tides, of draw-down data from long-term pumping tests, and of hydrochemical and thermal data from long-term observations of deep circulating systems (natural thermal springs) shows that the open water-conducting fractures and pore spaces form an interconnected network in the crystalline basement with characteristic hydraulic properties (e.g. Stober and Bucher 2014). Thus, the crystalline basement can be regarded as an aquifer in hydraulic terms.

Bucher and Stober (2000) and Pearson et al. (1991) summarised the hydrochemical characterisation of crystalline fluids in the Black Forest and adjacent areas. Three major types of groundwater can be distinguished (Fig. 8). Besides near-surface fresh type 1 water (Fig. 8a), CO<sub>2</sub>-rich mineral type 2 water (Fig. 8b) is predominantly occurring in the central Black Forest (e.g. Bad Peterstal, Bad Griesbach, Bad Teinach), whereas saline thermal type 3 water (Fig. 8c) is found mostly in the northern and southern Black Forest (e.g. Wildbad, Bad Liebenzell, Baden-Baden, Bad Säckingen, Zurzach). The latter results from the mixing of surface freshwater, saltwater, and a water–rock reaction component from an up to about 3–5 km deep reservoir. CO<sub>2</sub>-rich mineral water in the central Black





Forest is of low salinity and its chemical composition results from the reaction of CO<sub>2</sub>-rich water with the crystalline rock matrix at relatively shallow depth (<500 m) exclusively. The main water components are Ca, Na, and HCO<sub>3</sub> (Fig. 8b). In types 1 and 2, the total of dissolved solids (TDS) is enhanced. The type 1 groundwater resembles main water components of type 2, but has a significantly lower TDS and is poor in CO<sub>2</sub>. It develops due to interaction of rainwater with crystalline basement rocks. Thus, a distinct stratification in hydrochemistry with increasing depth results: TDS increases and the water type changes from Ca-(Na)-HCO<sub>3</sub> to Na-Cl rich waters.

Topography-driven deep circulation systems in the Black Forest occur in granites. Highly permeable fracture and fault zones in granites are used as ascent channels and flow paths by deep hot saline crystalline basement waters. Although spatially closely associated, the saline deep waters and the CO<sub>2</sub>-rich mineral waters are hydraulically and chemically unconnected (e.g. Bucher and Stober 2000).

### Preliminary criteria validation in the southern Black Forest

An exploration concept has been established to pre-characterise a suitable site for Geo-LaB in the Black Forest from the surface. It aims at indicating the subsurface condition that are relevant to CHFE in the run-up of large exploration including exploration wells. The concept is based on the recommendations for characterising, modelling, and monitoring fractured rock sites of the National Academies of Sciences (2015). It includes geometric characterisation using lineament mapping techniques, geomagnetic, geoelectric, georadar measurements, geological mapping. In the absence of boreholes, no geophysical logging or hydraulic testing is envisaged at this stage. In addition, a hydrochemical exploration is included. The concept was applied and tested along the Wilhelminenstollen, an exploration tunnel selected from about 700 abandoned mines in the Black Forest according to the selection criteria above. The study is to be updated upon the continuation of the project.

### Structural setting of the southern Black Forest

In addition to the geological and structural mappings summarised in the Geological Map of Baden-Württemberg (1:50,000, LGRB, 2015), lineaments of the southern Black forest

were mapped using high-resolution digital elevation models with up to  $5 \times 5$  m resolution. Compared to earlier studies (Franzke et al. 2003), a higher lineament density in the southern Black Forest and predominant (S)SW, (W)NW, and N trending strike directions are observed (Fig. 9). These directions are also observed in the geothermal reservoir at Riehen and Basel in the URG (Meixner et al. 2016). From stress measurements in the entire Black Forest a strike-slip regime with a  $S_{Hmax}$  orientation of  $N140^{\circ}E \pm 10^{\circ}$  was obtained.

The resulting fault and stress field models were used for slip- and dilation tendency analyses (Fig. 9). The reactivation potential reveals two local maxima. Faults that strike about  $N110^{\circ}E$  and  $N170^{\circ}E$  are prone for shear reactivation as dextral and sinistral strike-slip faults, respectively. Dilation is most likely to occur in directions parallel to  $S_{Hmax}$ . Highest lineament density is observed for the  $N110^{\circ}E$  strike direction that exhibits both slip and dilation tendency maxima.

#### **Possible sites for GeoLaB in the southern Black Forest**

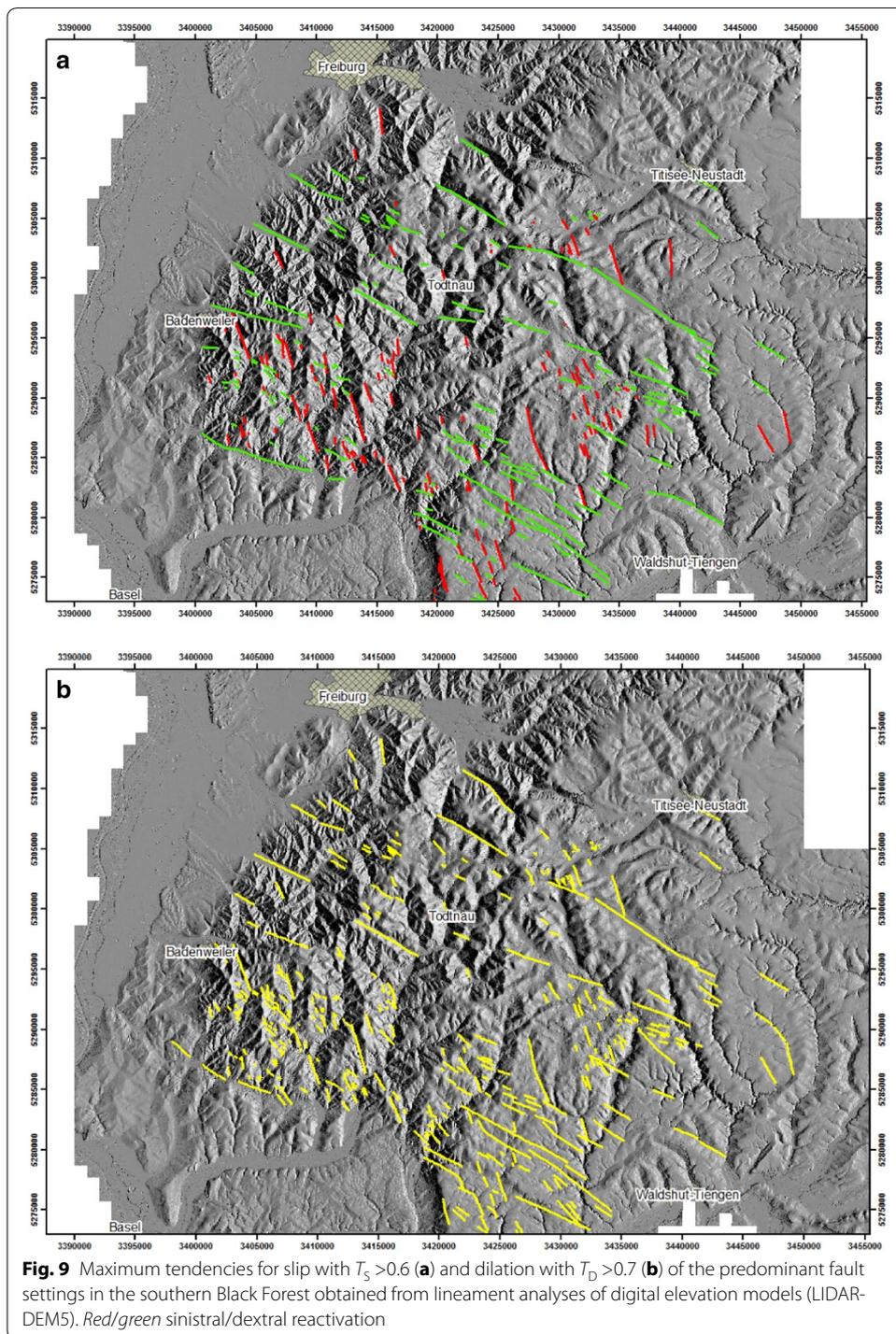
Generally, there are two main approaches to constructing a geothermal URL in the southern Black Forest: using and connecting to an existing tunnel or mine or constructing a new tunnel. Existing tunnels or mines may provide the necessary infrastructure, e.g. road access to the location. Moreover, rock properties, the fracture network, and hydraulic conditions can be investigated in situ before major investments are committed.

Of the more than 700 historic mines in the Black Forest (Steen 2004; Werner and Denkert 2004), 15 sites were pre-selected according to the size and accessibility of the tunnel (Fig. 6). To evaluate their suitability for CHFES, the lithology and overburden were analysed from literature. Fracture transmissivity can only be inferred occasionally from the water budget in the mines. Commonly, information on hydrothermal alteration is lacking. Regional stress conditions in the Black Forest are generally suitable for CHFES. Controllable hydraulic boundary conditions is one of the most important criteria for CHFES in pre-existing tunnel systems.

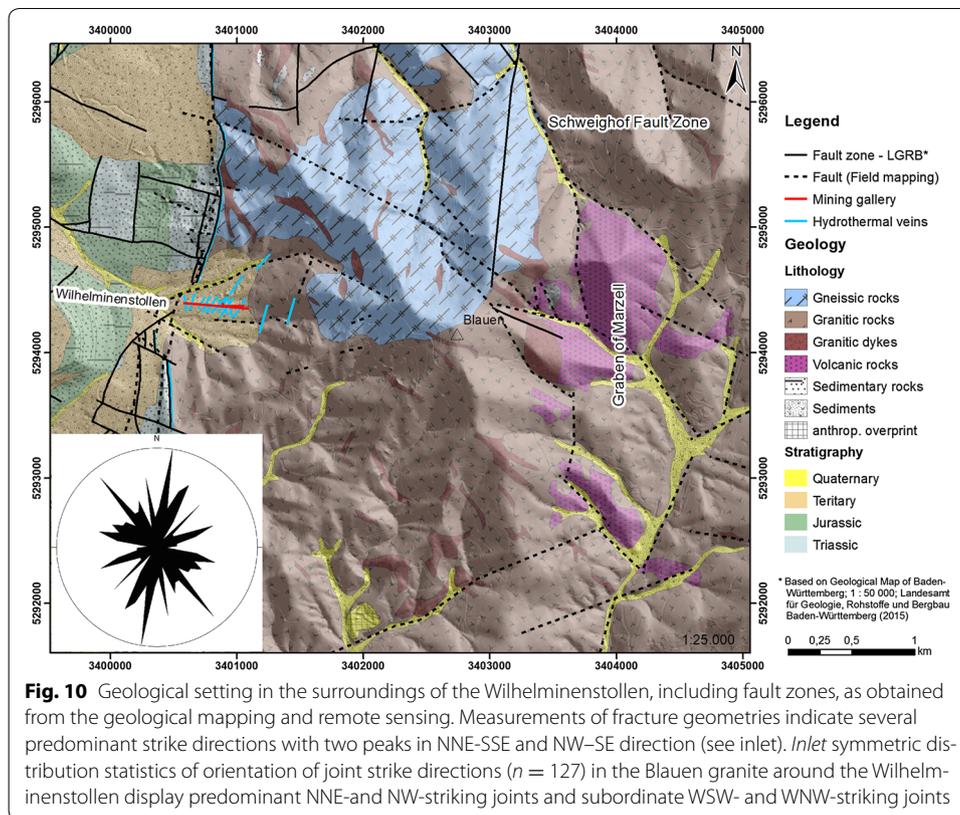
To avoid complex and unknown tunnel systems, we selected a single exploration tunnel, the Wilhelminenstollen near Badenweiler, as potential GeoLaB site. Wilhelminenstollen is documented well and led to no further mining activity. Furthermore, it fulfils a number of other criteria such as lithology, open fracture zones, and clay minerals comparable to the Soultz site. For these reasons, it was chosen as a case study site to test an assessment procedure for a geothermal URL in crystalline basement rock. Geological, hydrogeological, and geophysical methods have been applied to indicate the suitability of the Wilhelminenstollen for an URL.

#### **Geological setting at the Wilhelminenstollen**

The 521 m long, E–W trending Wilhelminenstollen is located SE of Badenweiler in the SSGC (Fig. 10). Together with the earlier constructed Sehringer Stollen, which is located approximately 50 m higher, it was installed around 1920 at Sehringen to explore the mineralised veins in the Blauen granite and was abandoned a few years later. The tunnel entrance is located immediately east of the Black Forest escarpment fault. Today, about  $37,500 \text{ m}^3$  of drinking water per year are collected from open fractures in the tunnel.



Structurally, three major features laterally frame the study area. To the north, segmented E–W striking normal faults separate the SSGC from the Badenweiler-Lenzkirch-Zone. East of the Mt. Blauen, the N to NNW striking Schweighof fault zone and the N–S trending graben structure of Marzell juxtapose the SSGC granites against Permian volcanics. To the west, the NNE striking Black Forest escarpment fault marks the structural



border between the exposed crystalline basement rocks and the Mesozoic cover. It is segmented by NE and SE striking transfer faults which accommodate an E–W extension in the form of oblique normal faults with a sinistral and dextral a strike-slip component. NW to NNW and NE to SW trending faults resulted from post-orogenic extensional tectonics during Variscan orogeny, but show polyphase reactivations in the Mesozoic and Cenozoic (Huber and Huber-Aleffi 1984; Schumacher 2002).

Two different petrologic units, the Blauen granite and the Wiese-Wehra formation, are exposed in the study area. The medium- to fine-grained biotite-type Blauen granite was linked to the about 328–333 Ma old Malsburg granite (Sawatzki et al. 2003). The second petrologic unit mainly consists of gneissic rocks commonly designated as diatexites of the Wiese-Wehra formation.

NNE striking faults and fracture zones are often filled by cataclastic material or by hydrothermally and mechanically altered secondary minerals, such as hematite, Fe-hydroxide, clay minerals, barite, or quartz. Especially the NNE striking escarpment fault zone is accompanied by several hydrothermal veins. These deposits are fault- and fracture-hosted veins and seem to be directly linked to brittle deformation processes. Formation ages indicate hydrothermal activity in the Black Forest area since Variscan times, with a peak in the Jurassic (Bons et al. 2014). But NNE alignment of the veins close to the escarpment fault may also indicate correlation of Cenozoic rifting and origin of hydrothermal circulation along this fault. Breccia textures of the veins also reflect repeated cycles of fault reactivation and mineral precipitation. The veins almost constantly

strike NNE-SSW with varying dip angles between about 45–80°. Interestingly, most of the veins dip to the E, opposite to the escarpment fault, which was active during URG formation. This may indicate that hydrothermal circulation and mineral precipitation took place at both conjugated shear angles during active normal faulting. The epigenetic ore deposits in the study area mainly consist of lead-bearing quartz-barite veins and were formed by mixture of fluids of different origin (Bons et al. 2014; Kneer 2006). The distribution of the inflow of water into the tunnel and the high Ba concentration of 442.3  $\mu\text{g L}^{-1}$  indicate a clear link between the barite-filled fractures and fluid pathways.

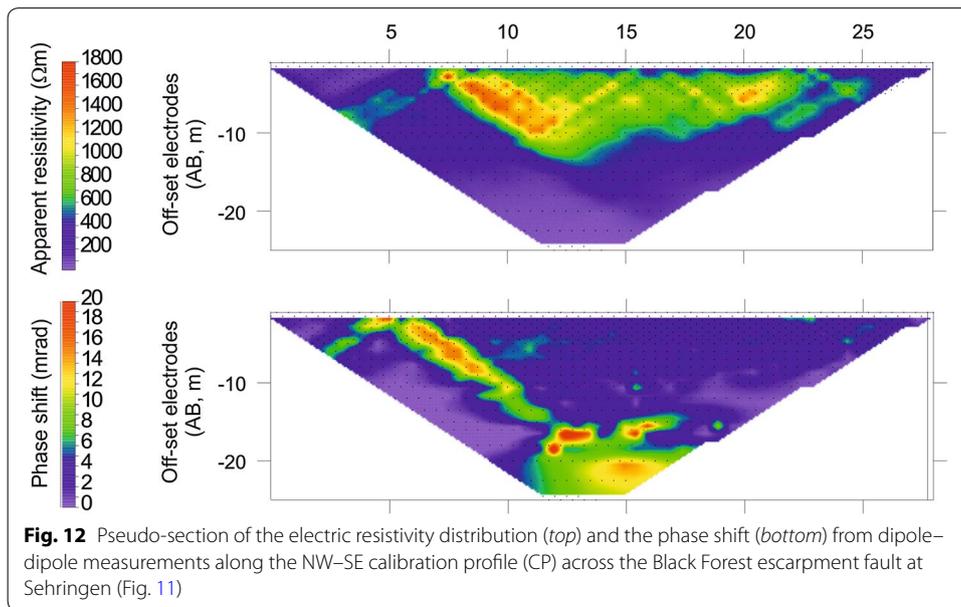
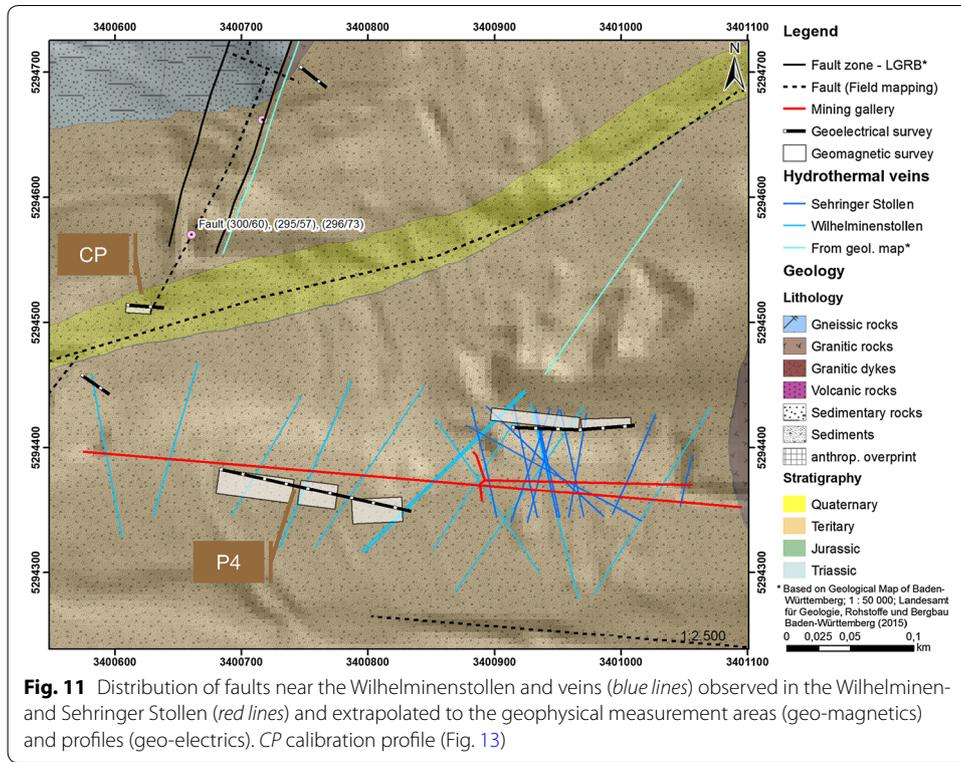
X-ray diffraction (XRD) analyses of powders of fracture fillings from the Black Forest escarpment fault and a fracture in the front part of the Wilhelminenstollen revealed an asymmetric peak at  $2\theta$  (CuK $\alpha$ ) = 10 Å characterised by tailing towards lower  $2\theta$  values. This indicates the presence of mica/illite together with an illite–smectite interstratification in the alteration products. Ethylene glycol treatment confirmed the presence of the swellable interstratification. No indication of free smectite was found.

### Fault characterisation

Due to the lack of geological outcrops in the southern Black Forest, the identification of faults from the surface requires geophysical measurements. In a first reconnaissance study, the faults and veins near the Wilhelminenstollen were identified successfully using electric resistivity measurements. Geo-electric measurements were conducted using a 4-point Light High Power with 60 electrodes (LMG) and Geo-Test (Geophysik Dr. Rauen). Dipole-dipole and pole-dipole geometries with an electrode offset of 0.5–45 m were used. Geographic coordinates were acquired using a Trimble R4 with Sapos-correction. In addition, geomagnetic and georadar data have been acquired (not shown). Compared to geoelectric measurements, they are less conclusive.

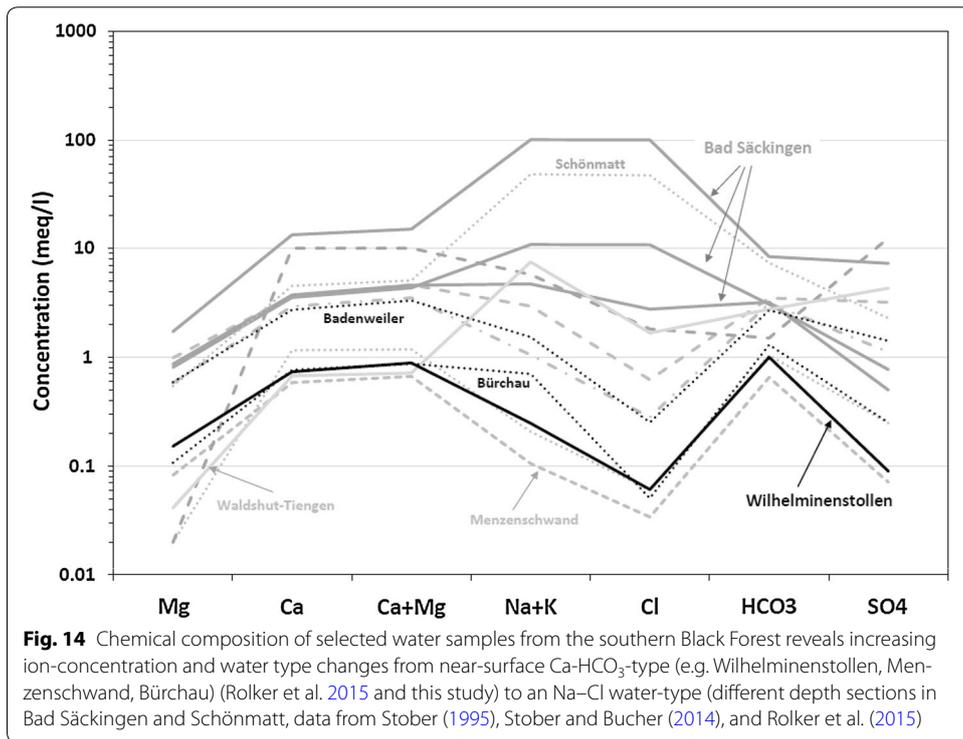
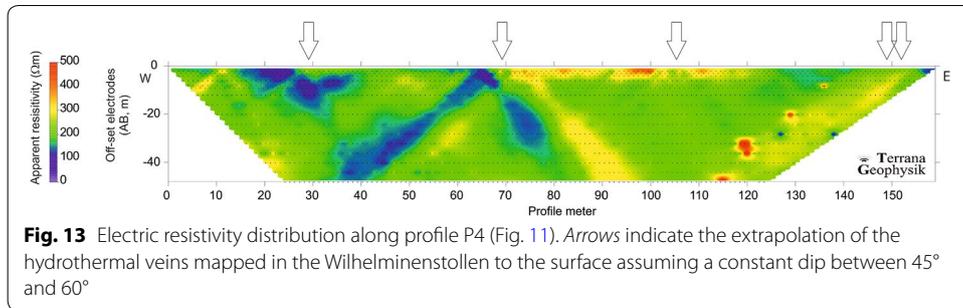
First, a calibration profile was measured across the Black Forest escarpment fault exposed along the road to Sehringen (CP, Fig. 11). The fault zone dips towards WNW with about 60°. As indicated by the geological map, the exact location and the number of branches of the targeted fault zone are a matter of discussion. Both, electric resistivity and phase shift indicate an anomaly between profile meters 5 and 10 (Fig. 12). The anomalies are observed to an off-set of >10 m corresponding to a depth of approximately 5 m. There is some minor indication of a smaller anomaly around profile meters 20 in the apparent resistivity.

Hydrothermal veins partly filled with quartz and Mg-, Pb-ore minerals and barite within the Wilhelminenstollen mostly dip to the ESE or ENE with about 45–60 °C. Here, they are mapped from the surface in variable quality using electric resistivity (Fig. 13). Correlation of the near-surface anomalies and the hydrothermal veins in the tunnel is possible when considering an E–W offset due to the dip of the structures. Two low resistivity anomalies in the western part of P4 coincide well with the shifted position of veins in the tunnel. These two veins are Pb-bearing structures. The vein at profile meter 102 is not detected by resistivity measurements. This may be attributed to the fact that this vein is filled by quartz and Mg only. The easternmost veins at the edge of the profile (profile meters 149.5 and 151.5) are not covered by the profile.



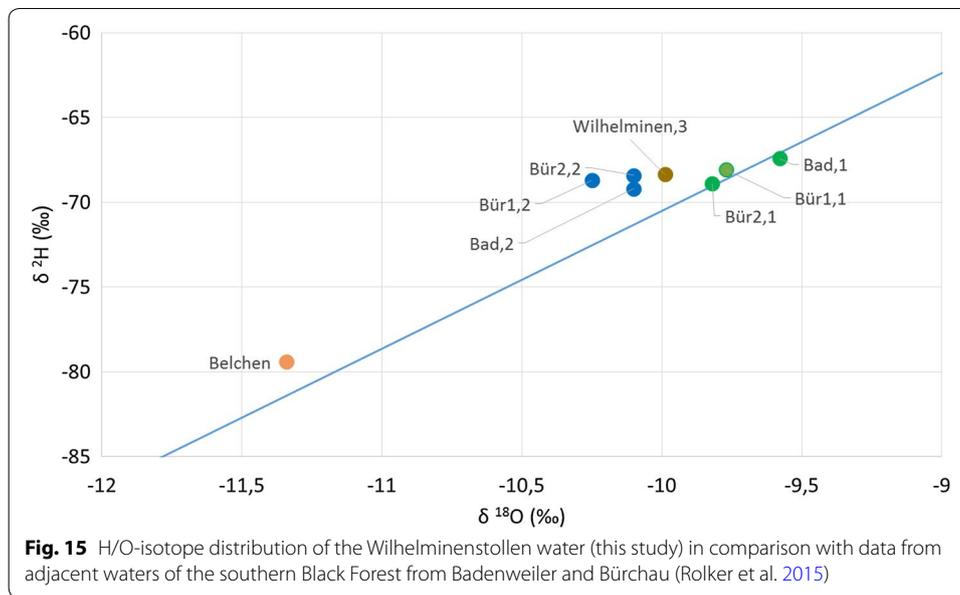
### Hydrogeology

Hydraulic tests performed in the granitic basement of the southern Black Forest suggest hydraulic conductivities of the order of  $4.5 \cdot 10^{-8} \text{ m s}^{-1}$  at 500 m depth. Fluids from the near-surface granitic basement exhibit similar Ca- or Na-HCO<sub>3</sub>-dominated chemical characteristics (Fig. 14). Near-surface waters generally are of low mineralisation. TDS increases with increasing depth, as indicated by the three analyses from Bad Säckingen.



The deepest well (600 m) shows the highest TDS and is dominated by Na-Cl, whereas both TDS and NaCl decrease at shallower depth. Near-surface waters (<100 m), in general, possess low TDS values and water chemistry is dominated by Ca and HCO<sub>3</sub> (e.g. Menzenschwand, Wilhelminenstollen). However, also thermal spring waters often have a near-surface water component (Fig. 14, e.g. Badenweiler, Bürchau). In contrast to Bürchau, the water from the Wilhelminenstollen has significantly lower Na and SO<sub>4</sub> concentrations. In Badenweiler and Bürchau, low mineralisation and maximum sulphate equilibrium temperatures of about 60–80 °C indicate a small potential for water-rock interaction only (Rolker et al. 2015).

The relationship between  $\delta^{18}\text{O}$  and  $\delta^2\text{H}$  of thermal springs from different sites in the southern Black Forest is shown in Fig. 15. The isotope ratio follows the global meteoric water line. The values from Bürchau and Badenweiler show differences between sampling campaigns 1 and 2. The values from Wilhelminenstollen (sampling campaign 3, this study) lie between the above values. A shift towards higher  $\delta^{18}\text{O}$  values in campaign

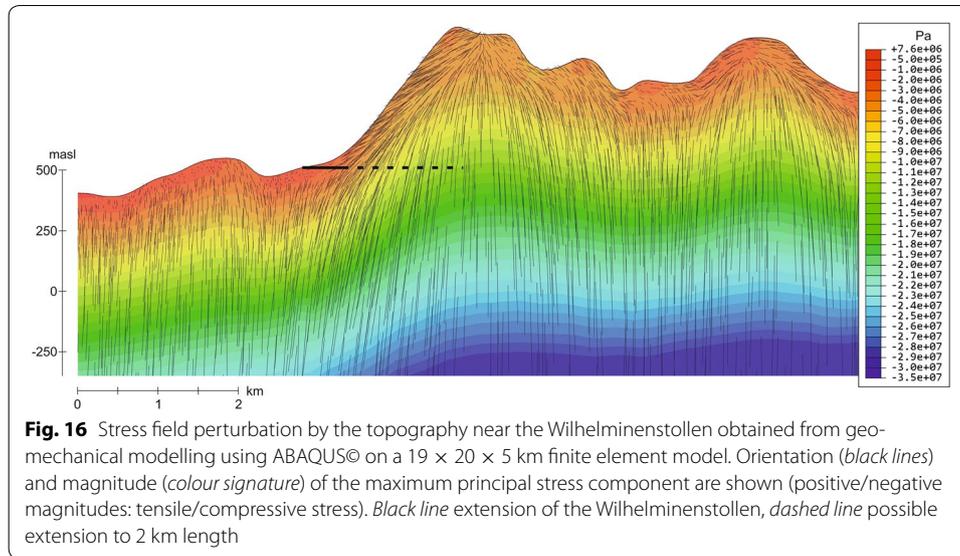


2 was attributed to a higher contribution of rainwater. The difference in  $\delta^{18}\text{O}$  and  $\delta^2\text{H}$  values between the Mt. Belchen and the sites of Bürchau, Badenweiler, and Wilhelminenstollen along the meteoric water line can be attributed to altitude effects, since there is a difference in altitude of several hundred metres between the sites and Mt. Belchen. Following earlier studies of Pearson et al. (1991), a local relationship is identified, including the southern Black Forest in the area of Bürchau. For Mt. Belchen, the best fit between this relationship and true infiltration elevation was obtained from  $\delta^{18}\text{O}$  values. This gives a minimum infiltration altitude for the Wilhelminenstollen of about 730 masl. The hydrochemical data on Wilhelminenstollen, its minimum infiltration altitude, and the topographic situation result in a locally controlled hydrogeological framework with a maximum catchment area of 0.5 km<sup>2</sup>.

#### Stress model for the topographic condition

Local stress in mountain areas is affected by the topography, the rheological properties of the rock, and the ambient tectonic state of stress. Geometry and mass of the topography may cause local reorientation and lateral variation of the magnitude of the principal stress directions (Miller and Dunne 1996; Pan et al. 1995; Savage and Morin 2002). Since GeoLaB aims at approximating reservoir condition best, the URL design strives for rather topography-independent conditions of the stress field.

Rock type and ambient stress state are rather homogenous across the planned GeoLaB tunnel and hence to solely assess the influence of topography on the stress field distribution near the Wilhelminenstollen, a finite element was generated for an area of 19 × 20 km around the Wilhelminenstollen (Fig. 6b) with a vertical extension from the topography down to 5 km b.s.l. (Fig. 16). First-order geomechanical modelling using ABAQUS© covers gravitational loading of the 3D model only. The resulting orientation and magnitude of the principal stress component are shown in Fig. 16.



Close to the surface, both, orientation and magnitude of the maximum principal stress component are strongly influenced by the topography. At steep slopes and shallow depth (first 100–200 m), the maximum principal stress component significantly deviates from vertical orientation due to topographic stresses. Here, the vertical component of the stress tensor is no longer a principal stress. As a result, failure conditions and fracture patterns in these areas deviate significantly from regional trends. Consequently, regional stress field models are no longer applicable to predict of the reactivation potential of faults and fractures. Subvertical orientation of the maximum principal stress component is observed below ridges and plateaus and at considerable depth beneath strong topographic gradients only. Note that the modelled local stress field changes significantly, when superposing on the gravitational stress field the ambient compressive far-field tectonic stress. At this early planning stage of GeoLaB, this more comprehensive model hampers evaluation of the stress perturbations that are purely driven by topography, but it will be considered for the design of the tunnel.

The onset of the Wilhelminenstollen is located at the foot of Mt. Blauen. With its current length of about 500 m, it is located entirely in the critical near-surface zone of highly perturbed stress states. For the specific setting of the Wilhelminenstollen, a tunnel length of  $>1.5$  km is suggested when considering the criteria of stress perturbation of  $<1$  MPa and approaching vertical orientation of the maximum principal stress direction for gravity. This results in a minimum overburden of about 500 m.

## Conclusion

Particular aspects of geothermal characterisation and operation can only be obtained through access to the underground environment. Engineering of geothermal production from fractured crystalline rocks using flow rates of more than  $30 \text{ L s}^{-1}$  requires knowledge of geological, physical, and chemical processes that can be gained partly on the downhole field scale and partly by large-scale research laboratory facilities.

As was pointed out by the NEA (2013), URLs provide important technical knowledge and increase confidence in the process of facility siting and design, engineering support, and evaluation of safety. Clearly, such a generic URL will not have all real reservoir conditions (such as temperature, magnitude of stress components, and chemical composition of water), but confidence in the suitability of a potential geological environment and engineering feasibility can be gained by a verification of individual processes and operation concepts. URLs offer an unparalleled opportunity to demonstrate the engineering concept of EGS and instil confidence in the wide range of stakeholders. A transparent underground experimentation and operation programme of an URL platform will yield specific information that also is of direct relevance to authorities assessing the risk of underground utilisation. In this context, a geothermal URL represents a worldwide unique research installation with specific environmental settings being required for EGS development.

Four criteria have been established based on EGS experience and applied to existing generic URLs. These are a relatively homogenous crystalline basement matrix with a well-connected fracture network with fracture transmissivities in the range of  $>10^{-4} \text{ m}^2 \text{ s}^{-1}$ . Fractures should be characterised by hydrothermal alteration including illite and smectite among others. The local stress field is characterised by strike-slip (to normal faulting) reactivation and fractures are favourably oriented. Furthermore, the stress field is rather homogeneous with a variation in magnitude  $<1 \text{ MPa}$  across the envisaged experimental volume. Obviously, a geothermal URL will not match reservoir conditions in terms of temperature, rock-water interaction, and the stress field. CHFES that address these parameters will rather study gradients of these fields.

Application of the four criteria to existing generic URLs in the crystalline basement worldwide reveals that apart from the inferred stress field, the Äspö HRL, and apart from overburden, the Lindau Test Site, provide favourable conditions for CHFES. These URLs may be used to carry out specific accompanying or complementary experiments.

Typical deep geothermal reservoir rocks of the URG are exposed in the Black Forest. In general, tectonic, geological, and hydrogeological conditions in the southern Black Forest match the established criteria for CHFES in a geothermal URL. In the Wilhelminestollen, controllable hydraulic boundary conditions are valid. An exploration concept to pre-characterise suitable GeoLaB sites in the Black Forest from the surface has been tested successfully. It involves exploration from the surface and aims at a first assessment of the established criteria in the run-up of large exploration including exploration wells. In this respect, the Wilhelminestollen area is characterised as follows:

- A dense fracture network inferred from lineament analyses is completed by observations in the existing tunnel and resistivity measurements.
- Alteration zones with clay minerals or ore mineralisation in fractures are characterised well by electric resistivity.
- Hydraulically active fractures and fault zones in a regional network are identified at several sites in the Black Forest. In the absence of wells, local transmissivities cannot be acquired, but a typical natural in-flow into the tunnel of several  $\text{L s}^{-1}$  can be estimated. Increasing TDS and higher NaCl concentration are expected.

- Low influence of topography-induced stress variations requires a minimum overburden of about 500 m.
- Regional reactivation potential is highest for large differential stresses. At Wilhelminenstollen, they are maximum for fractures and faults oriented N110°E and N170°E.

The analysis performed has provided key steps for developing a generic URL in the southern Black Forest. In first order, most of the criteria are fulfilled in the study area. For a final decision on the technical feasibility of GeoLaB at Wilhelminenstollen as well as the conceptualisation and optimisation of the design, a large geophysical exploration campaign as well as exploration wells including hydraulic testing is necessary.

#### Authors' contributions

ES reviewed the condition of the Soultz EGS site and the existing URLs and carried out the fluid chemical analyses and the geophysical surveys, JM carried out the remote sensing and slip- and dilation tendency analyses, CM contributed to the review of the Soultz EGS site and the existing URLs, MG reviewed the existing mines in Black Forest and performed the numerical simulation on the influence of topography, JG reviewed the geological condition of the Black Forest, IS reviewed the hydrogeological condition and TK summarized the scientific concept of GeoLaB. All authors established the criteria. All authors read and approved the final manuscript.

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#### Competing interests

The authors declare that they have no competing interests.

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