

Ductilisation of tungsten through cold rolling: Change of brittle to ductile transition temperature in highly deformed tungsten

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Outline

- Improvements through severe cold rolling
- Theory of BDT
- Motivation
- Microstructure
 - Inverse pole figure maps
 - ODF maps
 - Grain boundary character
- Mechanical testing
 - Influence of specimen thickness
 - Influence of microstructure

Summary



- BCC metal with melting temperature of 3422 °C
- High heat conductivity, high temperature strength and low thermal expansion coefficient
 - Tungsten (W) perfect material for high temperature vacuum applications



Poor oxidation resistance

- Brittle fracture at ambient temperature
 - Not in use as structural material, only applied as functional material nowadays

[1] Wendelstein X7 Newsletter[2] www.euro-fusion.org













Tensile test: Ductility and yield strength improved

[3] Reiser, J. et al.: Ductilisation of tungsten (W): On the increase of strength and room-temperature tensile ductility through cold-rolling







- Tensile test: Ductility and yield strength improved
- Fracture behavior: Stable crack growth at room temperature achieved

[4] Reiser, J. et al.: Ductilisation of tungsten (W) through cold-rolling: R-curve behaviour







- Tensile test: Ductility and yield strength improved
- Fracture behavior: Stable crack growth achieved
- Charpy tests: BDTT shifted to lower temperatures

[5] Reiser, J. et al.: Ductilisation of tungsten (W): On the shift of the brittle-to-ductile transition (BDT) to lower temperatures through cold rolling





Theory of BDT



- BCC metals exhibit two kinds of fracture
 - Low energy fracture brittle
 - High energy fracture tough
- Competition between critical resolved shear stress and cleavage stress
 - Mobility of (111) screw dislocation depends on temperature, loading rate
 - Cleavage stress independent on temperature
- If CRSS reaches cleavage stress, transition in fracture behaviour





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- If CRSS reaches cleavage stress, transition in fracture behavior
- Activation energy for BDT can be calculated



$$\dot{K} = A \exp(-\frac{Q_{BDT}}{k_{B} T_{BDT}})$$

[6] Hartmaier, A. et al.: On the Activation Energy for the Brittle/Ductile Transition

Motivation



- Observation: UFG microstructure affects strain rate sensitivity of BDT
- Hypothesis: Change of controlling mechanism



Question: Identification of controlling mechanism of BDT in ultra-fine grained W
Methods: Indirect by K-tests; direct via electron microscopy

[7] Németh, A. et al.: The nature of the brittle-to-ductile transition of ultra fine grained tungsten (W) foil

Material

- Five W sheets produced exclusively at PLANSEE SE, Reutte, Austria
- Processing through hot and cold rolling out of one single sintered compact

| Sheet thickness s /mm | 1.0 | 0.5 | 0.3 | 0.2 | 0.1 |
|------------------------------------|-----|-----|-----|-----|-----|
| Degree of cold work ϕ_{CR} /- | 1.8 | 2.5 | 3.0 | 3.4 | 4.1 |

- Extremely high degree of deformation through cold-rolling
- Five degrees of deformation causing
 - Five sheet thicknesses
 - Five microstructures
- No further heat treatment after rolling applied

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- Tungsten: Designated material for plasma facing components in fusion devices but inherently brittle up to 400 °C
- Motivation: Dramatic improvement of its mechanical properties through cold rolling
- Goal: Identification of mechanism causing BDTT in ultra-fine grained tungsten
- Experimental: Five cold rolled sheets, five microstructures made of same sintered compact
- Result 1: Grain refinement down to 300 nm
- Result 2: Alpha and gamma fiber, pronounced rotated cube orientation
- Result 3: BDTT less dependent of specimen thickness
- Result 4: BDTT shift of 500 K downwards to -100 °C for the 0.1 mm UFG W

Thank you for your attention

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