



Propagation of Nuclear Data Uncertainties in PWR Pin-Cell Burnup Calculations via Stochastic Sampling

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Content

- Introduction
- S/U analysis
- Methods
 - The SAMPLER sequence
 - Problem definition and modeling
 - Calculation flowchart
 - Stochastic sampling vs. GPT methods
- Results
 - k-inf vs. irradiation time + uncertainties
 - Reaction rates
 - Nuclide concentrations
- Summary

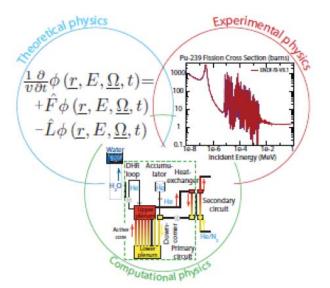


Preamble – "All models are wrong"



- In computer modelling, errors and uncertainties inevitably arise due to the mathematical idealization of physical processes stemming from insufficient knowledge regarding accurate model forms as well as the precise value of input parameters
- Even the best models can only be as accurate as their input parameters
- Reality does not have parameters
- Before trusting the results obtained by simulations one has to make sure that they are representative of reality



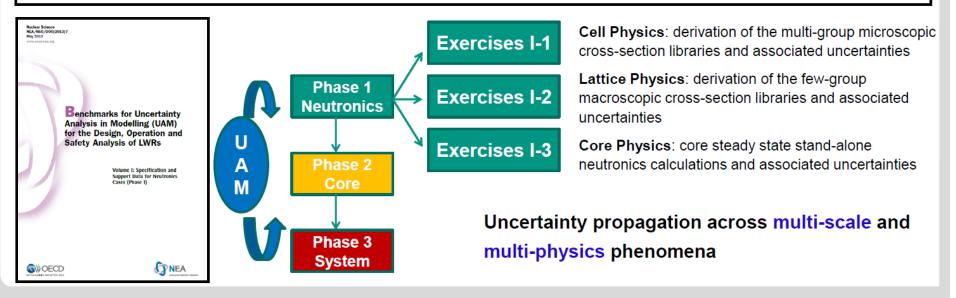


Introduction



- In recent year there has been an increasing demand from nuclear research, industry, safety, and regulatory bodies for best estimate predictions of LWRs performances to be provided with their confidence bound
- Understanding uncertainties of evaluated reactor parameters is important for introducing appropriate design margins and deciding where additional efforts should be undertaken to reduce those uncertainties

OECD/UAM Benchmark for <u>Uncertainty Analysis in Modeling for Design</u>, Operation and Safety Analysis of LWRs



S/U analysis

Different approaches

- 1. Direct perturbation
- 2. Perturbation/Generalized perturbation theories
- 3. Statistical sampling
- 4. Total Monte-Carlo (TMC)

The statistical approach to uncertainty

- Uncertainty in input values described by PDF's
- The model output is a random variable whose distribution reflects the uncertainty in the output associated with the uncertainty in the input
- If one would know the probability distribution of the output one would be able to answer as precise as possible all questions about the likelihood of its values. The assumption of normal distribution is made
- Statistics offers the means to "quantify the goodness" of the output values
- Wilk's formula

$$1 - \alpha^n \ge \beta$$
 (one sided)

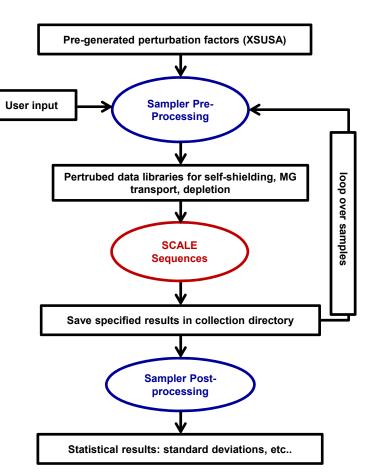
$$1 - \alpha^n - n \cdot (1 - \alpha) \cdot \alpha^{n-1} \ge \beta$$
 (two sided)

	One-s	ided stat limits	istical	Two-sided statistical limits			
β/α	0.90	0.95	0.99	0.90	0.95	0.99	
0.90	22	45	230	38	77	388	
0.95	29	59	299	46	93	473	
0.99	44	90	459	64	130	662	



The SAMPLER sequence

- The SAMPLER module within SCALE provides uncertainty in any computed results from any SCALE sequence due to uncertainties in:
 - Neutron cross sections
 - Fission yield and decay data
 - Geometry and composition
- SAMPLER employs sampling techniques to propagate UQ for random uncertainties
 - Given input PDF: $p(\overline{x})$
 - Given QOIs, forward model: $\overline{y} = \overline{F}(\overline{x})$
 - Compute N realizations of \bar{x} : { $\bar{x}_1, \bar{x}_2, \dots, \bar{x}_N$ }
 - Evaluate forward model of each realization $\{\overline{y}_1, \overline{y}_2, \dots, \overline{y}_N\}$
 - Construct uncertainty quantities from sampledependent QOI data
 - Means, SDs, correlation coefficients, histograms

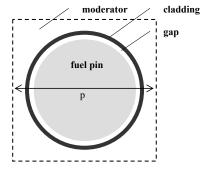




Problem definition and modeling

- The UAM burn-up pin cell (Exercise I-1b)
 - Power: 33.58 kW/kgU
 - Final burn-up: 61.GWd/MTU
 - Requested output
 - K-inf
 - One-group (n,f) and (n, γ) reaction rates for U and Pu isotopes
 - Actinides and FPs isotopic concentrations





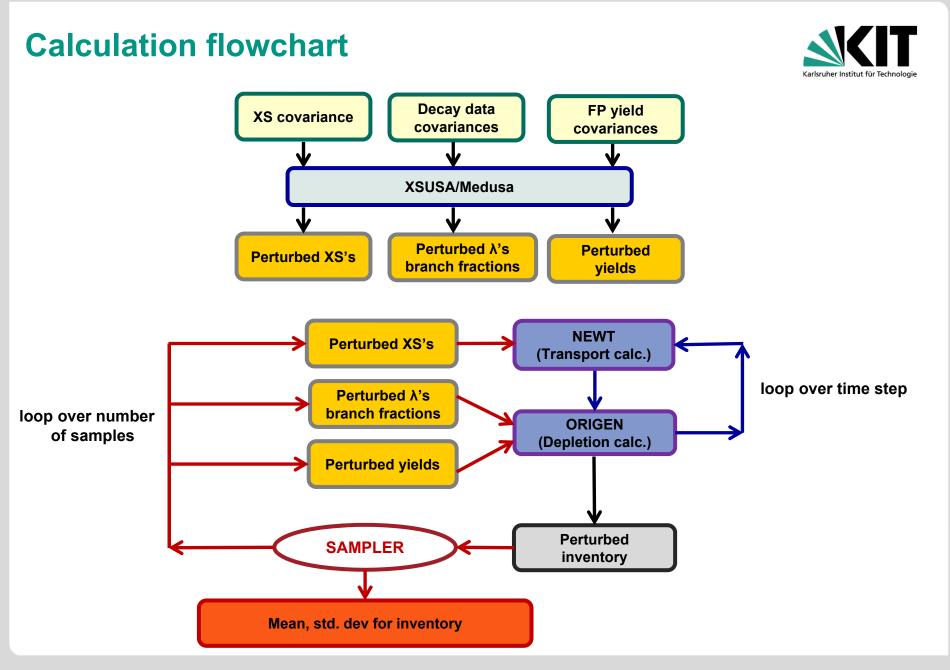
p – pitch of the unit cell

The SCALE 6.2.2 code and ENDF/B.VII.1 nuclear data have been used

- TRITON sequence (NEWT + ORIGEN-S)
 - NEWT used to calculate weighted burn-up dependent XS's
 - BONAMI and CENTRM solvers for XS self-shielding
 - 56-group ENDF/B.VII.1 XS library
 - 56-group ENDF/B.VII.1 covariance library

• SAMPLER

- 1000 samples



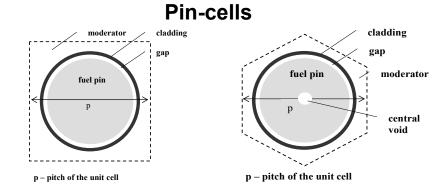
Stochastic sampling vs. GPT



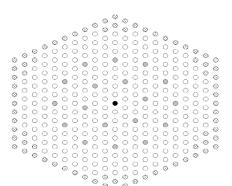
 Comparison of the stochastic approach against the GPT approach showed an excellent agreement of the results^(*)

Test		Calculation method						
	Operating condition	G	PT	Sampling				
case	condition	k _{inf}	Uncert.	k _{inf}	Uncert.			
BWR	HZP	1.3428	6.8E-01	1.3430	5.4E-01			
	HFP	1.2249	5.9E-01	1.2252	5.7E-01			
PWR	HZP	1.4253	5.4E-01	1.4254	5.0E-01			
	HFP	1.4063	5.5E-01	1.4064	5.0E-01			
VVER	HZP	1.3457	5.8E-01	1.3458	5.3E-01			
	HFP	1.3276	5.8E-01	1.3278	5.4E-01			

Test case: VVER – Kozloduy 6									
Response	TSUN	AMI	SAMPLER (N=93)						
	Value	δR/R	Value	δR/R					
Σ _f (gr. 1)	2,411E-03	5,071E-01	2,435E-03	5,505E-01					
Σ _f (gr. 2)	gr. 2) 5,615E-02		5,701E-02	3,368E-01					
Σ _a (gr. 1)	1,408E-02	1,343E+00	1,410E-02	9,076E-01					
Σ _a (gr. 1)	9,485E-02	8,810E-01	9,645E-02	1,994E-01					
nu-fission (gr.1)	6,159E-03	_	6,218E-03	8,418E-01					
nu-fission (gr.2)	1,368E-01	-	1,390E-01	4,539E-01					



FAs

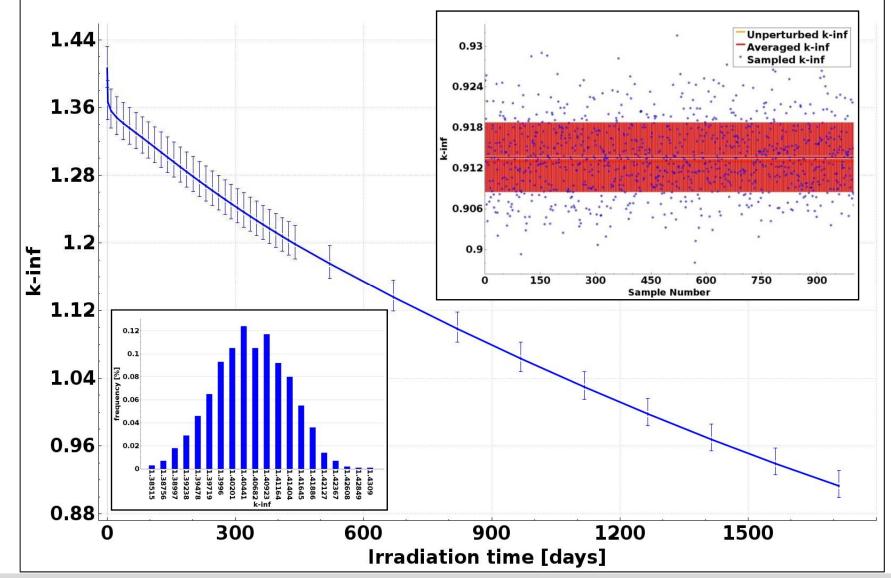


^(*)L. Mercatali et al.: "SCALE Modeling of Selected Neutronics Test Problems within the OECD UAM LWR's Benchmark", Science and Technology of Nuclear Istallations, ID 573697, Volume 2013 (2013).



k-inf vs. irradiation time







Uncertainty on k-inf



- Three sets of 1000 samples each:
 - 1. XS perturbation
 - 2. Decay data perturbation
 - 3. FY perturbation

Deserver	Perturbed case							
Burnup	XS	FY	Decay					
[GWd/MTU]	RSD (pcm)	RSD (pcm)	RSD (pcm)					
0	545	0	0					
10	503	10	4					
20	495	13	3					
30	494	18	3					
40	505	23	3					
50	527	28	2					
60	560	31	2					

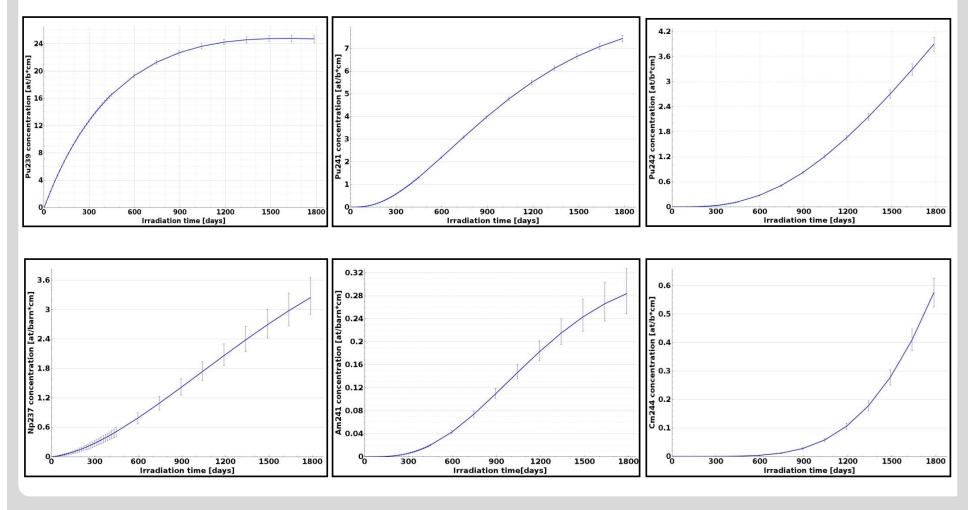
Contributions to the uncertainty on k-inf

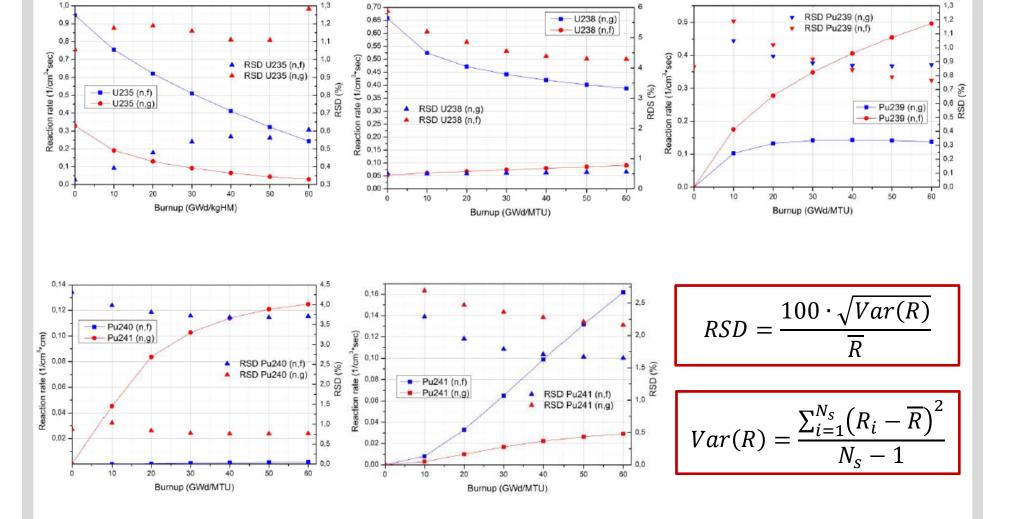
CPU time:19,46 days on a single processor

Concentrations of actinides



- Uncertainty mainly due to XS
- Uncertainty increases with irradiation time

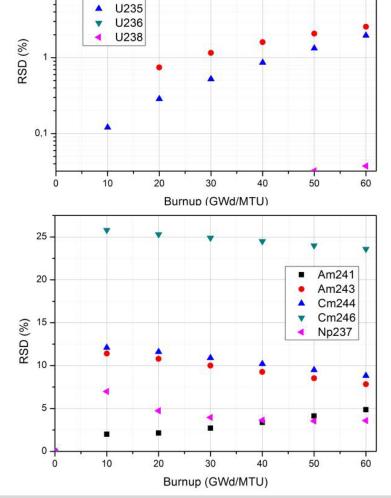




Reaction rates



¹⁴ ICONE26, July 22-26, 2018 (London, UK)



U233

U234

10 -

6 -					Pu:	242		
			-					
(%) - 4					-	-		
-		-	•					
2 -	*	•	\$	ŧ	•	•		
0	10	20	30	40	50	60		
			nup (GWd					
RSD [%]			ls	otop	es			
0 – 2	U ²³	⁵ , U ²³⁸	⁸ , Cs ¹³	³⁷ , Nd	¹⁴⁶ , No	d ^{148,} Cs	137	
2 – 5	Pu ²³⁸ , Pu ²³⁹ , Pu ²⁴⁰ , Pu ²⁴¹ , Pu ²⁴² , Am ²⁴¹ , Np ²³⁷ , Ag ¹⁰⁹ , Cs ¹³⁴ , Nd ¹⁴³ , Nd ¹⁴⁵ , Sm ¹⁴⁸ , Sm ¹⁵¹ , Sm ¹⁵² , Eu ¹⁵¹ , Eu ¹⁵³ , Gd ¹⁵⁶ , Gd ¹⁵⁸							
5 – 10	Am ²⁴³ , Cm ²⁴⁴ , Eu ¹⁵⁴ , Gd ¹⁵⁴							
> 20	Cm ²⁴⁶ , Eu ¹⁵⁵ , Gd ¹⁵⁵							

Uncertainties on nuclide concentrations

10

8



Pu238

Pu239

Pu240

Pu241

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Correlation analysis

- Pearson's coefficients (Pc)
- $\rho > 0 \rightarrow$ correlation, $\rho < 0 \rightarrow$ anti-correlation
- $|\rho| = 1 \rightarrow \text{perfect linear relationship}$

$$P_c = \frac{Cov(x, y)}{SD(x) \cdot SD(y)} \in [-1, 1]$$

0 GWd/MTU									
kinf	1.000								
$\Sigma_{a,1}$	-0.488	1.000							
$\Sigma_{a,2}$	-0.218	0.170	1.000						
$\Sigma_{f,1}$	0.405	-0.073	0.083	1.000					
$\Sigma_{f,2}$	0.345	0.038	0.415	0.319	1.000		4		
$v\Sigma_{f,1}$	0.630	-0.279	0.059	0.808	0.187	1.000			
νΣ _{f,2}	0.696	0.061	0.291	0.213	0.617	0.403	1.000		
D1	0.291	-0.858	-0.038	-0.001	-0.053	0.271	-0.053	1.000	
D2	-0.021	-0.146	-0.007	-0.129	-0.053	-0.078	-0.061	0.245	1.000

60 GWd/MTU									
k _{inf}	1.000								
$\Sigma_{a,1}$	-0.600	1.000							
$\Sigma_{a,2}$	0.051	0.401	1.000						
$\Sigma_{f,1}$	0.539	-0.262	0.678	1.000					
$\Sigma_{f,2}$	0.280	0.348	0.942	0.682	1.000				
$v\Sigma_{f,1}$	0.558	-0.265	0.638	0.972	0.636	1.000			
νΣ _{f.2}	0.275	0.368	0.944	0.667	0.996	0.625	1.000		
D1	0.610	-0.779	0.127	0.678	0.163	0.658	0.143	1.000	
D2	0.087	-0.291	-0.267	-0.151	-0.239	-0.143	-0.244	0.227	1.000



Summary



- A cell physics exercise has been performed, aiming to assess the uncertainties associated with the basic nuclear data in burn-up calculations for a typical PWR fuel pin-cell through a stochastic sampling approach
- Results obtained with the stochastic sampling method are in very good agreement with the ones obtained via GPT
- Uncertainties have been quantified as a function of the depletion time
- FY and decay constants have a negligible impact on the total uncertainty, the main contributor being the XS uncertainty
- The study represents the first step towards the uncertainty quantification for more complex burn-up problems (FAs, full core)