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Institute

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Reactor  
Engineering  
Division



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Reactor Engineering Division

# Thermal Fluctuations in Low-Prandtl Fluid Flows over a Backward Facing Step

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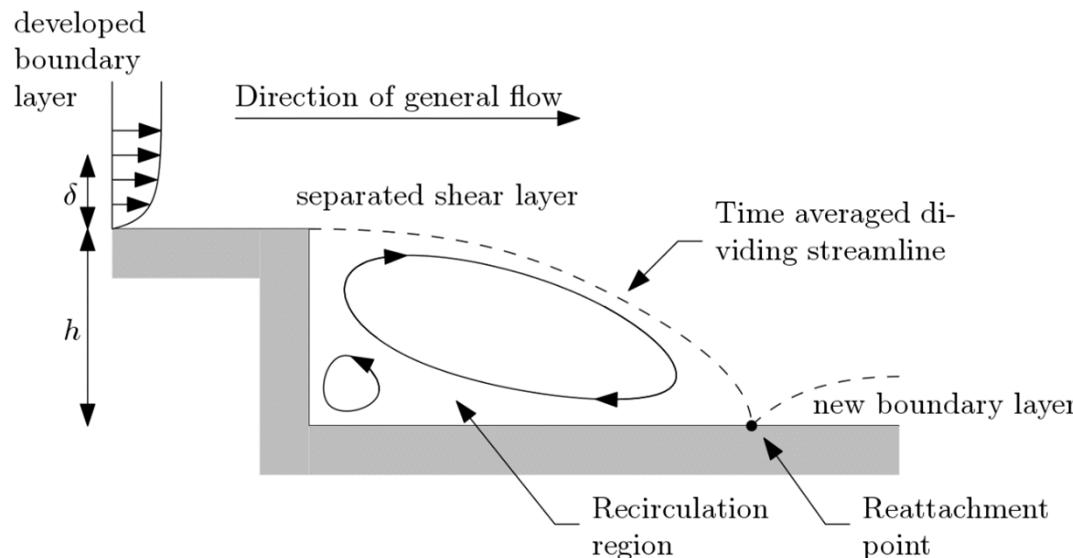
Nuclear Research and Consultancy Group (NRG), Petten, The Netherlands



# Outline

- Introduction
- Description of experiment
- DNS results, flow structure
- Comparison with RANS simulation

# Backward facing step

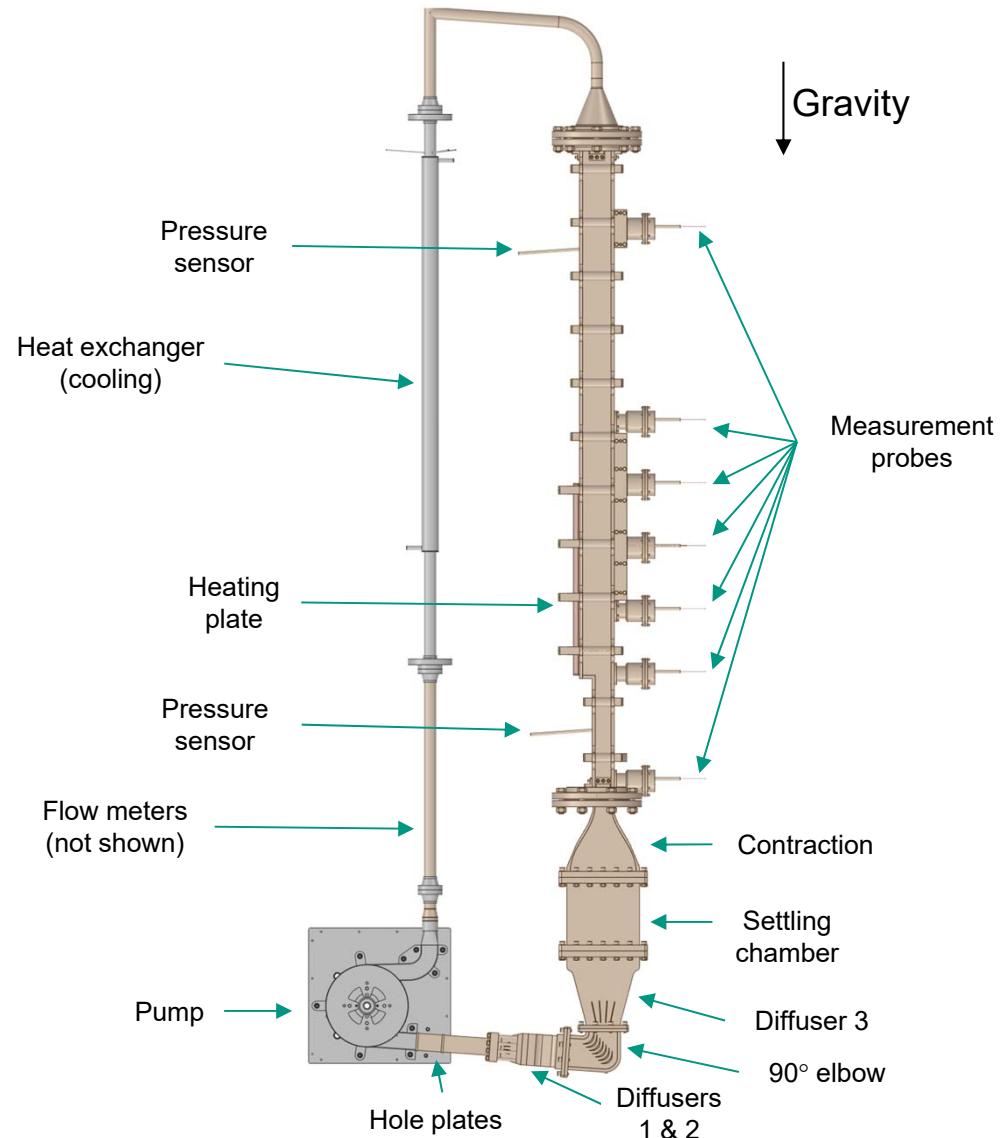


- representative geometry for sudden expansions
- expand reference database
- penetration of thermal fluctuations into solid walls

# DITEFA 2 – Facility description

- 30 liters of GaInSn ( $Pr = 0.025$  at  $50^\circ C$ )
- Temperature range:  $20 - 80^\circ C$
- Max. flow rate =  $1.5 \frac{L}{s}$
- 2 **flow meters** (turbine and inductive flow meter)
- 2 **hole plates** for flow correction
- 3 **wide angle diffusers** with vanes and screens at inlet and outlet
- **Settling chamber** with honeycomb and 3 screen stages
- **Contraction** with 5:1 contraction ratio
- 7 **Measurement probes** for local velocity and temperature measurement
- **Heating plate** with  $20800 [W/m^2]$
- Pressure difference measurement in test section

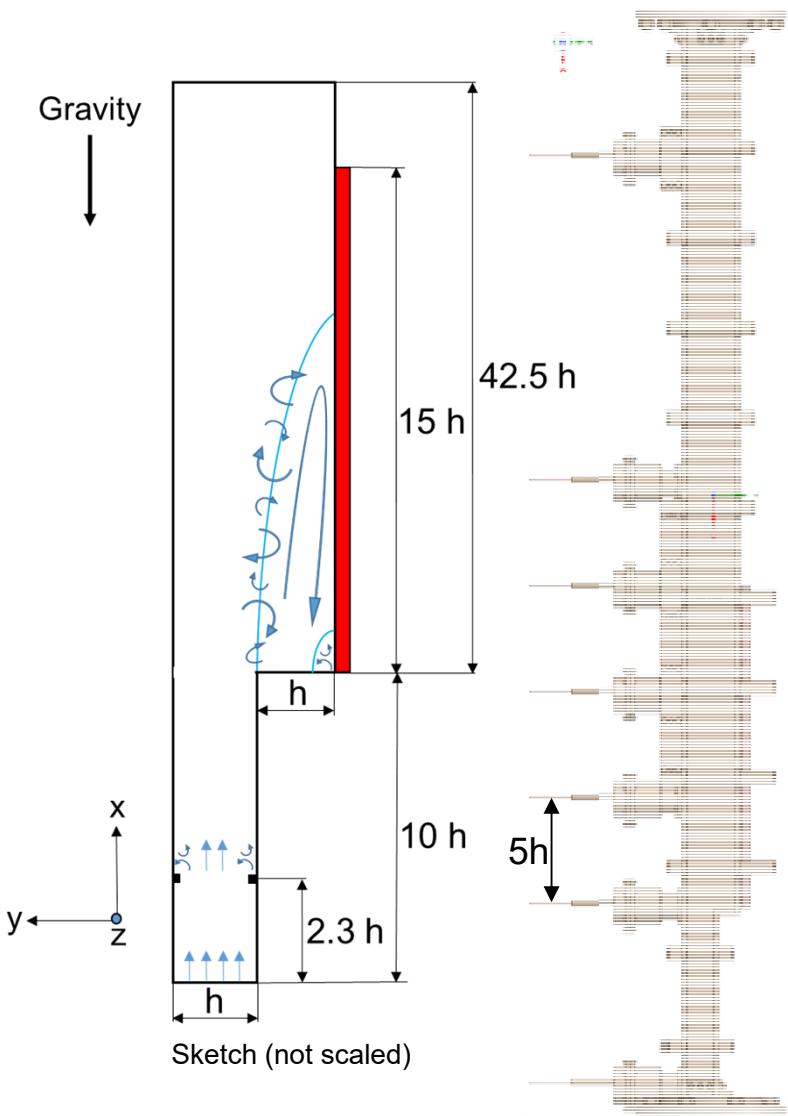
Manufacturing currently in its **final stage**



# DITEFA 2 – BFS parameters

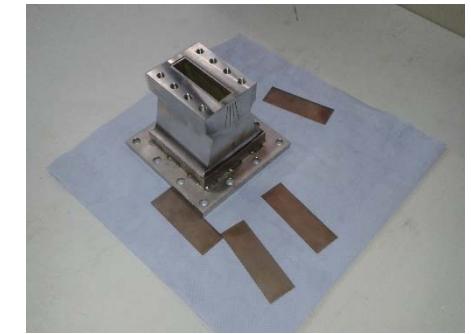
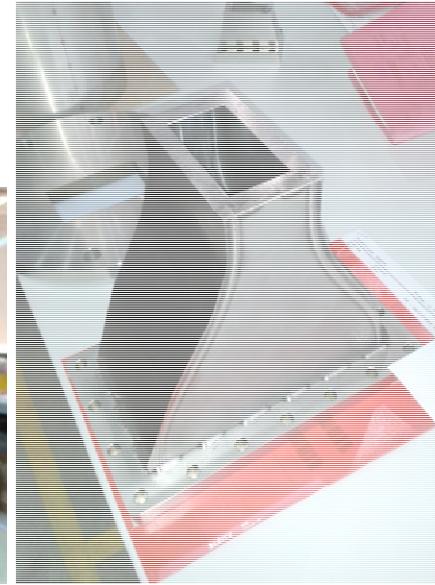
- Forced and mixed-convection regimes
- BFS aspect ratio = 2
- BFS expansion ratio = 2
- Low turbulence intensity and nearly constant velocity profile at inlet
- Trip-wire for forcing transition from laminar-to-turbulent boundary layer
- 120 thermocouples mounted in heating plate for wall-temperature profile measurement
- Double-walled test section required (metal+plastic)
- Dimensionless number ranges (see table)

|             | Expected minimum value | Expected maximum value | Comments   |
|-------------|------------------------|------------------------|--|
| $T_{inlet}$ | 20°C                   | 80°C                   | $\Delta T_{max} = \frac{\dot{q}h}{k_{ref}} \sim 30 [^{\circ}\text{C}]$ |
| $Re_h$      | 4 500                  | 54 000                 | $Re_h = \frac{U_b h}{\nu}, \nu = \nu(T = 50^{\circ}\text{C})$          |
| $Pr$        | 0.019                  | 0.031                  |  |
| $Pe_h$      | 115                    | 1 400                  | $Pr = Pr(T = 50^{\circ}\text{C})$                                      |
| $Ri_h$      | 0.005                  | 0.892                  | $Ri_h = \frac{g\beta\Delta Th}{U_b^2}$                                 |



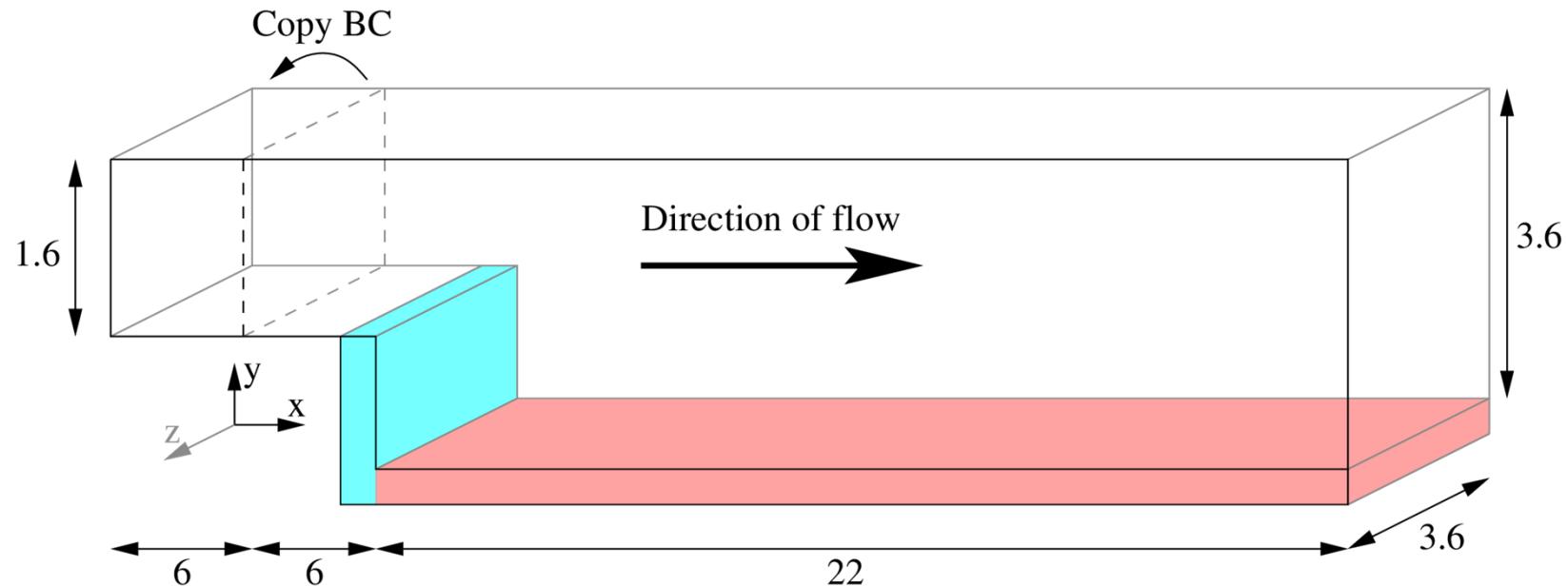
# DITEFA 2 – Time line

- Manufacturing of facility: ~ 05.19
- Manufacturing of PMP: ~ 06.19
- Commissioning: ~ 08.19
- Preliminary results ~ 10.19
- Final results ~ 12.19





# Geometry

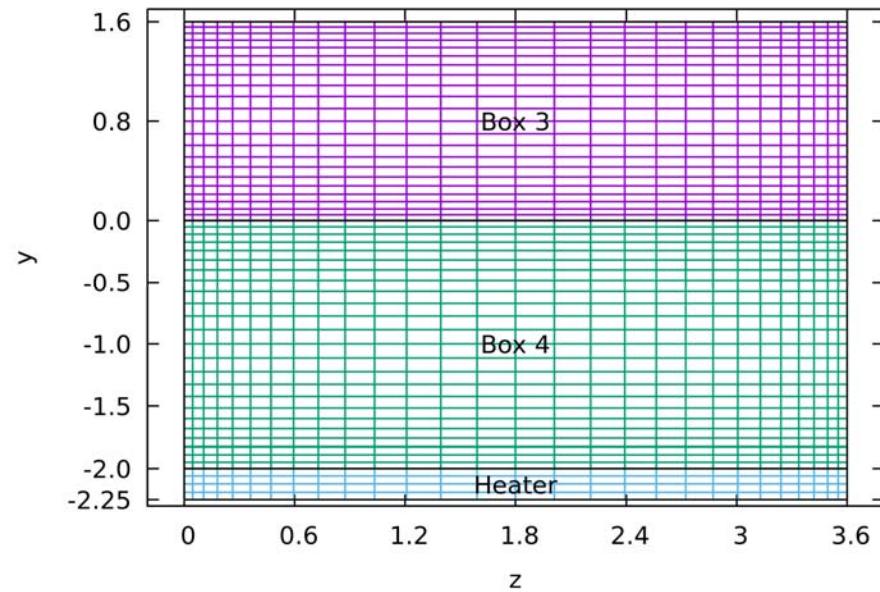
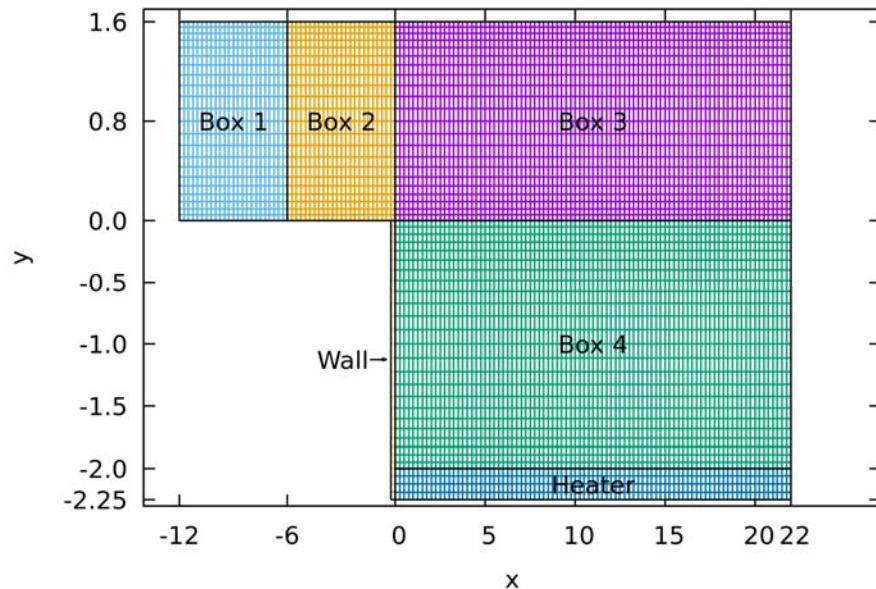


- Walls (for fluid) at all sides except inflow/outflow
- Expansion ratio 2.25
- Thickness of solid walls is 0.25 everywhere
- Recycling inflow boundary condition
  - Imposed average volumetric flux  $\langle u_x \rangle = 1$ ,  $Re = 3200$ ,  $Re_h = 6400$ ,  $Re_D = 7089$ ,  $Re_\tau = 207$
- Outflow pressure zero (with some corrections to eliminate backflow)
- $\frac{\lambda_f}{\lambda_w} = 3$ ,  $\frac{\alpha_f}{\alpha_w} = 10$ ,  $Pr_f = 0.005$ ,  $Pr_w = 0.1$



# Spectral element method

→ NEK5000 (open source, developed by

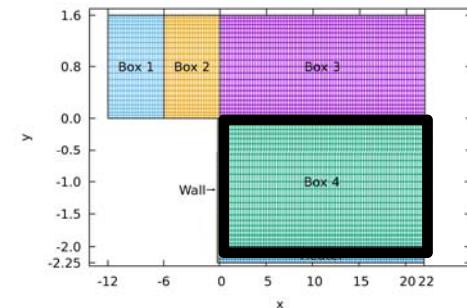
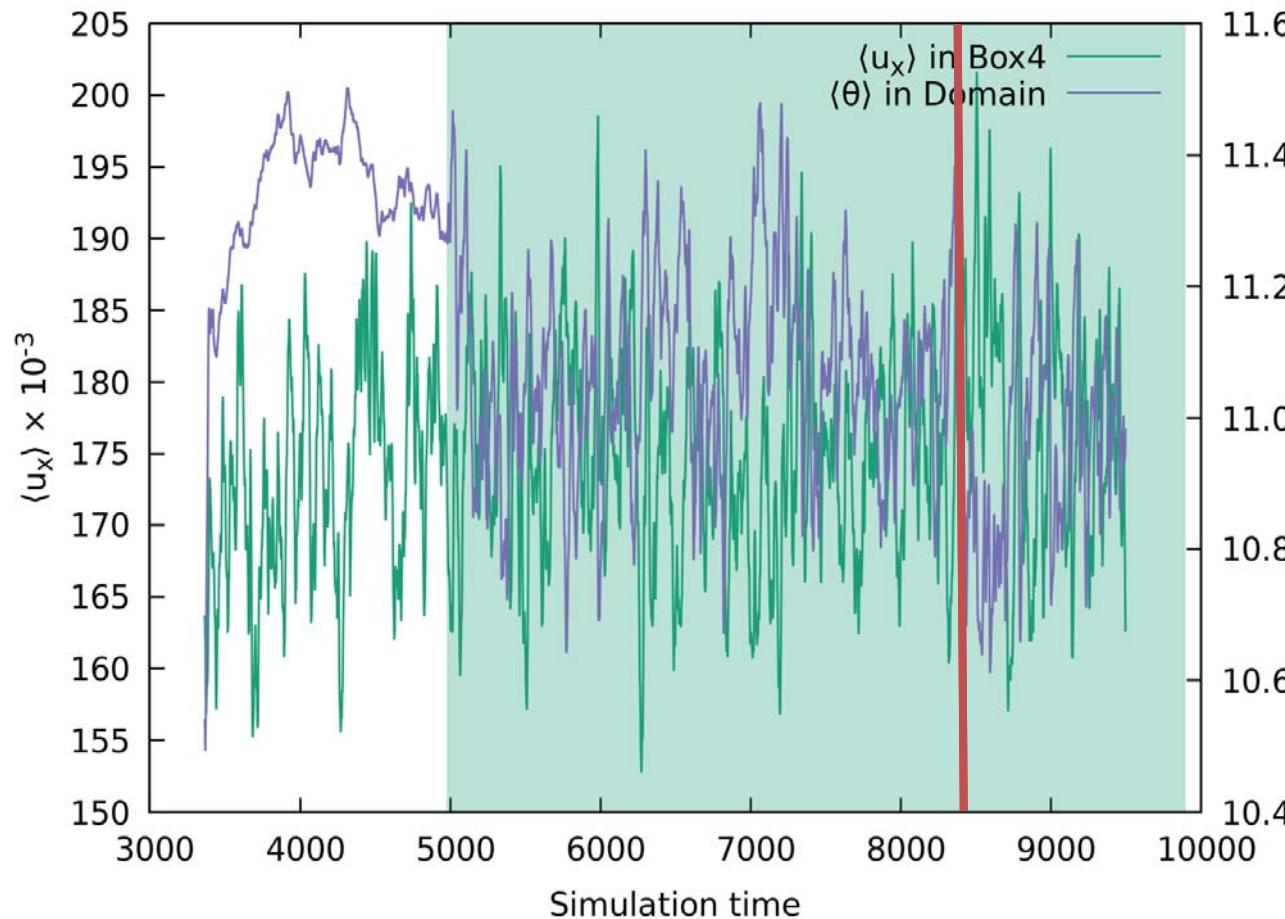


- Total of  $\sim 154 \times 10^3$  elements,  $11 \times 10^3$  solid elements
- 7 collocation points in each direction
- $\sim 49 \times 10^6$  points,  $\sim 31 \times 10^6$  unique points
- CFL  $\sim 0.1$  ( $\Delta t = 4 \times 10^{-4}$ ),  $y^+ < 0.8$



# Convergence

Meeting in Delft



Shaded:  
~3M CPU-hrs

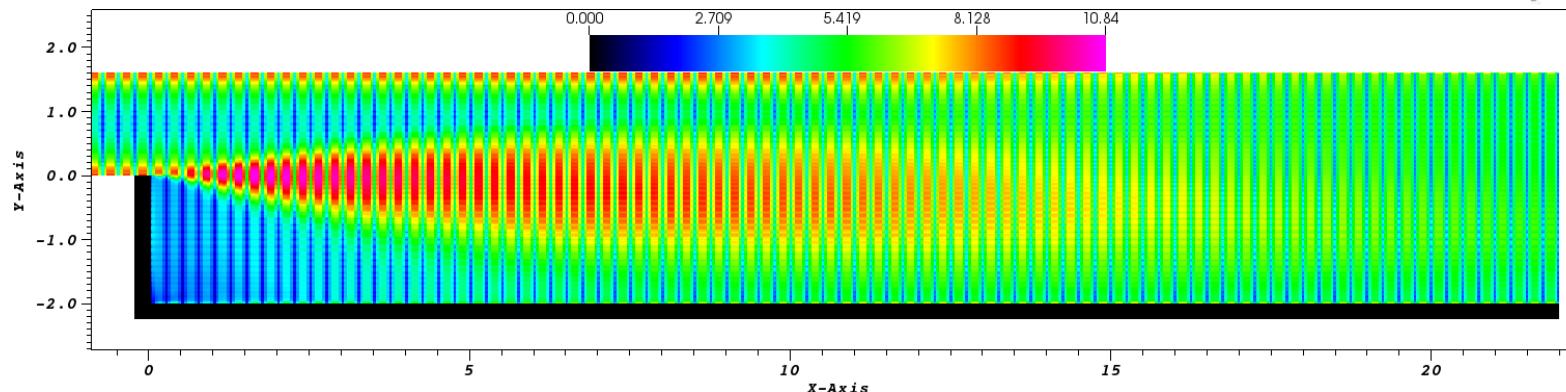
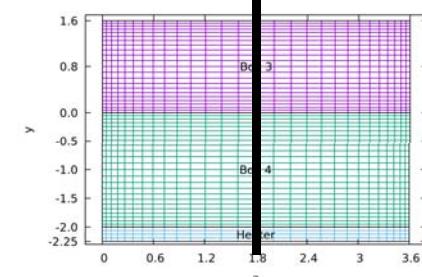
$12 \times 10^6$  steps

4900  
Dimensionless  
time units

1 dimensionless  
time unit  $\sim 0.48$ s



# Kolmogorov length scale



- Maximum diagonal distance between points divided by Kolmogorov length scale
- Ideal  $\frac{\Delta x}{\delta} < 2$  but comparable to Moser, Kim, Mansour DNS of channel flow
- Scale: [0.83,10.84]
- First points in the channel upstream of step:  $y^+ = 0.77$ ,  $z^+ = 0.83$
- Through domain based on friction Reynolds number in channel upstream of the step ( $Re_\tau = 207$ ):
  - $x^+ \in [4.39,12.13]$
  - $y^+ \in [0.77,5.56]$
  - $z^+ \in [0.83,10.20]$

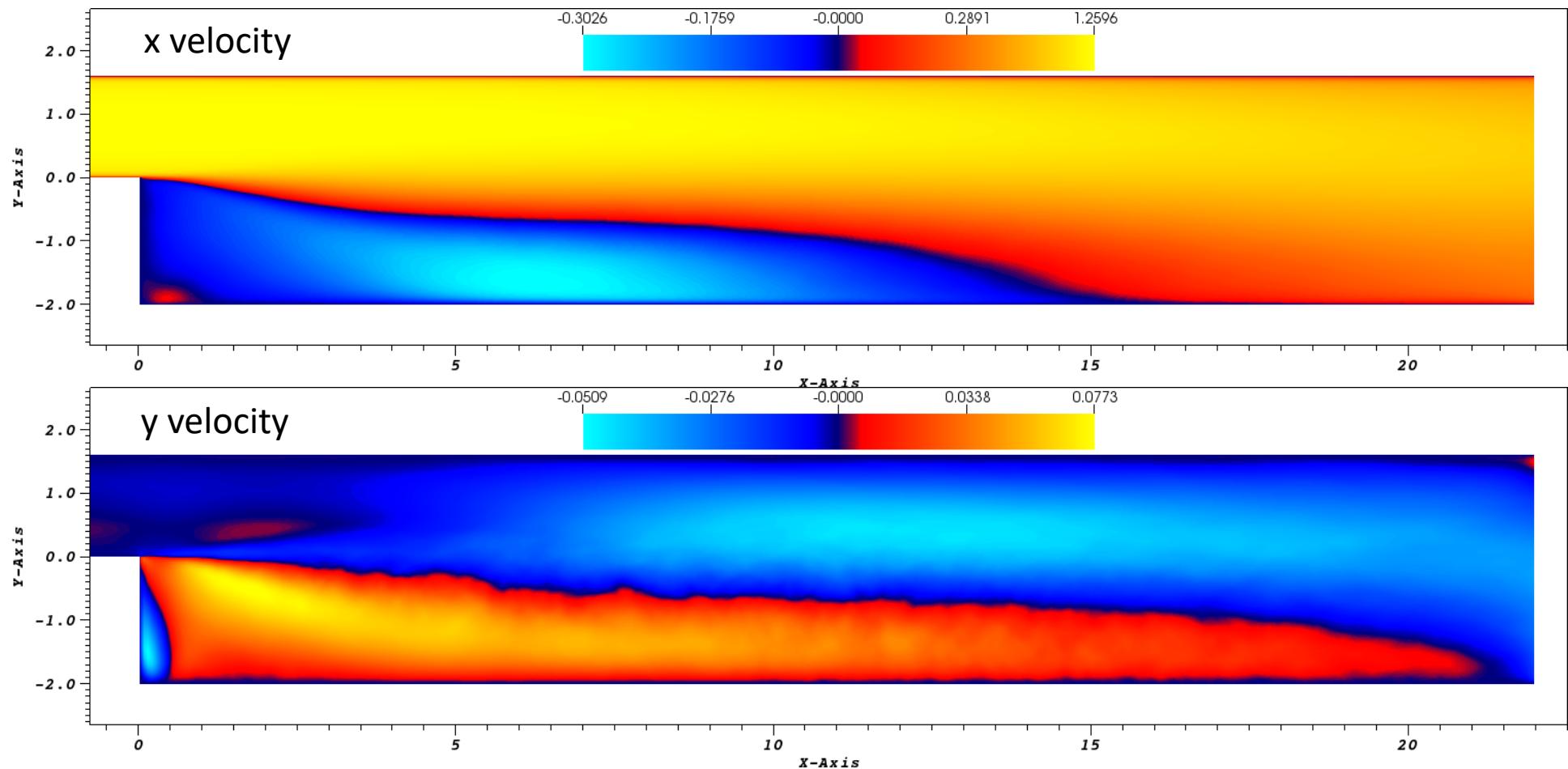
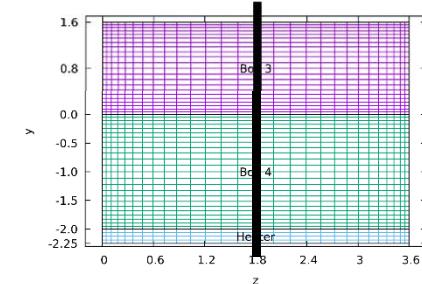


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# Average Flow Structure



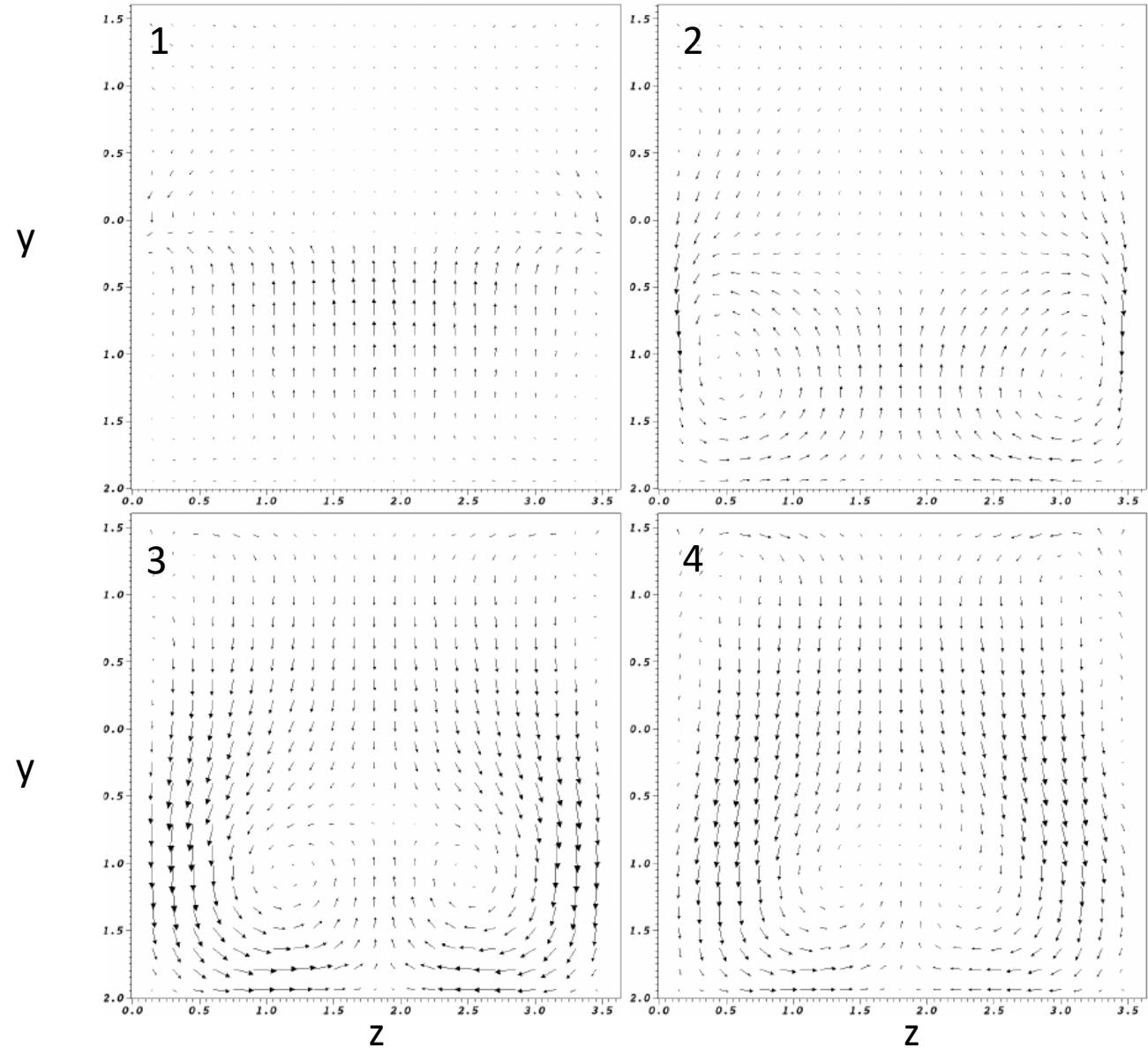
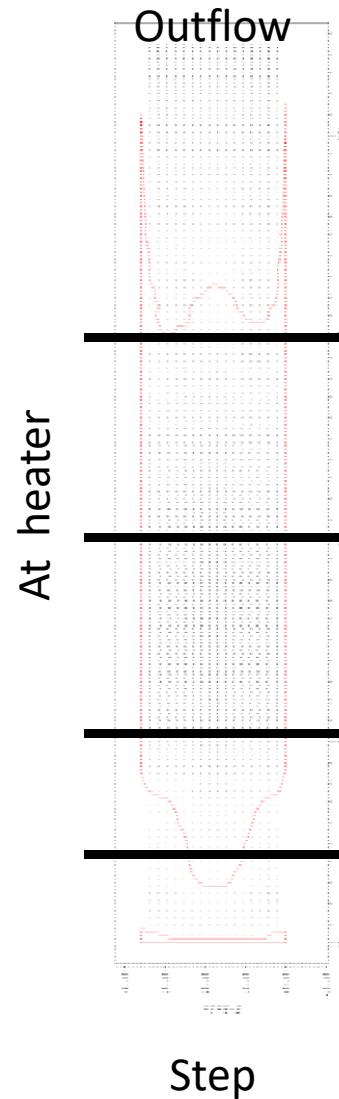


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# Average Flow Structure



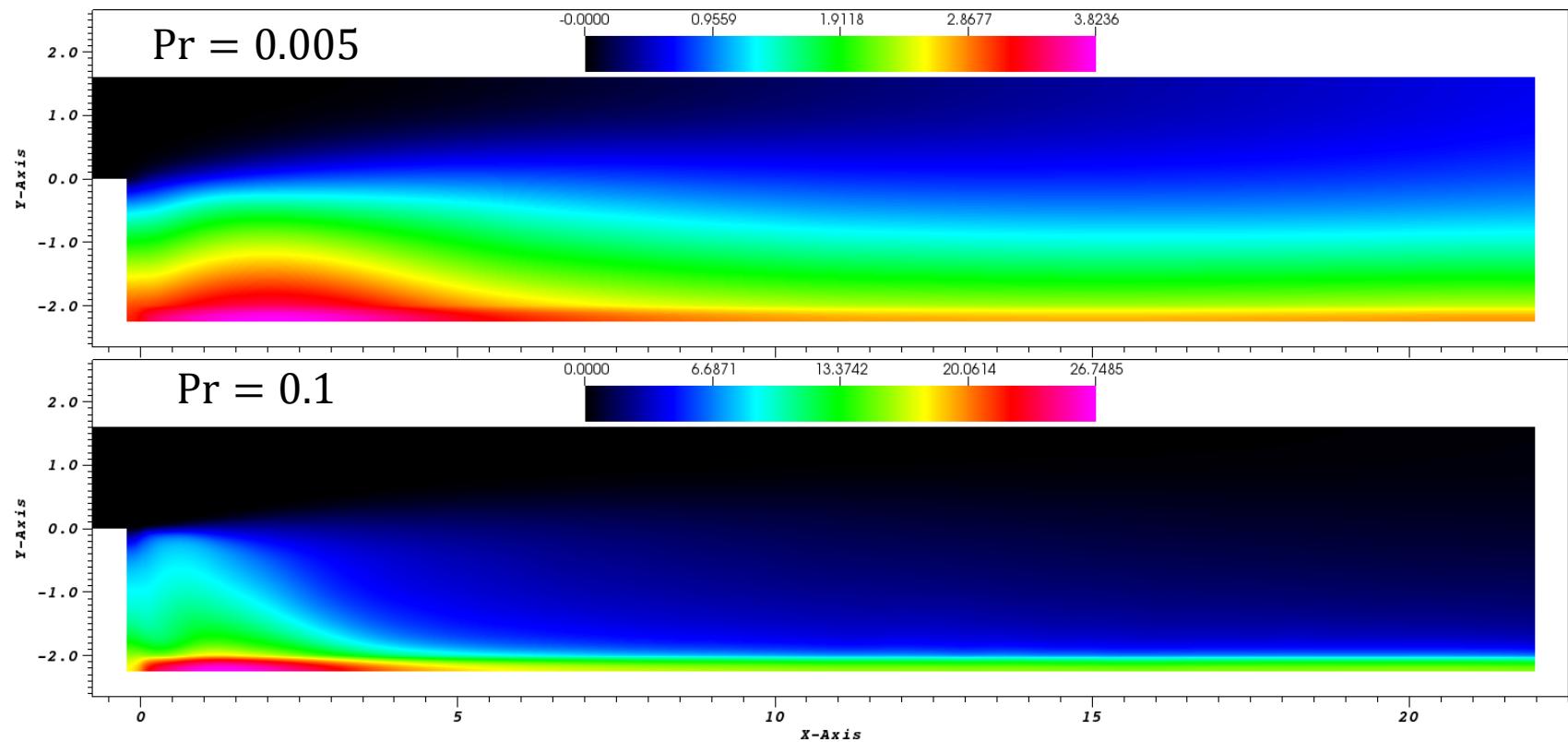
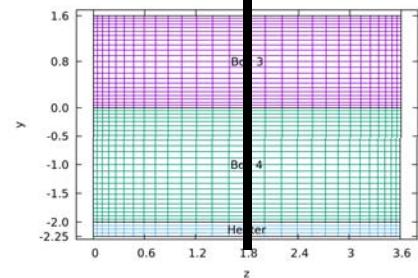


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# Average temperature (middle)



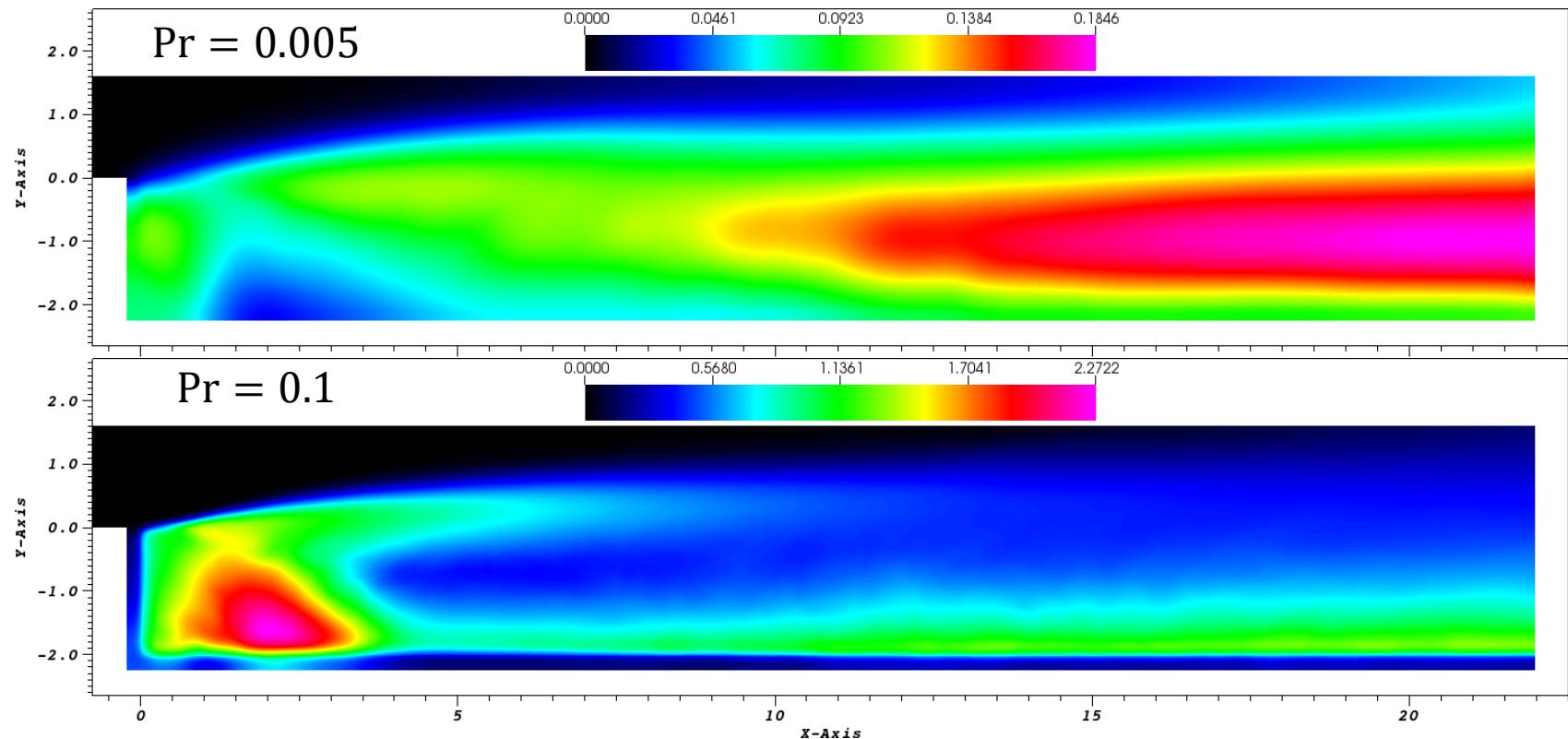
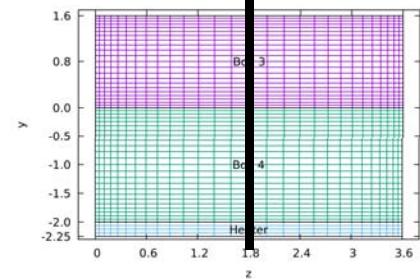


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# Thermal fluctuations (middle)



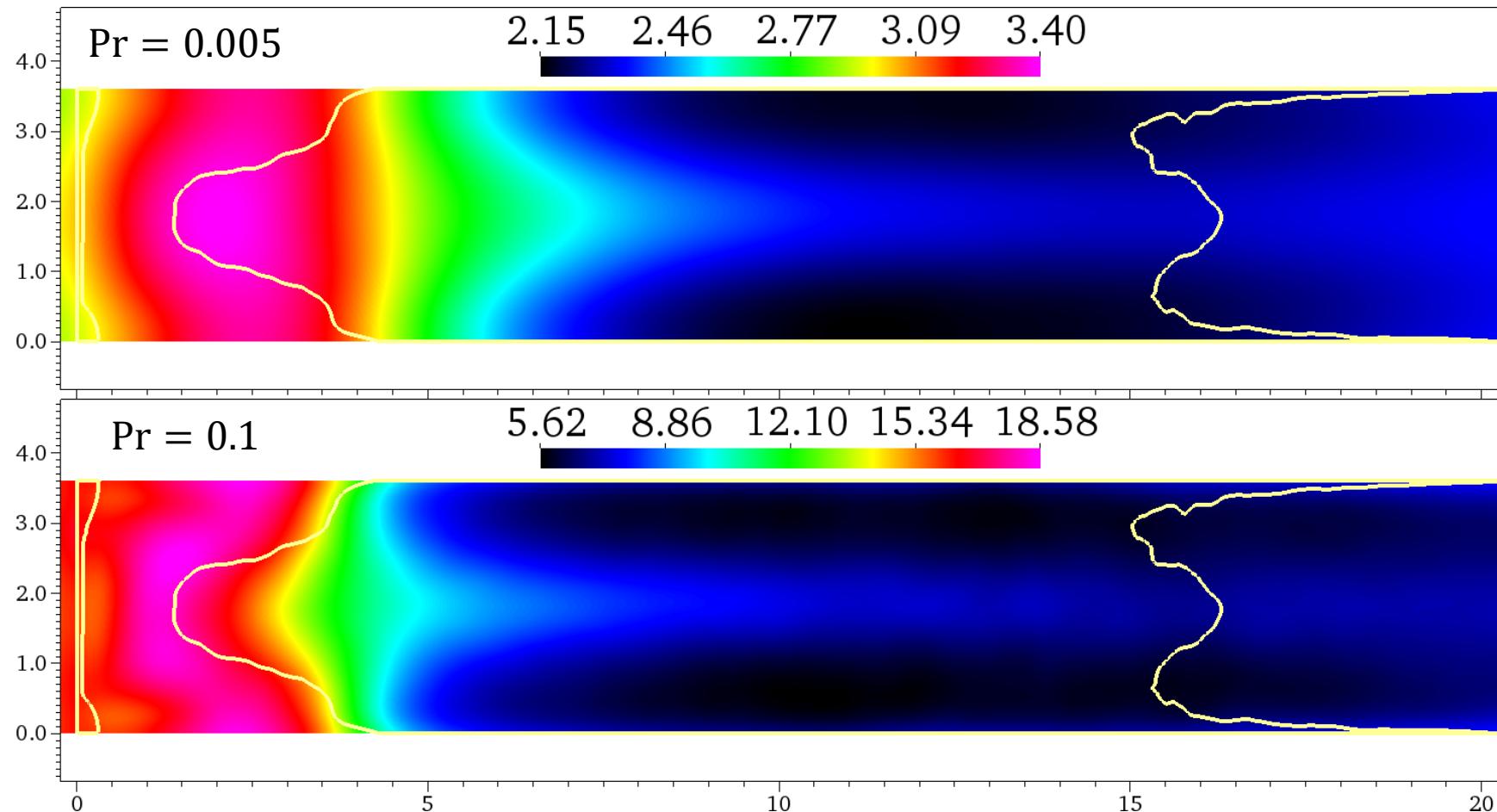
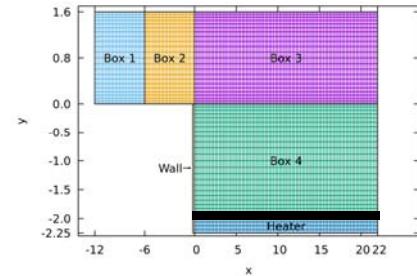


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# Average temperature at heater



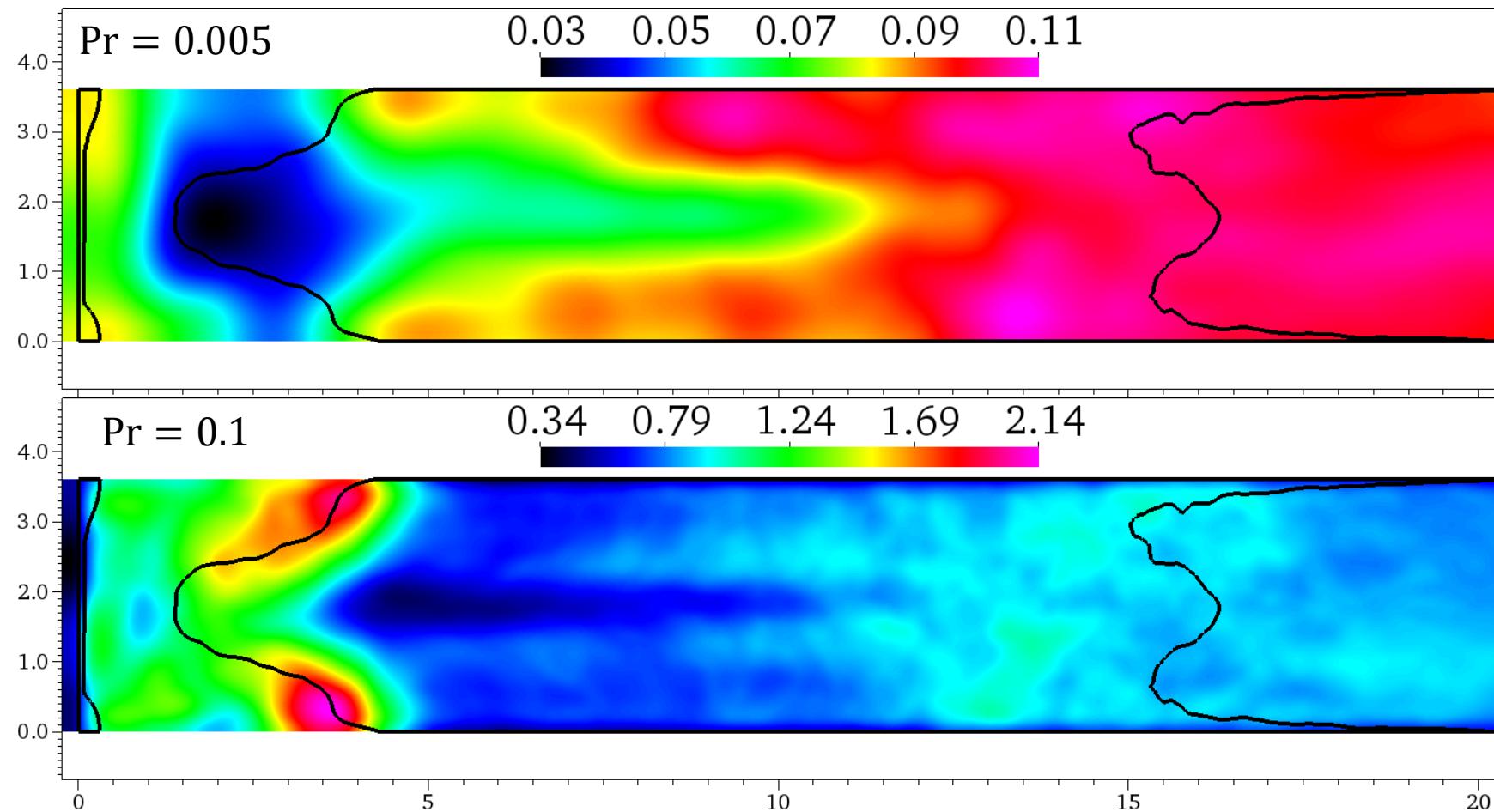
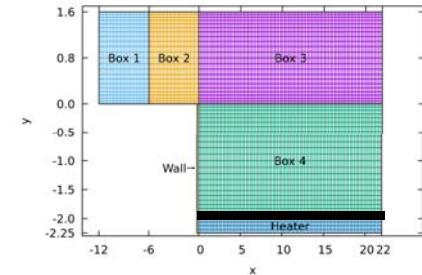


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# Thermal fluctuations at heater





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# RANS simulation

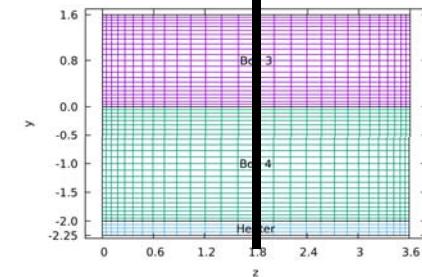
- Identical domain to DNS (including solid parts)
- 6 meshes ranging from 440k to 24.5M elements (4.4M element mesh selected)
- $y^+ < 1$  in whole domain
- Linear  $k - \varepsilon$  model
- AHFM-NRG model



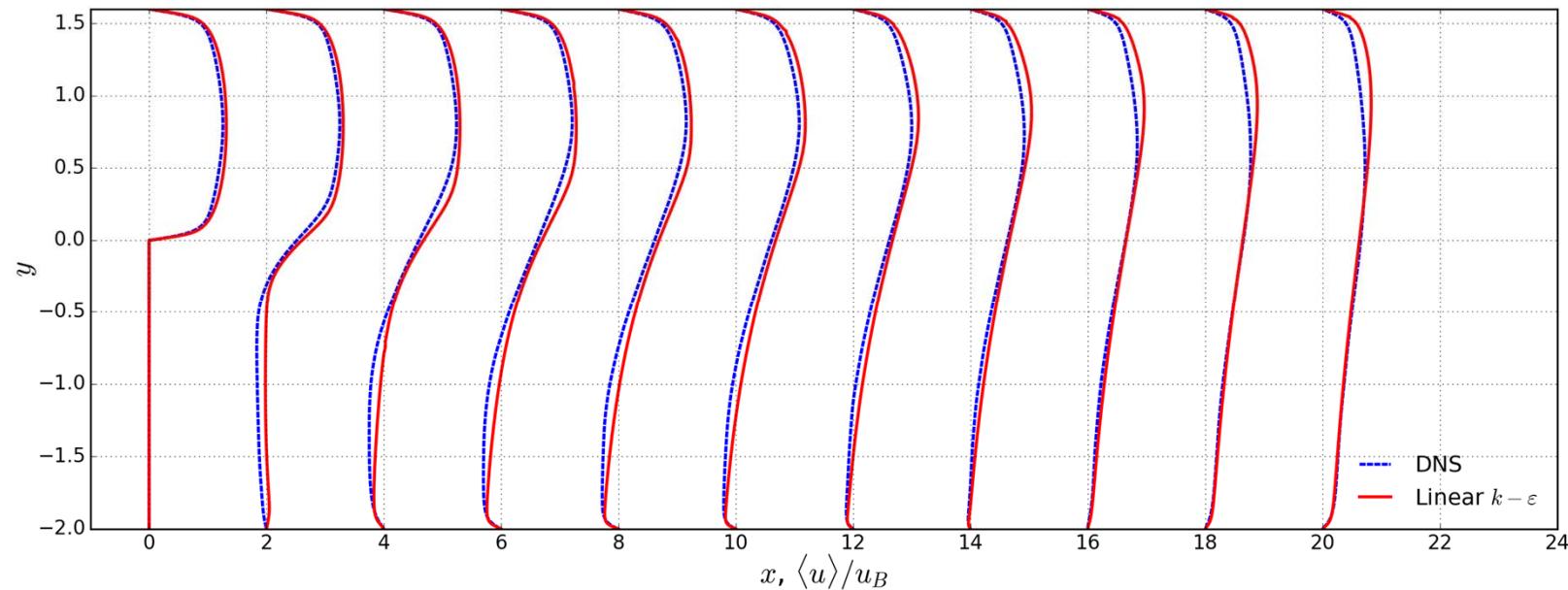
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# Comparison (streamwise velocity)

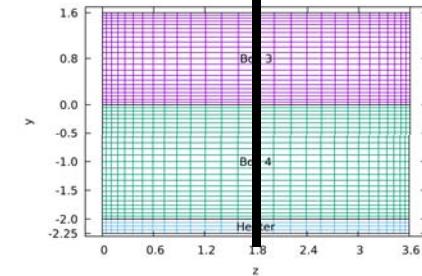




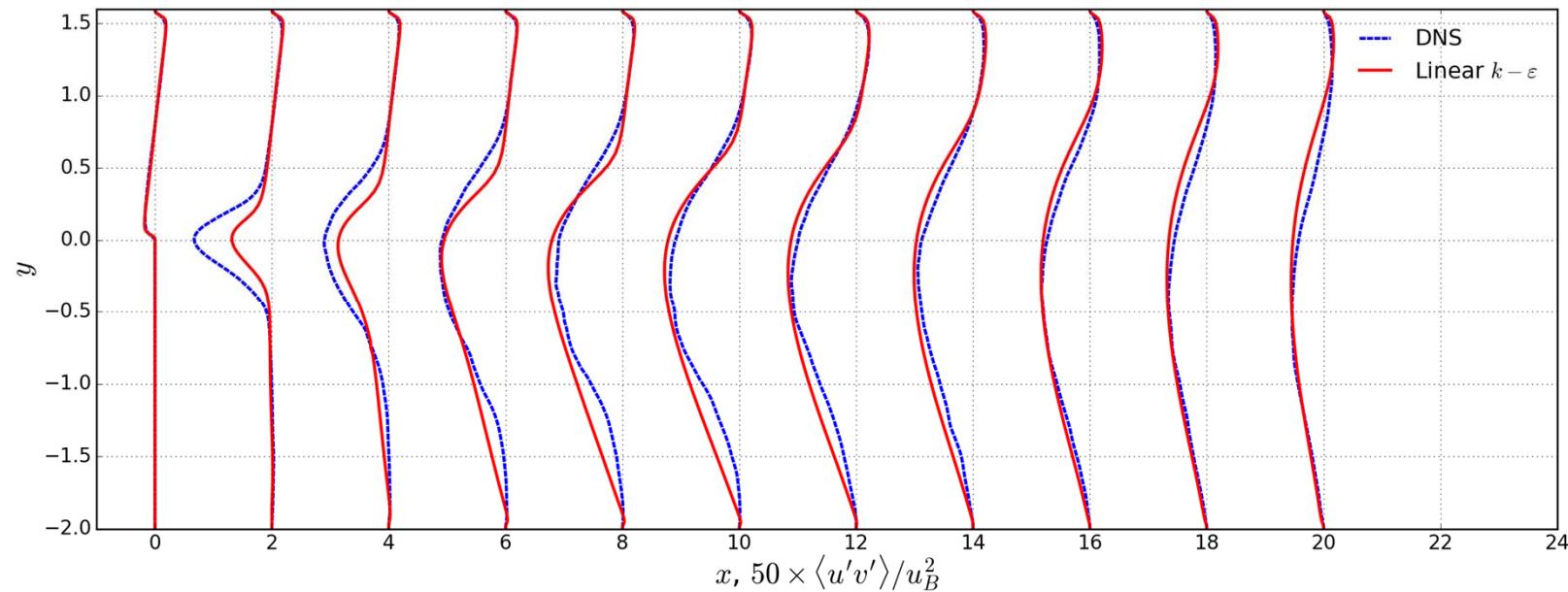
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# Comparison ( $\langle u'v' \rangle$ )

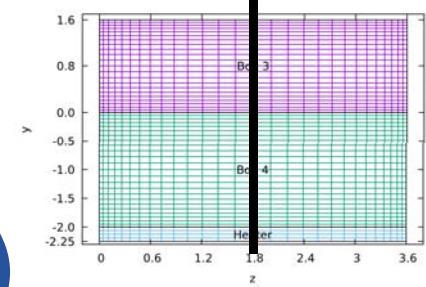




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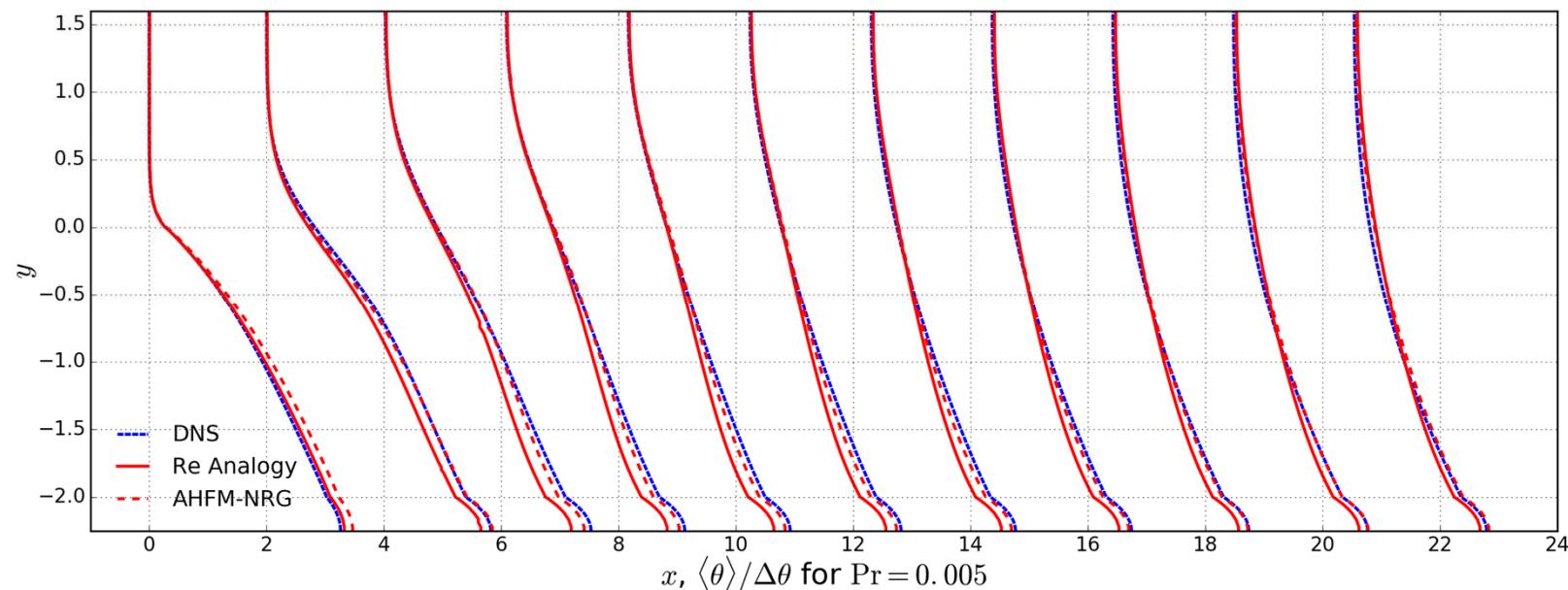


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# Comparison (temperature)

$\text{Pr} = 0.005$





# Summary

- Experimental data by end of year
- DNS data available
- More complicated flow structure than in unconfined BFS
- Thermal fluctuations found penetrating into the walls
- Good agreement in first order statistics between DNS and RANS simulation