

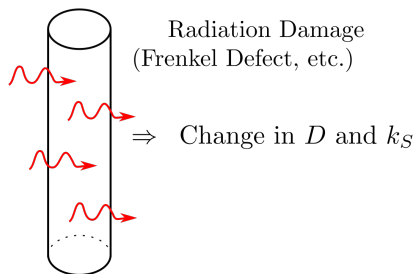
Analytical solution of a gas release problem considering permeation with time dependent boundary conditions

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- Influence of radiation damage on Diffusion and Sieverts' constant



- Setup-Material?
- Heating heals defects!
- How to recover D and k_S from data?

Experiments like this are relevant for:

- Reactor and Fusion-technology,
- Green energy: Storage and transport of H_2 ,
- repository exploration, . . .

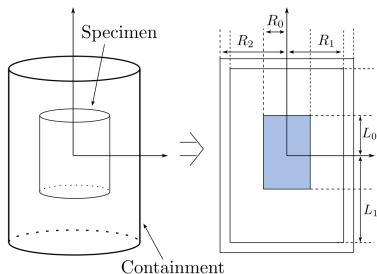
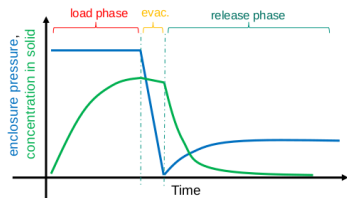
- Motivation
- Experiment, Setup
- Diffusion-Equation with time dependent boundary-conditions
- Explicit Solution for each time interval [Sample]
- Partial pressure of Hydrogen during Release-Interval

Experimental Setup

- Cylinder geometric isovolumetric setup
- Loading with Hydrogen at defined pressure p_L (and Temperature T)
- Evacuate the System
→ $p(t) = p_L \exp[-\lambda t]$
- Recover Sieverts' and Diffusion Constant

$$R_0 = 3.0 \cdot 10^{-3} \text{ m}, L_0 = 3.0 \cdot 10^{-2} \text{ m}$$

$$R_1 = 0.01 \text{ m}, R_2 = 0.02 \text{ m}, L_1 = 0.04 \text{ m}$$



Boundary Conditions

Note: (Sieverts' Law)

On the surfaces the Concentration of (Mono-atomic)-Hydrogen is given by

$$c \equiv k\sqrt{p(t)} \quad \forall t \geq 0$$

$$p(t) = \begin{cases} p_L, & t \in [t_0 = 0, t_1] \\ p_L \exp[-\lambda t], & t \in [t_1, t_2] \\ \text{unclear}, & t \in [t_2, t_3] \end{cases}$$

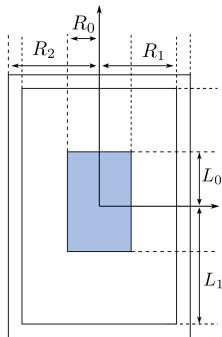
Note: (Diffusion-Equation)

$$\partial_t c^{(n)} - D_j \Delta c^{(n)} = 0, \quad j \in \{s, c\} \quad t \in [t_n, t_{n+1}]$$

$$c^{(n)}(r, z, t) = k_j \sqrt{p(t)} \quad \text{for} \quad \begin{cases} r \in \{R_0, R_1\} \\ z \in \{\pm L_0, \pm L_1\} \end{cases}$$

$$c^{(n)}(R_2, z, t) \equiv 0$$

$$c^{(n)}(r, z, t_n) = c^{(n-1)}(r, z, t_{n-1}), \quad c^{(-1)} \equiv 0$$



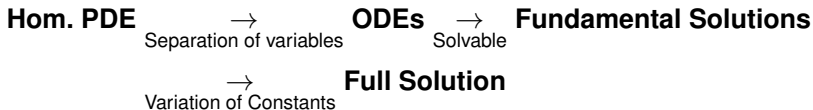
Solving These Equations

Zero-Boundary condition [Sample]

$$g_S(r, z, t) := c(r, z, t) - k_S \sqrt{p(t)}, r \in [0, R_0], z \in [-L_0, L_0]$$
$$\Rightarrow \partial_t g_S - D_S \Delta g_S = k_S \partial_t \sqrt{p}$$

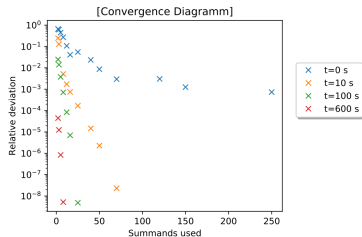
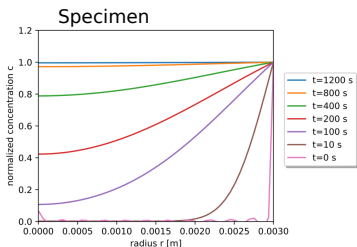
Zero-Boundary condition [Containment, neglecting z]

$$g_C(r, t) := c(r, t) - \tau(r) k_C \sqrt{p(t)}, \tau(r) = \frac{\log[r] - \log[R_2]}{\log[R_1] - \log[R_2]}, r \in [R_1, R_2]$$
$$\Rightarrow \partial_t g_C - D_C \Delta g_C = \tau k_S \partial_t \sqrt{p}$$



Sample: Analytical Solution

$$t \in [0, t_1], p(t) \equiv 3 \text{ kPa}, k_s = 1.829 \cdot 10^{-3} \frac{\text{mol}}{\sqrt{\text{Pam}^3}}, D_s = 7.879 \cdot 10^{-9} \frac{\text{m}^2}{\text{s}}$$



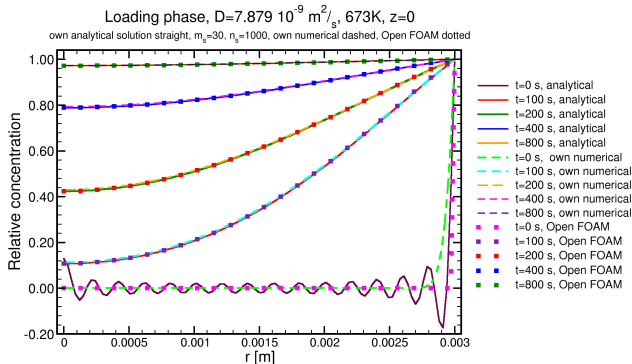
Concentration Profile for $z = 0$.

Relative error of approximation.

$$g_s(r, z, t) = \sum_{n,m} b_{n,m} \exp[-\gamma_{m,n}^2 t] \cos\left((2n+1)\frac{\pi}{2L_0}z\right) J_0\left(x_m \frac{r}{R_0}\right),$$

$$\gamma_{m,n}^2 = D_s \left(\frac{x_m^2}{R_0^2} + \frac{(2n+1)^2 \pi^2}{4L_0^2} \right), b_{m,n} = 8 \frac{(-1)^{n+1} k_s \sqrt{\rho L}}{\pi (2n+1) x_m J_1(x_m)}$$

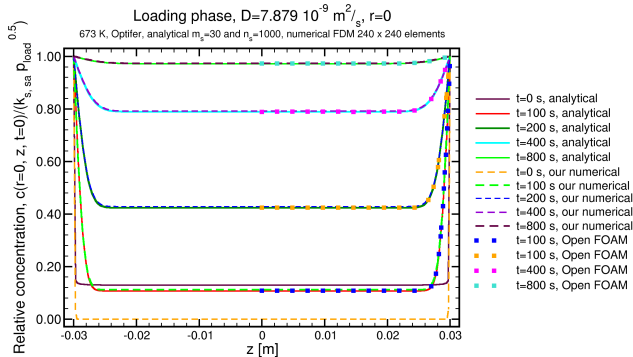
Compare: Numerical (Fortran), Analytical (Python), OpenFOAM



- Analytical Solution Python + Fortran
- Numerical Solution Fortran
- Numerical Simulation OpenFOAM

Different approaches show similar results!

Compare: Numerical (Fortran), Analytical (Python), OpenFOAM

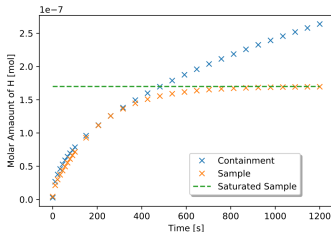
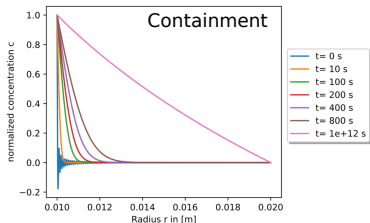


- Analytical Solution Python + Fortran
- Numerical Solution Fortran
- Numerical Simulation OpenFOAM

Different approaches show similar results!

Containment: Analytical Solution

$$t \in [0, t_1], p(t) \equiv 3 \text{ kPa}, k_c = 5.941 \cdot 10^{-4} \frac{\text{mol}}{\sqrt{\text{Pam}^3}}, D_c = 8.257 \cdot 10^{-10} \frac{\text{m}^2}{\text{s}}$$



Concentration Profile for $z = 0$.

Stored amount of Hydrogen.

$$g_c(r, z, t) = \sum_{n=1}^{\infty} A_n \exp\left[-\lambda_n^2 \frac{D}{R_1^2} t\right] \left(\frac{-Y_0(\lambda_n)}{J_0(\lambda_n)} J_0\left(\lambda_n \frac{r}{R_1}\right) + Y_0\left(\lambda_n \frac{r}{R_1}\right) \right)$$

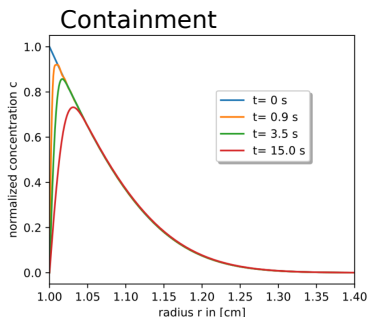
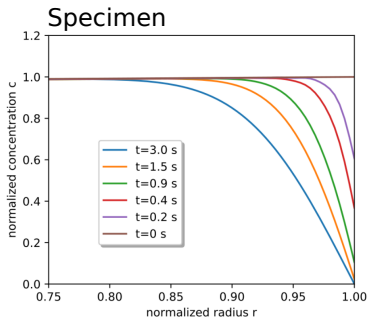
$$\det \begin{pmatrix} J_0(\lambda_n) & Y_0(\lambda_n) \\ J_0\left(\lambda_n \frac{R_1}{R_2}\right) & Y_0\left(\lambda_n \frac{R_1}{R_2}\right) \end{pmatrix} = 0, A_n = -k \sqrt{\rho_L} \frac{\int_{R_1}^{R_2} \tau(r) u_n(r) r dr}{\int_{R_1}^{R_2} u_n(r)^2 r dr}$$

Pumping Interval

Fick's Law $\rightarrow c(r, z, t) = p_L \exp[-\lambda t]$, for $r \in \{R_0, R_1\}, z \in \{L_0, L_1\}$

Fixed Ratio: 97 % He and 3 % H_2

Remaining Partial Pressure: $\Rightarrow p_{H_2}(0.9s) = 1\text{Pa}$



$$\frac{m_H^s(800\text{ s}+0.9\text{ s})}{k_s \sqrt{P_L} V_{\text{sample}}} \approx 96\%$$

$$\frac{m_H^c(800\text{ s}+0.9\text{ s})}{k_s \sqrt{P_L} V_{\text{sample}}} \approx 124\%$$

Release Interval

Problem: $p(t)$ in gaseous phase unknown \Rightarrow No Boundary Conditions

Note: (Initial Guess)

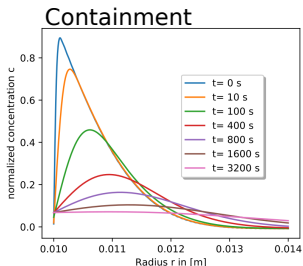
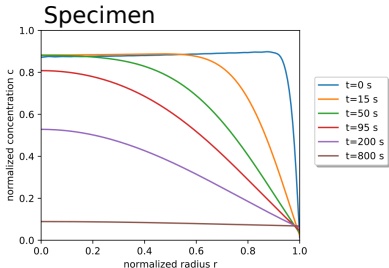
$$\sqrt{p(t)} = \frac{\sqrt{p_f} - \sqrt{p_0}}{1 - \exp[-\beta T]} (1 - \exp[-\beta t]) + \sqrt{p_0} \quad (1)$$

[Sedano et al., J. Nucl. Mater. (1999)]

$$\partial_t g_S - D_s \Delta g_S = k_s \underbrace{\partial_t \sqrt{p}}_{\text{Now Easy}}, \quad \partial_t g_C - D_c \Delta g_C = \tau k_c \partial_t \sqrt{p}$$

Note:

- β , T and p_f free parameters,
- Sieverts' Law still holds for the pressure above.



$$j_1^S(t) = -2\pi D_s \int_{-L}^L R_0 \partial_r c(R_0, z, t) dz$$

$$j_2^S(t) = -4\pi D_s \int_0^{R_0} \partial_z c(r, L_0, t) r dr$$

$$j_3^C(t) = -2\pi D_c \int_{-L_1}^{L_1} R_1 \partial_r c(R_1, z, t) dz$$

Flux of Hydrogen:

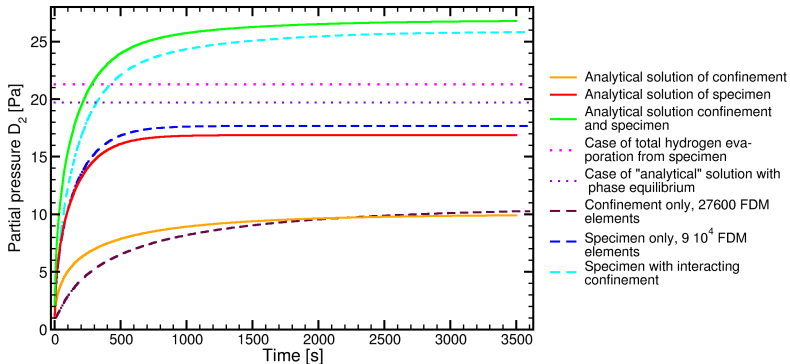
- Coat Containment j_3^C ,
- (2x Caps Containment),
- Coat Specimen j_1^S ,
- Caps Specimen j_2^S .

Pressure Increase

$$m(t) = \sum_k \int_0^t j_k(\tau) d\tau, \quad p_{H_2}(t) = \frac{(m_H^s(t) + m_H^c(t)) RT}{2(V_0 - V_S)}$$

$R_1=10 \text{ mm}, R_2=20 \text{ mm}, z_{cl}=40 \text{ mm}, z_{co}=50 \text{ mm}$

$r_{sa}=3 \text{ mm}, z_{sa}=30 \text{ mm}, D_{cu}=8.257 \cdot 10^{-10} \text{ m}^2/\text{s}, k_{s, cu}=5.914 \cdot 10^{-4} \text{ mol/m}^3/\text{sqrt(Pa)}, 673 \text{ K}$



- Fortran FDM and analytic (Python) model show similar results,
- Measure containment effect,
- Recover D and k with B&B (fast evaluation -> analytic solution),
- Estimate: Duration of Experiment,

copper containment may be usable

Open Problems:

- Guess function $\sqrt{p(t)}$ does not exactly fit. (Fixed-point Iteration),
- Melting Point of copper ≈ 1.300 K.

Acknowledgement:

The current talk summarizes results of two running projects:

Main goal of the first one is the determination of transport parameters of hydrogen in structural metallic materials used for components in fusion power stations: This work has been carried out within the framework of the EUROfusion Consortium, and has received funding from the Euratom research and training program 2014-2018 under grant agreement No. 633053. The views and opinions expressed herein do not necessarily reflect those of the European Commission

The authors are also thanking for support and fundings by MathSEE regarding the second project: *Neue Lösungen der Kontinuitätsdifferentialgleichung mit Phasengleichgewicht zur Verbesserung der Ergebnisse bei der Auswertung von Experimenten.*

- Sedano, Perujo, Wu, *Intrinsic hydrogen transport constants in the CFC matrix and fibres derived from isovolumetric desorption experiments*, in J. Nucl. Mater. (1999)
- Parsons, Reichanadter, Vicksman, Segur, *Explicit Solution for Cylindrical Heat Conduction*, in American Journal of Undergraduate Research (2016)
- von der Weth, Nagatou, Arbeiter, Dagan, Klimenko, Schulz, *Numerical analysis of an isovolumetric thermal desorption experiment*, Defect and Diffusion Forum (2019)