Scanner-Based Capillary Stamping

Peilong Hou,* Ravi Kumar,* Bastian Oberleiter, Richard Kohns, Dirk Enke, Uwe Beginn, Harald Fuchs, Michael Hirtz,* and Martin Steinhart*

Classical microcontact printing and polymer pen lithography (PPL) involve ink transfer to substrates using solid elastomeric stamps. Ink depletion thus limits the number of successive stamping steps without reinking. Porous stamps developed to overcome this limitation are used only for manual proof-of-principle experiments. Here, porous composite stamps for scanner-based capillary stamping (SCS) that can be mounted on automated printing devices designed for PPL are developed. Porous SCS composite stamps consist of a rigid controlled porous silica glass (CPG) layer and a porous polymeric stamping layer. The latter can be topographically structured with contact elements by replication molding. The mechanical stabilization by the CPG layer ensures that the contact elements are coplanar. SCS allows automated, continuous, high-throughput patterning enabled by ink supply through the porous SCS composite stamps. Even after more than 800 consecutive stamp–substrate contacts without reinking (the porous SCS composite stamps themselves are used as ink reservoirs), ink microdroplets are deposited without deterioration of the pattern quality. However, SCS also allows supply of additional ink during ongoing stamping operations through the pore systems of the porous SCS composite stamps. SCS can easily be adapted for multi-ink patterning and may pave the way for further upscaling of contact lithography.

1. Introduction

Chemical and/or topographical patterning of substrates by contact lithography has been the focus of significant research efforts for more than two decades. Serial scanning probe lithography allows pixel-by-pixel generation of arbitrary patterns on the substrates.[1] Modified scanning probe lithography configurations enable continuous fluidic ink supply to cantilever tips[2] similar as in the case of micropipetting techniques.[3] However, limited throughput and the limited sizes of the areas that can be patterned are inherent drawbacks of serial scanning probe lithography. Parallel high-throughput patterning of large substrate areas is possible by means of classical microcontact printing[4] and its derivative polymer pen lithography (PPL).[5] In these approaches, ink molecules adsorbed on the outer surfaces of solid elastomeric stamps are transferred to substrates by stamping. The capability to perform large numbers of successive stamping steps with short cycle times is a prerequisite for the upscaling of soft lithography from benchtop experiments to automatized production processes. However, conventional microcontact printing suffers from ink depletion in the course of consecutive stamp–substrate contacts; hence, time-consuming interruptions of the printing operations for the readesorption of ink on the outer stamp surfaces are required to avoid deterioration of the quality of the stamped patterns. To overcome this drawback, stamps containing spongy continuous pore systems have been investigated because the continuous spongy pore systems enable continuous ink supply to the stamps’ contact surfaces and can also be used as ink reservoirs themselves. For example, porous polymer stamps with pore sizes exceeding several 100 nm were produced by spinodal decomposition,[6] and mesoporous silica stamps with pores having diameters of a few 10 nm by sol-gel chemistry.[7] Porous block copolymer stamps with pore diameters of a few 10 nm were obtained by swelling-induced pore generation.[8] In all these cases, contact surfaces topographically structured with contact elements also penetrated by the continuous spongy pore systems can be generated by replication molding during stamp preparation. Thus, ink transported through the continuous spongy pore system is deposited where the contact elements of the porous stamp touch the substrates to be patterned. So far, porous stamps have predominantly been used in manual proof-of-principle stamping experiments. Furthermore, porous...
stamps typically exhibit macroscopic waviness, which results from mechanical stress formed during stamp preparation and pore formation. If wavy stamps approach a substrate, at first an exposed portion of contact elements will touch the substrate, whereas other contact elements will contact the substrate only if the porous stamp is pressed against the substrate. Therefore, the pressure at the stamp-substrate interface and, as a result, the deposited patterns are locally different.

An optimized embodiment of contact lithography would comprise the automated repetitive execution of stamping steps for parallel large-scale substrate patterning, as already realized for dip-pen lithography.[5] However, interruptions of the stamping operations for reinking by ink adsorption on the stamp surface, each time followed by leveling procedures to align the stamp with the substrate, should be avoided. Stamps with spongy continuous pore systems appear to be ideal for the implementation of such a contact-lithographic process as they enable continuous fluidic ink supply to the stamps’ contact surfaces. The objective of this work is the development of an SCS composite stamps and prevented bending. The continuous pore systems of the CPG layers 2 were characterized by an average pore diameter of 102 nm, while the porosity of the CPG layers 2 amounted to 34%. To prepare the porous SCS composite stamps, we sandwiched molten asymmetric PS-b-P2VP containing P2VP minority domains in a PS matrix between the CPG layers 2 and silicon molds prepared by standard top-down lithography under a load of ≈2.75 bar (Figure 1a). Since the CPG pores had oxidic walls with high surface energy, the PS-b-P2VP readily bonded to the CPG surfaces.

### 2. Results and Discussion

#### 2.1. Design of Porous SCS Composite Stamps

The porous SCS composite stamps comprised porous polystyrene-block-poly(2-vinylpyridine) (PS-b-P2VP) stamping layers 1 tightly attached to ≈500 µm thick, nondeformable controlled porous glass (CPG) layers 2. The CPG layers 2, which consisted of rigid silica scaffolds, mechanically stabilized the porous SCS composite stamps and prevented bending. The continuous pore systems of the CPG layers 2 were characterized by an average pore diameter of 102 nm, while the porosity of the CPG layers 2 amounted to 34%.

![Figure 1. Preparation of porous SCS composite stamps. a) Molten PS-b-P2VP is sandwiched between a CPG layer and a hydrophobically modified silicon mold. b) After cooling to room temperature, the PS-b-P2VP/CPG composite is detached from the hydrophobically modified silicon mold and immersed into hot ethanol. d) Swelling-induced pore formation during exposure to hot ethanol results in the formation of a continuous spongy pore system in PS-b-P2VP stamping layer 1 tightly adhering to CPG layer 2.](image-url)
reconstructed morphology. Thus, spongy continuous pore systems with walls consisting of coiled P2VP blocks form in lieu of the swollen P2VP domains. However, swelling-induced pore formation generates stress in the porous PS-b-P2VP stamping layers. While unsupported PS-b-P2VP stamping layers bend and develop macroscopic waviness, the CPG layers mechanically stabilize the ≈80 µm thick porous PS-b-P2VP stamping layers of the porous SCS composite stamps (Figure 1d). The porous SCS composite stamps thus having coplanar contact elements extended 25 mm² (Figure 2a,b), while they were still completely penetrated by continuous spongy pore systems (Figure 2c–f). The pyramidal contact elements had flattened contact areas with edge lengths of ≈1 µm at their tips (Figure S1, Supporting Information). The schematic representation of the porous SCS composite stamps in Figure 1 is somewhat simplified in that the PS-b-P2VP infiltrated the CPG layers up to a depth of ≈3 µm (Figure 2f). Hence, the CPG layers and the porous PS-b-P2VP stamping layers tightly adhered to each other, and no indications of delamination were apparent throughout the testing of the porous SCS composite stamps. Moreover, previous results suggest that swelling-induced pore generation also yields percolating pore systems even in local 2D confinement as it is imposed by the CPG pores.

2.2. Scanner-Based Capillary Stamping

For the SCS experiments, we used a commercial dip-pen nanolithography setup modified for PPL (Figure S2, Supporting Information). The device was controlled with an onboard software system that allows the design of arbitrary stamping patterns and the setting of parameters such as dwell times (i.e., the contact times between stamp and substrate). The porous SCS composite stamps were manually glued onto 2 mm thick custom-made metal stamp holders extending 30 mm × 80 mm with a square hole extending 10 mm × 10 mm (Figure S2a, Supporting Information, and Figure 3a–c). Thus, inking of porous SCS composite stamps is possible anytime in the course of their operation through hole 4 while mounted on a stamping device without the need to repeat time-consuming leveling procedures. Once leveled, an infinite number of stamping steps can be carried out without interruptions. Porous SCS composite stamps can, in principle, kept wet throughout their entire operational lifetime.

SCS stamping experiments were carried out using porous SCS composite stamps extending 0.5 cm × 0.5 cm. At first, the porous SCS composite stamp was filled with oligo(1-decene), which we selected as model ink because of its low vapor pressure (<1 × 10⁻⁷ torr at room temperature as specified by the
Figure 3. SCS stamping. a) Photograph of a stamp holder 3 with a central hole 4, through which ink can be supplied even during ongoing SCS operations. b) Photograph of an empty porous SCS composite stamp consisting of a porous PS-b-P2VP stamping layer 1 located on a CPG layer 2 mounted on a stamp holder 3 in such a way that the central hole 4 is covered. c) Porous SCS composite stamp mounted on a stamp holder 3 after inking; the central hole 4 of the stamp holder can be seen through the transparent porous PS-b-P2VP stamping layer 1 and the CPG layer 2. The lengths of the scale bars in panels (a)–(c) correspond to 1 cm. d) Schematic diagram of a cross section of a porous composite stamp. e) Schematic diagram of the SCS operation in which each contact element of a porous SCS composite stamp writes matrices of microdroplets by successive substrate contacts at different locations.

manufacturer). Typically, initial misalignment between stamp and substrate cannot be avoided. To compensate this misalignment, leveling of the porous SCS composite stamp was performed by adaptation of an optical leveling method reported previously.[13] We used silicon wafers modified with hexamethyldisilazane (HMDS), thereafter referred to as HMDS-Si, as substrates for SCS. The contact angle of oligo(1-decene) on HMDS-Si amounted to (49.6° ± 2.3°) (Table S1, Supporting Information). After leveling, HMDS-Si was mounted onto the substrate stage of the lithography device. Following predefined SCS programs, the porous SCS composite stamp was brought into contact with the HDMS-Si substrate multiple times. The porous SCS composite stamp was slightly displaced laterally between two successive SCS cycles so that the contact elements contacted the substrate at slightly shifted positions (Figure 3d,e). For example, we generated arrays of matrices containing 8 × 10 oligo(1-decene) microdroplets; these arrays extended 5 mm × 5 mm (Figure 4a; for a large-area optical microscopy image see Figure S3, Supporting Information)—corresponding to the extension of the PS-b-P2VP stamping layer 1. Each 8 × 10 matrix of oligo(1-decene) microdroplets (Figure 4b) was written with one and the same contact element that contacted the HDMS-Si in 80 successive SCS steps without reinking. Between two successive SCS steps, the porous SCS composite stamp and thus the individual contact elements were displaced by 20 µm, resulting in nearest-neighbor distances of 20 µm between adjacent oligo(1-decene) microdroplets. Hence, the distance between adjacent oligo(1-decene) microdroplets was one order of magnitude smaller than the distance between the tips of adjacent contact elements of the porous SCS composite stamp, which amounted to 200 µm.

Here, we applied a dwell time of 10 s; the diameter of the oligo(1-decene) microdroplets amounted to (7.78 ± 1.40) µm, and their height to (1.92 ± 0.16) µm, as revealed by white-light interferometry (Figure S4, Supporting Information).

Elastomeric nonporous poly(dimethylsiloxane) (PDMS) stamps used for polymer pen lithography can hold absorbed volatile solvents for a few hours.[14] In contrast, volatile solvents will rapidly evaporate from mesoporous materials[15] and, consequently, from porous SCS composite stamps. However, this problem can be overcome by either triggered or continuous supply of ink or solvent through hole 4 of the stamp holder (Figure S2, Supporting Information, and Figure 3a) via CPG layer 2 to porous PS-b-P2VP stamping layer 1. If nonvolatile inks are used, the pore systems of the PS-b-P2VP stamping layers 1 and the CPG layers 2 may act themselves as long-term ink reservoirs. In the case of oligo(1-decene), ink-filled SCS composite stamps could even be reused with same ink load after several days. To exploratively evaluate how many successive SCS cycles can be performed without reinking, we carried out a SCS sequence in which one 8 × 10 matrix of oligo(1-decene) microdroplets per contact element was stamped on HDMS-Si and repeated this sequence on nine more HDMS-Si substrates. As a result, ten 8 × 10 matrices of oligo(1-decene) microdroplets—corresponding to 800 oligo(1-decene) microdroplets—were generated per contact element without reinking the porous SCS composite stamps. Figure 4c,d shows optical microscopy images of 8 × 10 matrices of oligo(1-decene) microdroplets on the tenth HDMS-Si substrate. The diameter of the oligo(1-decene) microdroplets amounted to (7.20 ± 1.33) µm. Therefore, one
individual contact element of a porous SCS composite stamp can generate at least 800 microdroplets without reinking and without significant deterioration of the pattern quality. It is, of course, also possible to write arbitrary patterns instead of the $8 \times 10$ matrices displayed in Figure 4, as exemplarily shown in Figure S5 (Supporting Information).

In another set of experiments, we investigated the impact of the dwell time and the oligo(1-decene) contact angle on the counterpart substrates on size and shape of the deposited oligo(1-decene) microdroplets. In a first experiment, we stamped arrays of $4 \times 8$ matrices of oligo(1-decene) microdroplets onto HMDS-Si, i.e., each contact element of the porous SCS composite stamp stamped one $4 \times 8$ matrix by 32 successive contacts with HMDS-Si. For each of the four stamped columns, we varied the dwell time from 1 to 5 s to 10 to 20 s (Figure 5a,b). The average diameters of the oligo(1-decene) microdroplets amounted to $(4.0 \pm 0.6)$ $\mu$m for a dwell time of 1 s, to $(4.5 \pm 0.4)$ $\mu$m for a dwell time of 5 s, to $(5.9 \pm 0.8)$ $\mu$m for a dwell time of 10 s, and to $(6.4 \pm 0.7)$ $\mu$m for a dwell time of 20 s. Hence, with increasing dwell time a moderate increase in the oligo(1-decene) microdroplet diameter occurs. Next, we modified the contact angle of oligo(1-decene) on the counterpart substrate by replacing HMDS with (3-aminopropyl)triethoxysilane (APTES). On silicon wafers modified with APTES (APTES-Si), oligo(1-decene) spreads (i.e., the contact angle is $0^\circ$, see Table S1, Supporting Information). As in the case of HMDS-Si, we stamped $4 \times 8$ matrices of oligo(1-decene) microdroplets onto APTES-Si and varied the dwell time for each column. For a dwell time of 1 s, the diameter of the oligo(1-decene) microdroplets amounted to $(16.9 \pm 0.6)$ $\mu$m. However, for dwell times of 5, 10, and 20 s, the oligo(1-decene) microdroplets merged and formed microlines.

Since we focus on the problem of ink depletion in the course of successive stamping steps associated with the use of solid elastomeric stamps, we aimed at stamping large ink microdroplets even after 800 stamp–substrate contacts without reinking. Reductions of the feature sizes of the stamped structures should be straightforward by appropriate adaptations of the shape of the contact elements and/or the contact angles of the ink–substrate systems. Deposited structures with diameters in the 100 nm range consisting of nonvolatile ink components dissolved or dispersed in a volatile solvent may be accessible also.\(^{[7a]}\)
2.3. Multi-Ink SCS

Multi-ink patterning or multiplexing involves the application and integration of more than one ink in an interdigitated microscale pattern. In an exploratory activity, we evaluated a stamp configuration potentially allowing multiplexing SCS. We used 2 mm thick custom-made stamp holders extending 30 mm × 80 mm that contained two holes extending 5 mm × 10 mm. The holes are covered by two separated parts of a porous SCS composite stamp (denoted by I and II) consisting of the PS-b-P2VP stamping layer and the CPG layer. Parts I and II can then be independently loaded with different inks (ink I and ink II).

![Image of multi-ink SCS configuration](image)

Figure 6. Multi-ink SCS. a,b) Photographs of a SCS configuration adapted for multiplexing prior to and after inking. The stamp holder 3 contains two holes 4 extending 5 mm × 10 mm. The holes are covered by two separated parts of a porous SCS composite stamp (denoted by I and II) consisting of the PS-b-P2VP stamping layer 1 and the CPG layer 2. Parts I and II can then be independently loaded with different inks (ink I and ink II). c) Fluorescence microscopy image showing a two-color pattern obtained by multi-ink SCS (corresponding bright field images are shown in Figure S7, Supporting Information). The lengths of the scale bars correspond to (a, b) 0.5 cm and (c) 200 μm.
pen lithography. To this end, we have designed porous SCS composite stamps consisting of a porous polymeric stamping layer, which can be topographically patterned with contact elements by replication molding, and a rigid layer consisting of inorganic controlled porous glass. The CPG layers mechanically stabilizing the porous SCS composite stamps prevent bending and bulging so that a coplanar arrangement of the stamps’ contact elements is ensured. The SCS design enables ink supply anytime during ongoing stamping operations to the backside of the porous SCS composite stamps. The ink is then transported through the pore systems of the porous SCS composite stamps to the contact surfaces of the porous polymeric stamping layers. Porous SCS composite stamps can, in principle, kept wet during their entire operational lifetime. Especially if nonvolatile inks are stamped, the pore systems of the porous SCS composite stamps can be used as ink reservoirs. Using oligo(1-decene) as nonvolatile model ink, 800 ink microdroplets could be stamped successively with one single contact element by 800 successive substrate contacts without reinking and without deterioration of the pattern quality. Moreover, exploratory experiments revealed that SCS can be adapted for multi-ink patterning by multiplexing. Therefore, SCS may pave the way for further automatization and upscaling of contact lithography.

4. Experimental Section

*Chemicals:* Asymmetric PS-b-P2VP \( (M_w/(PS) = 101\,000\, g\, mol^{-1}; M_w/(P2VP) = 29\,000\, g\, mol^{-1}; M_w/(PS-b-P2VP) = 1.60, \) volume fraction of P2VP 21%; bulk period 51 nm) was obtained from Polymer Source Inc., Canada. P2VP homopolymer \( (M_w = 41\,000\, g\, mol^{-1}; M_M = 37\,000\, g\, mol^{-1}; M_w/(M_M = 1.11) \) was obtained from Sigma-Aldrich. HMDS was supplied by abcr GmbH. APTES and PFOTS were purchased from Sigma-Aldrich. Tetrahydrofuran (THF), hydrogen peroxide (30% \( H_2O_2 \)), sulfuric acid (98% \( H_2SO_4 \)), and ethanol were supplied by local manufacturers in the analytical grade.

*Silicon Molds:* Silicon molds were prepared as reported previously\(^{[15],[16]}\). The surface of the silicon molds was topographically patterned with tetragonal lattices of pyramidal indentations with a nearest-neighbor distance of 200 µm. The edge length of the quadratic pyramid bases amounted to 50 µm. The depth of the pyramidal indentations also amounted to 50 µm. Before use, the surface of the silicon molds covered by native oxide was silanized with PFOTS. For this purpose, silicon molds were at first treated with a boiling mixture containing 98% \( H_2SO_4 \) and 30% \( H_2O_2 \); at a volume ratio of 7:3 for 30 min, followed by rinsing with deionized water and drying in an argon flow. Then, the silicon molds were kept under a vacuum at room temperature for 5 h in the presence of 0.2 mL PFOTS.

*CPGs:* CPG layers extending 2 cm × 2 cm with an average pore diameter of 102 nm, a thickness of 500 µm, and porosity of 54% were prepared by spinodal decomposition of alkali borosilicate glasses and subsequent leaching of the boron-rich phase following procedures reported elsewhere.\(^{[17]}\) The CPG layers were characterized by mercury intrusion porosimetry (MIP) carried out on a Pascal 140/440 porosimeter (Thermo Fisher Scientific, Waltham, MA) over a pressure range of 0.15–200 MPa (Figure S8, Supporting Information). Pore size distributions were derived from the MIP data with Pascal software. The surface of the CPG layers was topographically patterned with contact elements by replication molding, and a rigid layer consisting of inorganic controlled porous glass. The CPG layers mechanically stabilizing the porous SCS composite stamps prevent bending and bulging so that a coplanar arrangement of the stamps’ contact elements is ensured. The SCS design enables ink supply anytime during ongoing stamping operations to the backside of the porous SCS composite stamps. The ink is then transported through the pore systems of the porous SCS composite stamps to the contact surfaces of the porous polymeric stamping layers. Porous SCS composite stamps can, in principle, kept wet during their entire operational lifetime. Especially if nonvolatile inks are stamped, the pore systems of the porous SCS composite stamps can be used as ink reservoirs. Using oligo(1-decene) as nonvolatile model ink, 800 ink microdroplets could be stamped successively with one single contact element by 800 successive substrate contacts without reinking and without deterioration of the pattern quality. Moreover, exploratory experiments revealed that SCS can be adapted for multi-ink patterning by multiplexing. Therefore, SCS may pave the way for further automatization and upscaling of contact lithography.

3. Conclusions

Classical microcontact printing with solid elastomeric stamps suffers from ink depletion if several consecutive stamping steps are carried out without reinking. Spongy porous stamps may overcome these drawbacks but have, so far, only been used for manual proof-of-principle experiments. Scanner-based capillary stamping involves the incorporation of porous stamps into automated stamping systems already established for polymer lithography. To this end, we have designed porous SCS composite stamps consisting of a porous polymeric stamping layer, which can be topographically patterned with contact elements by replication molding, and a rigid layer consisting of inorganic controlled porous glass. The CPG layers mechanically stabilizing the porous SCS composite stamps prevent bending and bulging so that a coplanar arrangement of the stamps’ contact elements is ensured. The SCS design enables ink supply anytime during ongoing stamping operations to the backside of the porous SCS composite stamps. The ink is then transported through the pore systems of the porous SCS composite stamps to the contact surfaces of the porous polymeric stamping layers. Porous SCS composite stamps can, in principle, kept wet during their entire operational lifetime. Especially if nonvolatile inks are stamped, the pore systems of the porous SCS composite stamps can be used as ink reservoirs. Using oligo(1-decene) as nonvolatile model ink, 800 ink microdroplets could be stamped successively with one single contact element by 800 successive substrate contacts without reinking and without deterioration of the pattern quality. Moreover, exploratory experiments revealed that SCS can be adapted for multi-ink patterning by multiplexing. Therefore, SCS may pave the way for further automatization and upscaling of contact lithography.

4. Experimental Section

*Chemicals:* Asymmetric PS-b-P2VP \( (M_w/(PS) = 101\,000\, g\, mol^{-1}; M_w/(P2VP) = 29\,000\, g\, mol^{-1}; M_w/(PS-b-P2VP) = 1.60, \) volume fraction of P2VP 21%; bulk period 51 nm) was obtained from Polymer Source Inc., Canada. P2VP homopolymer \( (M_w = 41\,000\, g\, mol^{-1}; M_M = 37\,000\, g\, mol^{-1}; M_w/(M_M = 1.11) \) was obtained from Sigma-Aldrich. HMDS was supplied by abcr GmbH. APTES and PFOTS were purchased from Sigma-Aldrich. Tetrahydrofuran (THF), hydrogen peroxide (30% \( H_2O_2 \)), sulfuric acid (98% \( H_2SO_4 \)), and ethanol were supplied by local manufacturers in the analytical grade.

*Silicon Molds:* Silicon molds were prepared as reported previously\(^{[15],[16]}\). The surface of the silicon molds was topographically patterned with tetragonal lattices of pyramidal indentations with a nearest-neighbor distance of 200 µm. The edge length of the quadratic pyramid bases amounted to 50 µm. The depth of the pyramidal indentations also amounted to 50 µm. Before use, the surface of the silicon molds covered by native oxide was silanized with PFOTS. For this purpose, silicon molds were at first treated with a boiling mixture containing 98% \( H_2SO_4 \) and 30% \( H_2O_2 \); at a volume ratio of 7:3 for 30 min, followed by rinsing with deionized water and drying in an argon flow. Then, the silicon molds were kept under a vacuum at room temperature for 5 h in the presence of 0.2 mL PFOTS.

*CPGs:* CPG layers extending 2 cm × 2 cm with an average pore diameter of 102 nm, a thickness of 500 µm, and porosity of 54% were prepared by spinodal decomposition of alkali borosilicate glasses and subsequent leaching of the boron-rich phase following procedures reported elsewhere.\(^{[17]}\) The CPG layers were characterized by mercury intrusion porosimetry (MIP) carried out on a Pascal 140/440 porosimeter (Thermo Fisher Scientific, Waltham, MA) over a pressure range of 0.15–200 MPa (Figure S8, Supporting Information). Pore size distributions were derived from the MIP data with Pascal software. The surface of the CPG layers was topographically patterned with contact elements by replication molding, and a rigid layer consisting of inorganic controlled porous glass. The CPG layers mechanically stabilizing the porous SCS composite stamps prevent bending and bulging so that a coplanar arrangement of the stamps’ contact elements is ensured. The SCS design enables ink supply anytime during ongoing stamping operations to the backside of the porous SCS composite stamps. The ink is then transported through the pore systems of the porous SCS composite stamps to the contact surfaces of the porous polymeric stamping layers. Porous SCS composite stamps can, in principle, kept wet during their entire operational lifetime. Especially if nonvolatile inks are stamped, the pore systems of the porous SCS composite stamps can be used as ink reservoirs. Using oligo(1-decene) as nonvolatile model ink, 800 ink microdroplets could be stamped successively with one single contact element by 800 successive substrate contacts without reinking and without deterioration of the pattern quality. Moreover, exploratory experiments revealed that SCS can be adapted for multi-ink patterning by multiplexing. Therefore, SCS may pave the way for further automatization and upscaling of contact lithography.
H$_2$SO$_4$ and 30% H$_2$O$_2$ at a volume ratio of 7:3 for 30 min, followed by rinsing with deionized water and drying in an argon flow. Then, the silicon wafers were heated for 5 h to 100 °C in the presence of 0.2 mL of the respective silane under ambient pressure. For further use, the silanized silicon wafers were cut into squares with an edge length of ~1 cm.

**Inks:** For single-ink stamping, oligo(1-decene) (Inland 45 vacuum pump fluid; kinematic viscosity at 40 °C as specified by the manufacturer: 53 cSt; vapor pressure $<1 \times 10^{-7}$ torr) purchased from Inland Vacuum Industries (Churchville, NY) was used as ink. Size exclusion chromatography revealed the following values for the molecular mass of oligo(1-decene): $M_w = 490$ g mol$^{-1}$; $M_n = 390$ g mol$^{-1}$; $M_w/M_n = 1.26$. For multi-ink stamping, the fluorescently labeled phospholipids (18:1 Liss Rhod PE (full name: [1,2-dioleoyl-sn-glycero-3-phosphoethanolamine-N-(lissamine rhodamine B sulfonyl) (ammonium salt)]) and 18:1 PE CF (full name: [1,2-dioleoyl-sn-glycero-3-phosphoethanolamine-N-(carboxy-fluorescein)]) supplied by Avanti Polar Lipids (USA) were used. Both dyes were applied as solutions in oligo(1-decene) containing 0.1 mg mL$^{-1}$ dye.

**Fabrication of Porous SCS Composite Stamps:** PS-b-P2VP films were prepared by dropping 50 μL (stamp for single-ink stamping) or 100 μL (stamp for multi-ink stamping) of a solution of 100 mg mL$^{-1}$ PS-b-P2VP in THF onto a silicon wafer extending 5 mm × 5 mm (stamp for single-ink stamping) or 10 mm × 5 mm (stamp for multi-ink stamping). After complete evaporation of the THF, the obtained PS-b-P2VP films were nondestructively detached by exposure to ethanol for 24 h at room temperature. Then, PS-b-P2VP films were sandwiched between CPG layers 1 and 2 and surface-modified silicon molds at 220 °C for 4 h under a vacuum while a load of ~2.75 bar was applied. After cooling to room temperature at ~1 K min$^{-1}$, the silicon molds were detached from the PS-b-P2VP by treatment with ethanol at room temperature for ~30 min. For swelling-induction of the PS-b-P2VP attached to CPG layers 2 was treated with ethanol at 60 °C for 4 h. Under the conditions applied here, spongy-continuous pore systems with a mean pore diameter of ~40 nm, a specific surface area of 10 m$^2$ g$^{-1}$, and a total pore volume of 0.05 cm$^3$ g$^{-1}$ formed.[iii]

**Stamping Device Used for SCS:** All stamping experiments were carried out with an NLP 2000 device (Nanoink Inc., USA) equipped with three encoded goniometer stages (settings are referred to $T_1$, $Y_1$, and $Z_1$) and a digital camera located atop of the CPG layer that allows viewing the stamping process. The general procedure for multi-ink stamping was an adaptation of a previously published approach.[iv,ivb,i] Multi-ink microdroplet patterns were stamped by repositioning the piezo-driven substrate stage in such a sequence that subpatterns of each particular ink were generated next to each other by repositioning the piezo-driven substrate stage in such a sequence. The leveling procedure could be monitored by optical microscopy using objectives and a digital camera located atop of the CPG layer 2 away from the contact surface of PS-b-P2VP stamping layer 1. A silicon test substrate mounted on a substrate stage adjustable by a goniometer was brought into contact with the pyramid-shaped contact elements of the ink-filled porous SCS composite stamp. As soon as the substrate stage was about 100–200 μm away from the contact elements, shadows appeared due to the reflective nature of the silicon test substrate (Figure S9a, Supporting Information). When the contact elements contacted the substrate stage, circular ink microdroplets formed at the contact sites (Figure S9b, Supporting Information). In the course of the initial approach of the silicon test substrate toward the porous SCS composite stamp, the tips of some of the pyramid-shaped contact element touch the silicon test substrate harder than others, resulting in local variations of the sizes of the deposited ink microdroplets. To compensate for this, the substrate stage was stepwisely tilted about the two goniometer axes. For each goniometer setting, a stamping test was carried out, and the variance in microdroplet sizes was evaluated by visual inspection of the corresponding optical microscopy images. This procedure was repeated until the microdroplet size was uniform all over the silicon test substrate, indicating that the plane of the silicon substrate stage was parallel to the plane of the stamp. For the leveling of the porous SCS composite stamps for multi-ink stamping, a similar method was applied, but only one of the two separated parts was leveled assuming conformity of the other part. Small misalignments are still to be expected after the leveling.

**General SCS Stamping Procedure:** After leveling, HMDS-Si or APTES-Si wafer was mounted onto the substrate stage of the NLP 2000 device and used as substrates. The substrates were approached to the porous SCS composite stamps until the distance amounted to ~100 μm. Then, the porus SCS composite stamps were further approached to the substrates in steps of 10 μm until contact was formed. Contact formation detected optically by the in-built camera was indicated by the formation of circular microdroplets at the tips of the contact elements. After a predefined dwell time, the substrates were retracted by 30 μm, moved to the next set position, and brought in contact with the SCS stamps again for the next stamping step. This cycle was repeated multiple times until the predefined stamping program was completed. The general procedure for multi-ink stamping was an adaptation of a previously published approach.[ivb,i] Multi-ink microdroplet patterns were stamped by repositioning the piezo-driven substrate stage in such a sequence that subpatterns of each particular ink were generated next to each other (Figure 6c and Figure S7, Supporting Information). The initial offset between parts I and II of the SCS stamps was corrected by visual in situ alignment using the optical microscope attached to the NLP 2000 device.

**Characterization:** The molecular mass of oligo(1-decene) was determined by gel permeation chromatography using a Waters 2695 Separations Module and THF as solvent against PS as standard for external calibration.

**Ink contact angles (Table S1, Supporting Information) were measured in the sessile drop mode at a humidity of 27% and a temperature of 23 °C using a drop shape analyzer DSA100 (Krüss, Germany). The values of the liquid droplets were 3 μL. All contact angle measurements for a specific sample type were repeated on six different samples. P2VP homopolymer films for the contact angle measurements were prepared by spin-coating a solution of 10 wt% P2VP in ethanol onto a silicon wafer at 1000 rpm, followed by drying in vacuum.

**Scanning electron microscopy (SEM) investigations were carried out on a Zeiss Auriga microscope operated at an accelerating voltage of 5 kV. Prior to the SEM investigations, the samples were coated with an ~5 nm thick iridium layer. The diameters of the microdroplets were determined using NIS-Elements imaging software by evaluating around 100 microdroplets per sample. White light interferenceometry was carried out on a ContourGT-K 3D Optical Microscope using VisionM4 Operation and Analysis Software. Fluorescence microscopy images were acquired with...
an upright fluorescence microscope (reflection mode, Eclipse 80i, Nikon Germany) equipped with a sensitive camera (Nikon DS-Qi2 camera from Nikon Germany), a broadband excitation light source (Intensilight, Nikon), a FITC filter set (B-2E/C, Nikon), and a Texas Red filter set (Y-2E/C, Nikon). For different colors, the fluorescence microscopy images were captured separately and then merged using NIS-Elements imaging software.

Supporting Information
Supporting Information is available from the Wiley Online Library or from the author.

Acknowledgements
P.H. and R.K. contributed equally to this work. The authors thank the European Research Council (ERC-CoG-2014, Project 646742 INCANA) for funding. This work was partly carried out with the support of the Karlsruhe Nano Micro Facility (KNMF, www.knmf.kit.edu), a Helmholtz Research Infrastructure at Karlsruhe Institute of Technology (KIT, www.kit.edu). The authors thank Richard Thelen (Institute of Microstructure Technology (IMT), Karlsruhe Institute of Technology (KIT)) for help with the white light interferometry measurements.

Conflict of Interest
The authors declare no conflict of interest.

Keywords
block copolymers, composite materials, microcontact printing, polymeric materials, porous materials

Received: February 18, 2020
Revised: March 23, 2020
Published online: April 26, 2020


