

Virtual ICCS23 in Porto/Portugal

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Motivation Optimising Fibre-Reinforced Composites

Composite Materials – Structural aspects

- High weight-specific stiffness/strength
- Anisotropic behaviour → requires particular attention

Early phases of component design

- Major design decisions necessary [Kle15]
 - Reinforcement type (uni-/bi-directional vs quasi-isotropic)
 - Material orientation
- Current approaches

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- Analytical, closed-form solutions,
 → limited to simple geometries and load cases
- Large, complex components require numerical approaches
 → time-intensive numerical optimisation

Rapid Determination of Suitable Reinforcement Type in

Continuous-Fibre-Reinforced Composites For Multiple Load Cases







Motivation Optimising Fibre-Reinforced Composites



Popular optimisation approaches

- Gradient-based, e.g. topology optimisation [Sig11]
 - generally fast (few iterations)
 - local optima, categorial variables
- Gradient-free, e.g. evolutionary algorithms [Sig11]
 - global optima

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- generally many iterations
- Optimality-criterion, e.g. *fully-stress-design*
 - potentially extremely fast (ideally 1 iteration)
 - definition of optimality-criteria difficult



Approach Overview and current limitation

Previous work

- Numerous approaches towards laminate optimisation, most concentrate on numerical optimisation
- Zink et al.: Anisotropy Analysis [Zin16,Zin17]
 - Optimality criterion (OC) based on principal stresses
 - Identify component regions suitable for FRP
 - Recommends material-type and -orientation

Current limitation

- Change of material behaviour and orientation alters stress distribution and thereby optimum material distribution
- Iterations necessary until convergence



Workflow during anisotropy analysis [Zin16,Zin17]

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Optimality Criterion for elements

- Maximum stiffness : Alignment of material orientations with principal stresses $\sigma_{P I,II}$ [Luo98]
- Multiple load cases: Consider variability of across load cases

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Available material types

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- unidirectional
- bidirectional
- quasi-isotropic



Approach Optimality criterion | Visualisation





Approach Optimality criterion | Formal evaluation example



Element-wise analysis of principal stresses

- 1. Determination of material orientations for UD and BD (QI has no material orientation)
 - Sum projection of principal stress vectors on candidate material orientation
 - Maximum projection yields material orientation $\alpha_{UD}^* = \arg \max(P(\alpha))$
 - Separate consideration of BD
- 2. Assessment of Reserve Factor R

3. Comparison and selection of best-fit material



$$P(\alpha) = \sum_{i} \sum_{p} |\sigma_{Pip} \cdot \cos(\varphi_{ip} - \alpha)|$$

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Approach Optimality criterion | Formal evaluation example



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3. Comparison and selection of best-fit material



$$P(\alpha) = \sum_{i} \sum_{p} \left| \sigma_{P i p} \cdot \cos(\varphi_{i p} - \alpha) \right|$$

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Approach Optimality criterion | Formal approach



Element-wise analysis of principal stresses

1. Determination of material orientations for UD and BD (QI has no material orientation)

2. Assessment of reserve factor $R_{i \text{ UD}}^p$

- Rotate stiffness matrix by material orientation, e.g. α_{UD}^*
- Determine Reserve Factor $R_{i \text{ MAT}}^p = \max\left(\frac{\sigma_{P i p}}{E(\alpha_{\text{UD}}^*)}\right)$ for each principal stress p...
- ...and load case i

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- Repeat for BD and QI
- 3. Comparison and selection of best-fit material



Approach Optimality criterion | Formal approach

Element-wise analysis of principal stresses

- 1. Determination of material orientations for UD and BD (QI has no material orientation)
- 2. Assessment of reserve factor R
- 3. Comparison and selection of best-fit material
 - Determine most critical load case for each material $R_{mat \, crit} = \max(R_{i \, mat})$
 - Determine best-fit material by

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 $M = \arg \min(R_{mat \operatorname{crit}})$







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Generic Plate

Example 1

Generic Plate

- Quadratic plate with central hole, line load applied to edges
- Convergence within 6 iterations







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Generic Plate

100%

90%

80%

70%

60%

50%

40%

30%

20%

10%

0%

1 2

Proportion of material type

- Quadratic plate with central hole, line load applied to edges
- Convergence within 6 iterations







Example 1 Generic Plate

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Generic Plate

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Generic Plate

Example 1

Generic Plate

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Example 2 Real-world example | Load Cases



Bicycle frame

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- Real-world application on a 3D bicycle frame [NLR20]
- 3 load cases considered [Liu10, NLR20]



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Example 2 Real-world example | Results

Bicycle frame

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- Convergence after 9 iterations
- Optimisation results support classical engineering strategies
 - UD-dominated truss-tubes, UD+BD in bent tubes



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Example 2 Real-world example | Multiple loads vs single load





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Nodal displacement in mm 200 -Highest stresses in LC-2: 150 100 Combined optimisation 50 approaches separate optimisation 30 -

- LC-1 and LC-3 show further potential in separate optimisation
 - Potential unexploited since LC-2 dominates component

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250 -

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10 -

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Example 2 Real-world example | Multiple loads vs single load

Bicycle frame

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- Synthesises of structural requirements from different load cases
- Automatic prioritisation of load cases with higher stresses
 - Displacement reduces in all cases





Summary Rapid Determination of Reinforcement Type

Summary

- Early recommendation of reinforcement type (UD, BD or QI) and respective orientation for multiple load-cases
- Extension of an existing, optimality-criterion-based approach [Zin16]
 - Rapid convergence when iterating recommendations
- Comparison of multi- and single-load-case optimisation
 - Automatic prioritisation of critical load cases observed

Outlook

- Automatically combine similar regions to coherent patches for manufacturability
- Handling of (near) hydrostatic stress states

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Thank you.

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