

Karlsruhe Institute of Technology

Institute for Neutron Physics and Reactor Technology (INR)

76344, Eggenstein-Leopoldshafen, Germany

**31<sup>st</sup> SYMPOSIUM ON FUSION TECHNOLOGY** Email: gaetano.bongiovi@kit.edu - Skype: gaetano19877

## Structural assessment of a whole toroidal sector of the **HELIAS 5-B breeding blanket**

<u>Gaetano Bongioví</u><sup>1</sup>, André Häußler<sup>1</sup>, Salvatore Giambrone<sup>2</sup>, Ilenia Catanzaro<sup>2</sup>, Ruggero Forte<sup>2</sup>, Guangming Zhou<sup>1</sup>, Pietro Alessandro Di Maio<sup>2</sup> and the W7-X team

<sup>1</sup>Karlsruhe Institute of Technology, INR, Germany - <sup>2</sup>Universitá degli Studi di Palermo, Dipartimento di Ingegneria, Italy

The European roadmap for the realization of fusion energy considers the stellarator line as a possible long-term alternative to a tokamak DEMO. Presently, the most promising option is a five-field period power plant called HELIcal-axis Advanced Stellarator (HELIAS) 5-B. It is a direct extrapolation of the Wendelstein 7-X, the largest stellarator reactor currently in operation. In order to allow the electricity production, the HELIAS 5-B reactor must be endowed with a breeding blanket (BB). Hence, in this paper, the advancements in the HELIAS 5-B BB design are reported.

## Displacement assessment of a whole toroidal sector of the HELIAS 5-B BB – HCPB and WCLL BB concepts Assessed loading scenarios • Less Conservative (LC) + Hot VV (E=10%, VV between 180 and 230 °C) • More Conservative (MC) + Hot VV (E=100%, VV between 180 and 230 °C) • Less Conservative (LC) + Cold VV (E=10%, VV between 40 and 90 °C) Ring 1 BB • More Conservative (MC) + Cold VV Ring 5 BB Ring 16 BB Ring 12 BB Vacuum Vessel (AISI 316L as structural material) (triangular shape section) (E=100%, VV between 40 and 90 °C) (bean shape section) 550,0 400,00 **Mechanical restraints** 525,0 • A and B: displacement prevented along 385,00 C 500.0 the local toroidal direction. °\_\_\_\_ 370,00 ature 475,0 • C and D: displacement prevented along 355,00 emper 450,0 the vertical (Z) direction. 340,00 425.0 **Displacement** [m] 325.00 0,0 2,5 5,0 7,5 10,0 12,5 15,0 17,5 20,0 22,5 25,0 🗔 MC+ Hot VV scenario 0,0 2,5 5,0 7,5 10,0 12,5 15,0 17,5 20,0 22,5 25,0 FW slice thickness [mm] FW slice thickness [mm] • Temperatures inferred from DEMO BB. 3D discrete temperature profiles HCPB BB imposed to Ring 5 and 12. Spatially averaged temperatures to the other Rings. Max = 0.0922 mmin = 0.0423 m<u>Ring 5</u> – minimum residual poloidal gaps [mm] (initial value 20 mm) HCPB BB WCLL BB Segment LC+ColdVV LC+HotVV MC+ColdVV MC+HotVV LC+ColdVV LC+HotVV MC+ColdVV MC+HotVV WCLL BB 9.9 5.6 10.1 16.0 16.6 2.6 9.7 12.5 1-2 0,1 0,0957 Max = 0.0893 m-3.2 4.7 -4.7 5.7 3.4 13.9 5.9 13.9 2-3 0,0914 min = 0.0457 m3-4 7.3 12.6 9.1 12.9 10.7 16.0 12.7 16.3 0,0871

4-5	-5.1	4.9	-3.5	4.1	3.5	13.6	6.0	13.7
5-1	4.7	11.1	7.3	11.5	10.3	16.4	12.6	16.6
		<mark>Ring 12</mark> – mir	nimum residu	<mark>ial poloidal g</mark> a	aps [mm] (ini	tial value 20	mm)	
		HCP	B BB			WCL	L BB	
Segment	LC+ColdVV	LC+HotVV	MC+ColdVV	MC+HotVV	LC+ColdVV	LC+HotVV	MC+ColdVV	MC+HotVV
1-2	-4.9	5.5	-3.6	4.3	3.7	14.2	6.2	14.0
2-3	-6.2	4.7	-5.3	3.2	2.6	13.5	4.8	13.3
4-5	0.5	8.6	0.1	7.3	7.4	15.6	8.1	15.2



## Design and stress assessment of the inboard internal components of a bean-shape ring – HCPB BB concept



RCC-MRx Level D Criteria									
	Segment 4 Path								
Criterion	S4_1	S4_2	S4_3	S4_4					
P <sub>m</sub> /S <sub>m</sub>	0.39	0.14	0.22	0.33					
(P <sub>m</sub> +P <sub>b</sub> )/(k <sub>eff</sub> ·S <sub>m</sub> )	0.31	0.11	0.16	0.23					
(P <sub>m</sub> +Q <sub>m</sub> )/S <sub>e</sub>	1.51	0.41	0.23	0.22					
(P <sub>m</sub> +P <sub>b</sub> +Q+F)/S <sub>et</sub>	0.24	0.06	0.04	0.04					
	Segment 5 Path								
Criterion	S5_1	S5_2	S5_3	S5_4					
P <sub>m</sub> /S <sub>m</sub>	0.30	0.45	1.75	1.34					
(P <sub>m</sub> +P <sub>b</sub> )/(k <sub>eff</sub> ·S <sub>m</sub> )	0.48	0.31	1.29	1.02					
(P <sub>m</sub> +Q <sub>m</sub> )/S <sub>e</sub>	0.18	0.36	0.87	0.29					
(P <sub>m</sub> +P <sub>b</sub> +Q+F)/S <sub>et</sub>	0.09	0.07	0.15	0.05					
	•	•	-	•					



Firstly, a displacement assessment of a whole toroidal sector of the HELIAS 5-B BB has been performed considering both WCLL and HCPB BB concepts. Homogenized geometric models have been set-up, adopting dummy components (full blocks without internal details). Results allow concluding that the proposed BB segmentation strategy is viable for more detailed BB design. Then, focusing on the HCPB BB concept, a preliminary design of internal components in the inboard blanket segments of the Ring 12 has been carried out. Structural analysis under the reference over-pressurization accidental conditions have been performed. Comparing the calculated stress against the RCC-MRx structural design criteria, one allows concluding that the adopted design approach is promising. Nevertheless, a more detailed assessment is necessary to develop design modifications aimed at improving the blanket structural performances, especially in the most critical regions highlighted by the present work.







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