Microstructural and Chemical Constitution of the Oxide Scale formed on a Pesting-Resistant Mo-Si-Ti Alloy

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Abstract

1 The oxidation behaviour of the pesting-resistant eutectic alloy Mo-20Si-52.8Ti was investigated by 2 addressing the microstructural and chemical constitution by grazing incidence X-ray diffraction GIXRD 3 and atom probe tomography APT of oxide scales formed at 800 and 1200 °C in order to understand their 4 protective character. The duplex Si-Ti-oxide scale formed at 800 °C in air, i.e. within the so-called 5 "pesting regime", is considerably slow growing with a scale thickness of $(11 \pm 3) \mu m$ after 1000 h of 6 exposure. It is composed of a Ti(+IV)-oxide with the chemical composition of approximately $TiO_{2.1}$ 7 confirmed by APT and SiO_2 islands, which are most likely amorphous. The oxide scale formed at 8 1200 °C, a potential application temperature, is characterised by a top single-phase scale and an 9 underlying duplex scale with a considerably increased thickness of $(68 \pm 11) \,\mu\text{m}$ in total. It consists of 10 rutile TiO₂ and some cristobalite SiO₂ as determined by GIXRD. APT analysis of the top Ti-oxide scale 11 confirms the stoichiometry TiO_{2.2}. The underlying duplex scale comprising Ti- and Si-oxide is characterised by strongly off-stoichiometric compounds, namely TiO_{1.4} and SiO_{1.6}. Initial linear oxide 12 13 scale growth kinetics are found at 800 °C, which change to cubic kinetics for exposure times longer than 14 100 h. At higher temperatures of 1100 and 1200 °C, diffusion-controlled, almost parabolic kinetics 15 prevail.

Keywords

refractory alloys; oxide scale; microstructure; chemical composition; crystal structure; oxidationkinetics

1. Introduction

18 The development of Mo-Si-based alloys for high-temperature applications as potential alternatives to state-of-the-art Ni-based superalloys is challenged by a judicious combination of sufficient creep 19 resistance with adequate oxidation resistance. At elevated temperatures, this oxidation resistance can be 20 21 achieved by: (i) Micro-alloving with B leads to a decrease in oxide scale viscosity [1] enabling quick 22 coverage of the substrate surface by a borosilicate layer retarding further O ingress [2-4]. (ii) M₅Si₃ 23 silicides with a higher Si content compared to M₃Si silicides (with M representing Mo or Ti, 24 respectively) can be stabilised [5], which facilitate formation of a SiO₂ oxide scale [6]. However at 25 temperatures below 1000 °C, catastrophic oxidation is characteristic for all Mo-Si-based alloys since 26 the kinetics of SiO₂ formation is too slow in order to outbalance the formation of volatile MoO₃ leading 27 to rapid mass loss [7, 8], called "pesting". Among multiple alloy design approaches, the ternary Mo-Si-28 Ti alloys were found to be the most promising regarding suppression of pesting [9]. A fully eutectic Mo-29 20Si-52.8Ti (at%) alloy possessing a two-phase, fine-scaled microstructure of Mo solid solution Moss 30 and (Ti,Mo)₅Si₃ was found not to undergo catastrophic oxidation at 800 °C [9]. An excellent oxidation 31 resistance was observed with negligible specific mass changes in the order of 2 mg/cm² (isothermal) 32 and 0.3 mg/cm² (cyclic) at 800 °C after 100 h [9]. This unexpected, outstanding oxidation behaviour has 33 been attributed to the formation of a mixed SiO₂-TiO₂ layer with a scale thickness of less than 10 µm 34 [9]. These observations were in striking contrast to the eutectoid Mo-Si-Ti alloy Mo-21Si-34Ti, being

35 composed of Moss and (Mo,Ti)₅Si₃, which suffered from severe pesting [9].

36 To summarise, our previous studies focused on the chemical and microstructural conditions for 37 achieving pesting-resistance in eutectic-eutectoid Mo-Si-Ti alloys. It turned out that a threshold in 38 nominal Ti content of minimum 43 at% is mandatory in order to obtain adequate oxidation resistance in 39 the pesting regime [10, 11]. Moreover, it was found that the fine length scale of the eutectic 40 microstructure is not required in order to achieve pesting-resistance since a considerably, artificially 41 coarsened eutectic alloy exhibited a similarly good oxidation behaviour [11]. Thus, the chemical 42 composition of the individual phases proved to be decisive whether pesting could be suppressed or not. While both M₅Si₃ silicides (with "M" being either Ti or Mo or a combination of both), hexagonal 43 44 $(Ti,Mo)_5Si_3$ and tetragonal $(Mo,Ti)_5Si_3$, exhibit an adequate oxidation resistance in the pesting regime 45 [12, 13], it is the pesting-critical Mo_{SS} phase which is responsible for the dominance of MoO_3 46 evaporation [11]. Continuous pathways of the Ti-oxide are present in the duplex scale connecting the 47 alloy substrate with the outer TiO₂ oxide scale among all investigated Mo-Si-Ti alloys [10]. This is 48 surprising with regard to the anticipated minor oxidation resistance of TiO_2 , which is well known to 49 exhibit scale cracking and spallation [14-17].

50 In conclusion, the reasons for the passivating character of the mixed Si-Ti-oxide scale formed on the 51 eutectic alloy at 800 and 1200 °C, and especially the non-detrimental character of Ti-oxide still remain 52 unclear. Therefore, this article addresses the crystallographic and chemical appearance of the oxide

- 53 scales and their growth characteristics. In particular, focus is placed on the solubility of the species Si,
- 54 Ti and Mo in the oxide phases by means of atom probe tomography (APT), in order to analyse its impact
- 55 on the pesting stability.

2. Experimental

56 The alloys were manufactured by repetitive arc-melting of the bulk high-purity elements Mo, Si and Ti 57 with purities of 99.95, 99.99 and 99.8%, respectively. Therefore, an AM/0,5 device provided by 58 Edmund Bühler equipped with a button-shaped, water-cooled Cu crucible was used. Subsequent to multiple evacuating ($< 2 \times 10^{-4}$ mbar) and Ar-flooding steps, a final Ar atmosphere of 600 mbar was 59 established, which was further cleaned from O residuals by pre-melting a Zr lump. Repetitive melting 60 61 (min. five times) ensured a homogenous element distribution. The resulting composition was confirmed to vary less than 0.5 wt% from the initial nominal composition by inductively coupled plasma optical 62 63 emission spectroscopy.

64 Cyclic oxidation experiments were performed on samples with dimensions of $(5 \times 5 \times 4)$ mm³ and a 65 surface finish of SiC grit P2500. Oxidation testing was conducted at laboratory air in muffle furnaces 66 by Carbolite Gero and Nabertherm at 800 and 1200 °C for a test duration in total of 1000 and 100 h, 67 respectively, with cycle durations varying between 1 to 10 h. The samples were cooled down to room 68 temperature between each cycle and their mass change was recorded by means of a balance (Sartorius 69 precision of $\pm 1 \mu g$). The samples were maintained in Al₂O₃ crucibles during testing, but turned around 70 after each cycle to allow uniform oxidation of all surfaces.

71 The cross sections of the oxidation samples were analysed by scanning electron microscopy (SEM) after 72 representative oxidation durations. Therefore, the oxidation samples were cold mounted and prepared 73 by grinding steps down to SiC grit P2500 and subsequent polishing with 3 and 1 µm diamond suspension 74 and finally with stabilised silica suspension provided by Struers. A LEO EVO 50 SEM by Zeiss was 75 used at an acceleration voltage of 20 kV. Backscattered electron (BSE) imaging contrast, providing 76 atomic number and thus material contrast, allowed the characterisation of the oxide scale morphology. 77 The used SEM was equipped with an energy dispersive X-ray spectroscopy (EDX) system, which allowed for an estimation of the chemical composition of the phases within the substrate. Quantitative 78 79 evaluation of the oxide scale thickness and the areal fractions of the respective oxides was performed 80 by applying image processing techniques, based on thresholding greyscale values and pixel connectivity 81 analysis using the software ImageJ and a self-written Matlab script.

In order to investigate the crystal structure of the formed oxide scales, grazing incidence X-ray diffraction (GIXRD) analyses were performed. Therefore, a Rigaku SmartLab diffractometer was used, equipped with a HyPix-3000 detector in 0D mode and a Cu K α radiation source. The sample was aligned by the usage of an Rx/Ry stage. The measurements were performed with a parallel beam and a 5° soller slit in the primary beam path at incident angles ω varying between 1.2 and 2.5°. Further analysis of the elemental distribution within the oxide scales was performed by means of 3D atom probe tomography (APT). The tips from the oxide layers were prepared in a Strata dual beam SEM/focused ion beam device by FEI. Firstly, the regions of interest were protected by a Pt layer to avoid damage caused by the Ga⁺ ion beam. Parts of an originally ($25 \times 4 \times 3$) μ m³ sized rod were set to Si micro-posts provided by Cameca. Next, tips were shaped by annular milling at 30 kV with decreasing inner diameter down to 0.2 μ m. Final milling with a closed circular pattern was performed at 5 kV

93 acceleration voltage to minimize the Ga⁺ affected layer at the surface.

Atom probe analyses were conducted in a LEAP 4000X HR by Cameca. The device was operated in laser mode (UV laser with $\lambda = 355$ nm) at a pulse energy of 50 or 100 pJ and a pulse repetition rate of 100 or 125 kHz. The temperature was set to 50 K and the standing high voltage was controlled according to a detection rate of 0.3 to 0.5 %.

98 Atom probe data were reconstructed and analysed by the IVAS 3.6.14 software by Cameca. The 99 chemical composition was determined using the peak deconvolution analysis to take the possible overlap of peaks into account, especially, the overlap of TiO^{2+} and O_2^+ at 32 Da. Furthermore, APT analyses of 100 101 oxides, as well as carbides and nitrides, have shown that the quantification of the chemical composition 102 may depend on the experimental conditions [18-21]. An underestimation of the O content could be 103 caused by preferential co-evaporation of O or O-containing ions during the same laser pulse leading to 104 multiple signals on the detector, which cannot be separated [20]. Hence, a critical discussion of the 105 obtained compositions is necessary. It can be assumed that a possible O underestimation is consistent 106 for experimental conditions not varying substantially. These conditions are strongly influenced by the 107 evaporation field which depends on, e.g. the pulse energy, tip radius and material. Varying evaporation 108 fields can lead to significant changes in (i) the fraction of pulses leading to multiple signals and/or (ii) 109 the ratio of detected ions of the same species with different charge. The tips discussed in this article 110 exhibit about 80 % single signals and comparable ratios of ions at different charge states. Hence, similar 111 experimental conditions can be assumed for the APT investigations. Additionally, it was guaranteed that no significant co-evaporation of O ions occurred during laser pulses. Therefore, a self-written software 112 113 by Boll et al. [22] was used to create separate mass spectra containing ions from single signals or 114 multiple signals, respectively. It was found that (i) the overall O content in the mass spectra derived 115 from multiple signals was lower than that from single signals and (ii) no disproportionally high amount 116 of O or O_2 ions occurred. Hence, it is unlikely that the APT analysis conditions cause a significant O 117 underestimation in the APT results.

118 The coefficient of thermal expansion (CTE) was determined by an optical dilatometer heating

119 microscope by LINSEIS. Here, the sample was compared to an Al₂O₃ reference during measurement.

120 The length difference was detected by a CCD camera. The CTE was analysed with a heating rate of

121 10 °C/min over the temperature range from 300 to 1200 °C under Ar flow of 3 sccm/min.

3. Results and discussion

122 In the following paragraphs we present structural (Sect. 3.1) and chemical investigations (Sect. 3.2) of the oxide scales formed on the eutectic Mo-20Si-52.8Ti alloy (at%) at 800 and 1200 °C. Thereafter, 123 124 oxide scale growth kinetics will be evaluated in order to assess the rate-controlling processes (Sect. 3.3). 125 In contrast to our previous article [10], where the distribution of the solid and volatile oxide forming species Ti, Si and Mo within the (sub-)oxide scales was evaluated, the evolution of the oxide scale 126 thickness with time at different temperatures is focused on. In the following, oxides, in which Ti cations 127 128 represent the major cationic component, are referred to as Ti-oxide, whereas oxides possessing majority 129 Si cations as metal ions will be designated as Si-oxide. These terms are only meant as general, 130 qualitatively distinction and are not to be misinterpreted by oxidation levels, or stoichiometry relations. 131 These will be named and discussed where they are of particular interest (Sect. 3.2).

132 3.1. Structural characterisation of the oxide scales formed at 800 and 1200 °C

The general oxidation behaviour of the eutectic Mo-20Si-52.8Ti alloy has been studied in detail in Refs. 133 134 [9, 11] for the as-cast and homogenised heat-treated condition with no significant differences in oxide 135 scale formation and oxidation behaviour observed. Thus, we now focus on the detailed investigation and understanding of the formed oxide scales of the as-cast (ac) condition. The two-phase eutectic 136 microstructure is differently fine-scaled and textured depending on the temperature profile during 137 cooling after arc melting, and thus also partially degenerated (see Fig. 1: Moss white and (Ti,Mo)₅Si₃ 138 bright grey in BSE contrast). After being cyclically exposed to air at 800 °C for 100 h a thin duplex 139 140 oxide scale of approximate $(5 \pm 2) \mu m$ in thickness is formed (see Fig. 1b), which grows to a thickness 141 of $(11 \pm 3) \mu m$ after 1000 h of oxidation (see Fig. 1c). It consists of a Ti-oxide (grey in BSE contrast) 142 with embedded islands of oxides rich in Si (dark-grey in BSE contrast) (see Fig. 1a to c). At 1200 °C 143 after 100 h, a significantly thicker oxide scale (approximately 70 µm in total) is observed. Two distinct 144 sub-scales are identified: (i) a single-phase, top Ti-oxide scale and (ii) a duplex scale comprising Ti- and 145 Si-oxide underneath (see Fig. 1d and e). The duplex oxide scale was found to comprise a considerable 146 fraction of Si-oxide of (52 ± 6) vol% [10]. The top Ti-oxide scale reveals a rather low porosity of (1.3) 147 ± 0.2) vol%.



Fig. 1 BSE micrographs of the eutectic alloy Mo-20Si-52.8Ti after cyclic oxidation in laboratory air for 1, (a) 100 (b) and 1000 h (c) at 800 °C as well as 1 (d) and 100 h (e) at 1200 °C. Dark grey is the Si-oxide, while the Ti-oxide is light grey.

- 149 GIXRD measurements at an incident angle of $\omega = 1.2^{\circ}$, presented in Fig. 2, confirmed the oxide scales
- 150 formed at 800 and 1200 °C to be mainly composed of rutile TiO₂, Ti(+IV)-oxide (space group P 4₂/m n
- m) and small amounts of cristobalite SiO₂, Si(+IV)-oxide (space group P $4_1 2_1 1$). Thus, with respect to
- 152 the considerable volume fraction of the (dark-grey) Si-oxide within the Si-Ti-oxide duplex scale formed
- 153 at 1200 °C (see Fig. 1e), it is expected that SiO₂ is mostly amorphous. This is in good agreement with
- 154 the results presented in Ref. [9] by electron back-scatter diffraction (EBSD). Besides, rutile TiO₂, some
- peaks at $2\Theta = 26.78$, 42.82, 63.04 and 65.57° can be assigned to ordered TiO (space group C 1 2/m 1).
- 156 While the peaks at $2\Theta = 42.82$, 63.04 and 65.57° are either superimposed by (Ti,Mo)₅Si₃ (in the case of
- 157 the 800 °C oxidation sample), or cristobalite SiO₂, the peak at $2\Theta = 26.78^{\circ}$ only matches the plane group

158	($\overline{111}$) of ordered TiO. However, more characteristic peaks of ordered TiO, for instance at $2\Theta = 30.29$,
159	or 46.74° of plane groups (111) and (021), respectively, would be expected, if a representative fraction
160	is prevalent in the oxide scale. Thus, the GIXRD results do not confirm the presence of TiO.
161	Additionally, some weak peaks at $2\Theta = 35.36$, 39.85 and 69.90° are assigned to the plane groups (410),
162	(501) and (621) of MoO ₃ (space group P b n m). Note that the peak at $2\Theta = 69.90^{\circ}$ is superimposed
163	by a rutile peak at 69.09° at 1200 °C. The detection of MoO_3 is attributed to re-deposition of volatile
164	MoO_3 on the oxide surface and partial incorporation into the growing oxide scale. Additionally, the
165	$800\ ^\circ C$ oxidation sample exhibits numerous peaks that can be assigned to $(Ti,Mo)_5Si_3$. This is reasonable
166	as the oxide scale possesses a rather low thickness and sub-oxide regions of the substrate were likely
167	detected even by GIXRD. This is confirmed by additional measurements with increasing incident angles
168	and therefore increased information depth, as the respective peaks become more pronounced (see Supp.
169	1 for GIXRD results with an increased incident angle of $\omega = 2.5^{\circ}$). Furthermore, peaks corresponding
170	to bcc Mo_{SS} are not detected, which is in good agreement with the observations made by SEM analysis
171	(see Fig. 1a and b), showing that surface-near Mo_{SS} regions suffer from oxidation while the $(Ti,Mo)_5Si_3$
172	regions remain almost unaffected. Moreover, there are two weak peaks at $2\Theta = 24.67$ and 31.32° in the
173	GIXRD pattern of the 1200 °C oxidation sample, which cannot be assigned unambiguously. However,
174	these peaks neither correspond to the already discussed crystal structures, nor to further verified ones
175	(see Table 1).

type	crystal structure	space group	matching peaks with GIXRD patterns
	rutile TiO ₂	P 4 ₂ /m n m	yes
			yes (superimposed by
	ordered TiO	C 1 2/m 1	peaks of other crystal
			structures)
Ti ovides	NaCl-type TiO	$F m \overline{3} m$	-
11-Oxides	monoclinic Ti ₃ O ₅	C 1 2/m 1	-
	pseudobrookite Ti ₃ O ₅	C m c m	-
	corundum Ti ₂ O ₃	R 3 c	-
	anatase TiO ₂	I 4 ₁ /a m d	-
	brookite TiO ₂	Pbca	-
Si-ovides	cristobalite SiO ₂	P 41 21 1	yes
SI-OAIdes	rutile SiO ₂	P 4 ₂ /m n m	-
	MoO ₃	P b n m	yes
Mo-oxides	VO ₂ -type MoO ₂	P 1 2 ₁ /c 1	-
	rutile MoO ₂	P 4 ₂ /m n m	-

	Table 1	Examined crystal structures for evaluation of the GIXRD patterns (see Fig. 2).	
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Fig. 2 GIXRD pattern of the surface of the oxidised sample at 800 (top) and 1200 °C (bottom) for 100 h. Note that the intensities are plotted in log scale. Diffraction angles that might correspond to ordered TiO (whose crystal structure cannot be identified unambiguously) are additionally labelled in green, whereas the non-assigned ones are labelled in violet colour.

3.2. Chemical analysis of the oxide scales formed at 800 and 1200 °C

The mass spectra of the investigated atom probe tips are displayed in Fig. 3, showing the characteristic parts with the main peaks indicated. At 800 °C, the Si-oxide tip could not be evaluated due to instabilities of tips manufactured from the oxide scale during APT analysis. Therefore, only the Ti-oxide tip was analysed (see Fig. 3a). For the 1200 °C sample, three regions of interest were evaluated (compare to BSE micrograph in Fig. 1e): (i) the top Ti-oxide scale (see Fig. 3b) and the underlying duplex scale of

- 181 both, (ii) the Ti- and (iii) the Si-oxide region (see Fig. 3c and d).
- 182 The mass spectrum of the Ti-oxide region formed at 800 $^{\circ}$ C (Fig. 3a) mainly exhibits TiO and TiO₂ as
- 183 well as O ion-related peaks. Additionally, the spectrum contains the main peak of Si^+ (28 Da) but no
- 184 side peaks or other O-containing Si peaks are identified. Furthermore, no peaks related to Mo are present,
- 185 which might have indicated the formation or incorporation of Mo-oxide. Thus, it can be concluded that
- 186 the peak at 32 Da predominantly results from TiO^{2+} ions. Nevertheless, the peak at 34 Da (a side peak
- 187 of O_2^+) indicates a significant contribution of O_2^+ to the peak at 32 Da, which has to be taken into account
- 188 for the determination of the chemical composition. After peak deconvolution the chemical composition

- 189 was found to be 34.4 at% Ti and 66.4 at% O (see Table 2), confirming the presence of TiO_2 , Ti(+IV)-
- 190 oxide as already indicated by GIXRD analyses (see Fig. 2).
- 191 The mass spectrum of the top Ti-oxide region formed at 1200 °C (see Fig. 3b) exhibits similar peaks to the spectrum of the 800 °C sample, except the ones for $A1^{+/2+}$ (27 and 13.5 Da) and $A1O^{2+}$ (21.5 Da). 192 These peaks presumably result from a reaction with the alumina crucible during oxidation. The main 193 194 peak of Si⁺ (28 Da) is identified as well and no Mo-related peaks are detected. Peak deconvolution 195 reveals the chemical composition to be 31.7 at% Ti and 68.3 at% O in the top Ti-oxide, 1200 °C sample 196 (see Table 2). Assuming no experimentally caused underestimate of the O content, (see Sect. 2), the 197 presence of TiO₂, Ti(+IV)-oxide, is confirmed in the top layer by APT. This was also expected from the 198 GIXRD analyses performed in this study (see Fig. 2) and from the EBSD results of the top Ti-oxide 199 scale revealing rutile TiO₂, see Ref. [9]. Although respective peaks are observed in the mass spectrum, 200 the concentration of Si and Al is below 0.1 at%.
- 201 The mass spectra of the Ti-oxide of the underlying duplex scale (see Fig. 3c) exhibits the same peaks 202 found in the mass spectra of the top layer tips, including a small Si⁺ peak at 28 Da. Again, no Mo peaks 203 are observed and the duplex layer shows no peaks related to Al. The latter suggests that no reaction with 204 the alumina crucible has occurred during oxidation testing. This is reasonable as the duplex scale is 205 assumed to grow inwards and is separated from the atmosphere by the top Ti-oxide scale. Thus, it is not 206 in contact with the crucible. In comparison to the top Ti-oxide, 1200 °C sample, a lower O content of 207 only 59.0 at% (equiv. to 41.0 at% Ti) is determined after peak deconvolution. As discussed, it can be 208 assumed that the APT analysis conditions did not cause an underestimation of the O content. EBSD 209 analyses by Schliephake et al. [9] unambiguously confirmed the top oxide scale to be rutile TiO_2 , 210 Ti(+IV)-oxide. However, in the underlying duplex scale, besides some rutile-assigned portions, multiple 211 un-indexed regions were assumed to be amorphous SiO₂. These un-assigned regions might represent 212 another Ti-oxide than rutile TiO₂, Ti(+IV)-oxide.
- The mass spectrum of the Si-oxide (see Fig. 3d) mainly exhibits peaks, which can be assigned to Si and O or combinations of both. Again, no Mo- or Al-related peaks are found. In contrast to all earlier discussed mass spectra, the peak at 32 Da results predominantly from O_2^+ ions. Small side peaks of TiO²⁺ ions can be observed at 31, 31.5, 32.5 and 33 Da. Using peak deconvolution, a total Ti content of about 0.4 at% is obtained for the Si-oxide. The concentrations of Si (38.0 at%) and O (61.6 at%) are close to the stoichiometry of Si(+IV)-oxide SiO₂, but this phase seems to be slightly depleted in O, too,
- 219 like the Ti-oxide in the duplex layer.
- 220 The corresponding subsets of the Ti-oxide, as well as of the Si-oxide regions within the duplex oxide
- scale, which were taken to determine the chemical composition of the phases, are included in Fig. 3e.
- 222 The reconstructions of tip from the top Ti-oxide scales at 800 and 1200 °C are included in Supp. 2 for
- the sake of completeness.



Fig. 3 Characteristic parts of the mass spectra of the top layer of the Ti-oxide-800 °C sample (a), the top Ti-oxide-1200 °C sample (b), as well as the duplex Si-oxide-1200 °C (c) and the duplex Ti-oxide-1200 °C (d) regions of the duplex layer formed at 1200 °C. Corresponding visualisation of the subsets for the analyses of the duplex oxide scale at 1200 °C (e), for reasons of clarity only 1 % of all identified ions is shown here.

 Table 2
 Chemical composition of the oxides in the investigated tips determined by APT after peak deconvolution (in at%) and comparison to the predominant oxide stoichiometry. * In this case, several presumable oxide stoichiometries are compared based on the experimental results.

/ at%	Ti	Si	0	Al	predominant oxide	
Ti-oxide- 800 °C	32.4	< 0.1	67.6	-	TiO _{2.1}	Ti(+IV)
top Ti-oxide-1200 °C	31.7	< 0.1	68.3	< 0.1	TiO _{2.2}	Ti(+IV)
duplex Ti-oxide-	41.0	< 0.1	59.0	-	TiO _{1.4}	Ti(+II) or Ti(+III)
1200 °C*					Ti ₂ O _{2.9}	Ti(+III)
					Ti ₃ O _{4.3}	Ti(+IV/+III)
duplex Si-oxide-1200 °C	0.4	38.0	61.6	-	SiO _{1.6}	Si(+IV)

The experimental results of the Ti- and Si-oxide regions of the duplex scale are corroborated by literature data proving that SiO₂ (Si(+IV)-oxide) and TiO₂ (Ti(+IV)-oxide) are in equilibrium at ambient pressure in air at 1100 [23] and 1200 °C [24], respectively. Moreover, there is only a solubility of 0.85 at% Si in rutile TiO₂ reported at 1300 °C for pressures of 3 GPa and higher [25]. Assuming a linear dependence of solved Si in TiO₂ with pressure, a solubility at ambient pressure of less than 0.57 at% can be extrapolated [25].

230 However, the unexpected stoichiometry and crystal structure of the Ti-oxide in the duplex scale at 231 1200 °C remains unsolved. As it is not clear what kind of oxidation level is prevalent in this oxide (see 232 Table 2, third row), for instance Ti(+II), Ti(+III) or Ti(+IV), the oxide is designated as Ti_xO_y with the 233 general description of the oxidation level Ti(+2y/x). This off-stoichiometric Ti_xO_y is present as rutile 234 TiO₂ as confirmed by GIXRD in this work, because other crystal structure types cannot be assigned. 235 Additionally, the presence of rutile was confirmed by EBSD in Ref. [9], whereas sub-surface regions 236 are not indexed and might represent Ti-oxide other than rutile Ti(+IV)-oxide. However, the chemical 237 composition determined by APT is not in agreement with the stoichiometry range of stable rutile TiO_2 238 reported in literature (TiO_{2-x} with x = 0 to 0.04 [26, 27]). From a thermodynamic point of view, besides 239 TiO₂, the presence of Ti₃O₅ would be expected (solubility range Ti₃O_{5+x} with x = 0 to 0.1 [26, 28]) as 240 illustrated by the isothermal sections of the ternary Ti-Si-O (see Fig. 4a) and Mo-Si-O systems (see Fig. 241 4b) at the relevant temperatures of 1200 and 700 to 1000 °C, respectively. The possibly formed oxidation 242 products of the phases Mo_{SS} and Ti_5Si_3 (when neglecting the influence of dissolved Mo of (11 ± 3) at% 243 (determined by EDX) in $(Ti,Mo)_5Si_3$) can be seen when the O concentration (comparably to the oxygen 244 partial pressure) is increased (dotted line). A stability region of Ti_5Si_3 , SiO_2 and Ti_3O_5 (highlighted in 245 blue in Fig. 4a) can be reached when Ti₅Si₃ is significantly enriched with O. With higher O concentration 246 or increased oxygen partial pressure, SiO_2 and TiO_2 are in equilibrium with O (highlighted in green in 247 Fig. 4a). Ti₄O₇ is here excluded, as it is not in equilibrium with (Ti,Mo)₅Si₃ and as the APT results do 248 not match the stoichiometry. During oxidation of Mo_{SS} the formation of MoO₂, SiO₂ and MoO₃ occurs 249 depending on the O concentration and oxygen partial pressure. Based on thermodynamics, it is likely that at the substrate surface SiO_2 (solid) + Ti_3O_5 (solid) + MoO_3 (volatile) are forming, while the 250

- 251 composition of the duplex oxide scale of $SiO_2 + Ti_3O_5 + MoO_3$ (volatile) changes to SiO_2 and TiO_2 with
- 252 increasing thickness. The presence of the top TiO_2 oxide scale seems to be determined by the kinetics
- 253 due to its observed fast-growing nature [13, 29] and the fast diffusion of Ti cations within TiO₂ [30].



Fig. 4 Isothermal sections of the ternary Ti-Si-O (a) and Mo-Si-O (b) systems at 1200 and 700 to 1000 °C, respectively, including selected, highlighted phase equilibria along the stability line of Ti₅Si₃ or Mo_{SS} (dotted grey line) with enrichment of O [23, 31].

3.3. Analysis of the oxidation kinetics

- In the following, the oxidation kinetics will be referred to as the kinetics of oxide scale growth, if not otherwise stated. Literature data on weight change oxidation kinetics, which are considered for comparison, are explicitly highlighted.
- 257 The evolution of the (sub-)oxide scale thickness d (internal oxidation d_{int} , duplex d_{duplex} and top scale
- 258 d_{top}) at 1200 °C is plotted in Fig. 5a as a function of time in double logarithmic manner (data at 100 h
- taken from our previous article [10]). The following power fit function for the oxide scale thickness d

in dependence of the exposure time t with the oxidation rate constant k_n for a specific exponent n was applied:

$$d^n = k_n \cdot t \qquad \qquad \text{Eq. 1}$$

262 First, the fit was performed with the exponent *n* being fixed to 2, which is equal to a parabolic oxide scale growth law [32]. Additionally, n was adjusted individually in order to achieve optimum fit quality 263 264 for comparison (dotted fit lines in Fig. 5a). It is revealed that: (i) The overall oxide scale growth at 265 1200 °C is dominated by the growth of the duplex scale (green circles). (ii) Both, the evolution of the oxide scale in total d_{total} (violet triangles) and the duplex scale d_{duplex} (green circles) are parabolic 266 267 with n values close to 2. (iii) Subtraction of the duplex scale data from the total oxide scale yields the change of the top single-phase oxide scale with time (blue triangles), which also seems to follow a 268 269 parabolic rate law. However, a fit itself for the data points of the top single-phase was not possible since 270 only two data points could be validly determined as for short oxidation times no separation of a top 271 single-phase oxide scale was observed. In conclusion, the oxidation kinetics are determined to be 272 parabolic and thus, the oxidation mechanism is regarded as bulk diffusion rate-controlled by either the 273 oxidant (O anion) or the reactant (metal cation) through the (sub-)oxide scales.

274 In order to assess whether there is a change in oxidation mechanism with decreasing temperature and 275 thus, less thermal activation for diffusion processes, the evolution of the total oxide scale thickness d_{total} at 1200 °C is compared to the observations made at 800 and 1100 °C (see Fig. 5b). It is 276 277 demonstrated that the oxide scales are considerably thicker at elevated temperatures, namely (26 ± 7) and (68 \pm 11) µm at 1100 and 1200 °C, respectively, as compared to only (5 \pm 2) µm at 800 °C after 278 279 100 h of cyclic oxidation. Moreover, it is found that the oxide scale evolution might be associated with 280 an almost cubic oxidation kinetics at 1100 °C as well, as revealed by an exponent of n = 2.94 (see Table 3). The cubic and parabolic growth observed at 1100 and 1200 °C, respectively, is attributed to diffusion 281 282 processes, especially relevant at high temperatures. This is confirmed by the estimated diffusion distance 283 of Ti⁴⁺ cations in TiO₂, Ti(+IV)-oxide at the respective temperatures, which is found to be 29 and 62 µm after 100 h at 1100 and 1200 °C, respectively, which is in excellent agreement to the experimental 284 285 values. The impact of the temperature on the evolution of the oxide scale thickness is underlined by Fig. 286 5c. The dependence of the total oxide scale thickness is highlighted as a function of temperature for 287 specific exposure durations of 1, 10 and 100 h.

In contrast, the overall evaluation of the oxide scale growth at 800 °C does not yield parabolic kinetics, even after exposure times of 1000 h, as a considerably increased exponent of n = 4.45 according to Eq. 1 is noted. Such high exponents in power-law oxidation kinetics are neither widely reported, nor discussed in literature. Additionally, as only a moderate fit quality ($R_{adj}^2 = 0.82$) is obtained, it is suggested that there are different oxidation stages with changing oxidation kinetics. This suggestion is supported by considering the initial oxidation stage up to 100 h and the ongoing stage from 100 to 1000 h 294 separately. During the initial oxidation stage, it is likely that the prevalent oxidation mechanism is reaction rate-controlled, as a linear fit leads to an excellent fit quality with $R_{adi}^2 = 0.97$ (see Table 3). 295 296 The obedience to linear oxidation kinetics is further corroborated by the discontinuous morphology of 297 the oxide scale for exposure times shorter than 100 h (see BSE micrographs in Fig. 1). It is shown that 298 the oxidation occurs locally, especially in the surface-near Moss regions, although not providing full 299 coverage of the alloy substrate (see Fig. 1a and b). Therefore, the kinetics up to 100 h are most likely to 300 be rate-determined by surface reactions occurring either at the oxide scale/atmosphere interface or at the 301 oxide scale/substrate interface. Other oxidation mechanisms leading to linear oxidation kinetics, such as 302 direct O access to the substrate through porous oxide scales or cracks, are unlikely, since neither 303 significant porosity nor cracks are observed in the oxide scale by SEM analysis (see Fig. 1a and b). Note 304 that this initial linear oxidation kinetics does not lead to catastrophic oxidation behaviour, as the oxidation rate constant of 8.25 x 10^{-12} ms⁻¹ is significantly low. For longer exposure times than 100 h, a 305 306 continuous mixed Si-Ti-oxide scale is formed (see Fig. 1c), which accounts for the change in oxidation 307 kinetics. Fitting the respective values according to Eq. 1 leads to an exponent of 3.18 with a good fit quality of $R_{adi}^2 = 0.94$. This reveals that the oxidation kinetics change from linear to cubic. In literature, 308 309 cubic oxidation kinetics are assumed to be determined by diffusion processes along grain boundaries 310 [33-35]. Thus, it might be that O inward diffusion along grain boundaries and Ti-oxide/Si-oxide phase 311 boundaries determines the oxidation mechanism for exposure times longer than 100 h. However, no 312 profound evidence can be given here for this assumption.





Fig. 5 Evolution of the oxide scale thickness in total d_{total} and of the respective sub-scales (top Ti-oxide d_{top} , duplex Siand Ti-oxide scale d_{duplex} and internal oxidation zone d_{int}) in dependence of the exposure time t at 1200 °C for the eutectic alloy (a). Fit functions according to Eq. 1 with n being adjusted variably (dotted lines) are included. In comparison d_{total} is displayed logarithmically at 800, 1100 and 1200 °C (b) and fitted accordingly as well (b). The total oxide scale thicknesses are compared for different times at 800, 1100 and 1200 °C (c).

Table 3 Determined oxidation rate constants k_n for 800, 1100 and 1200 °C. For 1100 and 1200 °C referring to Eq. 1. For 800 °C k^{*}, referring to a linear fitting method, is included. R_{adj}^2 values are provided as well.

<i>T</i> / °C	fitting range of <i>t</i> / h	n / -	$\boldsymbol{k_n} / \mathrm{m^n s^{-1}}$	k */ ms ⁻¹	R_{adj}^2 / -
	1 - 1000	4.45	1.16 x 10 ⁻²⁹	-	0.82
800	1 - 100	1 (linear)	-	8.25 x 10 ⁻¹²	0.97
	100 - 1000	3.18	4.51 x 10 ⁻²³	-	0.94
	100 - 1000	2 (parabolic)	4.41 x 10 ⁻¹⁷	-	0.61
1100	1 – 100	2.94	8.64 x 10 ⁻²⁰	-	0.99
1100	1 100	2 (parabolic)	2.38 x 10 ⁻¹⁵	-	0.86
1200	1 – 100	2.13	3.56 x 10 ⁻¹⁵	-	0.96
	1 100	2 (parabolic)	1.51 x 10 ⁻¹⁴	-	0.96

313 The high-temperature parabolic oxidation behaviour of the eutectic alloy Mo-20Si-52.8Ti is characterised by the parabolic oxidation rate constant $k_{n=2} = 2.38 \text{ x } 10^{-15} (1100 \text{ °C})$ to $1.51 \text{ x } 10^{-14} \text{ m}^2 \text{s}^{-1}$ 314 315 (1200 °C), which are thermally activated with an activation energy of 310 kJ/mol. These findings also 316 apply to certain eutectic-eutectoid alloys from Ref. [11] (see App. 1 for their chemical compositions), 317 as well as to the eutectoid alloy from Ref. [9], as parabolic oxidation kinetics with similar oxidation rate 318 constants to the eutectic alloy were revealed with activation energies in the range of 200 to 410 kJ/mol. 319 Note that the determination of these activation energies is based on only two data points and thus, only 320 serves as estimates when interpreting the activation energies.

Moreover, no difference was found between the pesting-resistant and non-pesting-resistant Ti-rich and Ti-lean (nominal Ti content < 43 at%) alloys, respectively, which could have been taken into consideration for further understanding the root causes of pesting resistance. However, in order to classify the oxidation behaviour of these Mo-Si-Ti alloys, their parabolic oxidation rate constants $k_{n=2}$ are compared to the relevant diffusion coefficients of this systems. Since the oxidation rate constants are known to be thermally activated [36], these can be visualised by an Arrhenius plot in Fig. 6. The following correlation between the oxidation rate constant and the diffusion coefficient *D* allows a direct comparison of the respective diagrams (see Eq. 2 [37]):

$$k_{n=2} = \frac{2 D C_0}{N}$$
 Eq. 2

Here, *D* is the diffusion coefficient of a specific species diffusing in the oxide, C_0 is the oxidant concentration at the scale surface and *N* is the number of oxidant species incorporated in the newly grown oxide of unit volume [37].

332 Generally, it is seen in Fig. 6 that Ti ion diffusion (solid blue line) is considerably faster than O ion 333 diffusion in TiO_2 (dotted, dashed and solid red lines). This is in good agreement with the assumption 334 that the top Ti-rich oxide scale is growing outward by Ti-cation outward diffusion, which has also been 335 experimentally verified by marker experiments by Azim et al. in Ref. [29] on Mo-Si-B-Ti alloys. In contrast, the diffusion coefficient for Si bulk diffusion in SiO_2 is significantly lower compared to the 336 diffusion coefficients for O. This is in accordance with the assessment of Deal and Grove in Ref. [38] 337 338 who stated that SiO₂ formation proceeds rather by the inward diffusion of O, than by the outward diffusion of Si. Furthermore, the respective oxidation rate constants of the eutectic alloy $(k_{n=2}^{eutectic})$, of 339 the intermediate eutectic-eutectoid alloys $(k_{n=2}^{eutectoid})$ and of the eutectoid alloy $(k_{n=2}^{eutectoid})$ 340 are found to be in the range of the diffusion coefficient of Ti in TiO_2 . Hence, it can be concluded that 341 342 the oxidation rate of these eutectic-eutectoid Mo-Si-Ti alloys is determined by the Ti diffusion in TiO₂.



Fig. 6 Temperature-dependence of the diffusion coefficients D of Ti and O ions in single-crystalline (SX) and polycrystalline (PX) TiO_2 (blue and red lines) and Si- and O ions in vitreous (v) SiO_2 (yellow and orange lines), respectively. Data taken from [39-44]. For comparative reasons, the values of $k_{n=2}$ for the eutectic (black solid circle), eutectic-eutectoid (half-opened circles) alloys and the eutectoid alloy (open black circle) are added.

- 343 In order to understand the observed oxidation kinetics in the Mo-Si-Ti system, the individual oxidation
- behaviour of the constitutional phases Mo_{SS} and $(Ti,Mo)_5Si_3$ will be discussed in the following. Mo is
- 345 known to undergo catastrophic oxidation due to volatilisation of MoO₃ at temperatures above 500 °C
- 346 [45-47]. The respective activation energy for temperatures beyond 800 °C was associated with a

diffusion-controlled process through the gas phase [45, 47, 48] with 82 kJ/mol [45]. However, the

348 tendency of forming volatile MoO₃ can be counterbalanced by the formation of solid Ti-rich oxides,

347

- 349 when alloyed with Ti [11]. Thus, the linear mass loss oxidation rate can be considerably decelerated at
- 350 800 °C, namely from -33 to -14 mg/cm²h⁻¹, when increasing the Ti content from 20 to 40 at% [11]. The
- here discussed eutectic alloy comprises a Ti-rich Mo_{ss} with an approximate Ti content of 45 at% [10].
- 352 This supports the observed pesting-resistance in Ti-rich Mo-Si-Ti and Mo-Si-B-TiC alloys at 800 °C
- 353 with considerable volume fractions of Ti-containing Moss [10, 11, 49]. Therefore, the improvement in
- oxidation behaviour is attributed to the formation of a (relatively) dense TiO₂ oxide scale [49].
- 355 In comparison, the silicide phase Ti_5Si_3 reveals different weight change oxidation kinetics, which are 356 dependent on the Si content and the oxidation duration [50]. The (Ti,Mo)₅Si₃ phase present in the 357 investigated eutectic alloy exhibits a constant Si ratio close to the ideal stoichiometry due to ingot 358 metallurgical manufacturing. Furthermore, there is a considerable Mo concentration of (13 ± 4) at% 359 [11]. Therefore, the phase composition is regarded to be comparable to the studies made by Majumdar 360 et al. in Ref. [12] on an Mo-30Si-40Ti alloy, which comprises a (Ti,Mo)₅Si₃ matrix, but with an increased 361 Mo content of 26 at%. The oxidation behaviour was reported to obey parabolic weight gain and oxide 362 scale growth kinetics in the temperature range of 900 up to 1300 $^{\circ}$ C [12]. Thereby, the formation of an outer TiO₂ scale and an underlying SiO₂-TiO₂ duplex scale was observed [12] like for the investigated 363 364 Mo-Si-Ti alloys from the present study (the eutectic alloy Mo-20Si-52.8Ti, as well as the other 365 derivatives from the Mo-Si-Ti system listed in App. 1). The authors concluded that the formation of 366 volatile MoO₃ is suppressed in (Ti,Mo)₅Si₃ [12]. The parabolic oxidation rate constant was found to be about half an order of magnitude lower than in the eutectic alloy at 1200 °C in Ref. [12] (compare with 367 368 Table 2). The corresponding activation energies were determined to be 72 and 325 kJ/mol in the temperature range between 900 to 1200 °C and 1200 to 1300 °C, respectively [12]. This first seems 369 comparably low, but was interpreted by the authors on the basis of the activation energy for diffusion of 370 371 oxygen in fused SiO_2 which was regarded to be in the same order [12]. At higher temperatures instead, 372 the activation energy is comparable to the activation energies found for the Mo-Si-Ti alloys in this study 373 (see App. 1). The difference in activation energies was attributed to a change in microstructural set-up 374 of the duplex oxide scale with an increased volume fraction of TiO_2 , which might lead to accelerated O 375 inward diffusion [12]. Conclusively, $(Ti,Mo)_5Si_3$ exhibits a diffusion-controlled oxidation behaviour, 376 which is mainly attributed to the inward diffusion of O through the SiO₂-TiO₂ duplex scale [12].
- This comparative study reveals that the oxidation kinetics are combined kinetics of the constituting phases Mo_{SS} and $(Ti,Mo)_5Si_3$. At high temperatures the diffusion processes are fast enough to form

379 continuous, solid oxide scales, which can be accounted for the parabolic bulk diffusion-controlled 380 oxidation, comparable to the oxidation kinetics of $(Ti,Mo)_5Si_3$. By contrast, the oxidation kinetics at 381 800 °C are different to the ones observed for the constituting phases Mo_{SS} and $(Ti,Mo)_5Si_3$, as the 382 eutectic alloy reveals linear oxidation kinetics at the beginning, turning into cubic kinetics for oxidation 383 times longer than 100 h.

These fundamental differences might be rationalised as follows: Generally, the defect structure of the oxide determines the oxidation kinetics. In the case of rutile TiO_2 the defect structure depends on temperature, oxygen partial pressure, the exact stoichiometry [51] and impurities [52]. At 1100 and 1200 °C, the main defects are O vacancies and Ti cations of different valences (Ti^{3+} , Ti^{4+}) [53]. While the first primarily contribute to the non-stoichiometry [53, 54], the latter are the defects dominating scale formation.

390 3.4. The role of the Ti-oxide within the oxide scales formed on the eutectic alloy Mo-20Si-52.8Ti 391 The good oxidation resistance of the Ti-oxide formed on the eutectic alloy Mo-20Si-52.8Ti (see Fig. 1) 392 in comparison to pure Ti is unexpected [36, 55]. Therefore, possible explanations are discussed in the 393 following: In essence, the oxidation resistance of Ti is improved by reducing its O solubility [55], e. g. 394 by alloying with Al or Si [16, 56]. A reduction in oxidation rate is attained in Ti-xSi alloys with x = 0.4395 to 1.7 or 12.7 at% Si at 500 to 700 and 850 °C, respectively [16, 56]. Moreover, a parabolic oxidation 396 behaviour is observed for Ti-Si alloys in contrast to a linear one, which is present in pure Ti [56]. When 397 3.3 at% Si or less are added, Si was found to be homogenously distributed within the oxide scale, either 398 solved as solid solution in rutile TiO_2 or as embedded SiO_2 islands with diameters of less than 1 μ m at 399 850 °C [56]. In contrast, higher additions up to 13 at% Si were found to be inhomogeneous distributed 400 within the oxide scale and even led to cracking at the substrate/oxide interface [16]. Hence, the Si 401 concentration presumably accounts for a transition in oxide scale morphology preventing pore formation 402 and spallation, which typically occurs in TiO₂ formed on pure Ti [56]. There are several impacts of Si 403 on the oxidation behaviour of Ti-Si alloys proposed: (i) Si might retard the inward diffusion of O and 404 therefore lead to a reduction in penetration depth [56], as interstitially solved Si ions might reduce the 405 amount of available O vacancy sites decelerating the diffusion rate of O in rutile TiO_2 [56]. (ii) The 406 presence of SiO_2 facilitates the formation of a denser, less porous oxide scale and prevents 407 recrystallisation and stratification of TiO₂ due to the change in stress relaxation processes within the 408 oxide scale [16, 56]. However, it is questionable whether the very low amount of Si/SiO_2 in TiO_2/Ti -409 oxide below 0.1 at% formed on the eutectic alloy (see Table 2 and Fig. 2) can be taken into account for 410 a reduction in O vacancies due to preoccupation by Si ions. For comparison, in Ti-Nb alloys, solution of Nb⁵⁺ ions was observed in rutile TiO₂ leading to a significant deceleration of oxide scale growth at 411 900 and 1000 °C in static air [57]. Thereby, Nb⁵⁺ ions were found to substitute Ti⁴⁺ ions with an 412 413 estimated ratio of less than 0.14 % [57].

414 Although, TiO₂ formed on Ti or Ti-based alloys often suffers from cracking [16, 55, 58-60], the oxide 415 scales (especially the Ti-oxide) formed on the eutectic alloy are crack-free with very low porosity of 416 less than 1.5 vol% along the oxide scale substrate interface [11]. This indicates that a change in density 417 and adherence of the oxide scales allow for the high oxidation resistance. The crack formation is often 418 caused by the formation of sub-layers like TiN [16], but none were observed on the current eutectic 419 alloy Mo-20Si-52.8Ti. Moreover, the mismatch of the CTE needs to be considered with regard to the oxide/substrate compatibility. For this purpose, CTE values are compared in Table 4. There is no 420 421 considerable difference in CTE, no matter whether TiO_2 is growing on Ti or on the eutectic alloy. 422 However, especially at longer exposure times and higher temperatures, the relationship between the top 423 TiO₂, the duplex scale and the eutectic alloy substrate has to be taken into account. The CTE of thermally 424 grown SiO_2 is about one order of magnitude lower, so it is likely that the SiO_2 portions balance the 425 thermal expansion of TiO₂ within the (duplex) oxide scale and suppress crack formation during cyclic 426 oxidation testing.

	CTE / K ⁻¹	Refs.
Ti	10.5 x 10 ⁻⁶ (20 – 700 °C)	[61]
TiO ₂	<i>a</i> -axis: 8.1 x 10 ⁻⁶ (276 °C) <i>c</i> -axis: 10.6 x 10 ⁻⁶ (276 °C)	[62]
SiO_2	5 x 10 ⁻⁷ (RT – 300 °C)	[63]
eutectic alloy	7.0 – 9.1 x 10 ⁻⁶ (300 – 1200 °C)	this study

427	Table 4	Comparison of	the coefficients c	of thermal ex	pansions	(CTE) of	Ti, TiO ₂ ,	SiO ₂ and	the eutectic all	oy Mo-20Si-52.8	Ti.
				./ .		· · · ·					

428 In conclusion, the beneficial impact of the Ti-oxide on the oxidation behaviour is attributed to the 429 interaction with the Si-oxide, which might lead to a reduction in available vacancies for O inward diffusion. Additionally, with regard to the diffusion of O, Si and Ti, the O concentration being available 430 431 for the formation of the duplex oxide scale at 1200 °C is determined by the O ion diffusion flux through 432 the top TiO_2 oxide scale. Once the duplex scale is formed, Ti ion diffusion (which might be faster along 433 the penetrating Ti-oxide regions through the oxide scale) to the top TiO_2 scale is necessary for further 434 growth of the top TiO_2 oxide scale. Therefore, it is concluded that the fast formation of the top TiO_2 435 scale is triggered by kinetics and that its growth is slowed down with ongoing formation of the 436 underlying duplex scale.

4. Summary and Conclusion

437 The analysis of the microstructural constitution of the oxide scales formed on the eutectic Mo-20Si-438 52.8Ti alloy at 800 °C revealed a single-layered mixed oxide scale comprising Ti- and Si-oxide. At 439 1200 °C, a top Ti-oxide scale with an underlying mixed duplex Ti- and Si-oxide scale is observed. 440 Besides rutile TiO₂ and some cristobalite SiO₂, GIXRD analyses indicate the presence of some MoO₃ 441 in the oxide scale formed at 1200 °C. However, the formation of MoO₃ is outbalanced and

- 442 overcompensated by solid oxide scale formation as documented by negligible mass changes even after 443 test durations of 100 h. The assessment of the compositional constitution of the oxide scales by APT leads to the following conclusions: (i) The chemical composition of the (top) Ti-oxide scales formed at 444 445 800 and 1200 °C is found to be comparable with a stoichiometry matching rutile-type TiO₂ Ti(+IV)-446 oxide. (ii) The duplex scale formed at 1200 °C is composed of an O-depleted Ti-oxide region off-447 stoichiometric to typical known Ti-oxide, among which Ti₃O₅ is the most likely one to be present. (iii) The Si-oxide region within the duplex scale is depleted in O as well, with a stoichiometry of SiO_{1.6} 448 449 closest to SiO₂. It is unlikely that this observed depletion in O is caused by an underestimation caused 450 by the measurement conditions. (iv) Virtually no solubility of Mo is found in the Ti- and Si-oxide, 451 respectively, for both oxide scales formed at 800 and 1200 °C. (v) There is a negligible amount of Si 452 solved in the Ti-oxide formed at 800 and 1200 °C.
- 453 The study of the oxide growth kinetics revealed that the oxide scale growth obeys a linear rate law at 454 800 °C up to 100 h pointing to a surface reaction-controlled oxidation. Longer exposure times facilitate 455 the formation of a continuous mixed oxide scale, which results in cubic oxidation kinetics. In contrast, 456 at 1100 and 1200 °C the thickness of the overall oxide scale and of the duplex scale grows with almost 457 parabolic oxidation kinetics. This is also found for the eutectoid and eutectic-eutectoid Mo-Si-Ti alloys. 458 The activation energies of the parabolic oxidation rate constants are in good agreement with published data on activation energies for self-diffusion of O, Ti and Si in the respective oxides [39-44, 64] 459 460 confirming the oxidation rate to be diffusion-controlled. The observed change in oxidation mechanism 461 between 800 and 1100 °C correlates with the oxidation kinetics of the microstructural constituents Moss and (Ti,Mo)₅Si₃. While Moss is known to undergo catastrophic oxidation with linear mass loss [45, 46], 462 463 which is decelerated with increasing Ti content [11], above 600 °C, (Ti,Mo)₅Si₃ was found to obey 464 parabolic oxide growth kinetics in the temperature range of 900 to 1300 °C [12].

465

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474

Appendix

eutectic-eutectoid alloys	nominal composition / at%
alloy #1	Mo-21Si-47Ti
alloy #2	Mo-21Si-43.4Ti
alloy #3	Mo-21.5Si-41.5Ti
alloy #4	Mo-21Si34Ti

App. 1 Nominal chemical composition of eutectic-eutectoid Mo-Si-Ti alloys corresponding to Refs. [9, 11].

Supplementary



Supp. 1 GIXRD diffraction patterns of the cyclically oxidised samples at 800 (top) and 1200 °C (bottom) for 100 h with incident angles of 1.2 (grey) and 2.5° (black). Note that the intensities are plotted with logarithmic scale.



475 Supp. 2 Visualisation of the subsets for the APT analyses of the top Ti-oxide scale at 800 (a) and 1200 °C (b). For reasons of clarity only 1 % of all identified ions is shown here. No SiO_x ions were identified.

Data availability statement

- 477 The raw and processed data required to reproduce these findings are available on request to
- 478 alexander.kauffmann@kit.edu.

References

479 1. M. F. Yan, J. B. MacChesney, S. R. Nagel, W. W. Rhodes, Sintering of optical wave-guide 480 glasses. Journal of Materials Science, 1980. 15(6): p. 1371-1378. DOI: 10.1007/BF00752116. 481 2. M. Mever, M. Kramer, M. Akinc, Boron-doped molybdenum silicides. Advanced Materials, 1996. 8(1): p. 85-88. DOI: 10.1002/adma.19960080118. 482 M. K. Meyer, A. J. Thom, M. Akinc, Oxide scale formation and isothermal oxidation behavior 483 3. of Mo-Si-B intermetallics at 600-1000°C. Intermetallics, 1999. 7(2): p. 153-162. DOI: 484 485 10.1016/S0966-9795(98)00058-2. K. Yoshimi, S. Nakatani, T. Suda, S. Hanada, H. Habazaki, Oxidation behavior of Mo₅SiB₂-486 4. 487 based alloy at elevated temperatures. Intermetallics, 2002. 10(5): p. 407-414. DOI: 488 10.1016/S0966-9795(02)00013-4. 489 Y. Yang, H. Bei, S. Chen, E. P. George, J. Tiley, Y. A. Chang, Effects of Ti, Zr, and Hf on the 5. phase stability of Mo_{SS}+ Mo₃Si+ Mo₅SiB₂ alloys at 1600°C. Acta Materialia, 2010. 58(2): p. 490 491 541-548. DOI: 10.1016/j.actamat.2009.09.032. 492 A. Rahmel, P. J. Spencer, Thermodynamic Aspects of TiAl and TiSi₂ Oxidation: The Al-Ti-O 6. 493 and Si-Ti-O Phase Diagrams. Oxidation of Metals, 1991. 35(1-2): p. 53-68. DOI: 494 10.1007/BF00666500. 495 7. T. A. Parthasarathy, M. G. Mendiratta, D. M. Dimiduk, Oxidation mechanisms in Mo-496 reinforced Mo₅SiB₂ (T2)-Mo₃Si alloys. Acta Materialia, 2002. 50(7): p. 1857-1868. DOI: 497 10.1016/S1359-6454(02)00039-3. 498 S. Paswan, R. Mitra, S. K. Roy, Oxidation behaviour of the Mo-Si-B and Mo-Si-B-Al alloys 8. 499 in the temperature range of 700-1300°C. Intermetallics, 2007. 15(9): p. 1217-1227. DOI: 10.1016/j.intermet.2007.02.012. 500 D. Schliephake, A. Kauffmann, X. Cong, C. Gombola, M. A. Azim, B. Gorr, H.-J. Christ, M. 501 9. 502 Heilmaier, Constitution, oxidation and creep of eutectic and eutectoid Mo-Si-Ti alloys. 503 Intermetallics, 2019. 104: p. 133-142. DOI: 10.1016/j.intermet.2018.10.028. 504 10. S. Obert, A. Kauffmann, M. Heilmaier, Characterisation of the oxidation and creep behaviour 505 novel Mo-Si-Ti alloys. Acta Materialia, 2020. 184: p. 132-142. DOI: of 10.1016/j.actamat.2019.11.045. 506

- 507 11. S. Obert, A. Kauffmann, S. Seils, S. Schellert, M. Weber, B. Gorr, H.-J. Christ, M. Heilmaier,
 508 On the chemical and microstructural requirements for the pesting-resistance of Mo-Si-Ti alloys.
 509 JMR&T, 2020. 9(4): p. 8556-8567. DOI: 10.1016/j.jmrt.2020.06.002.
- S. Majumdar, P. K. Singh, A. K. Pandey, G. V. S. N. Rao, Kinetics of oxide scale growth on a (Ti,Mo)₅Si₃ based oxidation resistant Mo-Ti-Si alloy at 900-1300°C. High Temperature Materials and Processes, 2019. 38(2019): p. 533-540. DOI: 10.1515/htmp-2019-0056.
- M. A. Azim, B. Gorr, H.-J. Christ, O. Lenchuk, K. Albe, D. Schliephake, M. Heilmaier, Effect of Ti content and nitrogen on the high-temperature oxidation behavior of (Mo,Ti)₅Si₃.
 Intermetallics, 2017. 90: p. 103-112. DOI: 10.1016/j.intermet.2017.05.023.
- J. Dai, J. Zhu, C. Chen, F. Weng, High temperature oxidation behavior and research status of modifications on improving high temperature oxidation resistance of titanium alloys and titanium aluminides: A review. Journal of Alloys and Compounds, 2016. 685: p. 784-798. DOI: 10.1016/j.jallcom.2016.06.212.
- J. Unnam, R. N. Shenoy, R. K. Clark, Oxidation of commercial purity titanium. Oxidation of Metals, 1986. 26(3-4): p. 231-252. DOI: 10.1007/BF00659186.
- 52216.D. Vojtěch, B. Bártová, T. Kubatík, High temperature oxidation of titanium-silicon alloys.523Materials Science and Engineering: A, 2003. 361(1-2): p. 50-57. DOI: 10.1016/S0921-5245093(03)00564-1.
- 52517.M. Yoshihara, Y.-W. Kim, Oxidation behavior of gamma alloys designed for high temperature526applications. Intermetallics, 2005. 13(9): p. 952-958. DOI: 10.1016/j.intermet.2004.12.007.
- J. Angseryd, F. Liu, H.-O. Andrén, S. S. A. Gerstl, M. Thuvander, Quantitative APT analysis
 of Ti(C, N). Ultramicroscopy, 2011. 111(6): p. 609-614. DOI: 10.1016/j.ultramic.2011.01.031.
- R. Kirchhofer, D. R. Diercks, B. P. Gorman, J. F. Ihlefeld, P. G. Kotula, C. T. Shelton, G. L.
 Brennecka, Quantifying Compositional Homogeneity in Pb(Zr, Ti)O₃ Using Atom Probe Tomography. Journal of the American Ceramic Society, 2014. 97(9): p. 2677-2697. DOI: 10.1111/jace.13135.
- 533 20. F. Liu, K. Stiller, Atom probe tomography of thermally grown oxide scale on FeCrAl.
 534 Ultramicroscopy, 2013. 132: p. 279-284. DOI: 10.1016/j.ultramic.2013.02.004.
- 535 21. F. Tang, B. Gault, S. P. Ringer, J. M. Cairney, Optimization of pulsed laser atom probe (PLAP)
 536 for the analysis of nanocomposite Ti–Si–N films. Ultramicroscopy, 2010. 110(7): p. 836-843.
 537 DOI: 10.1016/j.ultramic.2010.03.003.
- T. Boll, M. Thuvander, S. Koch, J. N. Wagner, N. Nedfors, U. Jansson, K. Stiller, An APT
 investigation of an amorphous Cr–B–C thin film. Ultramicroscopy, 2015. 159: p. 217-222. DOI:
 10.1016/j.ultramic.2015.01.001.
- J. I. Goldstein, S. K. Choi, F. J. J. V. Loo, G. F. Bastin, R. Metselaar, Solid-state Reactions and
 Phase Relations in the Ti-Si-O System at 1373 K. Journal of the American Ceramic Society,
 1995. 78(2): p. 313-322. DOI: 10.1111/j.1151-2916.1995.tb08802.x.
- 54424.A. Abba, A. Galerie, M. Caillet, High-temperature oxidation of titanium silicide coatings on545titanium. Oxidation of Metals, 1982. 17(1-2): p. 43-54. DOI: 10.1007/BF00606192.
- 54625.A. Escudero, F. Langenhorst, Incorporation of Si into TiO2 phases at high pressure. American547Mineralogist, 2012. 97(4): p. 524-531. DOI: 10.2138/am.2012.3941.
- 548 26. S. Andersson, B. Collén, U. Kuylenstierna, A. Magnéli, Phase analysis studies on the titanium-oxygen system. Acta Chemica Scandinavica, 1957. 11(10): p. 1641-1652.
- P. G. Wahlbeck, P. W. Gilles, Reinvestigation of the Phase Diagram for the System Titanium–
 Oxygen. Journal of the American Ceramic Society, 1966. 49(4): p. 180-183. DOI:
 10.1111/j.1151-2916.1966.tb13229.x.
- R. R. Merritt, B. G. Hyde, L. A. Bursill, D. K. Philp, The thermodynamics of the titanium + oxygen system: An isothermal gravimetric study of the composition range Ti₃O₅ to TiO₂ at 1304
 K. Philosophical Transactions of the Royal Society of London. Series A, Mathematical and Physical Sciences, 1973. 274(1245): p. 627-661. DOI: 10.1098/rsta.1973.0078.
- M. A. Azim, S. Burk, B. Gorr, H.-J. Christ, D. Schliephake, M. Heilmaier, R. Bornemann, P. H. Bolívar, Effect of Ti (Macro-) Alloying on the High-Temperature Oxidation Behavior of Ternary Mo–Si–B Alloys at 820–1300° C. Oxidation of Metals, 2013. 80(3-4): p. 231-242. DOI: 10.1007/s11085-013-9375-1.
- 561 30. D. A. Venkatu, L. E. Poteat, Diffusion of titanium of single crystal rutile. Materials Science and
 562 Engineering, 1970. 5(5): p. 258-262. DOI: 10.1016/0025-5416(70)90014-5.

56331.R. Beyers, Thermodynamic considerations in refractory metal-silicon-oxygen systems. Journal564of Applied Physics, 1984. 56(1): p. 147-152. DOI: 10.1063/1.333738.

565 32. G. B. Gibbs, Vacancy generation and the kinetics of oxidation. Philosophical Magazine, 1968.
566 18(156): p. 1175-1180. DOI: 10.1080/14786436808227748

- 33. Z. Liu, W. Gao, Y. He, Modeling of oxidation kinetics of Y-doped Fe–Cr–Al alloys. Oxidation of Metals, 2000. 53(3-4): p. 341-350. DOI: 10.1023/A:1004545421739.
- 569 34. D. Naumenko, B. Gleeson, E. Wessel, L. Singheiser, W. J. Quadakkers, Correlation between
 570 the microstructure, growth mechanism, and growth kinetics of alumina scales on a FeCrAlY
 571 alloy. Metallurgical and Materials Transactions A, 2007. 38(12): p. 2974-2983. DOI:
 572 10.1007/s11661-007-9342-z.
- 57335.W. J. Quadakkers, Growth mechanisms of oxide scales on ODS alloys in the temperature range5741000–1100°C. Materials and Corrosion, 1990. 41(12): p. 659-668. DOI:57510.1002/maco.19900411204.
- 576 36. P. Kofstad, Oxidation of Metals: Determination of Activation Energies. Nature, 1957.
 577 179(4574): p. 1362-1363. DOI: 10.1038/1791362a0.
- 57837.C.-J. Han, C. R. Helms, Parallel oxidation mechanism for Si oxidation in dry O2. Journal of The579Electrochemical Society, 1987. 134(5): p. 1297.
- 38. B. E. Deal, A. S. Grove, General Relationship for the Thermal Oxidation of Silicon. Journal of
 Applied Physics, 1965. 36(12): p. 3770-3778. DOI: 10.1063/1.1713945.
- M. Dechamps, P. Lehr, Sur l'oxydation du titane α en atmosphère d'oxygène: Rôle de la couche
 oxydée et mécanisme d'oxydation. Journal of the Less Common Metals, 1977. 56(2): p. 193207. DOI: 10.1016/0022-5088(77)90041-8.
- 585 40. J. C. Mikkelsen, Self-diffusivity of network oxygen in vitreous SiO₂. Applied Physics Letters,
 586 1984. 45(11): p. 1187-1189. DOI: 10.1063/1.95086.
- 587 41. D. K. Moore, D. J. Cherniak, E. B. Watson, Oxygen diffusion in rutile from 750 to 1000 degrees
 588 C and 0.1 to 1000 MPa. American Mineralogist, 1998. 83(7-8): p. 700-711. DOI: 10.2138/am589 1998-7-803.
- J. Rodríguez-Viejo, F. Sibieude, M. T. Clavaguera-Mora, C. Monty, ¹⁸O diffusion through amorphous SiO₂ and cristobalite. Applied Physics Letters, 1993. 63(14): p. 1906-1908. DOI: 10.1063/1.110644.
- 593 43. E. W. Sucov, Diffusion of Oxygen in Vitreous Silica. Journal of the American Ceramic Society,
 594 1963. 46(1): p. 14-20. DOI: 10.1111/j.1151-2916.1963.tb13763.x.
- 595 44. T. Takahashi, S. Fukatsu, K. M. Itoh, M. Uematsu, A. Fujiwara, H. Kageshima, Y. Takahashi,
 596 K. Shiraishi, Self-diffusion of Si in thermally grown SiO₂ under equilibrium conditions. Journal
 597 of Applied Physics, 2003. 93(6): p. 3674-3676. DOI: 10.1063/1.1554487.
- 598 45. E. A. Gulbransen, K. F. Andrew, F. A. Brassart, Oxidation of Molybdenum 550° to 1700°C.
 599 Journal of the Electrochemical Society, 1963. 110(9): p. 952-959. DOI: 10.1149/1.2425918.
- 600 46. E. S. Jones, J. F. Mosher, R. Speiser, J. W. Spretnak, The Oxidation of Molybdenum. Corrosion,
 601 1958. 14(1): p. 20-26. DOI: 10.5006/0010-9312-14.1.20.
- 47. M. Simnad, A. Spilners, Kinetics and Mechanism of the Oxidation of Molybdenum. JOM, 1955.
 603 7(9): p. 1011-1016. DOI: 10.1007/BF03377603.
- 60448.R. W. Bartlett, Molybdenum Oxidation Kinetics at High Temperatures. Journal of The605Electrochemical Society, 1965. 112(7): p. 744-746.
- 49. T. Hatakeyama, S. Ida, N. Sekido, K. Yoshimi, Significant improvement of the oxidation resistance of MoSiBTiC-based multiphase alloys by Ti enrichment. Corrosion Science, 2020: p. 108937. DOI: 10.1016/j.corsci.2020.108937.
- 50. Z. Tang, J. J. Williams, A. J. Thom, M. Akinc, High temperature oxidation behavior of Ti₅Si₃based intermetallics. Intermetallics, 2008. 16(9): p. 1118-1124. DOI:
 10.1016/j.intermet.2008.06.013.
- J. He, R. K. Behera, M. W. Finnis, X. Li, E. C. Dickey, S. R. Phillpot, S. B. Sinnott, Prediction 612 51. of high-temperature point defect formation in TiO₂ from combined ab initio and thermodynamic 613 614 calculations. Acta Materialia, 2007. 55(13): 4325-4337. DOI: p. 10.1016/j.actamat.2007.04.005. 615

- 618 53. P. Kofstad, Thermogravimetric studies of the defect structure of rutile (TiO₂). Journal of Physics
 619 and Chemistry of Solids, 1962. 23(11): p. 1579-1586. DOI: 10.1016/0022-3697(62)90240-8.
- 55. P. Kofstad, P. B. Anderson, O. J. Krudtaa, Oxidation of titanium in the temperature range 800–
 1200°C. Journal of the Less Common Metals, 1961. 3(2): p. 89-97. DOI: 10.1016/00225088(61)90001-7.
- 62556.A. M. Chaze, C. Coddet, Influence of silicon on the oxidation of titanium between 550 and626700°C. Oxidation of metals, 1987. 27(1-2): p. 1-20. DOI: 10.1007/BF00656726.
- 627 57. M. Yoshihara, K. Miura, Effects of Nb addition on oxidation behavior of TiAl. Intermetallics,
 628 1995. 3(5): p. 357-363. DOI: 10.1016/0966-9795(95)94254-C.
- 58. Z. Alam, D. K. Das, Effect of cracking in diffusion aluminide coatings on their cyclic oxidation
 performance on Ti-based IMI-834 alloy. Corrosion Science, 2009. 51(6): p. 1405-1412. DOI:
 10.1016/j.corsci.2009.03.027.
- 632 59. A. Ashrafizadeh, F. Ashrafizadeh, Structural features and corrosion analysis of thermally
 633 oxidized titanium. Journal of Alloys and Compounds, 2009. 480(2): p. 849-852. DOI:
 634 10.1016/j.jallcom.2009.02.079.
- 63560.J. Stringer, Some observations on the kinetics of oxidation of titanium at high temperatures.636Journal of the Less Common Metals, 1964. 6(3): p. 207-213. DOI: 10.1016/0022-6375088(64)90100-6.
- 638 61. P. Hidnert, Thermal expansion of titanium. J. Res. Natl. Bur. Stand, 1943. 30(1934): p. 101 639 105.
- 640 62. R. K. Kirby, Thermal expansion of rutile from 100 to 700 K. Journal of Research of the National
 641 Bureau of Standards. Section A, Physics and Chemistry, 1967. 71(5): p. 363-369. DOI:
 642 10.6028/jres.071A.041.
- 643 63. I. Blech, U. Cohen, Effects of humidity on stress in thin silicon dioxide films. Journal of applied
 644 physics, 1982. 53(6): p. 4202-4207. DOI: 10.1063/1.331244.
- 645 64. P. F. Dennis, R. Freer, Oxygen self-diffusion in rutile under hydrothermal conditions. Journal
 646 of Materials Science, 1993. 28(17): p. 4804-4810. DOI: 10.1007/BF00414275.

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