# Unravelling the Crystallization Process in Solution-Derived $YBa_2Cu_3O_{7-\delta}$ Nanocomposite Films with Preformed $ZrO_2$ Nanocrystals via Definitive Screening Design

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**ABSTRACT:** A low-cost chemical solution deposition technique was employed to prepare  $YBa_2Cu_3O_{7.6}$  (YBCO) nanocomposite films starting from a colloidal solution containing preformed ZrO<sub>2</sub> nanocrystals. As previous publications revealed, an increase in the amount of nanocrystals results in a progressive deterioration of the film properties. The parameters that control this process and their interplay are still unknown in detail. Using definitive screening design (DSD), a design-of-experiments approach, allowed determining which of the multiple growth parameters play a key role for improving the superconducting properties of YBCO nanocomposite films even with a large concentration of nanocrystals. In order to show the potential of DSD, it has been applied for the optimization of two different properties: the critical temperature  $T_c$  and the full width at half-maximum of the (005) YBCO reflection. This work shows that DSD is a powerful and efficient method that allows optimizing certain processes with a minimal number of experiments.



 $R^{EBa_2Cu_3O_{7-\delta}}$  (REBCO, RE = rare earth) films are the functional materials of coated conductors (CCs), a combination of a flexible metallic substrate and a superconducting functional layer as well as several buffer and protection layers. CCs have the potential to offer a highly efficient and environmentally friendly extension of tomorrow's energy conversion, transport, and usage.<sup>1</sup> Therefore, the reliable and low-cost large-scale fabrication of REBCO films is essential for enabling the construction of superconductorbased electric power applications such as motors and generators with working conditions at 77 K and low magnetic field range (<1 T).<sup>2</sup> Nowadays, there are major obstacles for the successful implementation and distribution of CCs throughout the energy market. First, pristine REBCO films typically exhibit a strong reduction of critical current densities  $(J_c)$  in applied magnetic fields  $B = \mu_0 H$  caused by vortex motion. Second, the highly anisotropic nature of the REBCO crystal structure with currents mainly flowing within the aboriented  $CuO_2$  planes as well as the  $J_c$ -limiting nature of largeangle grain boundaries<sup>3</sup> (due to the extremely short coherence lengths) necessitates near-perfect biaxial textures for large current carrying capabilities.<sup>4</sup> In order to overcome these difficulties, it becomes crucial to immobilize (to pin) the vortices and thus to enhance  $J_c$  for all magnetic fields and orientations as well as to achieve a perfect biaxial texture to ensure a continuity of the CuO2 planes and to avoid largeangle grain boundaries.

In recent decades, the incorporation of nanosized defects to the REBCO matrix has proved to be an effective approach to achieve the immobilization of vortices.<sup>5–7</sup> Many fabrication methods of REBCO and in particular of YBa<sub>2</sub>Cu<sub>3</sub>O<sub>7- $\delta$ </sub> (YBCO) nanocomposite films have been reported.<sup>8–11</sup> Among them, chemical solution deposition (CSD) has the potential to be easily scalable with reduced cost compared to vacuum deposition methods. In this work, the cost-effective CSD technique starting from colloidalYBCO solutions was used.<sup>12</sup> This so-called *ex-situ* approach (i.e., preformed nanocrystals in YBCO solutions) faces some challenges like the limitation of the nanocrystal amount that can be introduced without decreasing the superconducting properties.<sup>13</sup> This phenomenon has been related to Ba<sup>2+</sup> consumption of the metal oxide nanocrystals (e.g., HfO<sub>2</sub>, ZrO<sub>2</sub>, and CeO<sub>2</sub>) during the YBCO growth, leading to a poorer YBCO texture.<sup>14,15</sup>

Although the optimization of the growth of these nanocomposite films has been investigated in depth in the last years, all related reports reveal great effort and difficulties to achieve better performance in this type of films. Investigations at the lab scale via common experiments where one processing parameter at the time is studied, imply a large number of experiments due to the multitude of potentially important parameters. In order to optimize the resources and to decrease the effort (both in time and money) spent in these investigations, combinatorial approaches have emerged as an interesting option that allow to accelerate the research and development process through parallel and rapid sequential experimentation.<sup>16</sup> The continuous composition spread (CCS) approach has already been applied for film deposition of oxide materials via pulsed laser deposition and sputtering.<sup>17-19</sup> The CCS approach has the advantage of being able to grow thinfilms with several dozens of compositions at a time compared with conventional solid-state synthesis. However, this approach is not possible for CSD YBCO nanocomposites due to the complexity of CSD.<sup>12</sup> Definitive screening design (DSD), which is applied to CSD-based YBCO nanocomposites for the first time, is a powerful screening method to estimate the model coefficients of the main effects, two-factor interactions, and quadratic effects for k factors with only a minimal number of experiments.<sup>20-22</sup> It has been used previously to study the growth of pristine REBCO films by Hayasaka et al.<sup>23</sup> for the case of ErBCO films.

The objective of this work was to use DSD to investigate and determine the synthesis parameters that have a significant impact on the final properties, which in the end will lead to the optimization of YBCO ex-situ nanocomposite properties without having to perform an unreasonably high number of experiments. In addition, the DSD approach helps to clarify the effect and interplay of the synthesis parameters that control the microstructure and/or superconducting properties of CSD-YBCO nanocomposite films and therefore to obtain highquality films with a higher amount of preformed metal oxide nanocrystals. It is very important to consider the way in which DSD works. DSD usually focuses on the optimization of a single property without considering others. Therefore, the obtained optimized parameters for one property could be very different from the ones obtained for a different property and can even show opposing trends. This means that one should select the most adequate property for a certain application or purpose because the rest of the properties may not follow the same trend and can even have deteriorated.

In our case, in order to improve the properties of the films, the first requirement is to design a suitable growth process that allows obtaining epitaxial, c-axis oriented films. There are different strategies to improve the growth process to achieve that process: (1) adding silver to stabilize the *c*-axis nuclei,<sup>24</sup> (2) adjusting the stoichiometric ratio of Y:Ba:Cu in the YBCO precursor solution,<sup>25,26</sup> (3) introducing a pristine YBCO seed layer to ensure *c*-axis growth of the YBCO nanocomposite,<sup>13</sup> and (4) modifying the crystallization process. Applying DSD for these four points, we achieved YBCO nanocomposite films with larger amounts of ZrO2 nanocrystal than had been possible before (up to 12.5 mol %) without damaging yet even improving the YBCO microstructure and the superconducting properties of the films. Therefore, this work shows that the derived DSD model is able to optimize the growth conditions regarding a certain property. The introduction of DSD in CSD can be a reference for further projects in the fabrication of functional thin films in several material classes, including multiferroics,<sup>27</sup> ferromagnetics,<sup>27</sup> ferroelectrics,<sup>28</sup> and piezoelectrics.<sup>29</sup>

#### **EXPERIMENTAL SECTION**

ZrO<sub>2</sub> Nanocrystals. These nanocrystals were synthesized and purified according to De Keukeleere et al.<sup>30</sup> Zr(OiPr)<sub>4</sub>·iPrOH (1.55 g, 4 mmol), ZrCl<sub>4</sub> (1.166 g, 5 mmol), and 20 g tri-noctylphosphine oxide were mixed, and the temperature of this mixture was raised to 340 °C. The synthesis was carried out in an argon atmosphere and under vigorous stirring for 2 h. After the heating-up synthesis, the nanocrystals were purified by the addition of acetone (1:4 in volume) to the reaction mixture, which resulted in a white precipitate after centrifugation at a relative centrifugal force of 4508 g for 2 min. The precipitate was redispersed in methanol via the addition of a phosphonatecontaining copolymer, which lead to a transparent and stable  $ZrO_2$  nanosuspension (concentration of 0.3 M) with a solvodynamic diameter of 5.9  $\pm$  1.9 nm, as confirmed via dynamic light scattering measurements described in the literature.<sup>31</sup>

Chemical Solution Deposition of YBCO Nanocomposite Films. The YBCO precursor solution was prepared by dissolving  $Y(C_3H_5O_2)_3$ , Ba(CF<sub>3</sub>CO<sub>2</sub>)<sub>2</sub>, and Cu(C<sub>3</sub>H<sub>5</sub>O<sub>2</sub>)<sub>2</sub> in methanol with a Y:Ba:Cu stoichiometric ratio of 1:2:3. The ZrO<sub>2</sub> nanosuspension was added to the YBCO precursor solution with the desired molar percentage of  $ZrO_2$  nanocrystals (0, 2.5, 7.5, or 12.5 mol %) and adjusted to the total YBCO concentration (sum of salts) of 1.08 mol  $L^{-1}$ . The (100)oriented LaAlO3 single crystal substrates were supplied by a single manufacturer (CrysTec GmbH) to ensure their quality varies only insignificantly from substrate to substrate. These LaAlO<sub>3</sub> substrates were chemically and thermally treated in order to remove impurities and to reconstruct the surface termination as described in the literature.<sup>32</sup> Furthermore, they were cleaned with 2-propanol and heated to 400 °C to improve their wettability. First, an interfacial seed layer was prepared by depositing a more diluted pristine YBCO solution  $(0.24 \text{ mol } L^{-1})$  on the LaAlO<sub>3</sub> substrates by spin-coating (2000 rpm for 1 min) and pyrolyzing it before the deposition of the nanocomposite layer. The final thickness of this seed layer after all heat treatments was around 45 nm. Second, a standard YBCO thin film processing<sup>33</sup> was used: the YBCO solution was deposited by spin-coating (2000 rpm for 1 min) on LaAlO<sub>3</sub> substrates with pyrolyzed seed layer and subsequently dried at 65 °C on a hot plate in ambient atmosphere for 5 min. The dried films were pyrolyzed under humidified O<sub>2</sub> atmosphere with the heating ramps of 3 K  $min^{-1}$  from 25 to 195 °C, 0.1 K  $min^{-1}$  to 240 °C, and 5 K min<sup>-1</sup> to a final temperature of 400 °C. The pyrolyzed films were subsequently crystallized by heating them to 815 °C with a rate of 5.5 °C min<sup>-1</sup> and keeping this temperature for 45 min in a humid atmosphere of 200 ppm of  $O_2$  in  $N_2$ . The inlet gas was bubbled through a water bath with a temperature of 23 °C and a gas flow of 3 cm s<sup>-1</sup>. After the crystallization, the films were oxygenated in dry  $O_2$  flow (1 atm) at 450 °C for 2 h in order to convert the tetragonal YBa2Cu3O6 phase into the superconducting, orthorhombic YBa<sub>2</sub>Cu<sub>3</sub>O<sub>7</sub> phase. AgCF<sub>3</sub>CO<sub>2</sub> (Ag-TFA) in a molar percentage of 3 or 6 mol % was added in some pristine seed layers as indicated in Tables 1 and 2, cf ref 24.

Microstructural and Electrical Characterization. Microstructure and phase purity of the films were investigated by X-ray diffraction (XRD) using a Bruker D8 diffractometer with Cu K $\alpha$  radiation in Bragg–Brentano geometry. Self-field  $J_c$  at 77 K,  $J_c^{\rm sf}$ , and critical temperature  $T_c$  were measured inductively with Table 1. Seven Factors and Corresponding Factor Levels for the DSD Approach: the Concentration of  $ZrO_2$ Nanocrystals ( $\chi_1$ ), the Mole Percentage of Ag-TFA in the YBCO Seed Layer ( $\chi_2$ ), the Oxygen Partial Pressure during the Crystallization ( $\chi_3$ ), The Gas flow during the Crystallization ( $\chi_4$ ), the Crystallization Temperature ( $\chi_5$ ), and the Addition of Extra Ba<sup>2+</sup> ( $\chi_6$ ) and Extra Y<sup>3+</sup> ( $\chi_7$ )

factor	minimum	center	maximum
$\chi_1$ , ZrO <sub>2</sub> (mol %)	2.5	7.5	12.5
χ <sub>2</sub> , Ag-TFA (mol %)	0	3	6
χ <sub>3</sub> , O <sub>2</sub> (ppm)	100	300	500
$\chi_4$ , gas flow (cm s <sup>-1</sup> )	1	3	5
$\chi_5$ , $T_{\rm crys}$ (°C)	790	815	840
$\chi_{6}$ extra Ba <sup>2+</sup> (mol)	0	0.1	0.2
χ <sub>7</sub> , extra Y <sup>3+</sup> (mol)	0	0.15	0.30

a Cryoscan (*THEVA*, 50  $\mu$ V criterion) and with a mutualinductance method, respectively.  $T_c$  was defined as the value at 50% transition and the transition width as difference between the 10% and 90% values. Critical transport currents were measured in a 14-T Quantum Design Physical Property Measurement System in maximum Lorentz force configuration at 77 K with an electrical field criterion of 1  $\mu$ V cm<sup>-1</sup> on bridges of 800  $\mu$ m length and 50  $\mu$ m width prepared by wet chemical etching.

DSD Experiments. In order to identify the governing synthesis parameters ("factors" in DSD) for improving the superconducting properties of YBCO with higher content of nanocrystals, a DSD approach was introduced to monitor the so-called "responses" (Y), i.e., the resulting material properties, here  $T_c$  and the full width at half-maximum (fwhm) of the YBCO (005) reflections ( $2\theta \sim 38.5^{\circ}$ ). Seven factors ( $\chi$ ) had been identified as potentially affecting  $T_c$  and fwhm of YBCO

(005): the concentration of  $ZrO_2$  nanocrystals ( $\chi_1$ ), the mole percentage of Ag-TFA in the YBCO seed layer ( $\chi_2$ ), the oxygen partial pressure during the crystallization  $(\chi_3)$ , the gas flow during the crystallization ( $\chi_4$ ), and the crystallization temperature ( $\chi_5$ ) as well as excess Ba<sup>2+</sup>,  $\beta$  ( $\chi_6$ ), and excess Y<sup>3+</sup>,  $\alpha$  ( $\chi_7$ ), in the formula unit  $Y_{1+\alpha}Ba_{2+\beta}Cu_3O_7\delta$ . The concentration of the YBCO precursor solution, LaAlO<sub>3</sub> substrate, deposition and pyrolysis procedure were kept unchanged. DSD are constructed using conference matrices, which only work for an even number of factors k. When k is odd, a  $(k + 1) \times (k + 1)$ 1) conference matrix is used, of which the last column (dummy factor k + 1) is deleted.<sup>20</sup> With a center run added, a seven-factor (k = 7) design requires a minimum set of 2k + 3 =17 "trainings", i.e., single experiments, to identify the factors causing a significant nonlinear effect. The general structure of the design matrix consists of k foldover pairs with a center value (marked with gray in Table 2) in each column, two extra runs, and a center run. Adding the center run in the last row of the design matrix enables the model to include an intercept and all main and quadratic effects. Extra runs are constructed using dummy factors in the design matrix, improving its ability to identify active second-order effects.<sup>21</sup> DSD estimates main effects, two-factor interaction effects, and quadratic effects. An interaction effect is the simultaneous effect of two independent variables on at least one dependent variable, in which their joint effect is significantly greater than the sum of the parts.<sup>34</sup> The quadratic effects describe an optimum, which means that the "optimum" factor levels are not at the boundaries of the experimental region, but somewhere in between.<sup>22</sup>

The parameter values (minimum, center, and maximum) shown in Table 1 had been chosen based on previous work<sup>35</sup> and literature study. In preliminary experiments under similar conditions, the responses for pristine and 5 mol % ZrO<sub>2</sub> added

Table 2. Training Sets of Definitive Screening Design with Seven Factors: the Concentration of ZrO<sub>2</sub> Nanocrystals ( $\chi_1$ ), the Mole Percentage of Ag-TFA in the YBCO Seed Layer ( $\chi_2$ ), the Oxygen Partial Pressure during the Crystallization ( $\chi_3$ ), the Gas Flow during the Crystallization ( $\chi_4$ ), the Crystallization Temperature ( $\chi_5$ ), the Addition of Extra Ba<sup>2+</sup> ( $\chi_6$ ) and extra Y<sup>3+</sup> ( $\chi_7$ ), and the Obtained Critical Temperature ( $T_c$ ), Critical Current Densities ( $J_c$ ), and FWHM of YBCO (005) as Responses<sup>a</sup>

	parameters					responses					
	$\begin{array}{c} \chi_1, \operatorname{ZrO}_2\\ (\operatorname{mol}\%) \end{array}$	χ <sub>2</sub> , Ag-TFA (mol %)	χ <sub>3</sub> , O <sub>2</sub> (ppm)	$\chi_4$ , gas flow (cm s <sup>-1</sup> )	$\chi_{5}, T_{\text{crys}}$ (°C)	$\chi_{6}$ extra Ba <sup>2+</sup> (mol)	χ <sub>7</sub> , extra Y <sup>3+</sup> (mol)	$T_{\rm c}$ (K)	Δ <i>T</i> (K)	$J_{\rm c}(77 \text{ K})$ (MA cm <sup>-2</sup> )	fwhm YBCO (005)
T1	7.5	6	500	5	840	0.2	0.3	90.95	1.60	1.29	0.176(5)
T2	7.5	0	100	1	790	0	0	90.80	1.20	2.41	0.194(4)
Т3	12.5	3	500	5	790	0.2	0	91.75	0.60	2.22	0.195(2)
T4	2.5	3	100	1	840	0	0.3	_	_	_	0.299(2)
T5	12.5	0	300	5	840	0	0.3	90.90	0.80	3.21	0.164(1)
Т6	2.5	6	300	1	790	0.2	0	92.55	0.85	3.67	0.162(1)
T7	12.5	0	100	3	840	0.2	0	83.40	5.30	-	0.259(5)
T8	2.5	6	500	3	790	0	0.3	91.15	1.90	2.10	0.177(2)
Т9	12.5	6	100	1	815	0.2	0.3	88.25	3.35	0.60	0.219(1)
T10	2.5	0	500	5	815	0	0	88.40	3.50	0.84	0.192(5)
T11	12.5	0	500	1	790	0.1	0.3	90.30	3.90	1.34	0.187(2)
T12	2.5	6	100	5	840	0.1	0	-	_	-	0.274(3)
T13	12.5	6	100	5	790	0	0.15	88.00	2.45	0.99	0.245(1)
T14	2.5	0	500	1	840	0.2	0.15	91.75	0.55	3.25	0.159(2)
T15	12.5	6	500	1	840	0	0	93.15	1.20	3.99	0.176(3)
T16	2.5	0	100	5	790	0.2	0.3	82.10	4.80	-	0.240(1)
T17	7.5	3	300	3	815	0.1	0.15	90.30	0.90	2.96	0.165(1)

<sup>*a*</sup> The amount of extra  $Ba^{2+}$ ,  $\beta$ , and  $Y^{3+}$ ,  $\alpha$ , relates to the formula  $Y_{1+\alpha}Ba_{2+\beta}Cu_3O_{7-\delta}$ . Numbers in parentheses show the error of fwhm in the last digit. Some of the best values of  $T_{c}$ ,  $\Delta T$ ,  $J_c$  and fwhm are highlighted in bold, illustrating that high  $J_c$  values often concur with high  $T_c$  values and/or low fwhm values. Center values in the design matrix are marked with italics. nanocomposite YBCO films show similar outcomes for fwhm,  $J_{c^{\prime}}$  and  $T_{c}$  with insignificant variances. Therefore, the extra center runs to estimate the population variance of responses as described by Hayasaka et al.<sup>23</sup> were not included in the training set. For the analysis of the responses, the statistical software package JMP was used. The *p*-value (see Table 3) is

### Table 3. Coefficients of the Significant Main and Interaction Effects for the $T_c$ Model with the Respective *p*-Values

factor	coefficient	<i>p</i> -values
χ <sub>1</sub> , ZrO <sub>2</sub> (mol %)	0.388	0.48406
χ <sub>3</sub> , O <sub>2</sub> (ppm)	2.185	0.00265
$\chi_4$ , gas flow (cm/s)	-1.573	0.01489
χ <sub>6</sub> , extra Ba <sup>2+</sup> (eq)	-0.890	0.04365
$\chi_1$ , ZrO <sub>2</sub> (mol %) and $\chi_4$ , gas flow (cm/s)	1.681	0.01687

the tail probability in the standard *t*-distribution curve. It is computed by integrating the standard *t*-distribution function from *t* to infinity.<sup>20</sup> A *p*-value <0.05 indicates by definition a significant effect. The model selection is done by minimizing the corrected Akaike Information Criterion (AICc).<sup>36</sup> The AICc finds the optimum in the trade-off between the goodness of fit and the model's simplicity. This way, the risk of either over- or underfitting is minimized.

In order to show the usefulness of the DSD approach, the models for the dependencies of two different properties were obtained and compared.  $T_c$  and the fwhm of the (005) YBCO reflection in  $\theta - 2\theta$  scans were selected as target properties due to their simplicity and because they are fast and easy to obtain and at the same time very useful for our purpose of demonstrating on the usefulness of DSD. Both properties are of vital importance for optimizing the film properties. On the one hand,  $T_c$  yields information on the compositional homogeneity of the films and is related with the oxygen content of the films. Even though  $J_c$  (especially in applied magnetic fields) and  $T_c$  are not strictly correlated, an adequately high  $T_c$  value is a necessary although not sufficient condition for high current carrying capabilities. On the other hand, the fwhm of the (005) YBCO reflection is related with the crystallinity of the films in such a way that the lower the fwhm (i.e., the sharper the reflection), the larger is the crystallinity of the YBCO matrix in the nanocomposite films. This again has a positive effect on the stiffness of the superconducting phase, i.e., the Cooper pair density and therefore the pinning potential as well as  $J_{c}$ , especially under self-field conditions. Both properties are therefore very relevant and interesting to optimize. The results of the 17 experiments of the training set (samples "T") are shown in Table 2.

$$T_{c} = 89.296 + 0.388 \left( \frac{\chi_{1} - 7.5}{5} \right) + 2.185 \left( \frac{\chi_{3} - 300}{200} \right)$$
$$- 1.573 \left( \frac{\chi_{4} - 3}{2} \right) - 0.890 \left( \frac{\chi_{6} - 0.1}{0.1} \right)$$
$$+ 1.681 \left( \frac{\chi_{1} - 7.5}{5} \right) \left( \frac{\chi_{4} - 3}{2} \right)$$
(1)

The obtained  $T_c$  data set, Table 2, was analyzed regarding the significant effects (main-interaction-quadratic), and the optimum model according to the aforementioned AICc minimization is shown in Table 3 and eq 1. Two experiments showed no  $T_c$  values above 77 K; nevertheless, they yielded important information on the possible growth conditions for superconducting YBCO nanocomposite films. Due to the very long duration of the oxygenation step (2 h at 450 °C in 1 atm  $O_2$  flow) of these rather thin films (~350 nm),<sup>37</sup> this step is expected to allow for a complete oxygenation of the superconducting matrix. Hence,  $T_c$  must be determined by other parameters, i.e., the crystallization process. These films were grown with a combination of a low oxygen partial pressure of 100 ppm with a high crystallization temperature of 840 °C, which lies below the stability line of the YBCO phase in the oxygen partial pressure vs temperature diagram as described in the literature.<sup>38,39</sup> Those values clearly are not an option for producing high-quality superconducting YBCO nanocomposite films. These data had to be excluded when compiling the data in the model. The synthesis parameters that led to such low T<sub>c</sub> values are far away from optimum growth parameters of YBCO. Therefore, these low  $T_c$  values are related with a bad crystalline quality of the films due to a wrong growth process and, again, not to the oxygenation process.

Three main factors were identified as having a significant influence (p < 0.05) on the  $T_c$  response in the chosen parameter limits: the oxygen partial pressure during the crystallization  $(\chi_3)$ , the gas flow during the crystallization  $(\chi_4)$ , and the excess Ba<sup>2+</sup>  $(\chi_6)$ . Furthermore, one two-factor interaction effect, namely between the concentration of ZrO<sub>2</sub> nanocrystals  $(\chi_1)$  and the gas flow during the crystallization  $(\chi_4)$ , was observed. Their correlation indicates that the gas flow during the crystallization should be increased when the concentration of  ${\rm ZrO}_2$  nanocrystals is increased, which indicates kinetic reasons for the deterioration of ex-situ nanocomposites grown under conditions optimized for pristine films.<sup>15</sup> The concentration of  $ZrO_2$  nanocrystals ( $\chi_1$ ), the mole percentage of Ag-TFA in the YBCO seed layer ( $\chi_2$ ), the crystallization temperature ( $\chi_5$ ), and extra Y<sup>3+</sup> ( $\chi_7$ ) showed no significant influence on  $T_c$  (p > 0.05). Surprisingly,  $T_c$  does not significantly depend on the crystallization temperature, which seems to contradict multiple publications;<sup>24,37</sup> however, it does support the results of ref 40. Our conclusion is that, of course,  $T_c$  will depend on the crystallization temperature, but not in the studied range, between 790 and 840 °C, where other parameters play a more important role.  $T_c$  is expected to suffer a severe deterioration if this temperature is decreased far below 790 °C, where atomic ordering is slowed, or increased far above 840 °C, where secondary phase formation becomes considerable leading to a nonuniform cation depletion of the YBCO phase. As long as the phase is stable and well ordered, though,  $T_{\rm c}$  is mainly determined by the following oxygenation process.  $T_c$  values of the YBCO films in this work, however, are not subject to the severe variation caused by the crystallization temperature since the studied temperature range is rather narrow. The coefficient for the excess  $Ba^{2+}(\chi_6)$  is negative, which means  $T_c$  decreases with increasing Ba<sup>2+</sup> addition. Since this is expected from literature on the effects of Ba offstoichiometry, it supports the validity of the presented  $T_c$ model: Despite the nominal formula  $Y_{1+\alpha}Ba_{2+\beta}Cu_3O_{7\ \delta}$  with only positive values of  $\beta$ , the Ba stoichiometry of the matrix in our final YBCO films ranges from Ba-deficient, caused by Baconsumption through the ZrO<sub>2</sub> nanocrystals,<sup>15</sup> to Ba-rich due to the Ba addition ( $\chi_6$ ). Therefore, it ranges from  $Y_{1+\alpha}Ba_{1.88}Cu_3O_{7\,\delta}$  (for  $\chi_1 = 12.5$  and  $\chi_6 = 0$  and assuming a complete conversion of  $ZrO_2$  to  $BaZrO_3$  nanocrystals) to  $Y_{1+\alpha}Ba_{2.18}Cu_3O_7 \delta$  (for  $\chi_1 = 2.5$  and  $\chi_6 = 0.2$ ) and corresponds

to a decrease of  $T_c$  of roughly 2 K based on our  $T_c$  model. This coincides with the observations in the literature.<sup>41</sup> As mentioned in further literature reports,<sup>42–44</sup> a YBCO precursor solution with a slight barium deficiency can lead to a higher  $J_c$  and still maintain good  $T_c$ . The findings in these publications and in our  $T_c$  model are consistent with our previous work,<sup>15</sup> where the Ba<sup>2+</sup> deficiency caused by Ba<sup>2+</sup> consumption of ZrO<sub>2</sub> nanocrystals resulted in a delay rather than in a degradation of the YBCO nucleation and growth. In Figure 1, the



**Figure 1.** Measured  $T_c$  versus the predicted  $T_c$  according to the model, eq 1, for test samples T1–T17, Table 2, control samples C1–C4, and a "standard" sample S, Table 5. Samples T4 and T12 were omitted. Red full line: linear regression y = mx + n with two fitting parameters slope  $m = 0.92 \pm 0.14$  and intercept  $n = 8 \pm 12$  K and  $R^2$  of 0.78 and the RMSE of 2.07 K, including a 95% confidence band (green dashed line) and a 95% prediction band (blue dotted line). The fit function equals identity within error bars.

experimental  $T_c$  is plotted against the  $T_c$  values predicted by the model. The regression analysis with a linear fit shows a coefficient of determination ( $R^2$ ) of 0.78 and a root mean square error (RMSE) of 2.07 K and indicates a good compliance between theoretical and experimental values while overfitting is avoided.

The analysis of the (005) fwhm values led to the significant effects and model presented below in Table 4 and eq 2. Figure

## Table 4. Coefficients of the Significant Main, Interaction, and Quadratic Effects for the Model with Their Respective *p*-Values for FWHM YBCO (005) Values

factor	coefficient	<i>p</i> -values
χ <sub>3</sub> , O <sub>2</sub> (ppm)	-0.0335	0.00002
$\chi_5, T_{\rm crys} (^{\circ}{\rm C})$	0.0077	0.14060
$\chi_{3}$ , O <sub>2</sub> (ppm) and $\chi_{5}$ , $T_{crys}$ (°C)	-0.0168	0.00746
$\chi_3$ , O <sub>2</sub> (ppm) and $\chi_3$ , O <sub>2</sub> (ppm)	0.0502	0.00096

2A displays a plot of the measured fwhm vs the predicted fwhm according to the fwhm model, eq 2, which has an  $R^2$ value of 0.87 and an RMSE of 0.0002°. This indicates a better predictability of the fwhm compared to  $T_c$  and  $J_c$  which is most likely at least partly due to the missing data points in the two latter cases. Similar to  $T_c$  the effect of the oxygen partial pressure ( $\chi_3$ ) is significant, inferred by the low *p*-value. The oxygen partial pressure ( $\chi_3$ ) has even a quadratic effect on the fwhm, and thus the optimized parameter is found around the factor level "0", i.e., near 300 ppm. The other parameters with significant impact in the previous  $T_c$  case, on the other hand, are not significant here. In the fwhm model, the crystallization temperature  $(\gamma_5)$  is a factor of interest because of the significant interaction effect with the oxygen partial pressure  $(\chi_3)$ , Figure 2B. This is in accordance with the literature since the increase of crystallization temperature in the growth of YBCO is related with an improvement of the texture quality,<sup>1,45</sup> and unlike the previous case of  $T_{cr}$  the change between 790 and 840 °C makes a clear difference in the crystallinity of the films. As described in ref 24, the addition of Ag can help to enhance the stability of *c*-axis nucleation at the film/substrate interface during the crystallization process, ensuring the growth of a highly epitaxial crystalline YBCO film. However, both fwhm and the  $T_{\rm c}$  model reveal that the presence of Ag in the seed layer  $(\chi_2)$  shows no significant importance.

FWHM = 
$$0.1634 - 0.0335 \left( \frac{\chi_3 - 300}{200} \right) + 0.0502$$
  
 $\left( \frac{\chi_3 - 300}{200} \right)^2 + 0.0077 \left( \frac{\chi_5 - 820}{30} \right)$   
 $- 0.0168 \left( \frac{\chi_5 - 820}{30} \right) \left( \frac{\chi_3 - 300}{200} \right)$  (2)

The two models discussed above are clearly distinctly different. Whereas the fwhm is only determined by the two parameters,  $O_2$  pressure and  $T_{crys}$ ,  $T_c$  needs to also take care of the gas flow, extra Ba<sup>2+</sup>, and the amount of ZrO<sub>2</sub> besides the  $O_2$  pressure, whereas the influence of  $T_{crys}$  is insignificant there. It should be noted that DSD, as applied here, focuses on the improvement of an individual property without necessarily considering others. This means that if one property is being optimized, it may happen—and as shown does—that others deteriorate. However, that is the nature of the DSD approach and material chemistry in general.

Presumably, also other important film characterizations, such as  $J_c(sf, 77 \text{ K})$ , will depend on the oxygen partial pressure as do both  $T_c$  and the fwhm as stated by the low *p*-values of the main effect of  $\chi_3$  in both models as well as the quadratic effect in the fwhm model. Other properties, e.g., related to pinning, may show entirely different correlations, though, and even be independent of O2 in the gas flow. We have shown two different models for the two investigated properties, showing how important it is to choose the right property for the optimization, because the resulting parameters will be unique for this particular property. In order to prove that DSD provides reliable models, we have selected the  $T_{\rm c}$  model to conduct four control experiments (C1–C4 in Table 5) of nanocomposite films containing 12.5 mol %. ZrO<sub>2</sub> nanocrystals. This amount of ZrO<sub>2</sub> nanocrystals was chosen because growing a crystalline YBCO film with such a high amount of preformed ZrO<sub>2</sub> nanocrystals is a challenge. The gas flow ( $\chi_4$ ) and the stoichiometric ratio of Y:Ba:Cu ( $\chi_6$ ,  $\chi_7$ ) were set to 1 cm  $s^{-1}$  and 1:2:3, while the addition of Ag in the seed layer  $(\chi_2)$  was avoided due to its low significance for  $T_c$ . A Monte Carlo simulation for the  $T_c$  model was conducted via JMP prediction profiler to determine the operating conditions necessary to grow such a YBCO nanocomposite with optimum  $T_{\rm c}$ . An oxygen partial pressure of 500–600 ppm was chosen via prediction profiler in combination with the crystallization



**Figure 2.** (A) Measured fwhm of (005) YBCO vs the predicted fwhm of (005) YBCO according to the model, eq 2, for test samples T1–T17, Table 2. Red full line: linear regression y = mx + n with two fitting parameters slope  $m = 1.07 \pm 0.10$  and intercept  $n = 0.01 \pm 0.02$ , an  $R^2$  of 0.87, and the RMSE of 0.0002°, including 95% confidence band (green dashed line) and 95% prediction band (blue dotted line). The fit function equals identity within error bars. (B) 3D plot showing the behavior of fwhm of (005) YBCO over  $\chi_3$  ( $p_{O_2}$ ) and  $\chi_5$  ( $T_{crys}$ ).

Table 5. Control Experiments (C1-C4) and Experiment under Standard Conditions (S) with a Y:Ba:Cu Stoichiometric Ratio of 1:2:3, 12.5 mol % ZrO<sub>2</sub> Nanocrystals, and a Pristine Seed Layer without the Addition of Ag-TFA to Validate the  $T_c$  Model

	Parameters			Responses		
sample	χ <sub>3</sub> , O <sub>2</sub> (ppm)	$\chi_4$ , gas flow (cm s <sup>-1</sup> )	$\chi_{5}, T_{crys}$ (°C)	$T_{\rm c}$ (K)	$\Delta T$ (K)	$J_{\rm c}(77 \text{ K})$ (MA cm <sup>-2</sup> )
C1	500	1	820	91.25	0.60	2.27
C2	500	1	840	92.65	0.45	3.72
C3	600	1	820	92.10	0.65	6.40
C4	600	1	840	92.05	1.35	1.30
S	200	3	815	85.90	6.80	-

temperature of 820–840 °C. The obtained  $T_c$  values, samples C1–C4 in Table 5, imply a remarkable improvement for  $T_c$  of YBCO + 12.5 mol % ZrO<sub>2</sub> with respect to such films grown under standard conditions of 200 ppm of O<sub>2</sub> with a gas flow of 1 cm s<sup>-1</sup> at the crystallization temperature of 815 °C as described in ref 15 (sample "S" in Table 5). It is noteworthy that sample C3 even surpasses the best sample in ref 15 with a much lower ZrO<sub>2</sub> concentration of 5 mol % ( $T_c = 91.6$  K,  $J_c = 5.8$  MA cm<sup>-2</sup>), for which such a DSD optimization was not done.

The pristine YBCO film and the above-mentioned YBCO+5 mol % ZrO2 film grown under standard conditions described in ref 15 are compared with sample C3. Transport  $J_{c}(B)$  of these three films (Figure 3) were measured at 77 K and normalized to the self-field  $J_c$  to show the trend of the performance of vortex pinning. Clearly, the addition of more nanocrystals leads to a smoother decay of the critical current density with increasing magnetic field and thus to a better performance. This result of increased flux pinning by increasing the amount of  $ZrO_2$  nanoparticles was only possible by optimizing  $T_c$ toward the values of the samples with lower amount of nanoparticles, which shows that the DSD approach is a very valuable tool for the optimization of superconducting nanocomposite films with a large amount of preformed ZrO<sub>2</sub> nanocrystals. With this knowledge, the next step is to build new DSD experiments to optimize the amount of nanoparticles



**Figure 3.** Comparison of the magnetic field dependence of transport  $J_c$  normalized to the self-field  $J_c$  at 77 K for YBCO films with different amounts of ZrO<sub>2</sub> nanocrystals. All samples had a comparable  $T_c$  of around 92 K.

for a certain range of temperature and magnetic field as well as to study other internal properties such as nanocomposite film thickness and the kind of the nanocrystals in the YBCO matrix.

For the first time, we employed a design of experiment method, namely the definitive screening design (DSD), to investigate the synthesis parameters that control the microstructural and superconducting properties of CSD-YBCO nanocomposite films. By performing a design of experiment with  $T_c$  and fwhm models, we showed that the main parameter for improving both YBCO crystallinity and  $T_{\rm c}$  is the oxygen partial pressure as it has the most significant influence (lowest p-value). The  $T_c$  model refines the results of our previous work where the addition of  $ZrO_2$  nanocrystals resulted in a delay of YBCO growth due to Ba2+ deficiency, which, as we concluded there, can be further optimized via tailoring the processing parameters during the crystallization. The fwhm model reveals that the oxygen partial pressure can improve the crystallinity of the YBCO matrix in the nanocomposite film. These observations are confirmed by the growth of YBCO nanocomposite films with a very high amount of ZrO<sub>2</sub> nanocrystals that previously led to poor superconducting properties. On the basis of the prediction of our DSD model, we were able to grow such films with outstanding, unexpected properties. This

work indicates that DSD is a powerful and efficient method that allows optimizing certain processes, even in large-scale experiments and fabrication, with a minimal number of experiments, saving time, material, and money and even avoiding scientific frustration. This work on design-of-experiments in material chemistry can be a reference for further optimization of the fabrication of superconducting or other functional thin films.

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#### Notes

The authors declare no competing financial interest.

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