

Drop impingement on heated hydrophobic surfaces

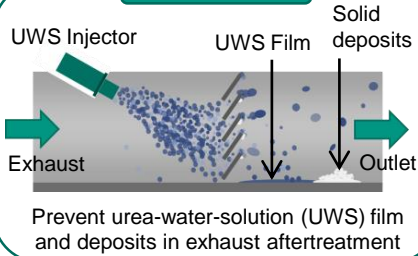
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1 - Motivation



2 - Numerical method and set-up

$$\frac{\partial C}{\partial t} + \nabla \cdot (\mathbf{u}C) = M \nabla^2 \phi$$

$$M = \chi \varepsilon^2$$

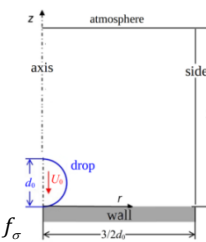
$$\phi = \frac{\lambda}{\varepsilon^2} C(C^2 - 1) - \lambda \nabla^2 C + \nabla \lambda \cdot \nabla C$$

$$\lambda = \frac{3\sqrt{2}}{4} \sigma \varepsilon$$

$$\frac{\partial T}{\partial t} + \nabla \cdot (\mathbf{u}T) = -\nabla \cdot (\alpha \nabla T)$$

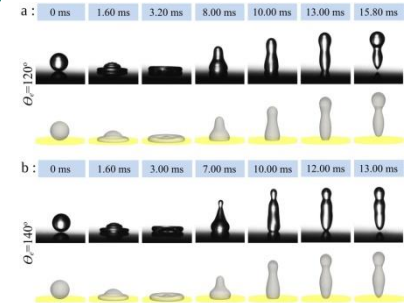
$$\alpha = \frac{k}{\rho c_p}$$

$$\frac{\partial (\rho \mathbf{u})}{\partial t} + \nabla \cdot (\rho \mathbf{u} \mathbf{u}) = -\nabla p + \rho \mathbf{g} + \nabla \cdot [\mu (\nabla \mathbf{u} + (\nabla \mathbf{u})^T)] + \mathbf{f}_\sigma$$



- Phase field method using Cahn-Hilliard Navier-Stokes eqs.
- Foam-extend-4.0
- Axisymmetric domain
- $Cn = \varepsilon/d_0 = 0.01$
- $\chi = 1 \text{ m s/kg}$
- Water droplet in air impinging on a hot hydrophobic wall

3 - Hydrodynamics



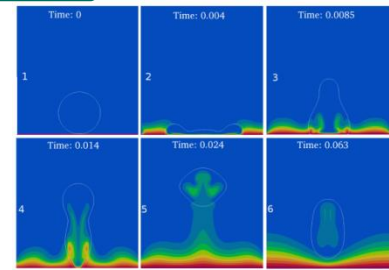
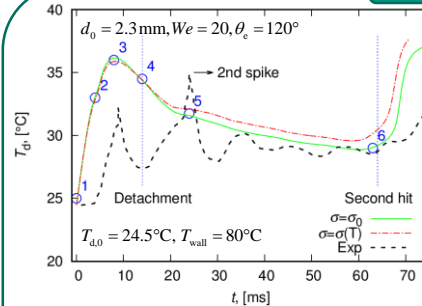
5 - Conclusions

- Weber number (We) and wettability (contact angle θ_e) mostly affect maximum spreading β_{\max} and contact time τ
- Correlations derived from a large number of simulations varying d_0 , U_0 , θ_e

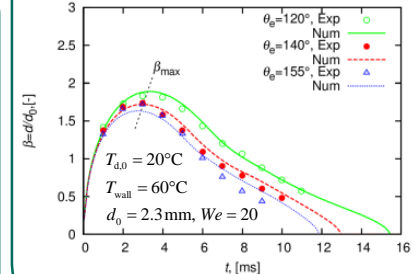
$$\beta_{\max} = \frac{d_{\text{wetted,max}}}{d_0} = \sqrt{\frac{1.872 + 0.152 \cdot We}{1 - \cos \theta_e}}$$

$$\tau = \frac{1.88}{1 - \cos \theta_e} We^{0.465}$$

4 - Heat transfer



Mean drop temperature T_d over time. 1: initial impact, 2: maximum spreading, 3: recoil (maximum mean temperature) 4: detachment, 5: bouncing, 6: before second impact.



Experiment: Guo, Maynes, Crockett and Zhao, *Int. J. Heat Mass Transfer* **137** (2019) 857-867