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## **Time-domain poroelastic full-waveform inversion of shallow seismic data: methodology and sensitivity analysis**

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## **SUMMARY**

Full-waveform inversion (FWI) is considered as a high-resolution imaging technique to recover the geophysical parameters of the elastic subsurface from the entire content of the seismic signals. However, the subsurface material properties are less well estimated with elastic constraints, especially for the near-surface structure, which usually contains fluid contents. Since Biot theory has provided a framework to describe seismic wave propagations in the poroelastic media, in this work, we propose an algorithm for the 2-D time-domain (TD) poroelastic FWI (PFWI) when the fluid-saturated poroelastic equations are applied to carve the physical mechanism in the shallow subsurface. To detect the contribution of the poroelastic parameters to shallow seismic wavefields, the scattered *P*-*SV*&*SH* wavefields corresponding to a single model parameter are derived explicitly by Born approximation and shown numerically afterward. The Fréchet kernels are also derived and exhibited in *P-SV&SH* schemes to analyse the sensitivities of the objective function to different poroelastic parameters. Furthermore, we verify the accuracy of the derivations through model parameter reconstructions. We perform a series of numerical tests on gradients with respect to different model parameters to further evaluate inter-parameter trade-offs. PFWI holds potential possibilities to directly invert fluid-related physical parameters of the shallow subsurface.

**Key words:** Permeability and porosity; Waveform inversion; Surface waves and free oscillations; Wave scattering and diffraction.

#### **1 INTRODUCTION**

The accurate estimation of the Earth's subsurface properties is a challenging task for seismic exploration. Since seismic waves carry the underground structural heterogeneities information, full-waveform inversion (FWI) has become a multiparameter reconstruction technique that can exploit the entire information contents of seismograms (Virieux & Operto [2009\)](#page-14-0). In general, the main interest in seismic detection is to extract the information of the physical material properties (e.g. lithology, porosity and fluid content) from different seismic attributes (e.g. *P*- and *S*-wave velocities) based on rock physical relations (Butler [2005\)](#page-13-0). To extend FWI into the application of seismic reservoir characterization, Queißer & Singh [\(2013\)](#page-14-1) employ the Gassmann model to relate *P*-wave velocity with CO<sub>2</sub> saturation directly in order to estimate CO<sub>2</sub> storage (Gassmann [1951\)](#page-13-1). Dupuy *et al.* [\(2016\)](#page-13-2) adopt a two-step workflow based on acoustic FWI to estimate rock-physics properties by inverting the effective medium properties. Hu *et al.* [\(2021\)](#page-13-3) attempt to link the elastic properties with different rock-physics models to recover fluid properties (e.g. porosity  $\phi$ ) through elastic FWI. However, the rock properties related to the fluid information from the fluid-filled subsurface are still poorly considered by the elastodynamic FWI. The near-surface sediments are usually unconsolidated and composed of solid and fluid components. How to exploit the fluid information directly from the seismic waveforms has still not attracted enough attention.

Over the past decades, Biot's theory (Biot [1956a,](#page-13-4) [b;](#page-13-5) Biot & Willis [1957\)](#page-13-6) has been widely used as a reliable model to govern the poroelastic response since they build a framework relating poroelastic parameters to the seismic wave properties (Zhu & McMechan [1991;](#page-14-2) Masson *et al.* [2006;](#page-13-7) Morency & Tromp [2008\)](#page-14-3). Morency *et al.* [\(2009\)](#page-14-4) present sensitivity kernels for specific parametrizations in the poroelastic model based on adjoint methods. De Barros *et al.* [\(2010\)](#page-13-8) introduce Biot's theory into frequency-domain FWI, which is limited to utilizing reflected waves. Yang *et al.* [\(2018\)](#page-14-5) discuss the radiation patterns for different parametrizations in poroelastic media and implement several synthetic reconstruction tests based upon frequency-domain poroelastic FWI (Yang & Malcolm [2020\)](#page-14-6). However, it is still an open question for time-domain (TD) FWI to directly employ Biot's theory to describe the physical mechanism of the near-surface structure.

This paper aims to introduce Biot's theory into the direct description of the shallow subsurface and make preparation for shallow-seismic TD poroelastic FWI (TD-PFWI). In Section 2, we first outline the fluid-saturated poroelastic equations and show the shallow seismic *P*-*SV*&*SH*

poroelastic wavefields numerically. In Section 3, We derive the explicit scattered wavefields of different poroelastic parameters in *P*-*SV*&*SH* patterns based on the high-frequency approximation (Wu & Aki [1985\)](#page-14-7). The scattered wavefields corresponding to different model parameters are simulated numerically to investigate the sensitivities of the model parameters. In Section 4, we use the classic least-squares error functional as the objective function and derive the Fréchet kernels with respect to different poroelastic parameters (Tarantola & Valette  $1982$ ). Besides, the Lagrangian augmented functional (Plessix [2006\)](#page-14-9) is explained to derive the adjoint poroelastic wavefields. Furthermore, we present the sensitivity kernels of different poroelastic parameters from the views of *P*-*SV*&*SH*, and implement a series of reconstruction tests on the synthetic Rayleigh/Love-wave data to justify the accuracy and feasibility of PFWI. In Section 5, we take a step to analyse the inter-parameter issues by a series of cross-comparisons on the descent directions from different gradients. Finally, we draw a brief discussion on the sensitivity analysis of the poroelastic parameters in the conclusion part. All the wavefields are solved by the fourth-order finite-difference (FD) method. Since the observed data for fluid components can not be obtained separately, the fluid adjoint source is not estimated for PFWI.

#### **2 METHODOLOGY**

#### **2.1 Fluid-saturated poroelastic equations**

Following the steps of Biot's theory (Biot [1956a,](#page-13-4) [b;](#page-13-5) Biot & Willis [1957\)](#page-13-6), the macroscopic equations of motion [\(1–](#page-1-0)[2\)](#page-1-1) can describe the saturated solid-fluid system across the seismic band of frequencies. Within the Biot's characteristic frequency, the fluid flow regime is treated as Poiseuille type, where the internal drag forces on the solid/fluid interface are negligible.

$$
\rho \dot{v}_i + \rho_f \dot{w}_i = \partial_j \sigma_{ij},\tag{1}
$$

<span id="page-1-1"></span><span id="page-1-0"></span>
$$
\rho_f \dot{v_i} + m \dot{w_i} = -\partial_i P - \frac{\eta}{\kappa_0} w_i. \tag{2}
$$

The dots above variables denote the time differentiation and Einstein notation is applied in the equations.  $v_i$  is the solid particle velocity, and  $w_i = \phi(v_i^f - v_i)$  is the Darcy filtration velocity.  $\phi$  is the effective porosity of the porous medium and  $v^f$  is the fluid velocity. The mass coupling coefficient  $m = T \rho_f / \phi$ , where the tortuosity  $T > 1$  is a dimensionless parameter concerns pore geometry (Ghanbarian *et al.* [2013\)](#page-13-9). The average density  $\rho = (1 - \phi)\rho_s + \phi \rho_f$  is comprised of the fluid density  $\rho_f$  and the solid particle density  $\rho_s$ ,  $\eta$  denotes the fluid viscosity and  $\kappa_0$  is the hydrological permeability. The stress tensor  $\sigma_{ij}$  and fluid pressure *P* are formatted by using Biot constitutive eqs [\(3\)](#page-1-2) and [\(4\)](#page-1-3)

$$
\sigma_{ij} = c_{ijkl}\epsilon_{kl} - \alpha P\delta_{ij} + s_i,\tag{3}
$$

<span id="page-1-3"></span><span id="page-1-2"></span>
$$
-\dot{P} = M(\alpha \partial_i v_i + \partial_i w_i) + s^f,\tag{4}
$$

where the Biot–Wills coefficient

$$
\alpha = 1 - \frac{K_d}{K_s},\tag{5}
$$

and the fluid storage coefficient

$$
M = \left(\frac{\phi}{K_f} + \frac{\alpha - \phi}{K_s}\right)^{-1},\tag{6}
$$

where *cijkl* is the stiffness tensor and the strain

$$
\dot{\epsilon}_{ij} = \frac{1}{2}(\partial_j v_i + \partial_i v_j). \tag{7}
$$

Here, *i*, *j*, *k*, *l*  $\in$  [1, 3],  $K_d = \lambda_d + 2/3\mu_d$ ,  $K_s$  and  $K_f$  represent the bulk modulus of the drained frame, solid and fluid, respectively.  $\lambda_d$  and  $\mu_d$  are the drained Lamé parameters. (For simplification, they are not mentioned specifically and represented by  $\lambda$  and  $\mu$  respectively in the following parts.)  $\delta_{ij}$  is the Kronecker delta. The external sources  $s_i$  and  $s^f$  can be distributed in several ways: that is, only a source in the solid phase while  $s<sup>f</sup> = 0$ ; the source is distributed between the solid and fluid phase (Carcione *et al.* [2010\)](#page-13-10). At the macroscopic scale, here, the viscosity of the fluid and attenuation mechanism are not considered during FWI under the quasi-static condition.

#### **2.2 Boundary conditions on the free surface**

At the boundary of the air-earth, the surface is free from external stress (Aki & Richards [1980\)](#page-13-11). Generally, the shallow subsurface mainly consists of unconsolidated materials. Under this previous circumstance, the porous frame is drained and the pores in the porous medium are connected with the air on the traction-free surface. In the absence of dissipation  $(\eta = 0)$ , the boundary condition on the free surface can be generalized by eqs [\(8\)](#page-1-4) and [\(9\)](#page-1-5) (Deresiewicz [1960\)](#page-13-12)

$$
\sigma_{ij} = 0, \qquad (i = \{1, 2, 3\} \equiv \{x, y, z\}, j = 3 \equiv z), \tag{8}
$$

<span id="page-1-5"></span><span id="page-1-4"></span> $P = 0.$  (9)

<span id="page-2-1"></span>

<span id="page-2-0"></span>**Figure 1.** Snapshots of the shallow-seismic poroelastic *P*-*SV*&*SH* wavefields at 90 ms: triggered by Ricker wavelet with a centre frequency of 40 Hz. The model parameters are listed in Table [1.](#page-2-0)

	Parameter	Symbol	Unit	Value
Grain	Bulk modulus	$K_{s}$	Pa	$0.7 \times 10^{10}$
	Density	$\rho_s$	$\text{kg m}^{-3}$	2650
Matrix	Bulk modulus	$K_d$	Pa	$5.1 \times 10^{8}$
	Shear modulus	$\mu$	Pa	$3.45 \times 10^{8}$
	Porosity	φ		0.2
	Tortuosity	T		$\mathcal{D}_{\mathcal{L}}$
Fluid	Bulk modulus	$K_f$	Pa	$2.2 \times 10^{9}$
	Density	$\rho_f$	$\text{kg m}^{-3}$	1000
	Viscosity	$\eta$	$N \cdot s m^{-2}$	$\Omega$
Velocity	Fast- $P$ wave	$V_{fp}$	$\rm m\,s^{-1}$	1562.23
	$Slow-P$ wave	$V_{sp}$	$\rm m\,s^{-1}$	303.17
	Shear wave	$V_{\rm s}$	$\rm m\,s^{-1}$	394.21

**Table 1.** Rock properties of the fluid-saturated porous subsurface.

Fig. [1](#page-2-1) shows the wavefields of the shallow poroelastic subsurface by solving the eqs  $(1)$ –[\(9\)](#page-1-5) with FDTD method. As the solid vertical sources on the free surface, the triggered signal is Ricker wavelet with the centre frequency of 40 Hz. Typically, there are three types of waves: the fast compressional wave, slow compressional wave and shear wave in the poroelastic wavefields. Surface waves are involved in the shallow subsurface, such as Rayleigh wave in the *P*-*SV* scheme, and Love wave exists in the *SH* case, while the subsurface is inhomogeneous. From the perspective of fluid pressure, the shear waves have vanished. The fast-*P* wave can not be observed easily in the shallow poroelastic wavefields as its rapid propagation compared to other wave types. Although the slow-*P* wave is usually attenuated since the seismic band of the triggered source is normally below the Biot relaxation frequency (Johnson *et al.* [1987\)](#page-13-13), here, we only consider a non-dissipation condition without the fluid viscosity ( $\eta = 0$ ) as the surface waves will occupy most energies in the wavefields. It is shown in Fig. [1](#page-2-1) that the velocities of the slow-*P* and *S* waves could be relatively closed under non-dissipation condition.

#### **3 SINGLE -SCATTERING PROBLEM**

The subsurface materials can be decomposed into the background medium and the perturbations. The scattered wavefields generated by small diffractors can give direct insight into the sensitivity of different parameters (Wu & Aki [1989\)](#page-14-10). Although the wave front shapes of the scattered wavefields can be described by the radiation patterns, which build a connection between the incident and scattering angles (Operto *et al.* [2013;](#page-14-11) Yang *et al.* [2018\)](#page-14-5), the radiation patterns of surface waves also depend on the source depth and frequencies, which makes difficulties on the analytical derivation of the radiation patterns concerns surface waves (Ben-Menahem & Harkrider [1964\)](#page-13-14). Alternatively, the scattered wavefields from diffractor points concerned with various model parameters are derived explicitly and numerically visualized from a certain incident angle.

From the equations of motion and constitutive law for the fluid-saturated porous media  $(1)$ – $(4)$ , the reference model  $\mathbf{m}_0$  is represented by several individual parameters  $(10)$  and the background fields  $\mathbf{u}_0$   $(12)$  consist of solid phase  $\mathbf{u}_s$  and fluid phase  $\mathbf{u}_f$ , which is excluded in the *SH* equations.

<span id="page-2-2"></span>
$$
\mathbf{m_0}^{P-SV} = \{\lambda, \mu, \rho_s, \rho_f, K_s, K_f, \phi\},\tag{10}
$$

$$
\mathbf{m}_0^{SH} = \{\mu, \rho_s, \rho_f, \phi\},\tag{11}
$$

<span id="page-3-0"></span>
$$
\mathbf{u_0}^{P-SV} = \{\mathbf{u_s}, \mathbf{u_f}\},\tag{12}
$$

$$
\mathbf{u_0}^{SH} = \left\{ \mathbf{u_s}^{SH} \right\},\tag{13}
$$

$$
f: \mathbf{m} = \mathbf{m}_0 + \delta \mathbf{m} \to \mathbf{u} = \mathbf{u}_0 + \delta \mathbf{u},\tag{14}
$$

<span id="page-3-6"></span>here *f* maps an element of model space **m** to the element of data space **u**. Using the Born approximation, the total fields **u** can be decomposed into the primary fields  $\mathbf{u}_0$  and scattered fields  $\delta \mathbf{u}$  linearly.

$$
f(\mathbf{u}, \mathbf{m}) = \mathbf{L}\mathbf{u} - \mathbf{s} = 0,\tag{15}
$$

<span id="page-3-5"></span>
$$
\mathbf{L}^{P-SV} = \mathbf{A} + \mathbf{B} + \mathbf{C},\tag{16}
$$

$$
\mathbf{L}^{SH} = \mathbf{M} + \mathbf{N} + \mathbf{P},\tag{17}
$$

$$
\mathbf{u}^{P-SV} = (v_x, v_x^f, v_z, v_z^f, \sigma_{xx}, \sigma_{zz}, \sigma_{xz}, P)^T,
$$
\n(18)

$$
\mathbf{u}^{SH} = (v_y, \sigma_{xy}, \sigma_{zy})^{\mathrm{T}},\tag{19}
$$

$$
\mathbf{s}^{P-SV} = (s_x, s_x^f, s_z, s_z^f, s_{xx}, s_{zz}, s_{xz}, s_p)^T,\tag{20}
$$

$$
\mathbf{s}^{SH} = (s_y, s_{xy}, s_{zy})^{\mathrm{T}},\tag{21}
$$

where the forward operator  $f(\mathbf{u}; \mathbf{m})$  maps the relations between the poroelastic seismic wavefields **u** and the model parameter **m**. When we only consider the isotropic medium, the differential operator **L** in *P-SV* format is given by eqs [\(22\)](#page-3-1)–[\(26\)](#page-3-2).  $\mathbf{L}^{SH}$  represents the differential operator in *SH* format, which is complemented by eq. [\(27\)](#page-3-3).

<span id="page-3-1"></span>
$$
\mathbf{A} = \begin{bmatrix} \mathbf{0}_4 & \mathbf{D}^1 \\ \mathbf{D}^2 & \mathbf{0}_4 \end{bmatrix} \partial_x, \tag{22}
$$
\n
$$
\begin{bmatrix} -A\phi m & 0 & 0 & -A\rho_2 \\ 0 & 0 & -A\rho_2 & -A\rho_1 \end{bmatrix} \qquad \begin{bmatrix} -(\lambda + 2\mu) & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \end{bmatrix}
$$

$$
\mathbf{D}^{1} = \begin{bmatrix} A(\rho_{f} - \phi m) & 0 & 0 & A\rho_{1} \\ 0 & 0 & -A\phi m & 0 \\ 0 & 0 & A(\rho_{f} - \phi m) & 0 \end{bmatrix}, \quad \mathbf{D}^{2} = \begin{bmatrix} -\lambda & 0 & 0 & 0 \\ 0 & 0 & -\mu & 0 \\ M(\alpha - \phi) & M\phi & 0 & 0 \end{bmatrix},
$$
(23)

$$
\mathbf{B} = \begin{bmatrix} \mathbf{0}_4 & \mathbf{D}^3 \\ \mathbf{D}^4 & \mathbf{0}_4 \end{bmatrix} \partial_z,\tag{24}
$$

$$
\mathbf{D}^{3} = \begin{bmatrix} 0 & 0 & -A\phi m & 0 \\ 0 & 0 & A(\rho_{f} - \phi m) & 0 \\ 0 & -A\phi m & 0 & -A\rho_{2} \\ 0 & A(\rho_{f} - \phi m) & 0 & A\rho_{1} \end{bmatrix}, \quad \mathbf{D}^{4} = \begin{bmatrix} 0 & 0 & -\lambda & 0 \\ 0 & 0 & -(\lambda + 2\mu) & 0 \\ -\mu & 0 & 0 & 0 \\ 0 & 0 & M(\alpha - \phi) & M\phi \end{bmatrix},
$$
(25)

<span id="page-3-2"></span>
$$
\mathbf{C} = \begin{bmatrix} \mathbf{I}_4 & \mathbf{0}_4 \\ \mathbf{0}_4 & \mathbf{D} \end{bmatrix} \partial_t, \quad \mathbf{D} = \begin{bmatrix} 1 & 0 & 0 & \alpha \\ 0 & 1 & 0 & \alpha \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix},
$$
(26)

<span id="page-3-3"></span>
$$
\mathbf{M} = \begin{bmatrix} 0 & -A\phi m & 0 \\ -\mu & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix} \mathbf{\partial}_{x}, \quad \mathbf{N} = \begin{bmatrix} 0 & 0 & -A\phi m \\ 0 & 0 & 0 \\ -\mu & 0 & 0 \end{bmatrix} \mathbf{\partial}_{z}, \quad \mathbf{P} = \mathbf{I}_{3} \mathbf{\partial}_{t},
$$
 (27)

where  $A = 1/(\rho_f(\rho T - \phi \rho_f))$ .  $\rho_1 = (1 - \phi)\rho_s$  and  $\rho_2 = \phi \rho_f$  are the mass per unit volume of aggregate for the solid phase and the fluid phase, respectively. When the porosity  $\phi = 0$ , the forward operator *f* is able to map the elastic wavefields. The symbol  $\mathbf{0}_n$  represents the  $n \times n$  zero matrix, while  $I_n$  is the identity matrix.

Suppose that a corresponding first-order perturbation is applied on a random parameter of the reference model  $m_0$ , the scattered wavefields δ*u* perturbated by single parameter are obtained by eqs [\(28\)](#page-3-4)–[\(30\)](#page-4-0) under the Born approximation (Appendix A). For example, if there is a small scattered variable  $\delta \lambda$  added on the reference parameter  $\lambda$ , the corresponding excitation of the scattered wavefields can be summarized as eq.  $(31)$ ,

<span id="page-3-4"></span>
$$
\mathbf{L}\delta\mathbf{u}_m = \delta\mathbf{m}\delta\mathbf{s}_m,\tag{28}
$$

<span id="page-4-2"></span>

Figure 2. Shallow-seismic scattered *P-SV* poroelastic wavefields (solid profile in vertical direction *Z*) corresponding to different model parameters with 5 percent perturbations. The red star represents the location of the point diffractor.

$$
\delta \mathbf{m}^{P-SV} \in \{\delta \lambda, \delta \mu, \delta \rho_s, \delta \rho_f, \delta K_s, \delta K_f, \delta \phi\}, \quad \delta \mathbf{m}^{SH} \in \{\delta \mu, \delta \rho_s, \delta \rho_f, \delta \phi\},\tag{29}
$$

<span id="page-4-3"></span>
$$
\delta \mathbf{s}_{m}^{P-SV} \in \{\delta \mathbf{s}_{\lambda}, \delta \mathbf{s}_{\mu}, \delta \mathbf{s}_{\rho_{s}}, \delta \mathbf{s}_{\rho_{f}}, \delta \mathbf{s}_{K_{s}}, \delta \mathbf{s}_{K_{f}}, \delta \mathbf{s}_{\phi}\}, \quad \delta \mathbf{s}_{m}^{SH} \in \left\{\delta \mathbf{s}_{\mu}^{SH}, \delta \mathbf{s}_{\rho_{s}}^{SH}, \delta \mathbf{s}_{\rho_{f}}^{SH}, \delta \mathbf{s}_{\phi}^{SH}\right\},\tag{30}
$$

<span id="page-4-1"></span><span id="page-4-0"></span>
$$
\delta \mathbf{s}_{\lambda} = \begin{bmatrix}\n\partial_x & 0 & \partial_z & 0 & \cdots & 0 & \frac{1}{K_s} \partial_t \\
\partial_x & 0 & \partial_z & 0 & \cdots & 0 & \frac{1}{K_s} \partial_t \\
0 & & \cdots & & & 0 & 0 \\
0 & & \cdots & & & & 0 \\
\frac{M}{K_s} \partial_x & 0 & \frac{M}{K_s} \partial_z & 0 & \cdots & 0 & \frac{M}{K_s^2} \partial_t\n\end{bmatrix} \mathbf{u}_0^{P-SV}.
$$
\n(31)

For instance, it shows clearly in eq. [\(31\)](#page-4-1) that the signal of the scattering point can be calculated based on the unperturbed wavefields. The scattered wavefields are generated from the same forward operator **L** and solved by the FDTD method afterward. To be noted, since the scattering source signals are changed with various perturbed parameters, the scattering wavefields for different parameters are obtained separately.

## **3.1 Analysis of scattered wavefield produced by individual model parameter perturbations**

In this part, a series of scattering tests are implemented on a  $45 \text{ m} \times 9 \text{ m}$  poroelastic half-space to detect the effects of the model parameters on the different wave types. The explicit expressions of the scattering point corresponding to various model parameters are shown in Appendix A. By solving eqs [\(10\)](#page-2-2)–[\(30\)](#page-4-0) with the FDTD method, both the incident and scattered wavefields are simulated numerically. A Ricker wavelet triggers the unperturbed shallow poroelastic subsurface with a centre frequency of 40 Hz on the free surface, and the scattering point (eq. [30\)](#page-4-0) is set in the middle on the free surface. Model parameters can be found in Table [1.](#page-2-0)

Here we take the wave information from the solid phase as examples. The scattered wavefields corresponding to different model parameters are shown in Fig. [2](#page-4-2) for the *P*-*SV* scheme and Fig. [3](#page-5-0) for the *SH* scheme. Both for *P*-*SV* and *SH* cases, scattered waveform comparisons from a single trace are shown in Figs [4](#page-5-1) and [5](#page-6-0) separately. The number of the model parameters in the *SH* scheme is reduced since the main stress is not considered. The wave amplitude of the scattered wavefields in *P*-*SV* and *SH* schemes is shown consistently to make a comparison.

Different wave types in the shallow *P-SV&SH* poroelastic wavefields have been shown in Fig. [1.](#page-2-1) As shown in Fig. [3,](#page-5-0) there are only shear waves from the *SH* scheme in a homogeneous half-space, and it shows the slightest perturbation from a scattering point of the fluid density  $\rho_f$ . Shear modulus  $\mu$  and solid grain density  $\rho_s$  take the main responsibility for the shear wave, while porosity has a relatively small effect. When it turns to the *P*-*SV* scheme in Fig. [2,](#page-4-2) Rayleigh and compressional waves are generated in the meantime. The fast-*P* wave propagates

<span id="page-5-0"></span>

<span id="page-5-1"></span>Figure 3. Shallow-seismic scattered *SH* poroelastic wavefields (Solid profile in horizontal direction *Y*) corresponding to different model parameters with 5 percent perturbations. The red star represents the location of the point diffractor, which is the same with the *P*-*SV* case.



**Figure 4.** Scattered single-trace waveform comparison from *P*-*SV* scheme: vertical-component velocity of the solid phase. The receiver is on the free surface at offset  $= 10.8$  m in Fig. [2,](#page-4-2) and the black line represents the unperturbed reference waveform from the homogeneous poroelastic background at the same position.

in the fastest way with relatively small energy. Besides, the velocities of the *P* and *S* waves have a significant difference since the subsurface is poroelastic, which is consistent with the scattered result from  $\delta\phi$  that the porosity of the subsurface can influence body waves sensitively. Solid bulk modulus  $K_s$  shows minor effects on the shallow poroelastic wavefields. Fluid bulk modulus  $K_f$  and fluid density  $\rho_f$  take response for shear wave slightly. Furthermore, porosity  $\phi$  is quite sensitive to both shear and compressional waves. A similar analysis also can be told from the single-trace waveform comparison in Figs [4](#page-5-1) and [5.](#page-6-0) The results indicate the potential trade-off relations between parameters during multiparameter FWI. Based on the physical condition in the poroelastic medium, the parameters with fewer similarities in the radiation patterns are likely to be recovered together.

<span id="page-6-0"></span>

**Figure 5.** Scattered single-trace waveform comparison from SH scheme: horizontal-component velocity of the solid phase. The receiver is on the free surface at offset  $= 10.8$  m in Fig. [3,](#page-5-0) and the black line represents the unperturbed reference waveform from the homogeneous poroelastic background at the same position.

#### 4 FULL-WAVEFORM INVERSION FOR FLUID-SATURATED POROELASTIC MEDIA

The elements in the model space  $M : \mathbf{m}$  and data space  $U : \mathbf{u}$  can be decomposed as in Section 3. FWI tries to minimize the misfit functional  $J$ , which is normally designed in a simple least-squares format (eq. [32\)](#page-6-1)

<span id="page-6-1"></span>
$$
\mathcal{J}(\mathbf{m}) = \frac{1}{2} \|\mathbf{u}(\mathbf{m}) - \mathbf{d}_{\text{obs}}\|^2 = \frac{1}{2} \sum_{\text{sources}} \int_0^T dt \sum_{r=1}^N \|\mathbf{u}(\mathbf{x}_r, t) - \mathbf{d}_{\text{obs}}(\mathbf{x}_r, t)\|^2.
$$
\n(32)

*T* is the recording time and *N* indicates the number of receivers at the receiver position **r**, **u** is the synthetic data and  $\mathbf{d}_{obs}$  is the recorded data. To solve the minimization problem, the adjoint-state method was developed in order to avoid massive computing on the high order Frechet ´ derivatives (Chavent [1974;](#page-13-15) Plessix [2006\)](#page-14-9).

From the perspective of Born approximation, when a perturbation  $\delta$ **m** is introduced into the reference model  $\mathbf{m}_0$ , the Fréchet derivative of the misfit functional is

<span id="page-6-3"></span>
$$
\frac{\partial \mathcal{J}(\mathbf{m})}{\partial \mathbf{m}} = \sum_{\text{sources}} \int_0^T dt \sum_{r=1}^N \frac{\partial \delta \mathbf{u}_m}{\partial \delta \mathbf{m}} (\mathbf{u}(\mathbf{x}_r, t) - \mathbf{d}_{\text{obs}}(\mathbf{x}_r, t)).
$$
\n(33)

Assuming a differentiable function **u**<sup>∗</sup> that satisfies

$$
\mathbf{L}^* \mathbf{u}^* = \mathbf{u} - \mathbf{d}_{\text{obs}},\tag{34}
$$

for example, for two column vectors  $\vec{a}$  and  $\vec{b}$ ,  $\vec{a} \cdot \vec{b} = \vec{a}^T \vec{b}$ , then the Fréchet derivative of the misfit functional  $\vec{J}$  is simplified as eq. [\(35\)](#page-6-2) based on the eq. [\(28\)](#page-3-4).

$$
\frac{\partial \mathcal{J}(m)}{\partial m} = \sum_{\text{sources}} \int_{T} dt (\mathbf{L}^{-1} \delta \mathbf{s}_{m})^{T} \mathbf{L}^{*} \mathbf{u}^{*},
$$
\n(35)

while  $\mathbf{L}^* = \mathbf{L}^T$  and  $\mathbf{u}^*$  represent the backpropagating adjoint wavefields (see Appendix A for  $\delta s_m$  and Appendix B for the Fréchet kernels with respect to different parameters),

$$
\frac{\partial \mathcal{J}(m)}{\partial m} = \sum_{\text{sources}} \int_{T} dt (\delta \mathbf{s}_{m})^{T} \mathbf{u}^{*}.
$$
\n(36)

<span id="page-6-2"></span>Alternatively, when a dual space  $\mathcal{U}^*$ :  $\tilde{\mathbf{u}}^*$  is added into the mapping *f*, the augmented functional  $\mathcal{L}$  can be defined as

$$
\mathcal{L}(\widetilde{\mathbf{u}}, \widetilde{\mathbf{u}}^*, \mathbf{m}) = h(\widetilde{\mathbf{u}}, \mathbf{m}) - \langle \widetilde{\mathbf{u}}^*, f(\widetilde{\mathbf{u}}, \mathbf{m}) \rangle_{\mathcal{U}}, \qquad (\widetilde{\mathbf{u}} \in \mathcal{U}),
$$
\n(37)

where  $\tilde{\mathbf{u}}$  and  $\tilde{\mathbf{u}}^*$  are independent of **m** (Plessix [2006\)](#page-14-9), under the physical constraint in eq. [\(15\)](#page-3-5),

$$
\mathcal{L}(\mathbf{u}, \widetilde{\mathbf{u}}^*, \mathbf{m}) = h(\mathbf{u}, \mathbf{m}) - \langle \widetilde{\mathbf{u}}^*, f(\mathbf{u}, \mathbf{m}) \rangle_{\mathcal{U}} = \mathcal{J}(\mathbf{m}),
$$
\n(38)

or

$$
\mathcal{L}(\mathbf{u}, \mathbf{u}^*, \mathbf{m}) = h(\mathbf{u}, \mathbf{m}) - \langle \mathbf{u}^*, f(\mathbf{u}, \mathbf{m}) \rangle_{\mathcal{U}} = \mathcal{J}(\mathbf{m}),\tag{39}
$$

<span id="page-7-1"></span>

**Figure 6.** Frechet kernels involving Rayleigh waves in  $P-SV$  for  $\lambda$ ,  $K_s$  and  $K_f$ . The red star is the location of the forward source, and the inverted triangle represents the adjoint source. Both are located on the free surface.

for instance, the Lagrange multiplier for *P*-*SV* formulations

$$
\mathbf{u}^* = (v_x^*, v_x^{f*}, v_z^*, v_z^{f*}, \sigma_{xx}^*, \sigma_{zz}^*, \sigma_{xz}^*, P^*)^{\mathrm{T}}, \qquad (\mathbf{u}^* \in \mathcal{U}^*), \tag{40}
$$

and  $(\mathbf{u}, \mathbf{u}^*)$  is the saddle point of  $\mathcal{L}$ . From the integration by parts, in the physical spatial domain  $\Omega$  within the time duration [0, *T*], we have

$$
\langle \mathbf{u}^*, \partial_t \mathbf{u} \rangle_T = - \langle \partial_t \mathbf{u}^*, \mathbf{u} \rangle_T, \tag{41}
$$

and

$$
\langle \mathbf{u}^*, \partial_i \mathbf{u} \rangle_{\Omega} = -\langle \partial_i \mathbf{u}^*, \mathbf{u} \rangle_{\Omega}, \qquad (i = \{1, 2, 3\} \equiv \{x, y, z\}), \tag{42}
$$

when **u**<sup>∗</sup> = 0 as the final time condition and the physical boundary conditions are applied as well, then the adjoint equations are generalized by

$$
\frac{\partial \mathcal{L}(\mathbf{u}, \mathbf{u}^*, \mathbf{m})}{\partial \widetilde{\mathbf{u}}} = \frac{\partial \mathcal{J}(\mathbf{m})}{\partial \widetilde{\mathbf{u}}} - \mathbf{L}^* \mathbf{u}^* = 0.
$$
\n(43)

After expanding the residual function  $\mathcal J$  near a starting point, the model update

<span id="page-7-0"></span>
$$
\Delta \mathbf{m} = -\gamma \mathbf{H}^{-1} \frac{\partial \mathcal{J}(\mathbf{m})}{\partial \mathbf{m}},\tag{44}
$$

which is used to approximate the real model iteratively during FWI. Here  $\gamma$  is the step length and **H** is the Hessian matrix. The problem of the singularity of Hessian is dealt with by approximating the inverse of Hessian with different optimization methods (Nocedal & Wright [2006\)](#page-14-12).

#### **4.1 Sensitivity kernels**

The effects of different model parameters on the waveforms are evaluated from the analysis of the scattering problem in Section 3.1. As complements, the sensitivity of the various model parameters to the data space can be detected from the corresponding sensitivity kernels, which are the hearts of the related gradients as well. The full expressions of different kernels derived from the eqs [\(32\)](#page-6-1)–[\(43\)](#page-7-0) are in Appendix B. To clarify the effects of various wave types on the model parameters, the primary sensitivity kernels in a shallow poroelastic subsurface are calculated both in *P*-*SV* and *SH* equations. The numerical model is a homogeneous poroelastic half-space, with a circular anomaly within the Fresnel zone. For concerns on shallow detection, surface waves are considered. The acquisition geometry is set as the same as Section 3 within the duration time of 15 ms, and the parameters can be found in Table [1.](#page-2-0)

The kernels' galleries in Figs [6](#page-7-1) and [7](#page-8-0) show the wave paths for different scattering bodies. The updates along the ray path give contributes to the background values and source frequencies heavily affect the minor radius of the first-Fresnel zone. Unlike the traditional reflected wave exploration which concerns more reflections beyond the ray path, surface waves will travel along the free surface and the long wavelength parts on the fast  $P$  wave are less involved for shallow seismic detection. According to the wavelength  $\Lambda$ , here, the sequences of main wave types are  $\Lambda_s > \Lambda_{\text{Love}} > \Lambda_{\text{Rayleigh}}$ , and  $\Lambda_s > \Lambda_{sp}$ . Fig. [6](#page-7-1) shows the galleries of the sensitivity kernels for  $\lambda$ ,  $K_s$  and  $K_f$ , which are only considered in *P*-*SV* case. It indicates  $\lambda$  concerns more on the Rayleigh waves compared to  $K_s$  and  $K_f$ , while  $K_s$  and  $K_f$  are more sensitive to the compressional waves. Especially, *Ks* mainly gets benefits from the long wavelength components, which gives less contribution to the shallow seismic wavefields. *Kf* mainly concerns the slow-*P* wave, which will be attenuated in a viscous porous media within the seismic band.

Fig. [7](#page-8-0) contains the sensitivity kernels of  $\mu$ ,  $\rho_s$ ,  $\rho_f$  and  $\phi$  in *P-SV* and *SH* profiles. The galleries of the same parameter are shown consistently for comparison. Compared to  $\rho_f$  and  $\phi$ , it is clear in *SH* that  $\mu$  and  $\rho_s$  are more sensitive to the shear wave components and the

<span id="page-8-0"></span>

<span id="page-8-1"></span>**Figure 7.** Frence kernels in *SH* & *P-SV* for  $\mu$ ,  $\rho_s$ ,  $\rho_f$  and  $\phi$ : surface waves are involved. Geometry is the same as in Fig. [6.](#page-7-1)



**Figure 8.** Acquisition geometry for a shallow poroelastic inclusion model. Horizontal *Y* component for *SH* equations is considered as well.

main energy of  $K_{\mu}^{SH}$  distribute along the free surface.  $\rho_f$  shows less effects from shear wave components, but  $K_{\rho_f}$  indicates  $\rho_f$  is sensitive to the slow-*P* wave modes. Similarly,  $K_{\phi}^{SH}$  and  $K_{\phi}$  tell that  $\phi$  takes response for shear waves but is also sensitive to *P* waves, especially the slow-*P* wave. Since Rayleigh waves are coupled from compressional waves and shear waves in *P*-*SV* profile, φ also makes substantial contributions to surface waves.

#### **4.2 Synthetic examples of P-SV&SH PFWI for a shallow inclusion model**

In this section, we perform reconstruction tests on a poroelastic inclusion model to validate the derived gradients (Appendix B) and give a preliminary insight on the feasibility of PFWI for shallow seismic data. The inclusion model consists of poroelastic background media and a circle porous anomaly in the centre. There are 10 sources and 75 receivers on the free surface. The forward wavefields are generated by Ricker wavelet with the central frequency of 40 Hz in 0.12 s. The initial model parameters come from Table [1,](#page-2-0) and Fig. [8](#page-8-1) shows the acquisition geometry. A multistage strategy (10–20–40 Hz) is applied to avoid the cycle-skipping artifacts and a pre-conditioned steepest descent method is adopted over the course of iterations. We aim to recover anomalies of every single parameter while keeping others remain the same as the initial model, which is a homogeneous poroelastic background.

Figs [9](#page-9-0) and [10](#page-9-1) show a 1-D reconstruct model comparison from the middle log profile. On the basis of the derived kernels, the poroelastic parameters are well recovered by *P*-*SV*/Rayleigh- and *SH*/Love-wave PFWI. In Fig. [9,](#page-9-0) *Ks* and *Kf* exhibit an over-fitting problem since they are more sensitive to the long wavelength component, which makes less contribution to shallow seismic wavefields. Fig. [10](#page-9-1) gives comparisons of the recovered  $\mu$ ,  $\rho_s$ ,  $\rho_f$  and  $\phi$  based on *P-SV* and *SH* equations. Especially,  $\rho_f$  is better inverted in the *P-SV* profile, which demonstrates  $\rho_f$  can get extra benefits from compressional waves. Correspondingly, Fig. [11](#page-10-0) exhibits the changes of the poroelastic inclusion model with iterations, which show the convergence of the reconstructed model. In contrast with *SH*-wave data, the PFWI of Rayleigh-wave data usually needs more iterations as the complexity of wavefields.

#### **5 TRADE-OFF ANALYSIS**

To prepare an approach for the multiparameter inversion in fluid-saturated poroelastic media, the similarity of the sensitivities of the data to vary parameters needs to be investigated (Métivier *et al.* [2014\)](#page-14-13). As derived in Section 4, the explicit expressions for kernels of the gradients in *P-SV* and *SH* formats are given by eqs [\(B1\)](#page-15-0)–[\(B11\)](#page-16-0) in Appendix B. We perform a series of numerical tests on the gradients of model parameters for the anomaly model in Fig. [8,](#page-8-1) and explore the correlations of their patterns. The acquisition and model parameters are the same as in Section 4.2. The inclusion model parameters are changed individually, and corresponding results are exhibited in Figs [12–](#page-10-1)[18.](#page-12-0)

<span id="page-9-0"></span>

<span id="page-9-1"></span>**Figure 9.** PFWI of Rayleigh-wave data: 1-D logging profile in the middle of the true, initial and reconstructed models for  $\lambda$ ,  $K_s$  and  $K_f$ .



**Figure 10.** PFWI of *SH*/Love- and *P-SV*/Rayleigh-wave data: 1-D logging profile in the middle of the true, initial and reconstructed models for  $\mu$ ,  $\rho_s$ ,  $\rho_f$  and φ.

According to the equations derived in Section 4, we know that the correlations between the gradients of different parameters can not be eliminated under the assumption of Born approximation. Because the subsurface parameters are reconstructed simultaneously during the multiparameter inversion, how to minimize the cross-talk issue and implement an applicable inversion strategy are difficult tasks. Unlike the acoustic and elastic FWI, where fewer parameters can be handled flexibly with parametrizations, we seek to divide the poroelastic parameters with low correlations into the same groups for multiparameter inversion. In this section, we vary the interference parameter of the anomaly body at the same location in the inclusion model and cross-compare the corresponding influences between the gradient patterns of other parameters. Although the values of the gradients depend on the magnitude of the related material parameters, the descent direction from the gradients panels still can indicate the correlations. Figs [12–](#page-10-1)[14](#page-11-0) only present the correlations in *P*-*SV*, while Figs [15–](#page-11-1)[18](#page-12-0) display the comparison results of the common parameters in *P*-*SV* and *SH* cases. To make clear evaluations, all the panels are scaled with their absolute maximum

<span id="page-10-0"></span>

<span id="page-10-1"></span>**Figure 11.** Model misfit changes of the poroelastic inclusion model with iterations: corresponding to the results in Figs [9](#page-9-0) and [10.](#page-9-1)



**Figure 12.** Gradient gallery in *P-SV* for correlation test in Section 5: { $\Delta\lambda$ ,  $\Delta K_s$ ,  $\Delta K_f$ }  $\rightarrow$  { $G_\lambda$ ,  $G_{K_s}$ ,  $G_{K_f}$ } involving Rayleigh waves. The model geometry is shown in Fig. [8,](#page-8-1) and the parameters are listed in Table [1,](#page-2-0) which are the same as the followings.

values, which indicate the descent directions as well. To mitigate footprints from the sources and receivers, all the gradients are tapered by an error function.

The location of the absolute extreme in gradient *G* is likely to be closer to the surface if the related parameter has more impact on the surface waves. The key point of achieving good results by multiparameter inversion is to recover the parameters with less coherency. For example, Fig. [12](#page-10-1) shows a map from disturbance  $\{\Delta\lambda, \Delta K_s, \Delta K_f\}$  in the anomaly to the gradients  $\{G_\lambda, G_{K_s}, G_{K_f}\}$  obtained from the *P-SV* poroelastic model.  $\Delta \lambda \to G_{K_f}$  and  $\Delta K_f \to G_{\lambda}$  indicate a strong coherency between  $\lambda$  and  $K_f$ , while the panels of  $\Delta \lambda \to G_{K_s}$  and  $\Delta K_s \to G_{K_s}$  $G_{\lambda}$  show fewer similarities.  $\Delta K_f \rightarrow G_{K_s}$  and  $\Delta K_s \rightarrow G_{K_f}$  are similar, but their descent directions are opposite. The results indicate that  $\lambda$ and  $K_s$  will be better to be considered in a same group during multiparameter inversion, and  $\{\Delta\lambda, \Delta K_f\}$  should make changes toward the opposite direction of  $\{\Delta K_s\}$  to achieve better recovery of the same anomalies.

<span id="page-11-2"></span>

<span id="page-11-0"></span>**Figure 13.** Gradient gallery in *P-SV* for correlation test in Section 5: { $\Delta\lambda$ ,  $\Delta K_s$ ,  $\Delta K_f$ }  $\rightarrow$  { $G_\mu$ ,  $G_\beta$ ,  $G_{\rho_f}$ ,  $G_{\phi}$ } involving Rayleigh waves.



<span id="page-11-1"></span>**Figure 14.** Gradient gallery in *P-SV* for correlation test in Section 5: { $\Delta \mu$ ,  $\Delta \rho_s$ ,  $\Delta \rho_f$ ,  $\Delta \phi$ }  $\rightarrow$  { $G_\lambda$ ,  $G_{K_s}$ ,  $G_{K_f}$ } involving Rayleigh waves.



**Figure 15.** Gradient panel in *SH* & *P*-*SV* for cross-comparison:  $\Delta \mu \rightarrow \{G_n, G_n^{SH}\}, n \in \{\mu, \rho_s, \rho_f, \phi\}.$ 



**Figure 16.** Gradient panel in *SH* & *P*-*SV* for cross-comparison:  $\Delta \rho_s \rightarrow \{G_n, G_n^{SH}\}, n \in \{\mu, \rho_s, \rho_f, \phi\}.$ 



<span id="page-12-0"></span>**Figure 17.** Gradient panel in *SH* & *P*-*SV* for cross-comparison:  $\Delta \rho_f \rightarrow \{G_n, G_n^{SH}\}, n \in \{\mu, \rho_s, \rho_f, \phi\}.$ 



**Figure 18.** Gradient panel in *SH* & *P*-*SV* for cross-comparison:  $\Delta \phi \rightarrow \{G_n, G_n^{SH}\}, n \in \{\mu, \rho_s, \rho_f, \phi\}.$ 

Figs [13](#page-11-2) and [14](#page-11-0) exhibit the maps  $\Delta m \to G_n$ , where  $m \in \mathbf{M}$  and  $n \in \mathbf{N}$  (M,  $\mathbf{N} \subseteq \{(\lambda, K_s, K_f), (\mu, \rho_s, \rho_f, \phi)\}\$ ,  $\mathbf{M} \neq \mathbf{N}$ ). By the crosscomparison of  $G_n$  mapped from  $\Delta m$ , the gradients performing without concentrated descent direction at the location of the anomaly shows fewer correlations between *m* and *n*. For instance,  $\Delta m \rightarrow G_{\phi}$  and  $\Delta \phi \rightarrow G_n$  indicate that porosity φ can raise cross-talk issues easily when inverted together with  $m \in (\lambda, K_s, K_f)$ . Besides,  $\Delta \lambda \rightarrow G$  and  $\Delta K_f \rightarrow G$  have similar patterns, and the result is consist with Fig. [12.](#page-10-1) Compared to  $\rho_f$ ,  $(\mu, \rho_s)$  have less coherency with  $(\lambda, K_s, K_f)$ .

Figs [15–](#page-11-1)[18](#page-12-0) present the results of the cross comparison  $\Delta m$ :  $G_n(m, n \in \{\mu, \rho_s, \rho_f, \phi\})$  in both *SH* and *P-SV* cases, while Love and Rayleigh waves exist separately. The gradient panels are shown consistently in *P-SV* and *SH*. In *SH* panels,  $\Delta \mu \to G_n^{SH}(n \in \{\rho_s, \rho_f, \phi\})$  and

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 $\Delta m \to G_{\mu}^{SH}(m \in \{\rho_s, \rho_f, \phi\})$  illustrate that  $\mu$  is a harmless and essential parameter for multiparameter PFWI. The panels of  $\Delta \rho_s \to G_n(n)$  $\in \{\mu, \rho_f, \phi\}$  and  $\Delta m \to G_{\rho_s}(m \in \{\mu, \rho_f, \phi\})$  show the correlations of gradients in *P-SV* are decreased compared to *SH*, which indicates it is more realistic to invert  $\rho_s$ ,  $\mu$  and  $\phi$  simultaneously in *P-SV* PFWI. Besides,  $G_{\rho_s}$  and  $G_{\rho_f}$  look similar, and the descent direction of  $G_{\phi}$  and  $(G_{\rho_s}, G_{\rho_f})$  is opposite. The analysis based on Figs [12](#page-10-1)[–18](#page-12-0) can provide insights into the parametrization of multiparameter PFWI.

#### **6 CONCLUSIONS**

We present a theoretical framework for TD poroelastic FWI, especially for shallow-seismic data. The shallow-seismic *P*-*SV*&*SH* poroelastic wavefields are simulated numerically. Based upon Born approximation, we derived the single-scattering *P*-*S*&*SH* wave equations for the fluid-saturated poroelastic media. The contributions of the single poroelastic parameters  $(P-SV: \lambda, \mu, \rho_s, \rho_f, K_s, K_f, \phi; SH: \mu, \rho_s, \rho_f, \phi)$  on the shallow-seismic wavefields are discussed by comparing the corresponding scattered wavefields, respectively. With the help of the adjoint-state method, the explicit formulations of the sensitivity kernels for different model parameters are derived by perturbation theory and Lagrange augmented functional. The kernel galleries in *P*-*SV*&*SH* are used to further illustrate the sensitivities of the poroelastic parameters to different wave components. Besides, we implement reconstruction tests on a poroelastic inclusion model to verify the accuracy of the derived kernels, and the recovery ability of PFWI on *P*-*SV*/Rayleigh- and *SH*/Love-wave data is compared, respectively. As a preliminary preparation for multiparameter FWI, we have also investigated the inter-parameter issues based on the descent direction in the *P*-*SV*&*SH* panels of gradients.

Similar to the elastic FWI, the results indicate that shear modulus  $\mu$  and grain density  $\rho_s$  are mainly responsible for generating shear waves. The fluid density  $\rho_f$ , which is extracted from the overall density  $\rho$ , pays primary attention to the slow-*P* wave mode.  $\lambda$ , which also exists in elastodynamic equations, and grain bulk modulus  $K_s$  has similar effects. In addition, fluid bulk modulus  $K_f$  and porosity  $\phi$  mainly concern with the slow-*P* wave mode.  $\phi$  has effects on all the wave types but prefers compressional waves. According to the real subsurface condition, it is necessary to classify the parameters with fewer correlations as a group to minimize the cross-talk issues during multiparameter PFWI. For instance, λ and *Kf* are not suitable to invert together in PFWI of Rayleigh-wave data. ρ*<sup>s</sup>* and ρ*<sup>f</sup>* can hardly be detected together in PFWI of Love-wave data, but their correlation is minimized in *P*-*SV* equations. Since the effective velocities of the poroelastic subsurface are coupled with different parameters (Appendix C), we can hardly obtain the updates on their gradients directly during the inversion. The feasibility and reconstructability of multiparameter TD-PFWI will be discussed in subsequent publications, especially for the fluid information.

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#### DATA AVAILABILITY

The numerical data used in this work are available on request.

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#### **APPENDIX A: FIRST-ORDER SCATTERING PULSES**

The perturbated body can be treated as a point scatterer when the size of the scatterer is much smaller than the wavelength (Wu & Aki [1989\)](#page-14-10). Following the eqs [\(10\)](#page-2-2)–[\(14\)](#page-3-6), by using Born approximation, the explicit expressions of secondary sources δ**m**δ**s***<sup>m</sup>* (eqs [28–](#page-3-4)[29\)](#page-4-3) for the remained single perturbated parameter in the isotropic fluid-saturated porous media are given by eqs [\(A1\)](#page-14-14)-[\(A6\)](#page-15-1).



$$
\delta \mathbf{s}_{K_f} = \left[\begin{bmatrix} \mathbf{s}_{K_f} \\ \mathbf{u}_0^{P-SV}, \\ \mathbf{0} & \cdots & \mathbf{0} & \frac{\phi M}{K_f^2} \partial_t \end{bmatrix} \right]
$$
(A5)

<span id="page-15-1"></span>
$$
\begin{bmatrix}\nT\rho_s \partial_t & -T\rho_f \partial_t & 0 & \cdots & 0 \\
(T-1)\rho_s \partial_t & -(T-1)\rho_f \partial_t & 0 & \cdots & \vdots \\
0 & 0 & T\rho_s \partial_t & -T\rho_f \partial_t & 0 & \cdots \\
0 & 0 & (T-1)\rho_s \partial_t & -(T-1)\rho_f \partial_t & 0 & \cdots & 0 \\
\vdots & \vdots & \vdots & \vdots & \vdots & \vdots \\
\frac{\alpha M}{A\rho_f \phi} \partial_x & 0 & \frac{\alpha M}{A\rho_f \phi} \partial_z & 0 & \cdots & 0 & \frac{\alpha M}{A\rho_f \phi K_s} \partial_t\n\end{bmatrix}
$$
\n(A6)

Here,  $\rho_1 = (1 - \phi)\rho_s$  and  $\rho_2 = \phi \rho_f$  represent the mass of solid and fluid per unit volume of aggregate, respectively (Biot [1956a\)](#page-13-4). Besides, the scattering sources for *SH* equations are also summarized as eqs [\(A7\)](#page-15-2)–[\(A8\)](#page-15-3).

<span id="page-15-2"></span>
$$
\delta \mathbf{s}_{\mu}^{SH} = \underbrace{\begin{bmatrix} \partial_{x} & 0 & 0 \\ \partial_{z} & 0 & 0 \end{bmatrix} \mathbf{u}_{0}^{SH}, \quad \delta \mathbf{s}_{\phi}^{SH} = -A\rho_{f}[(T-1)\rho_{f} - T\rho_{s}] \underbrace{\begin{bmatrix} \partial_{t} & 0 & 0 \\ & & \end{bmatrix}}_{(3\times3)} \mathbf{u}_{0}^{SH}.
$$
\n(A7)\n
$$
\delta \mathbf{s}_{\rho_{s}}^{SH} = -A T\rho_{f}(1-\phi) \underbrace{\begin{bmatrix} \partial_{t} & 0 & 0 \\ & & \end{bmatrix}}_{(3\times3)} \mathbf{u}_{0}^{SH}, \quad \delta \mathbf{s}_{\rho_{f}}^{SH} = -A (T-1)\rho_{2} \underbrace{\begin{bmatrix} \partial_{t} & 0 & 0 \\ & & \end{bmatrix}}_{(3\times3)} \mathbf{u}_{0}^{SH}
$$
\n(A8)

## **APPENDIX B: SENSITIVITY KERNELS WITH RESPECT TO INDIVIDUAL PARAMETERS**

Since the Fréchet or sensitivity kernels are the volumetric densities of Fréchet derivatives (Fichtner [2010\)](#page-13-16), when the unknown variables in the misfit function are the displacement differences, the explicit 2-D sensitivity kernels *K* in the direction δ**m** are derived on the basis of the eq. [\(33\)](#page-6-3). Both the *P*-*SV* and SH equations are considered bellow.

<span id="page-15-3"></span>For elastic modulus,

$$
\boldsymbol{K}_{\lambda} = -\int_{0}^{T} dt \left\{ A\rho_{f} \left[ T \left( \frac{\partial u_{x}^{*}}{\partial x} + \frac{\partial u_{z}^{*}}{\partial z} \right) + (T - 1) \left( \frac{\partial u_{x}^{f*}}{\partial x} + \frac{\partial u_{z}^{f*}}{\partial z} \right) \right] + \frac{M}{K_{s}} P^{*} \right\} \left( \frac{\partial u_{x}}{\partial x} + \frac{\partial u_{z}}{\partial z} + \frac{1}{K_{s}} P \right).
$$
\n(B1)

<span id="page-15-0"></span>For shear modulus,

$$
\mathbf{K}_{\mu} = -\int_{0}^{T} dt \left\{ A\rho_{f} \left[ T \left[ 2 \left( \frac{\partial u_{x}^{*}}{\partial x} \frac{\partial u_{x}}{\partial x} + \frac{\partial u_{z}^{*}}{\partial z} \frac{\partial u_{z}}{\partial z} \right) + \left( \frac{\partial u_{z}^{*}}{\partial x} + \frac{\partial u_{x}^{*}}{\partial z} \right) \left( \frac{\partial u_{z}}{\partial x} + \frac{\partial u_{x}}{\partial z} \right) \right] \right\} + (T - 1) \left[ 2 \left( \frac{\partial u_{x}^{f*}}{\partial x} \frac{\partial u_{x}}{\partial x} + \frac{\partial u_{z}^{f*}}{\partial z} \frac{\partial u_{z}}{\partial z} \right) + \left( \frac{\partial u_{z}^{f*}}{\partial x} + \frac{\partial u_{x}^{f*}}{\partial z} \right) \left( \frac{\partial u_{z}}{\partial x} + \frac{\partial u_{x}}{\partial z} \right) \right] \right] + \frac{2}{3K_{s}} \left[ \frac{1}{\alpha} P \left[ A \left( \rho_{2} \left( \frac{\partial u_{x}^{*}}{\partial x} + \frac{\partial u_{z}^{*}}{\partial z} \right) - \rho_{1} \left( \frac{\partial u_{x}^{f*}}{\partial x} + \frac{\partial u_{z}^{f*}}{\partial z} \right) \right) - P^{*} \right] + MP^{*} \left( \frac{\partial u_{x}}{\partial x} + \frac{\partial u_{z}}{\partial z} + \frac{1}{K_{s}} P \right) \right] \right\}, \tag{B2}
$$

and

$$
\boldsymbol{K}_{\mu}^{SH} = -\int_{0}^{T} dt A T \rho_{f} \left( \frac{\partial u_{y}^{*}}{\partial x} \frac{\partial u_{y}}{\partial x} + \frac{\partial u_{y}^{*}}{\partial z} \frac{\partial u_{y}}{\partial z} \right). \tag{B3}
$$

For solid particle density,

$$
\boldsymbol{K}_{\rho_{s}} = -\int_{0}^{T} dt A \rho_{f} (1-\phi) \left\{ \frac{\partial v_{x}}{\partial t} \left[ T u_{x}^{*} + (T-1) u_{x}^{f*} \right] + \frac{\partial v_{z}}{\partial t} \left[ T u_{z}^{*} + (T-1) u_{z}^{f*} \right] \right\},\tag{B4}
$$

and

$$
\mathbf{K}_{\rho_s}^{SH} = -\int_0^T dt A T \rho_f (1-\phi) u_y^* \frac{\partial v_y}{\partial t}.
$$
 (B5)

For fluid density,

$$
\boldsymbol{K}_{\rho_f} = -\int_0^T dt \left\{ A \left( T - 1 \right) \left[ \frac{\partial v_x}{\partial t} \left( \rho_2 u_x^* - \rho_1 u_x^{f*} \right) + \frac{\partial v_z}{\partial t} \left( \rho_2 u_z^* - \rho_1 u_z^{f*} \right) \right] + \frac{1}{\rho_f} \left( \frac{\partial v_x^f}{\partial t} u_x^{f*} + \frac{\partial v_z^f}{\partial t} u_z^{f*} \right) \right\},
$$
\n(B6)

and

$$
\mathbf{K}_{\rho_f}^{SH} = -\int_0^T dt A (T-1) \rho_2 u_y^* \frac{\partial v_y}{\partial t}.
$$
 (B7)

For solid bulk modulus,

$$
\boldsymbol{K}_{K_s} = \int_0^T dt \frac{1-\alpha}{K_s} \left\{ A\rho_f P \left[ T \left( \frac{\partial u_x^*}{\partial x} + \frac{\partial u_z^*}{\partial z} \right) + (T-1) \left( \frac{\partial u_x^{f*}}{\partial x} + \frac{\partial u_z^{f*}}{\partial z} \right) \right] + MP^* \left[ \frac{\partial u_x}{\partial x} + \frac{\partial u_z}{\partial z} + \frac{1-2\alpha+\phi}{K_s(1-\alpha)} P \right] \right\}.
$$
\n(B8)

For fluid bulk modulus,

$$
\boldsymbol{K}_{K_f} = -\int_0^T dt \frac{\phi M}{K_f^2} P P^*.
$$
\n(B9)

<span id="page-16-0"></span>For porosity,

$$
\mathbf{K}_{\phi} = \int_{0}^{T} dt \left\{ -A\rho_{f} \left[ \left( \rho_{f} \frac{\partial v_{x}^{f}}{\partial t} - \rho_{s} \frac{\partial v_{x}}{\partial t} \right) \left( Tu_{x}^{*} + (T - 1) u_{x}^{f*} \right) + \left( \rho_{f} \frac{\partial v_{z}^{f}}{\partial t} - \rho_{s} \frac{\partial v_{z}}{\partial t} \right) \left( Tu_{z}^{*} + (T - 1) u_{z}^{f*} \right) \right] - \frac{\alpha M}{\phi} P^{*} \left( \frac{\partial u_{x}}{\partial x} + \frac{\partial u_{z}}{\partial z} + \frac{1}{K_{s}} P \right) \right\},
$$
\n(B10)

and

$$
\boldsymbol{K}_{\phi}^{SH} = -\int_{0}^{T} dt A \rho_f [(T-1)\rho_f - T\rho_s] u_y^* \frac{\partial v_y}{\partial t}
$$
(B11)

Here *u* and *u*<sup>\*</sup> represent the displacement in the forward system and adjoint system, respectively. It is worth to know that the Fréchet kernels also depend on the model parametrization and the forward component applied in the calculation of the misfit function. Both the components of the fluid phase in the forward and adjoint wavefields are vanished when the porosity is equal to zero, which supplies a way to simplify the poroelastic media into an elastic and acoustic medium.

#### **APPENDIX C: EFFECTIVE VELOCITIES**

The parameters and formulations for the calculation of the velocities in the poroelastic media are summarized below (Biot & Willis [1957;](#page-13-6) Dai *et al.* [1995\)](#page-13-17). The definition of the parameters has already been explained in the main text.

$$
\begin{cases}\nP = [(1 - \phi)(\alpha - \phi) + \frac{\phi K_d}{K_f}]M + \frac{4}{3}\mu \\
Q = \phi M(\alpha - \phi) \\
R = \phi^2 M \\
A' = T\phi \rho \rho_f - (-\phi \rho_f)^2 \\
B' = \rho R + T\phi \rho_f P + 2\phi \rho_f Q \\
C' = PR - Q^2\n\end{cases} (C2)
$$

Then, the velocity of the fast compressional wave

$$
V_{fp} = \sqrt{\frac{B^{\prime 2} + \sqrt{B^{\prime 2} - 4A^{\prime}C^{\prime}}}{2A^{\prime}}},
$$
(C3)

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the velocity of the slow compressional wave

$$
V_{sp} = \sqrt{\frac{B^{\prime 2} - \sqrt{B^{\prime 2} - 4A^{\prime}C^{\prime}}}{2A^{\prime}}}.
$$
\n(C4)

The fluid viscosity is absent in the non-dissipative case ( $\eta = 0$ ) and then the shear wave velocity is (Deresiewicz [1960;](#page-13-12) Morency & Tromp [2008\)](#page-14-3)

$$
V_s = \sqrt{\frac{\mu}{\rho - \frac{\phi \rho_f}{T}}}.\tag{C5}
$$