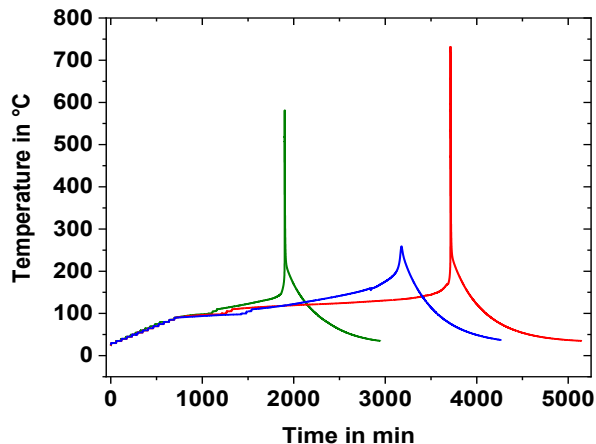


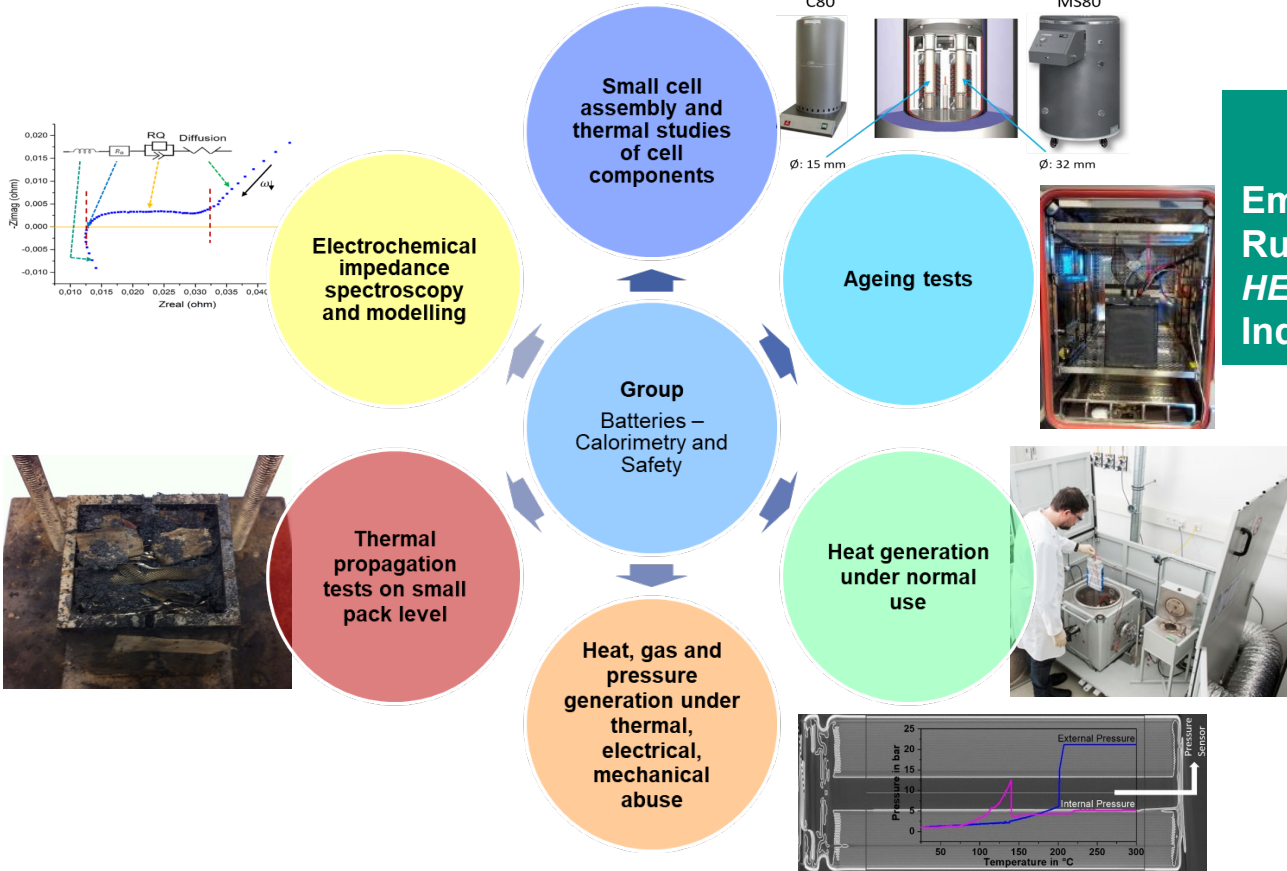
# How battery calorimeters can help in advancing thermal management and safety of cells and packs

*C. Ziebert, N. Uhlmann, N. Löffelholz, S. Ohneseit, P. Finster, M. Yasseri, M. Rohde, H.J. Seifert*

*KIT, Institute for Applied Materials – Applied Materials Physics*



# The Group Batteries – Calorimetry and Safety



**Data 2022**

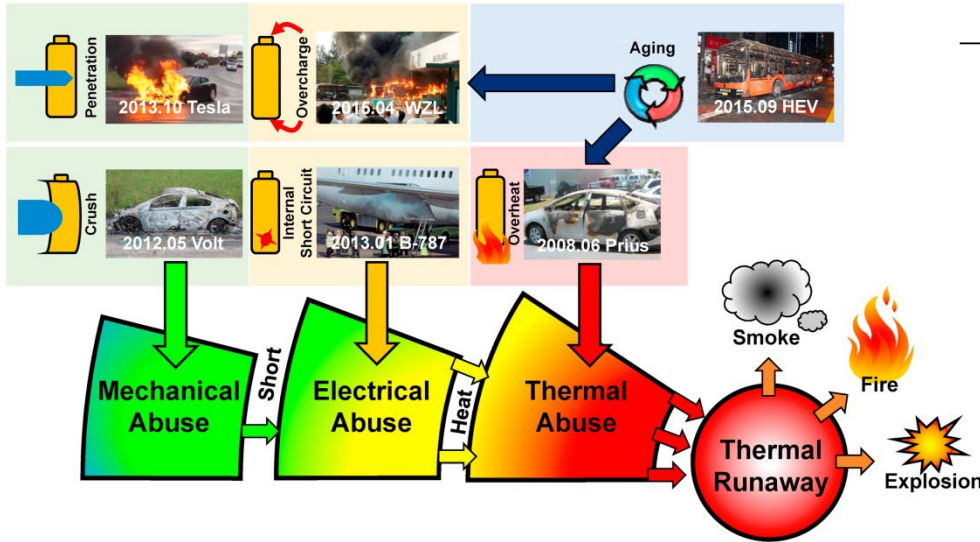
Employees:	15
Running LIB projects:	4
<i>HELIOS, POLiS, BatgasMod, AnaLiBa</i>	
Industry cooperation:	8



Dr. Carlos Ziebert  
Group leader Batteries – Calorimetry and Safety”

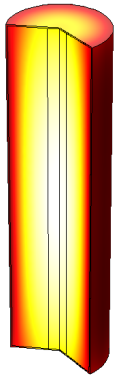
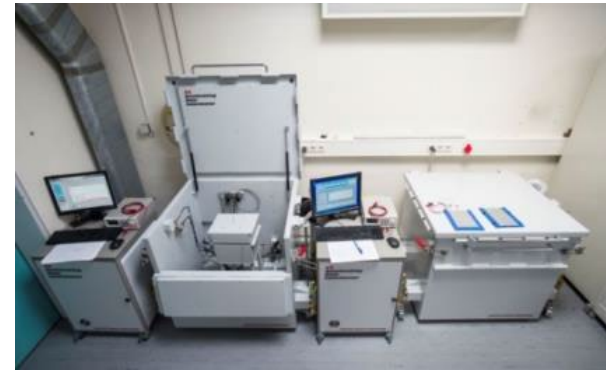
E-Mail: [Carlos.Ziebert@kit.edu](mailto:Carlos.Ziebert@kit.edu)

# Motivation: Increase of safety and reliability of LIB



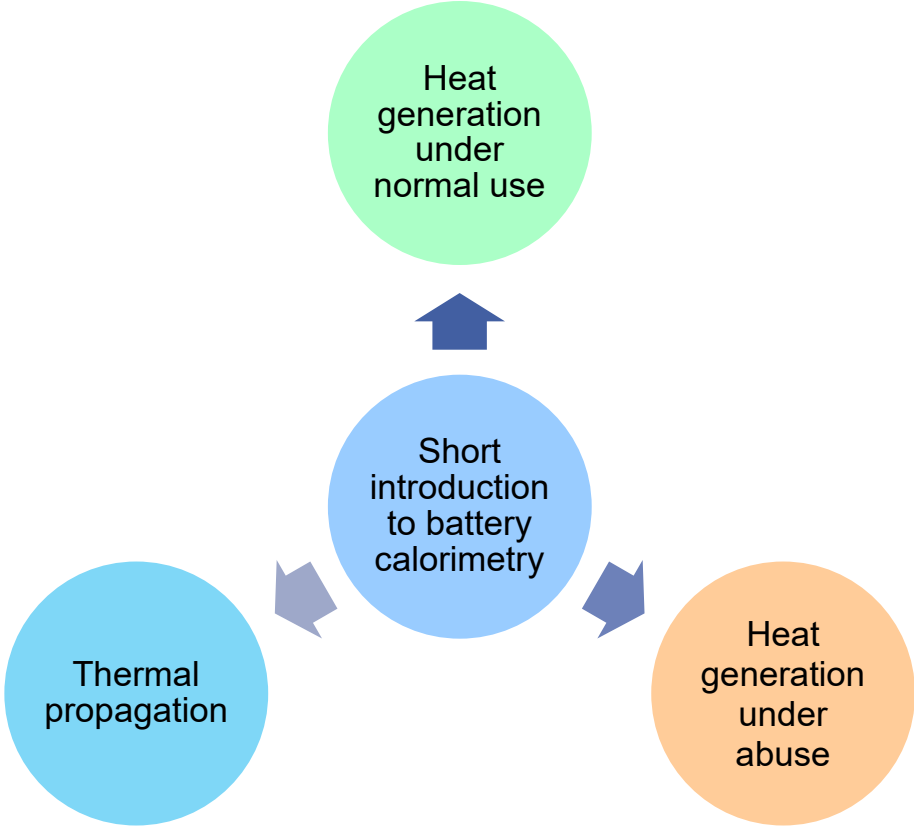
Feng et al., Energy Storage Materials 10 (2018) 246

→ For improving battery management system (BMS) and thermal management system (TMS) electrochemical and thermal behavior of the cells have to be thoroughly studied

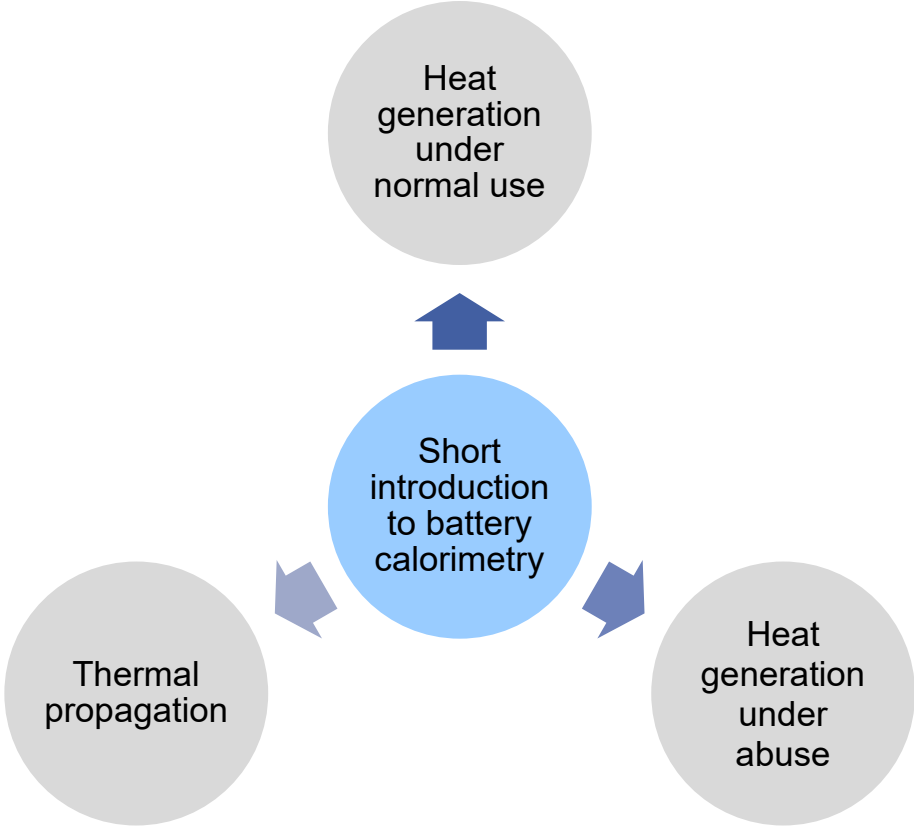


**Aim: Improvement of TMS and BMS by determination of quantitative data of thermal properties using calorimeters**

# Overview



# Overview



# At IAM-AWP: Europe`s Largest Calorimeter Center



3 EV+ ARC: Ø: 40 cm  
h: 44 cm



2 ES-ARC: Ø: 10 cm    2 EV-ARC: Ø: 25 cm  
h: 10 cm                      h: 50 cm

Equipment: 7 Accelerating rate calorimeters (ARC); 2 Tian-Calvet calorimeters; 5 DSC; IR camera; 13 Temperature chambers (23l - 400 l; -40°C to 180°C); 11 Cyclers (210 channels, 0.01-800 A); EIS; 2 GC/MS



# How can calorimetry help in battery research?

## Research for improving performance parameters

- Higher energy or power density
- Smaller heat release during operation
- Faster charging rates
- Increased cycle life and thermal life

## Research for improving safety parameters

- Higher safe operating temperature
- Better resistance to thermal/mechanical/electrical abuse
- Less energy release during decomposition

Differential scanning calorimeters



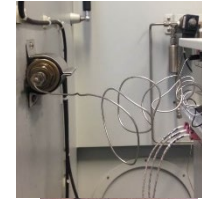
Tian-Calvet calorimeters



Small ARC



Medium-size ARC



Pressure measurement in ARC



Nail penetration test in ARC

Large-size ARC



Components



1 - 80 mAh



3 - 5 Ah



40 - 75 Ah

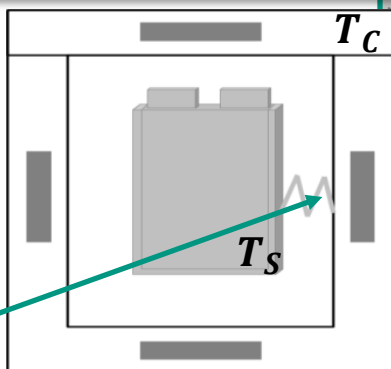
Cell Size and Capacity

# Possible conditions in an ARC

An ARC provides **isoperibolic** and **adiabatic** conditions

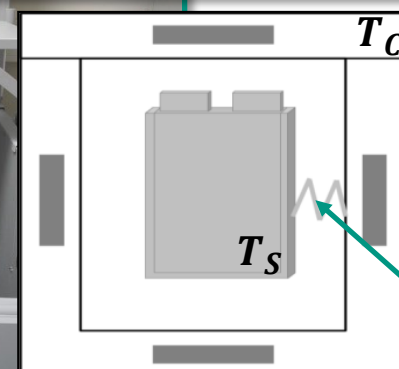
Under isoperibolic conditions the environmental temperature is kept constant.

Under adiabatic conditions the heaters follow immediately any change of the bomb thermocouple thus preventing that the cell can transfer heat to the walls.



$T_C$  constant

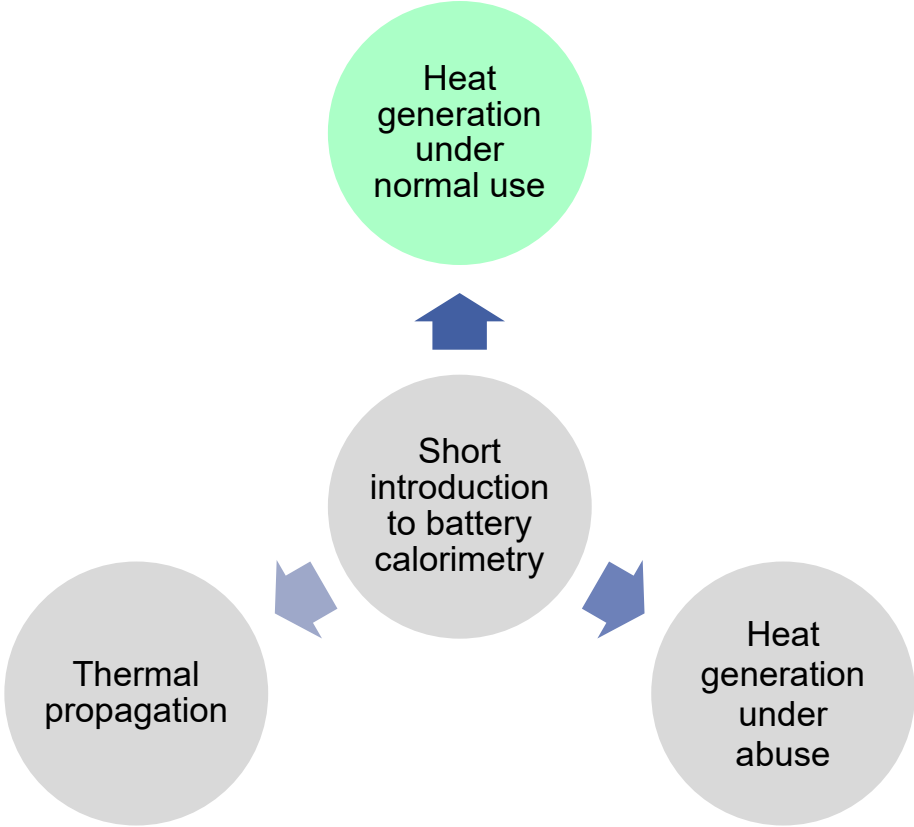
$$T_S(t) = T_{S_0} + \alpha \cdot t$$



$$\begin{aligned} T_C &= T_C(t) \\ &= T_{C_0} + \alpha \cdot t \end{aligned}$$



# Overview



# Isoperibolic measurements

Ideal conditions

→ Single cell

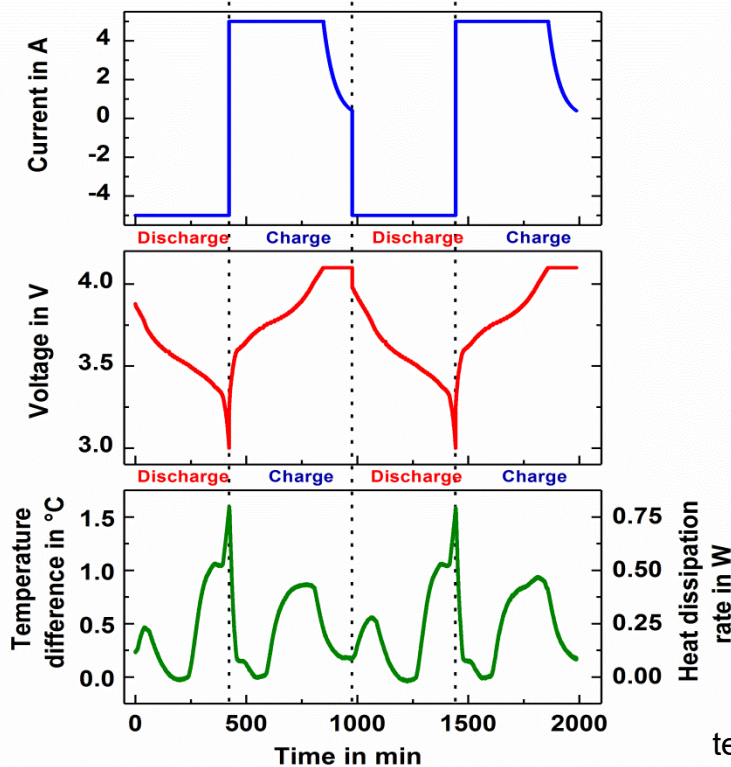
Discharge parameter:

- method: constant current (CC)
- $U_{\min} = 3.0\text{V}$
- $I = 5\text{A} \rightarrow \text{C}/8\text{-rate}$

Charge parameter:

- method: constant current, constant voltage (CCCV)
- $U_{\max} = 4.1\text{V}$
- $I = 5\text{A} \rightarrow \text{C}/8\text{-rate}$
- $I_{\min} = 0.5\text{A}$

→ after one electrochemical cycle the cell temperature reaches its initial value again



40 Ah pouch cell

$$\left(\frac{\delta E}{\delta T}\right) < 0$$

temperature coefficient negative!

# Adiabatic Measurements

## Worst Case Conditions

→ Cell in a pack surrounded by other cells

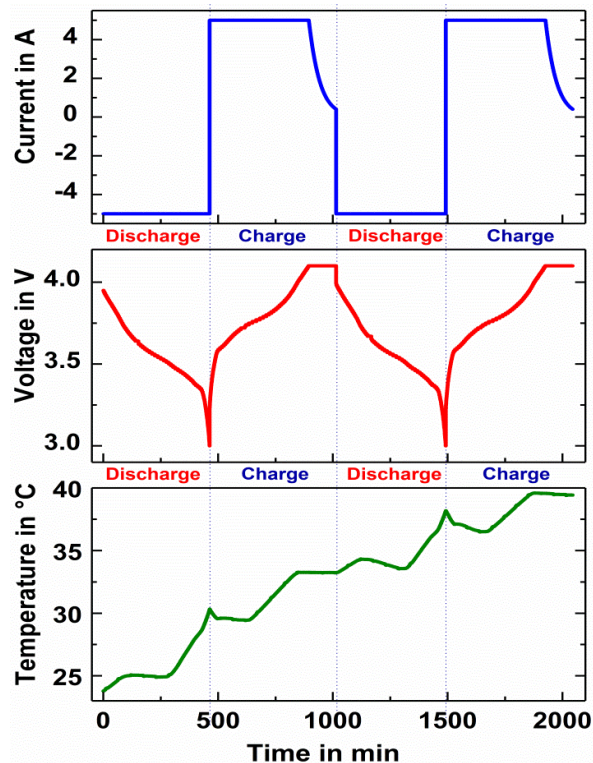
### Discharge parameter:

- method: constant current (CC)
- $U_{\min} = 3.0\text{V}$
- $I = 5\text{A} \rightarrow \text{C}/8\text{-rate}$

### Charge parameter:

- method: constant current, constant voltage (CCCV)
- $U_{\max} = 4.1\text{V}$
- $I = 5\text{A} \rightarrow \text{C}/8\text{-rate}$
- $I_{\min} = 0.5\text{A}$

→ after each electrochemical cycle the cell temperature increases further



40 Ah pouch cell

$T_{\text{st}} = 23^{\circ}\text{C}$  (RT)

# Determination of total generated heat

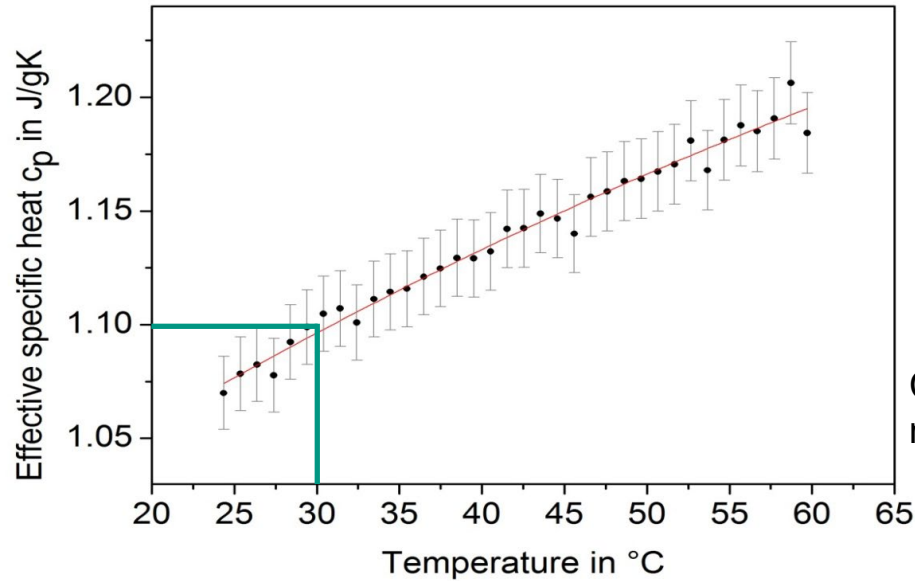
## Heat generation of the cell during charging and discharging – Key data for thermal management and safety

Conversion of thermal data (temperature, temperature rate) to heat (Joule) and power (Watt) with the aim of understanding of heat release to determine heat removal requirements for thermal management.

To be measured:

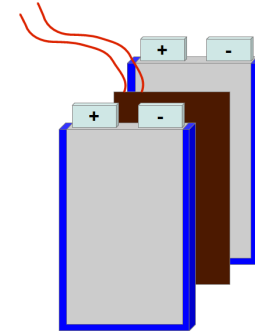
- **Effective specific heat capacity**
- **Heat transfer coefficient**
- **Reversible heat rate and irreversible heat rate**

# Effective specific heat capacity $c_p$



e.g. at 30 °C  $c_p = 1.095 \text{ J/g} \cdot \text{K}$

**Important input data for simulation**



40 Ah pouch cell

Sandwich setup  
for pouch cells

Control of the current applied to the heater  
mat to ensure a constant heating rate

$$c_p = \frac{\Delta Q}{m \cdot \Delta T_{ad}} = \frac{\int U \cdot I dt}{m \cdot \Delta T_{ad}}$$

$m$ : Mass of the cell

$\Delta T_{ad}$ : Temperature difference under  
adiabatic conditions

# Heat transfer coefficient

## Working principle of heat flux sensor (hfs)



gSKIN®-XP  
(10mm x 10mm)

Tiny, serially connected semiconductor piles inside the sensor generate a voltage, which is proportional to the heat passing through the surface. The voltage is read out and depending on the sensor's sensitivity the results are converted into the heat flux.

### Sensitivity:

$$S_0 = 10.04 \frac{mV \cdot m^2}{W}$$

Room temperature sensitivity

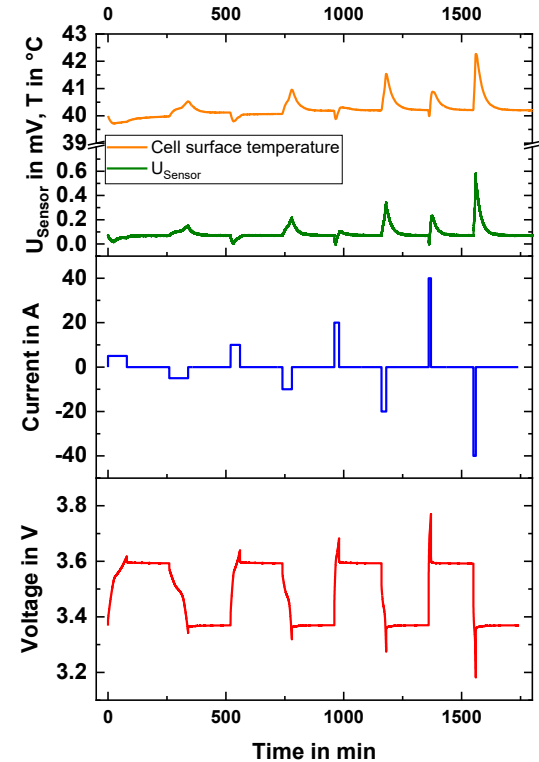
$$\Rightarrow h = \frac{\int \frac{U_{\text{sensor}}}{S(T)} dt}{\int_0^t (T - T_C) dt}$$

<http://shop.greenteg.com/shop/products-rd/gskin-xp/>  
<https://www.greenteg.com/faq-heat-flux-sensing/>

$$S(T) = S_0 + (T - 22.5 \text{ } ^\circ\text{C}) \cdot S_C$$

$$S_C = 0.0049 \cdot \frac{mV \cdot m^2}{W \cdot ^\circ\text{C}}$$

Temperature correction factor



# Comparison of values for generated heat

## 1) Adiabatic Measurement

$$\dot{Q}_{gen} = mc_p \frac{dT}{dt}$$

## 2) Isoperibolic Measurement

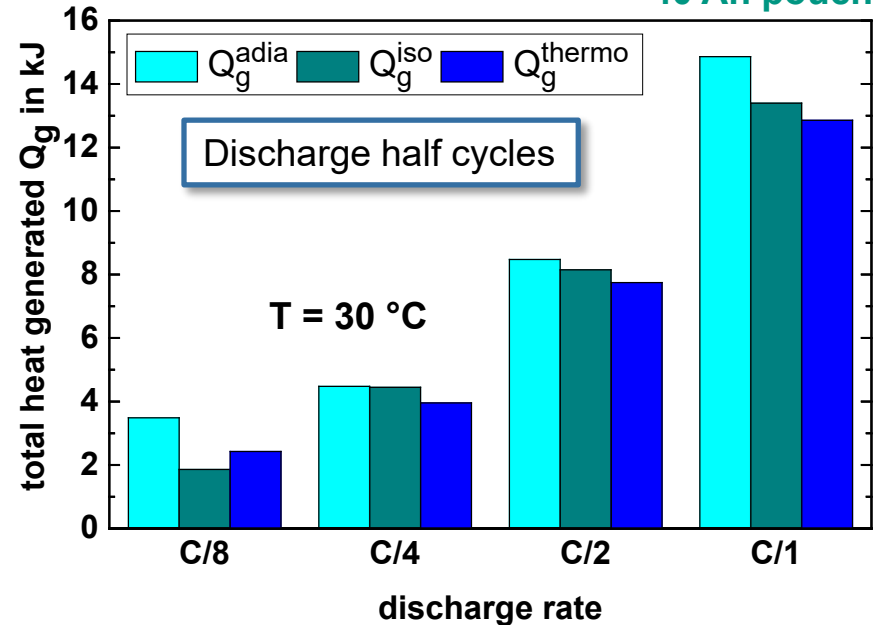
$$\dot{Q}_{gen} = mc_p \frac{dT}{dt} + Ah \cdot (T_S - T_C)$$

## 3) Measurement of irreversible and reversible heat

$$\dot{Q}_{gen} = -I(E_0 - E) - IT \frac{dE_0}{dT}$$

$E_0$ : Open circuit voltage (OCV),  $E$ : cell potential

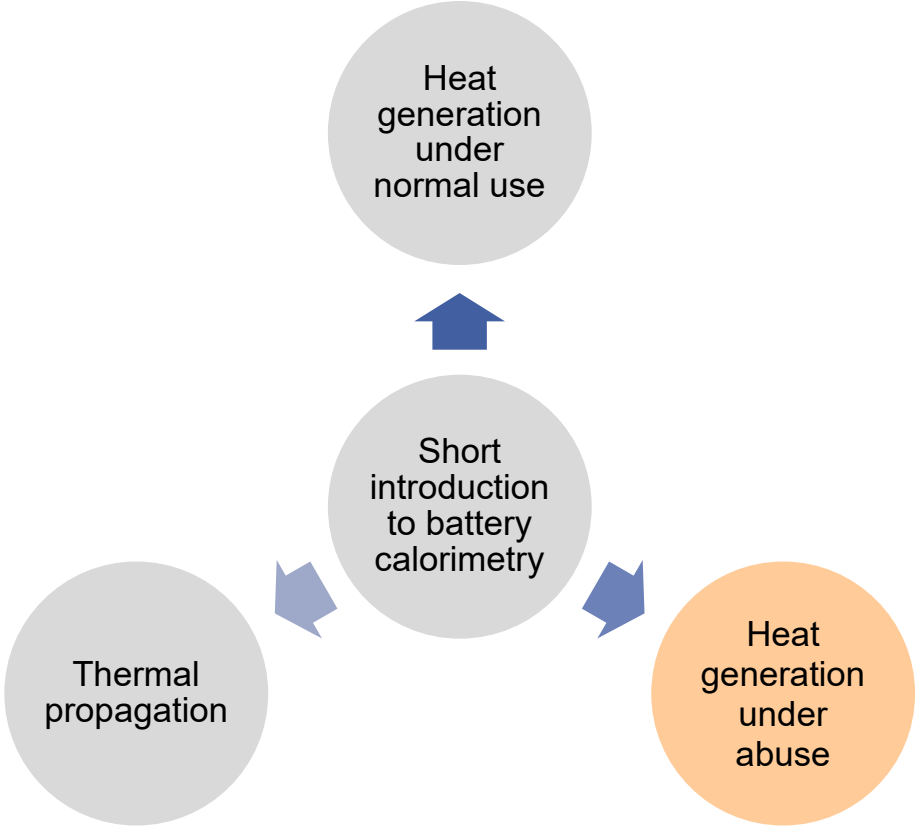
40 Ah pouch cell



**Conclusion: good agreement between the values determined by the different methods**

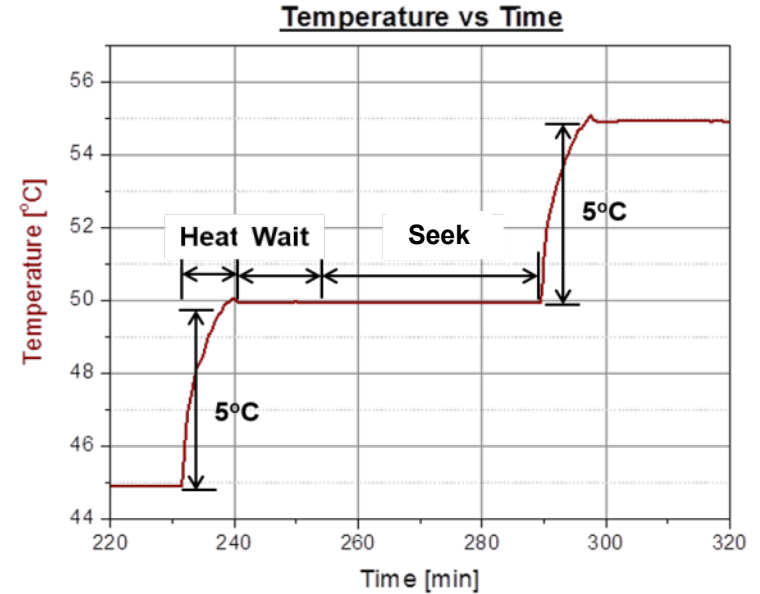
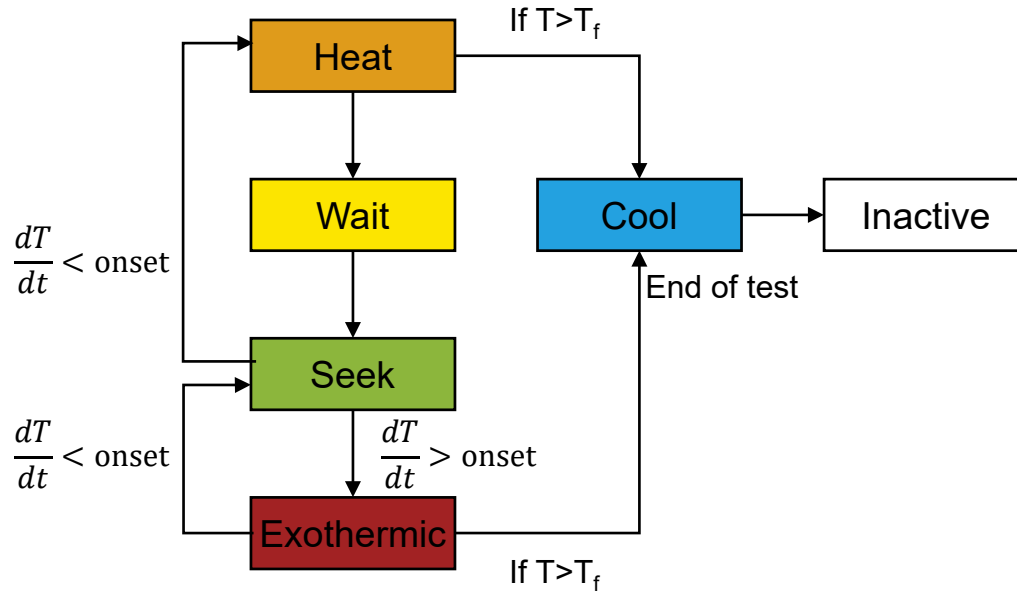
E. Schuster, C. Ziebert, A. Melcher, M. Rohde, H.J. Seifert, J. Power Sources 268 (2015) 580-589

# Overview





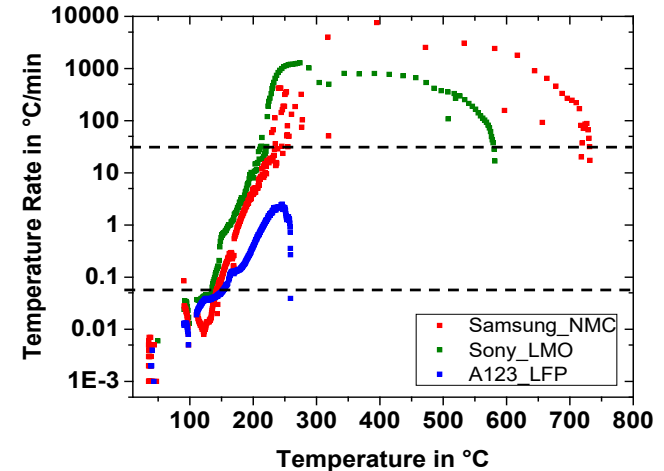
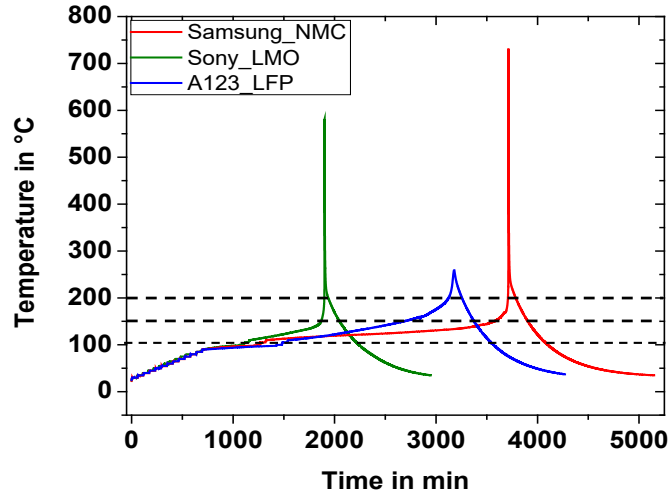
# Thermal abuse: Heat-Wait-Seek (HWS) Method in ARC



Example of a Heat-Wait-Seek step

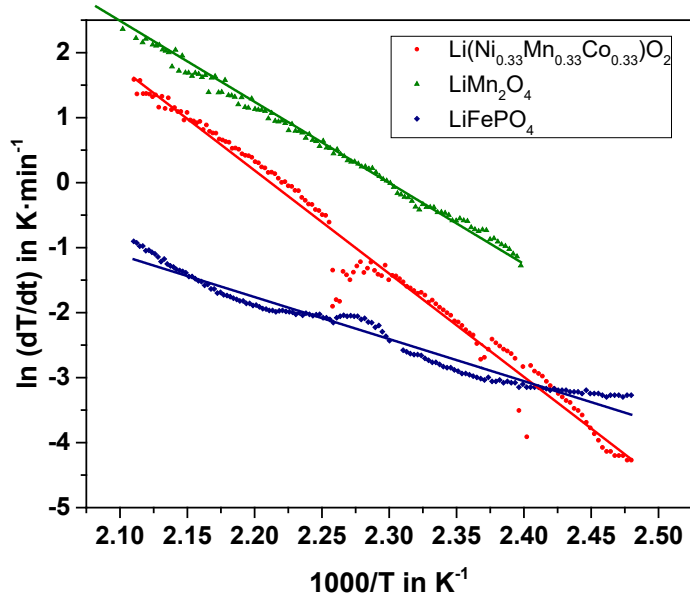
C. Ziebert, A. Melcher, B. Lei, W.J. Zhao, M. Rohde, H.J. Seifert, *Electrochemical-thermal characterization and thermal modeling for batteries*, in: L.M. Rodriguez, N. Omar, Eds., *EMERGING NANOTECHNOLOGIES IN RECHARGABLE ENERGY STORAGE SYSTEMS*, Elsevier Inc. 2017, ISBN 978032342977.

# Comparison of 18650 cells with different cathode materials



- $80 < T < 130^{\circ}\text{C}$ : low rate reaction,  $0.02 - 0.05^{\circ}\text{C}/\text{min}$ : exothermic decomposition of the SEI
- $130 < T < 200^{\circ}\text{C}$ : medium rate reaction,  $0.05 - 25^{\circ}\text{C}/\text{min}$ : solvent reaction, exothermic reaction between embedded Li ions and electrolyte  $\Rightarrow$  reduction of electrolyte at negative electrode
- $T > 200^{\circ}\text{C}$ : high rate reaction, higher than  $25^{\circ}\text{C}/\text{min}$ : Exothermic reaction between active positive material and electrolyte at positive electrode  $\Rightarrow$  rapid generation of oxygen

# Activation energies and reaction heats



Cathode Material	$\text{LiMn}_2\text{O}_4$ (LMO)	$\text{LiFePO}_4$ (LFP)	$\text{Li}(\text{Ni}_{0.33}\text{Mn}_{0.33}\text{Co}_{0.33})\text{O}_2$ (NMC)
Onset temperature of self-heating in °C	91	90	91
$T_{\max}$ in °C	303	259	731
$(dT/dt)_{\max}$ in °C/min	1429	3	7577
$c_p$ at 60°C SOC100 in J/g·K	0.83	1.19	0.95
$E_a$ in eV	1.07	0.56	1.37
Reaction heat in J/g	180	184	597
Reaction heat in J/g	350-640 [1,2]	260 [2]	600 [2]

[1] R. Spotnitz, J. Franklin, J. Power Sources, 113, 81 (2003).

[2] H. F. Xiang, H. Wang, et al., J. Power Sources, 191, 575 (2009).

Activation energy:  $\ln\left(\frac{dT}{dt}\right) \approx \ln(\Delta T_{ad} \cdot A) - \frac{E_a}{k_b \cdot T}$

$E_a$ : Activation energy, A: pre-exponential factor

$k_b$ : Boltzmann constant =  $8.62 \times 10^{-5} \text{ eV} \cdot \text{K}^{-1}$

Reaction heat:  $\frac{\Delta H}{m} = c_p \cdot \Delta T_{ad}$

Important input data for simulation

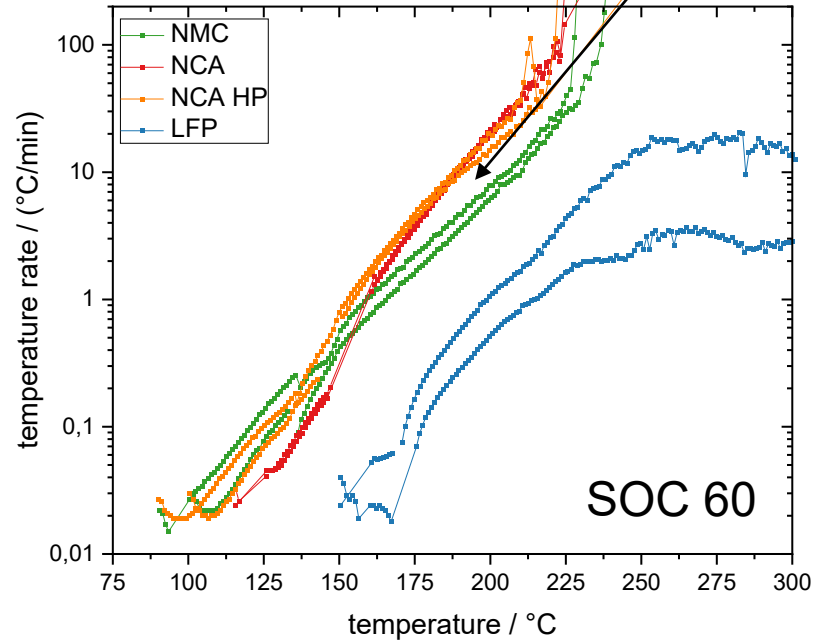
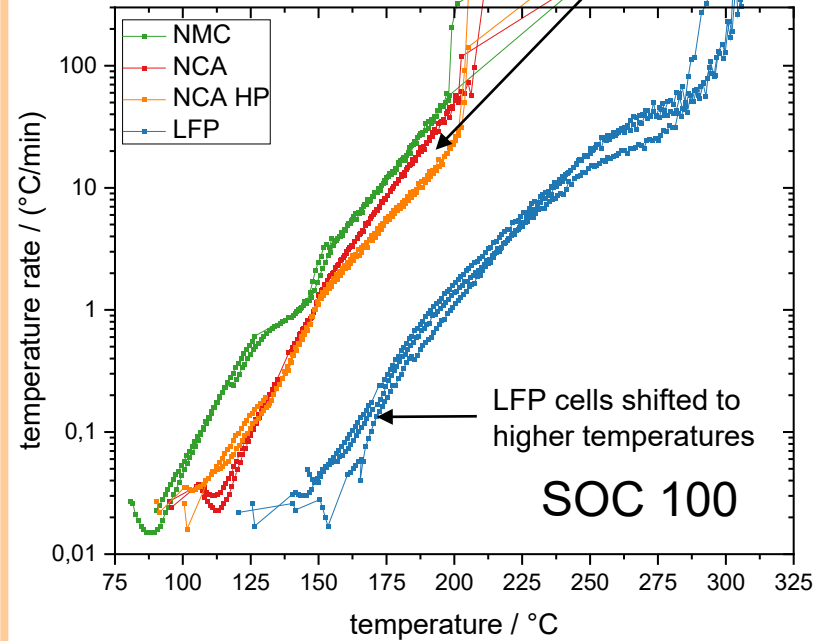
# Comparison of 21700 cells with different cathode materials and SOC

NCA and NMC cells behave comparably

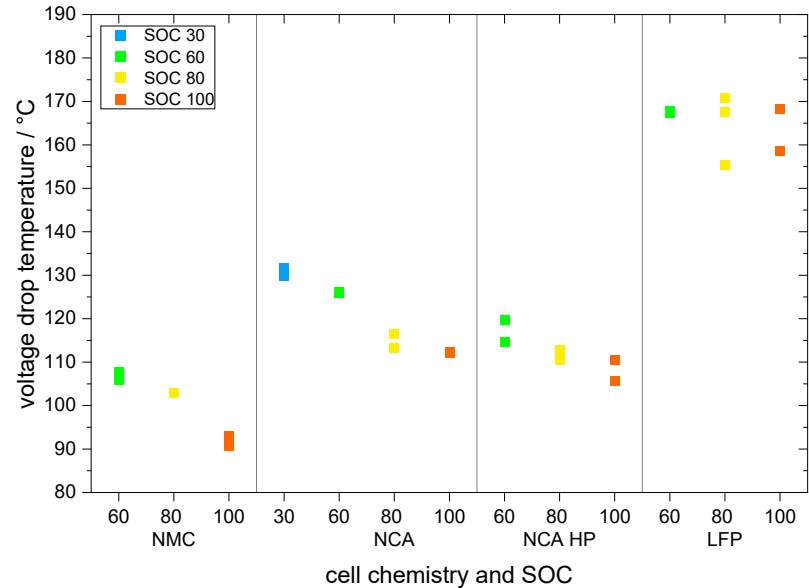
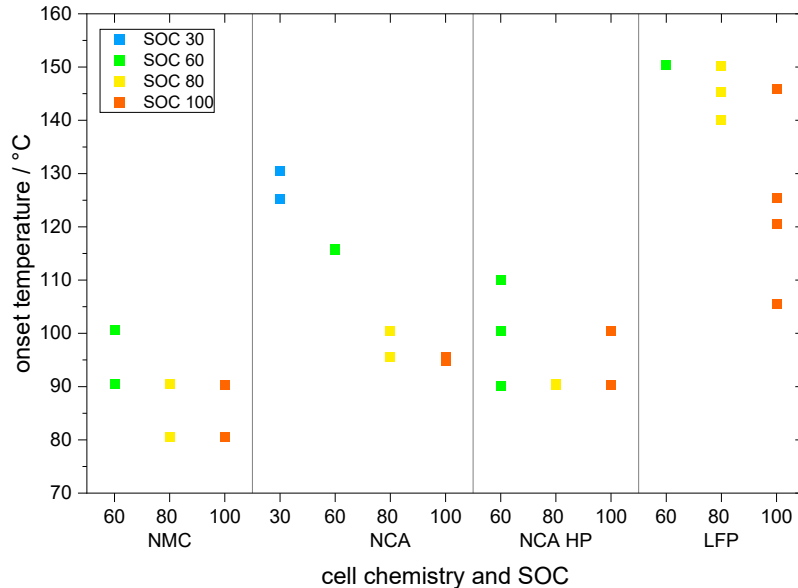
NCA and NCA HP cells behave comparably

NCA HP cells behave differently

NMC cells behave differently

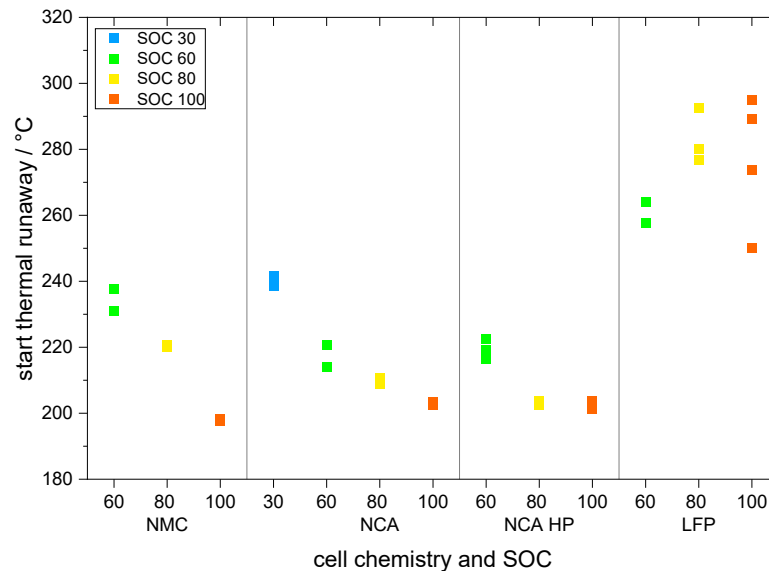
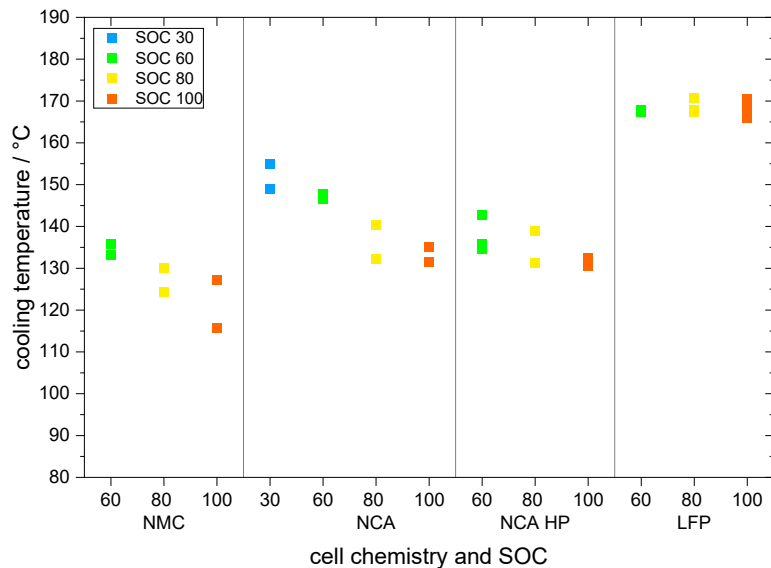


# Onset and CID triggering temperature



- NCA and NMC (on the right also NCA HP): **higher SOC results in lower temperature**
- NMC: **lower temperature than NCA, NCA HP and LFP cells**
- LFP: **significantly higher temperatures, no clear SOC influence**  
=> data has higher variation, therefore more experiments have been conducted

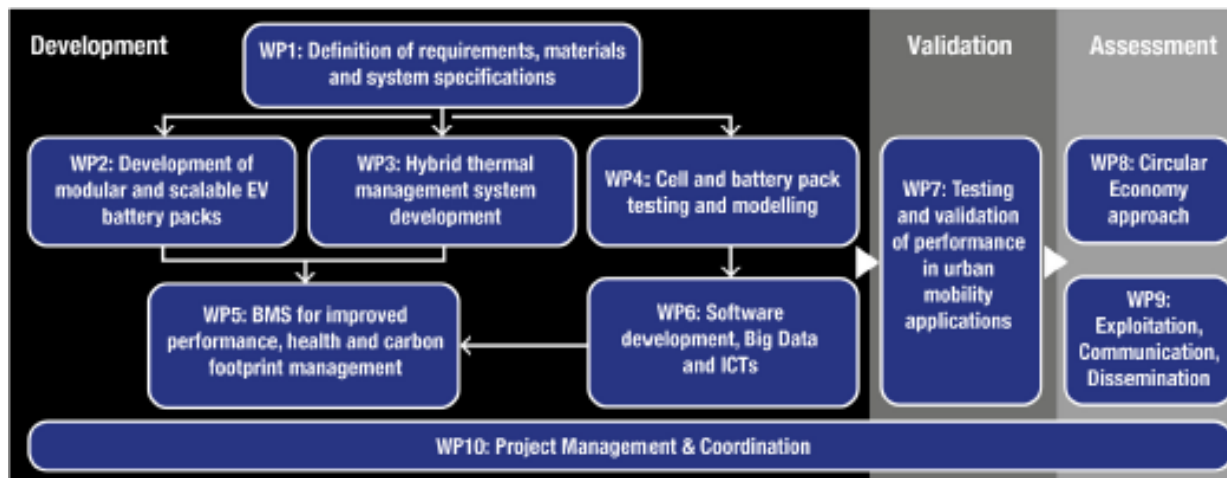
## Venting and start of thermal runaway / highest rate (LFP) temperature



- NMC, NCA, NCA HP: **clear influence of SOC, temperatures close to each other**
- NMC: **slightly earlier than NCA cells (for cooling)**
- LFP: **significantly higher temperatures, influence of SOC unclear**  
**but step between CID triggering and venting is much smaller as well as the self heat rates => harder to detect**

# HELIOS (High-performance modular packs for sustainable urban electromobility Services)

The HELIOS project aims at developing and integrating innovative materials, designs, technologies and processes to create a **new concept of smart, modular and scalable battery pack for a wide range of electric vehicles used in urban electromobility services**, from mid-size full-electric vehicles to electric buses, **with improved performance, energy density, safety and Levelized Cost of Storage (LCoS).**



Start date: 01-01-2021  
 Funding source: EC  
 Funding: appr. 10 million Euro  
 Partners: 18 from 8 countries

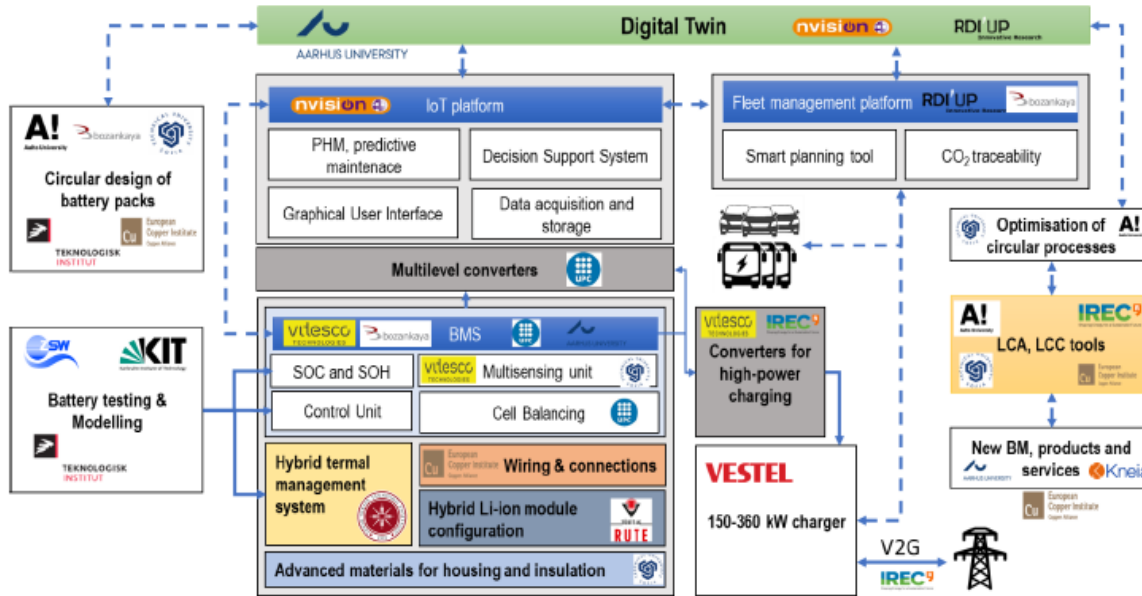
HELIOS WP Overview

<https://www.helios-h2020project.eu/project>

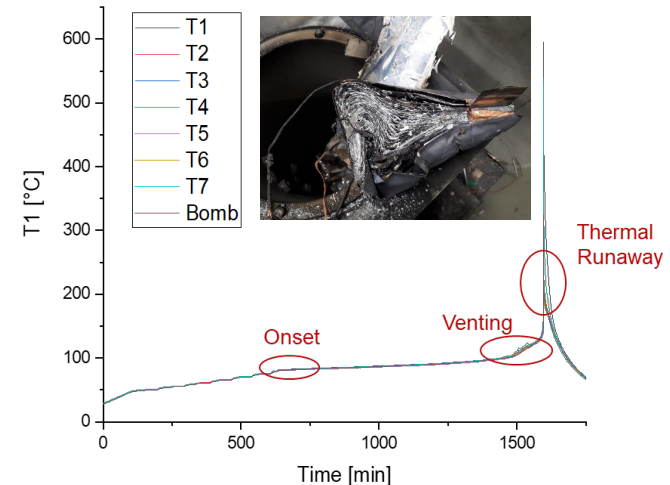
# HELIOS (High-performance modular packs for sustainable urban electrOmobility Services)



Sileo S12 e-bus produced by Bozankaya



HELIOS main building blocks



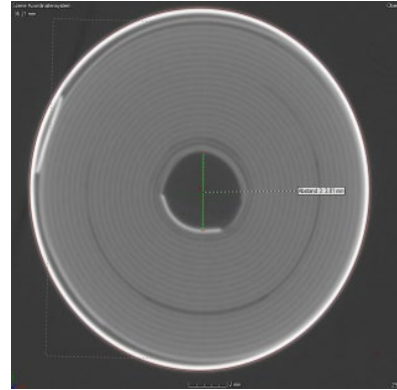
Exemplary safety test on large pouch cell



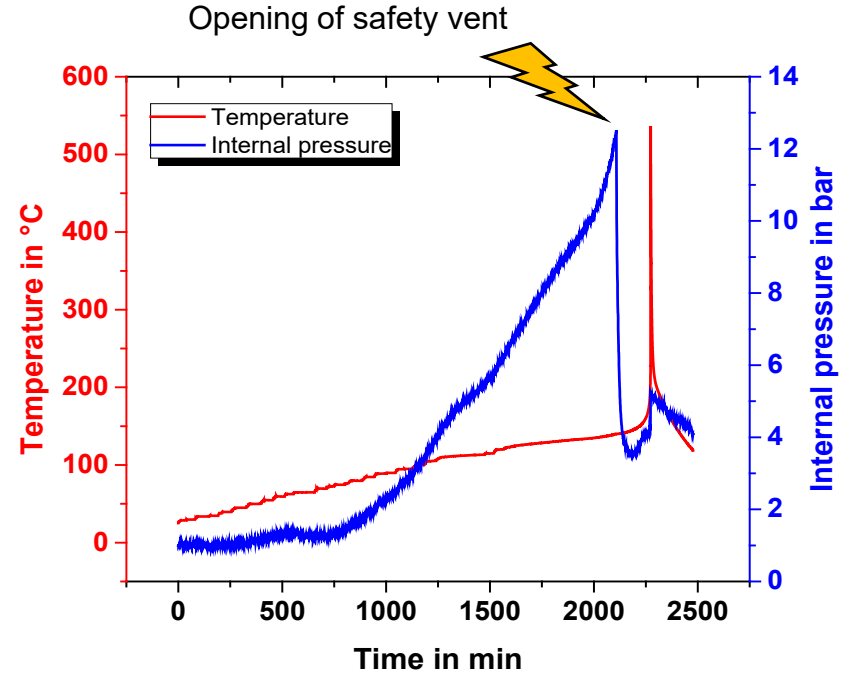
# Internal pressure measurements on 18650 cells



Pressure line ( $\varnothing$  1.5 mm)



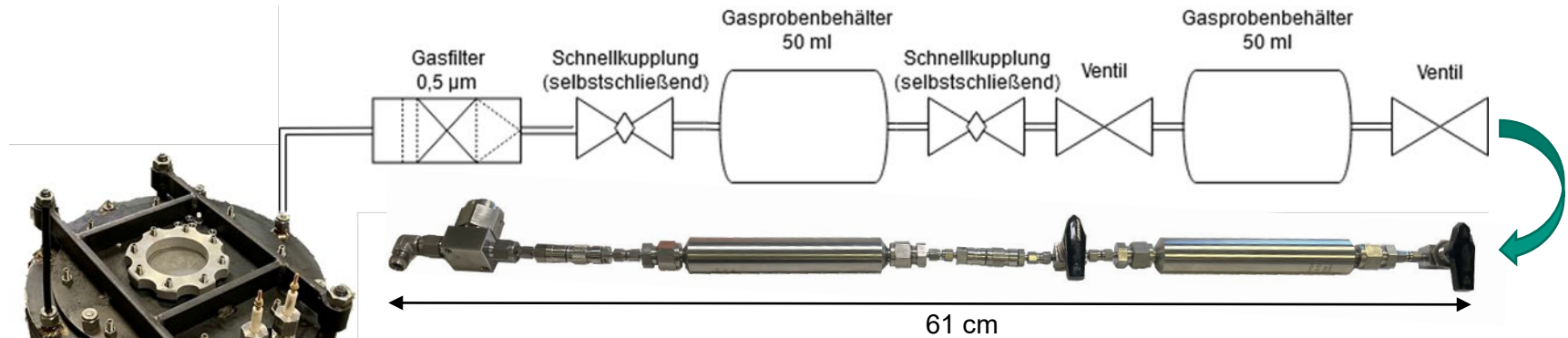
1.6 Ah 18650 cell



Internal pressure could be used in BMS for early prediction of processes leading to thermal runaway

B. Lei, W. Zhao, C. Ziebert, A. Melcher, M. Rohde, H.J. Seifert, *Batteries* 2017, 3, 14, [doi:10.3390/batteries3020014](https://doi.org/10.3390/batteries3020014).

# Gas collection after ARC Abuse-Tests



Large canister (20 l)  
for cells with up to 30 Ah (THT)



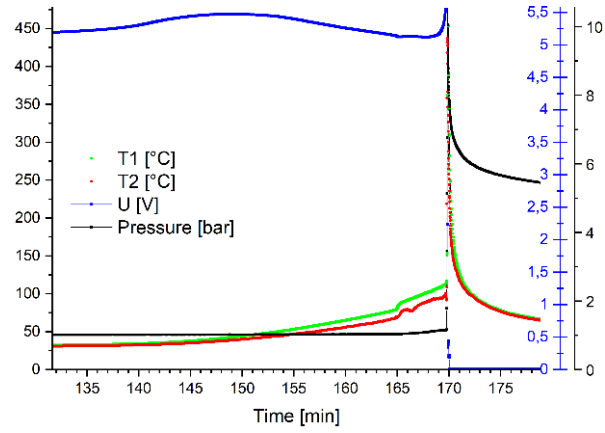
Large canister in EV+ ARC

- Collection option for gases through the Swagelok system
- Measurement of various parameters (two temperatures, pressure in the canister, voltage of the cell)
- Coupling to GC-MS Perkin-Elmer Clarus 690 Arnel 4019

# Gas analysis after 0.5 overcharge test of 14 Ah prismatic cell

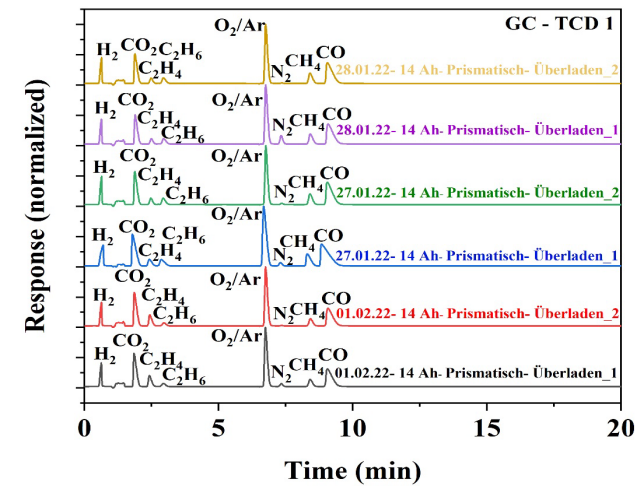


14 Ah prismatic cell

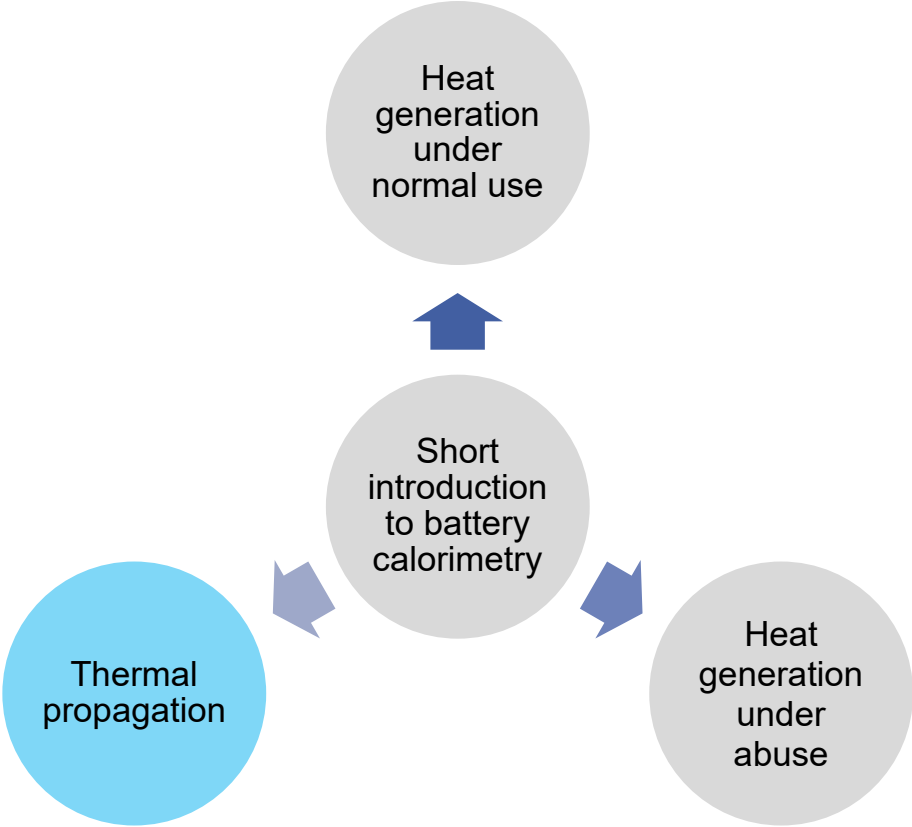


GC-MS Perkin-Elmer Clarus 690 Arnel 4019

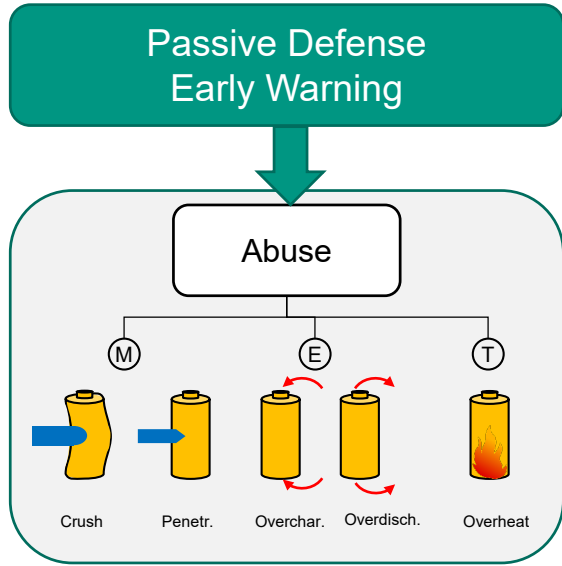
- Cell shows venting after 165 min and goes into thermal runaway after 170 min
- Data determined:
  - Maximum temperature: 534 °C
  - Maximum pressure: 12.5 bar
  - Evolved gas volume: 60 l (at 25 °C, 1013 mbar)



# Overview

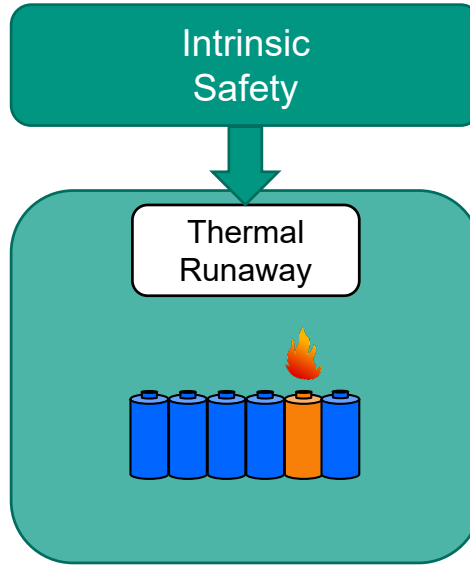


# Thermal propagation



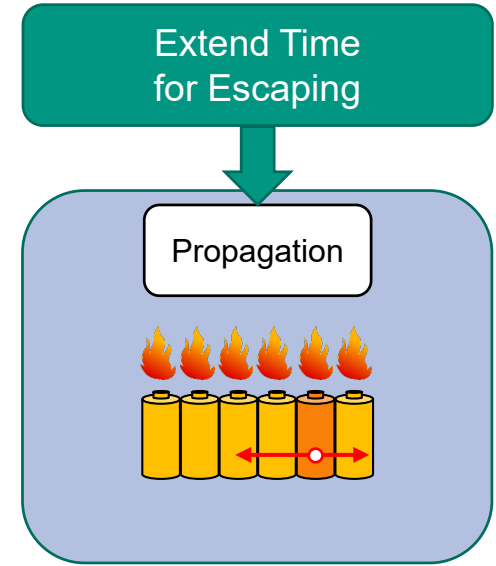
## Step 1 – BMS

Detection of mechanical, electric, thermal abuse



## Step 2 – Cell

Venting, CID, PTC

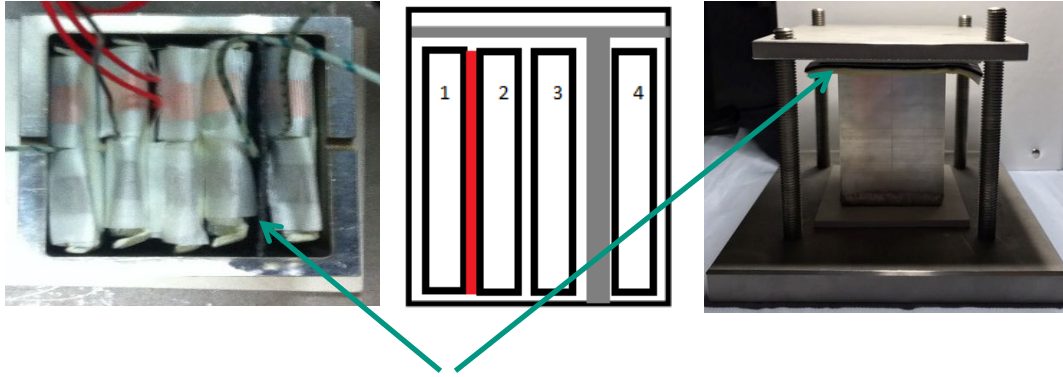


## Step 3 – Pack

Passive propagation prevention

Adapted from: Feng et al., Energy Storage Materials 10 (2018) 246

# Thermal propagation tests on small pack level

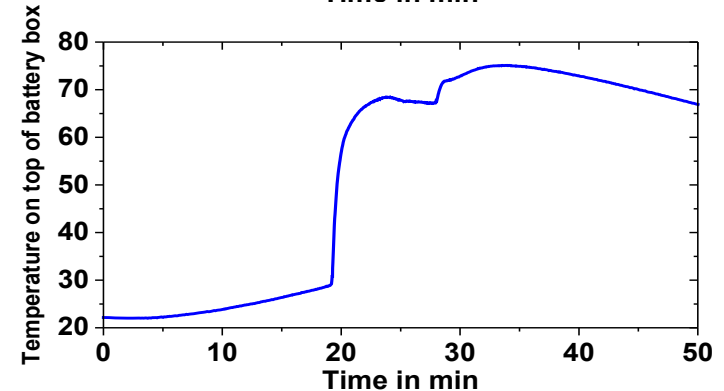
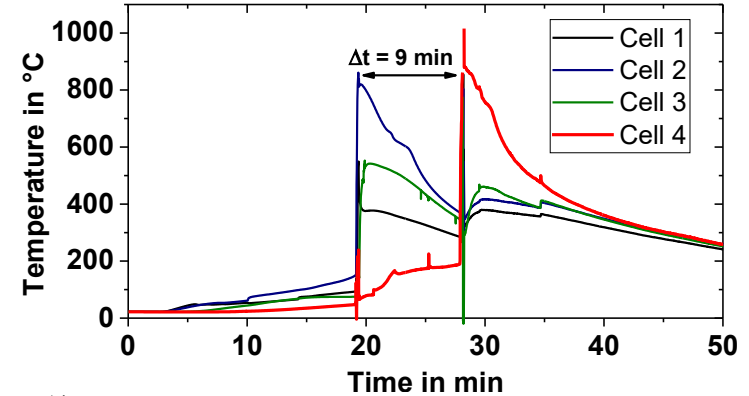


Gray: protective material for cell 4 and lid of battery box  
Red: heater mat for thermal runaway initiation

## Material qualification for propagation prevention

### Optimized Multilayer:

- Extended time for propagation: 9 min
- Improved heat protection: temperature on top of battery box < 80 °C during thermal runaway



# Summary: Possible calorimetric measurements

## Normal use conditions

- Isoperibolic or adiabatic measurements

- For each:**
- Measurement of temperature curve and temperature distribution during cycling (full cycles, or application-specific load profiles), ageing studies
  - Determination of the generated heat, Separation of heat in reversible and irreversible parts

## Abuse conditions

- Thermal abuse: Heat-wait-see test, ramp heating test, thermal propagation test
- Electrical abuse: External short circuit, Overcharge, Deep discharge
- Mechanical abuse: Nail penetration test

- For each:**
- Temperature measurement
  - External or internal pressure measurement
  - Gas collection and analysis, Post Mortem Analysis, Ageing studies



**Important data for BMS, TMS and safety systems**

# Acknowledgement

## Thank you for your attention!

### Contact data

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<https://www.iam.kit.edu/awp/169.php>

### We thank

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Bundesministerium  
für Bildung  
und Forschung



Projektträger Jülich  
Forschungszentrum Jülich



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