Mitteilung

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Experimental control of crossflow-dominated transition using 2-d AC-DBD plasma actuators

Marc T. Hehner^{1,3,4}, Srikar Yadala^{2,3}, Jacopo Serpieri³, Markus J. Kloker¹, Marios Kotsonis³

¹Institut für Aerodynamik und Gasdynamik, Universität Stuttgart, Pfaffenwaldring 21, D-70550, ²Insitut PPRIME, Université de Poitiers (CNRS UPR 3346, ISAE-ENSMA), Boulevard Marie et Pierre Curie, BP 30179, 86962 Futuroscope, France, ³AWEP Department, Section of Aerodynamics, Delft University of Technology, Kluyverweg 1, 2629 HS Delft, The Netherlands, ⁴Presently at Institut für Strömungsmechanik, Karlsruhe Institut für Technologie (KIT), Kaiserstraße 10, 76131 Karlsruhe, <u>marc.hehner@kit.edu</u>

Commercial airliners typically feature backward-swept wings that give rise to a threedimensional boundary-layer, exhibiting a highly unstable crossflow (CF) component. The CF functions perpendicular to the inviscid-flow streamline and provokes a crossflow instability (CFI) that dominates laminar-to-turbulent transition. Compared to laminar flow, turbulent flow increases the skin-friction drag of an aircraft significantly, resulting in a lack of fuel efficiency. The CFI is strongly dependent on the level of freestream turbulence and surface roughness, evolving in either stationary or traveling crossflow vortices (CFVs) (Wassermann & Kloker, 2002, 2003, Downs & White, 2013). The control method of Discrete Roughness Elements (DRE), generalized as Upstream Flow Deformation (UFD) by Wassermann & Kloker, 2002, triggers subcritical stationary CFVs that attenuate the growth of the naturally most unstable stationary CFI mode (Saric et al., 1998). Recently, DNS studies scrutinised the control performance of a body force, instilled into a three-dimensional boundary layer to reduce the CF component through base-flow manipulation, hence delaying transition (Dörr & Kloker, 2015b). Alternate-current dielectric-barrier-discharge (AC-DBD) plasma actuators retain the authority to exert such body forces (Yadala et al., 2018).



Figure 1: Forcing mechanism of base-flow manipulation with flow from the left (U_{∞}) . (a) Body force F_{-x} along -x. (b) Body force F_{+x} along +x. The exposed (grey) and encapsulated (orange) electrode and the DREs (black dots) are indicated.

In the current investigation base-flow manipulation with AC-DBD plasma actuators was performed on a 45-degree swept-wing boundary-layer flow for active control of CF-induced transition. The experimental campaign was carried out in the low-turbulence wind tunnel at Delft University of Technology. The wing model is a modified version of the NACA 66018, named 66018M3J, and was extensively validated (Serpieri & Kotsonis, 2015). In the experiments, transition is dominated by stationary

CFI. The AC-DBD plasma actuators were manufactured with a special spray-on technique to secure minimum surface roughness and were operated at 10kHz, inducing a spanwise uniform, two-dimensional body force (Yadala et al., 2018). The force directions, sketched in figure 1, were either partially against (-x) or along (+x)the local CF component (w_{ISL}). In addition, a row of DREs was spaced at the wavelength of the most unstable CFI mode, artificially promoting transition to turbulence with maximal impact (Yadala et al., 2018). Thus, this testing configuration constitutes the 'worst case scenario' for any given control scheme. Preliminarily, a simplified numerical model estimated a positive effect on the boundary-layer stability when forcing along -x and vice versa when forcing along +x. In the experiments infrared thermography was used to detect and quantify the transition-front locations. The results are shown in figure 2 that demonstrate the typical jagged transition-front pattern, suggesting that traveling CFI modes were of minor importance (Downs & White, 2013). A significant, well-defined transition delay of about 4.5% of chord is observed. The subtraction in figure 2 (c) visualizes the transition delay as a white toothed area. As expected, forcing along +x promotes the CF and thus advances the transition (figure 2 (d) to (f)). This study presents the first experimental demonstration of sweptwing transition delay via base-flow manipulation with AC-DBD plasma actuators.



Figure 2: IR thermography time-averaged fields for $U_{\infty}=25\text{ms}^{-1}$ ($Re_{\infty}=2.08\cdot10^6$). The flow comes from the left. The x-scale of the deskewed images is projected on z/c=0. (a) to (c) from left to right: No forcing, -x forcing, subtraction of (a) from (b). (d) to (f) from left to right: No forcing, +x forcing, subtraction of (d) from (e).

References

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