

The Status of The KIT Contribution to The Rostov-2 VVER-1000 Multi-Physics Transient Benchmark

Nuri Beydogan

nuri.beydogan@partner.kit.edu

INSTITUTE for NEUTRON PHYSICS and REACTOR TECHNOLOGY (INR)



Outline

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- Comparison of SSS2/SCF and PARCS Results
- Conclusion and Outlook

Objectives

- Core analysis with improved neutronic methodologies to account for increased heterogeneity and complex material composition.
 - **Use of high-fidelity Serpent2(SSS2)/Subchanflow(SCF)* for the analysis of VVER-cores.**
 - **Use of PARCS/SCF and TRACE/PARCS for 3D Nodal Core analysis.**
- Provide a reference solution for Rostov-2 Benchmark** Phase I with high-fidelity **pin-by-pin SSS2/SCF.**
- Development of the detailed model for the begin-of-cycle (BOC) Rostov-2 VVER-1000 **fresh-core.**

* Diego Ernesto Ferraro. 2021. Monte Carlo-based multi-physics analysis for transients in Light Water Reactors. PhD thesis, Karlsruhe Institute of Technologie (KIT), Karlsruhe, GERMANY

** M. Avramova, K. Ivanov, K. Velkov, S. Nikonov, P. Gordienko, B. Shumskiy and O. Kavun, "Benchmark on reactivity compensation of boron dilution by stepwise insertion of control rod cluster into the VVER-1000 core, Specifications and Support Data, Version 1.6," OECD/NEA. NEA/EGMPEBV/DOC(2021), Paris, 2021.

Tools

The master-slave SSS2/SCF coupling

Main aspects:

- Codes are integrated in a single tool.
- Interchange of fields internally by memory.
- Coupled flow control managed by master code SSS2.

CASMO5

- 2D lattice neutronic behavior analysis code.

PARCS: Purdue Advanced Reactor Core Simulator

- 3D multi group neutron diffusion solver code.

Rostov-2 VVER 1000 Core (1/2)

BOC Characteristics

■ Core loading at BOC (Date: 20.02.2010)

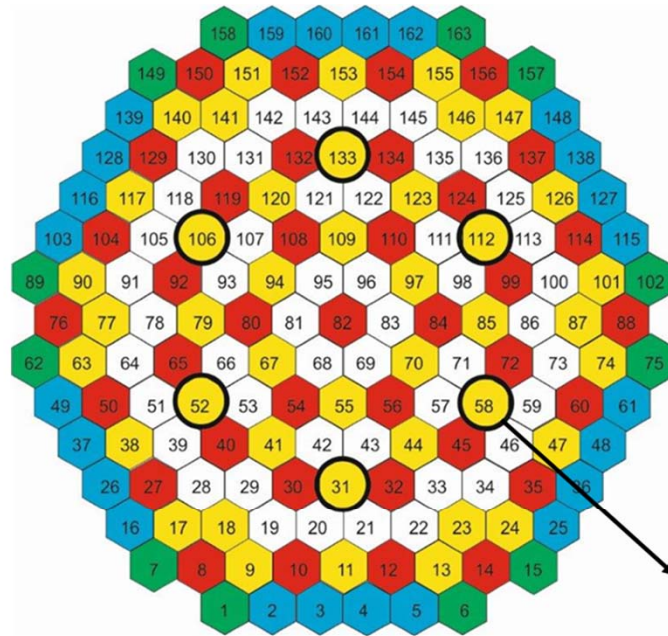
- Effective day (TEF)= 0.0
- Fuel Assemblies: 163 FAs with 5 different types loaded
- Control Assemblies: 10 CR group banks located in 61 FAs
 - Control Rod position: CR group 1-9 out and only CR group 10 72.9% (from core bottom) inserted
- Boric Acid concentration: 6.5 g/kg
 - Boric Acid (H_3BO_3) density= 1.435 g/cm³






■ Thermal-hydraulic parameters at BOC

- Core power= 44.4 MW
- T_{inlet} = 552.95 K
- System Pressure= 15.7 MPa
- Total circuits mass flow rate (100% total flow)=87342.7 m³/h (18558.29 kg/s)
 - Core mass flow rate (97% of the total mass circuit flow) =18001.53 kg/s

Rostov-2 VVER 1000 Core (2/2)

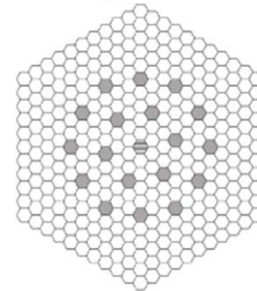
Core Loading






-  FA type U39A9 with Uranium-235 3.89% average enrichment (243 fuel rods with 4.0% enrichment, 60 fuel rods with 3.6% enrichment, 9 fuel rods with Gd with 3.3% enrichment, content of Gd2O3 – 5%)
-  FA type U30Y9 with Uranium-235 2.98% average enrichment (303 fuel rods with 3.0% enrichment, 9 fuel rods with Gd with 2.4% enrichment, content of Gd2O3 – 8% by weight)
-  FA type U39B6 with Uranium-235 3.9 % average enrichment (240 fuel rods with 4.0% enrichment, 66 fuel rods with 3.6 % enrichment, 6 fuel rods with Gd with 3.3% enrichment, content of Gd2O3 – 5%)
-  FA type U22 with Uranium-235 2.2% enrichment
-  FA type U13 with Uranium-235 1.3% enrichment

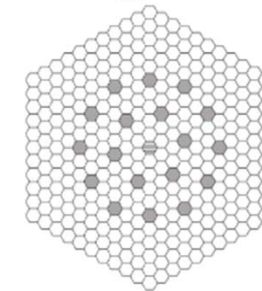
Fuel-loading map of the reactor core of Rostov Unit 2, Cycle 1




FA type U13



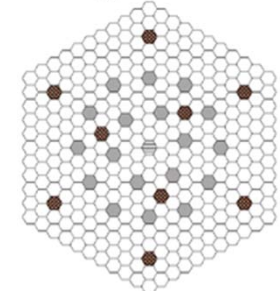
-  Fuel element with enrichment 1.3%
-  Control channel
-  Central tube





FA type U22



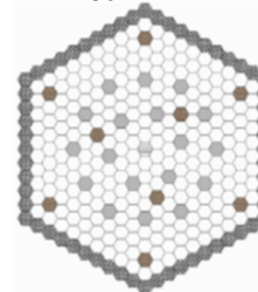
-  Fuel element with enrichment 2.2%
-  Control channel
-  Central tube






FA type U30Y9



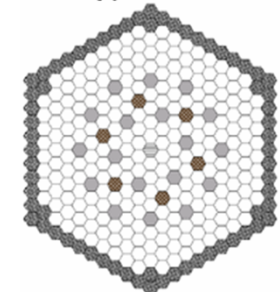
-  Fuel element with enrichment 3.0 %
-  Control channel
-  Gadolinium element (x = 2.4 %, e = 8 %)
-  Central tube






FA type U39A9



-  Fuel element with enrichment 4.0 %
-  Control channel
-  Gadolinium element (x = 3.3 %, e = 5 %)
-  Fuel element with enrichment 3.6 %
-  Central tube

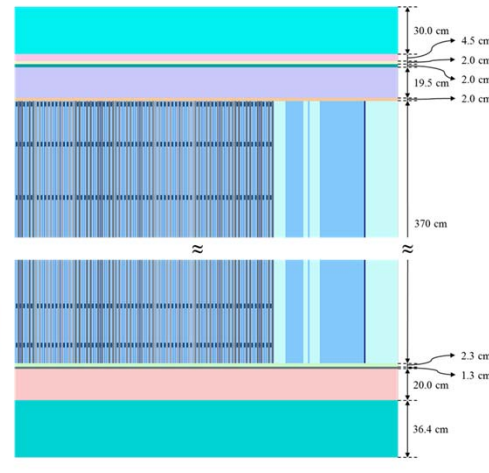
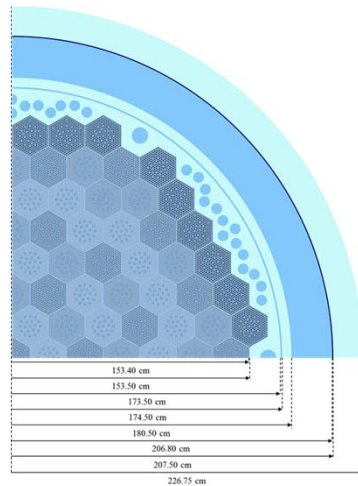
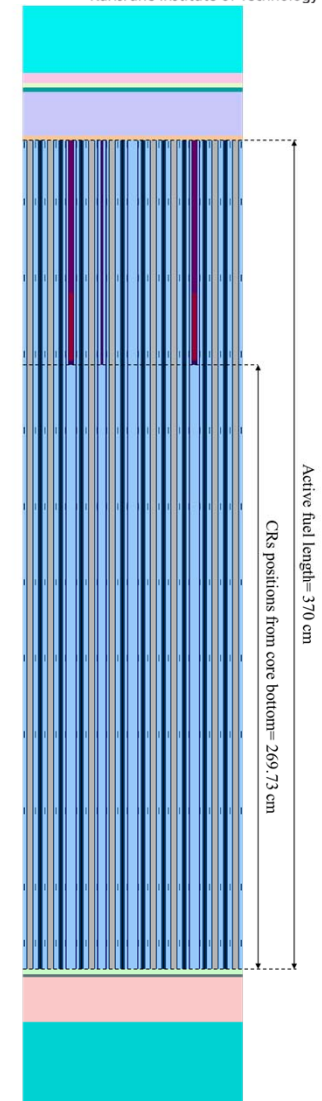
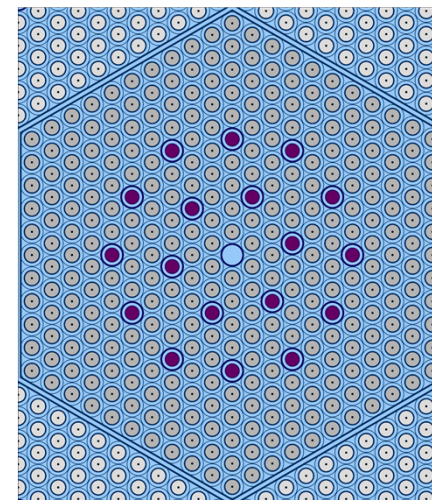
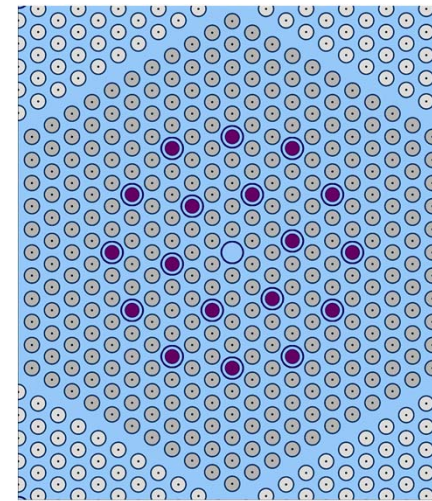
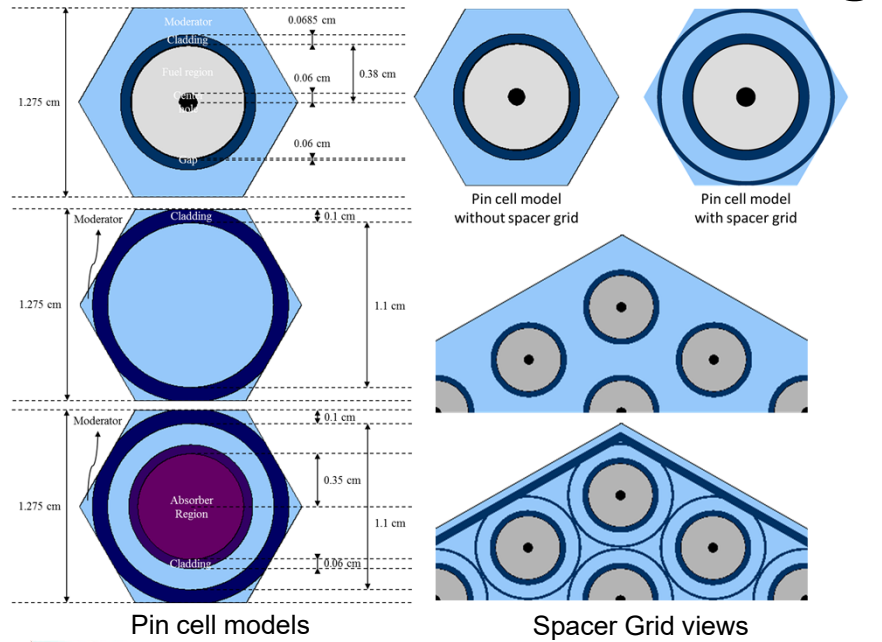
FA type U39B6



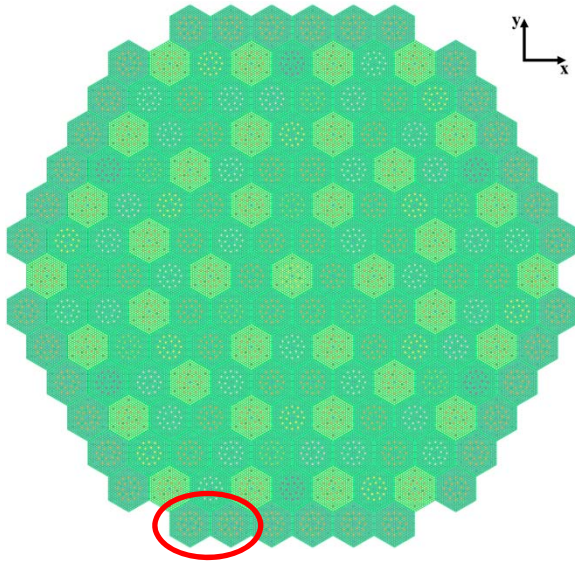
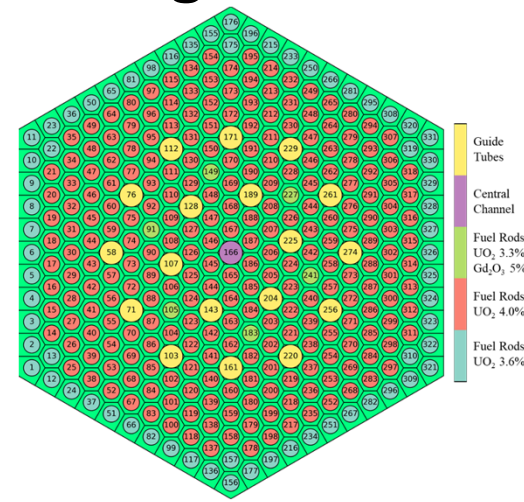
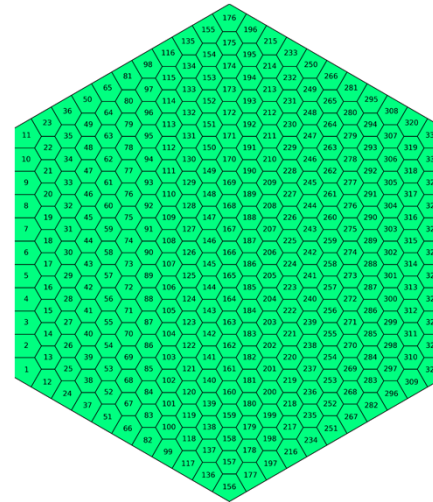
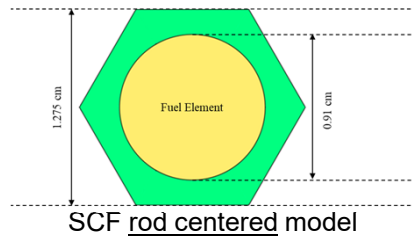
-  Fuel element with enrichment 4.0 %
-  Control channel
-  Gadolinium element (x = 3.3 %, e = 5 %)
-  Fuel element with enrichment 3.6 %
-  Central tube

Radial arrangement of elements in the fuel assemblies

SSS2 Pin Level Core Modeling



SCF Sub-channel Level Core Modelling



SCF FA model - channel indexing

SCF FA model - rod indexing

- Python based preprocessor was used to generate rod and channel layout and connectivity relations and "ifc" files for code feedback exchange.

SSS2/SCF Criticality Simulation Features

➤ Serpent 2

- Serpent 2 Version 2.1.32
- Active cycle and inactive cycle: **5000** and **500**, respectively
- Particle number: **10,000,000**
- **tft** temperature card option for the multi-physics calculations
- **ifc** used files for multi-physics interface
- ENDF/B-VII neutron library

➤ Subchanflow

- SCF Version 3.7.1
- VVER-specific thermophysical properties in SCF was used.
- Axially **30** nodes
- Doppler temperature predicted as in benchmark formulation.

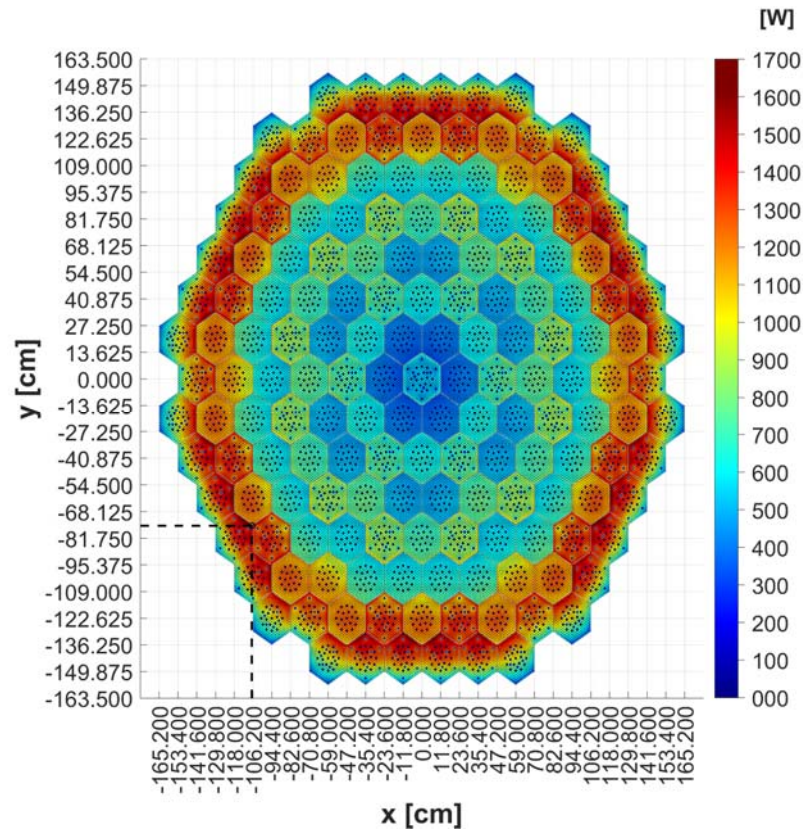
➤ Simulation Architecture

- 100 OpenMPI node and 152 OpenMP task for the coupled simulation on HoreKa HPC (KIT/SCC).
 - Intel Xeon Platinum 8368
- Convergence criteria:
 - rho : **5 pcm**
 - Fuel Temperature: **5 K**
 - Coolant Temperature: **5 K**
 - Coolant Density: **0.001 g/cm³**

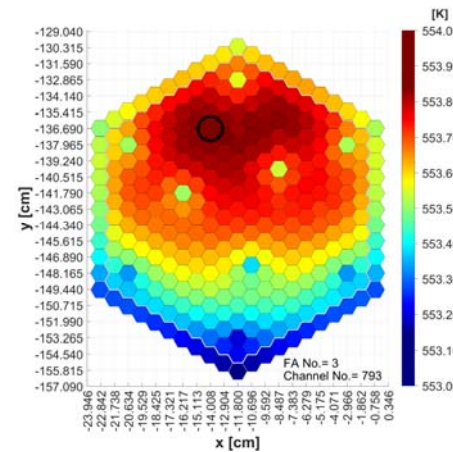
SSS2/SCF Core Analysis

Global Results and Local Results

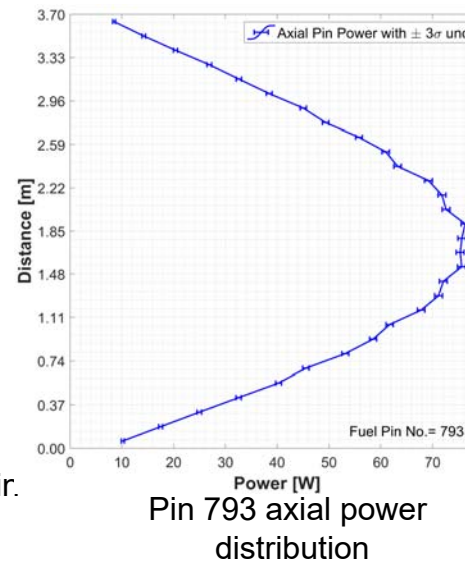
$k_{\text{effective}}$	0.997860 ± 0.0000029
ρ_{initial}	-214.5 pcm



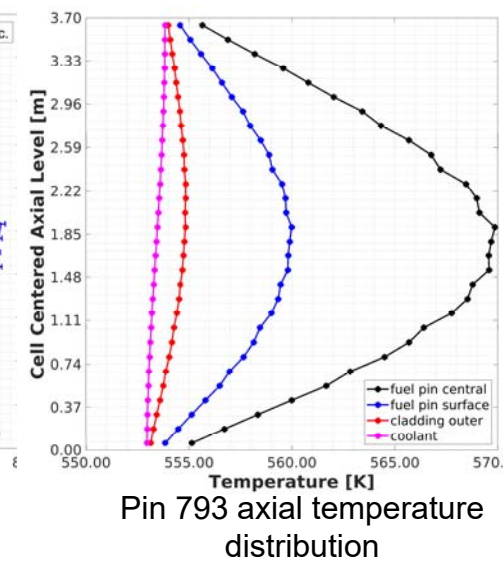
Pin power distribution in the core with the location of the pin with the highest power: FA number 26, pin number 8606



Sub-channel level coolant exit temperature distribution and Pin-level power distribution in the FA No. 3 and the sub-channel location which has the hottest coolant exit temperature



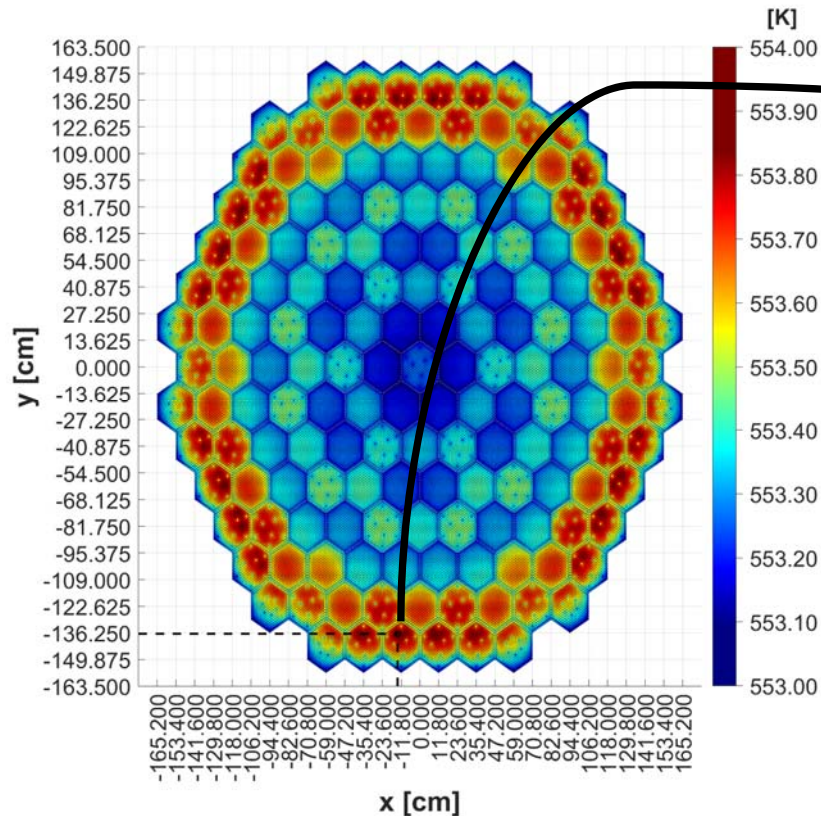
Pin 793 axial power distribution



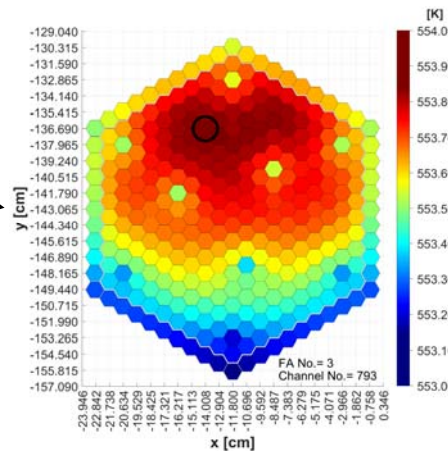
Pin 793 axial temperature distribution

SSS2/SCF Core Analysis

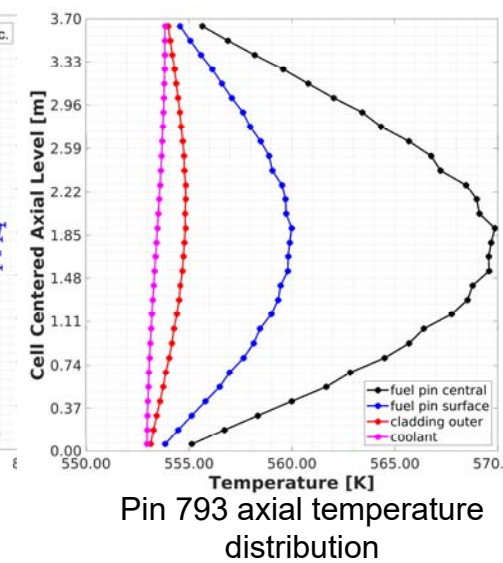
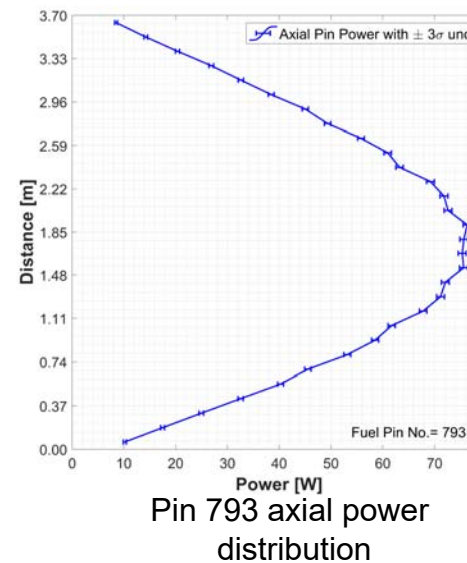
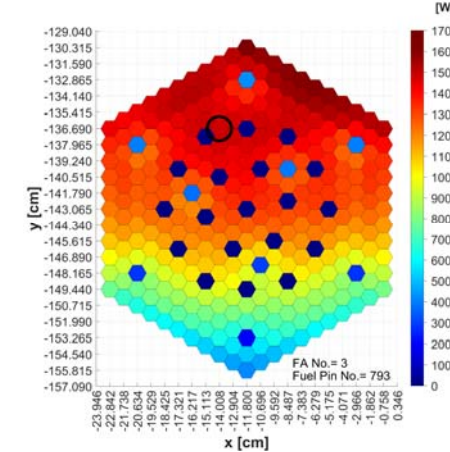
Local Results



Sub-channel level coolant exit temperature distribution in the core and the sub-channel location which has the hottest coolant exit temperature

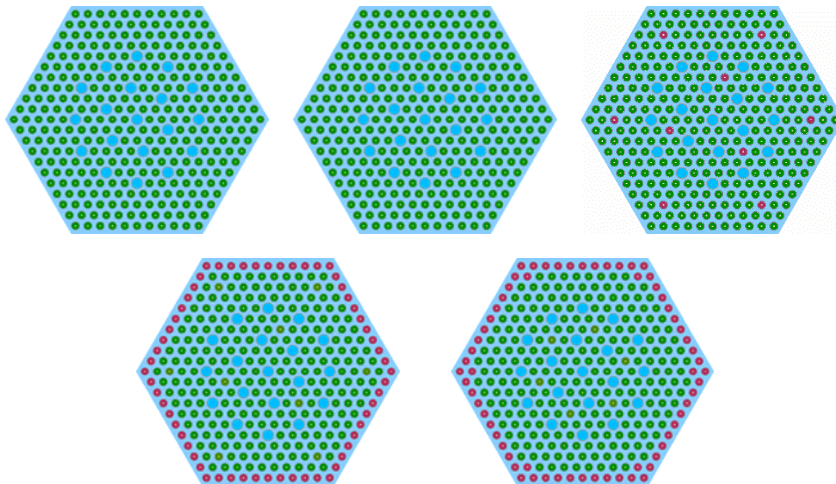


Sub-channel level coolant exit temperature distribution and Pin-level power distribution in the FA No. 3 and the sub-channel location which has the hottest coolant exit temperature

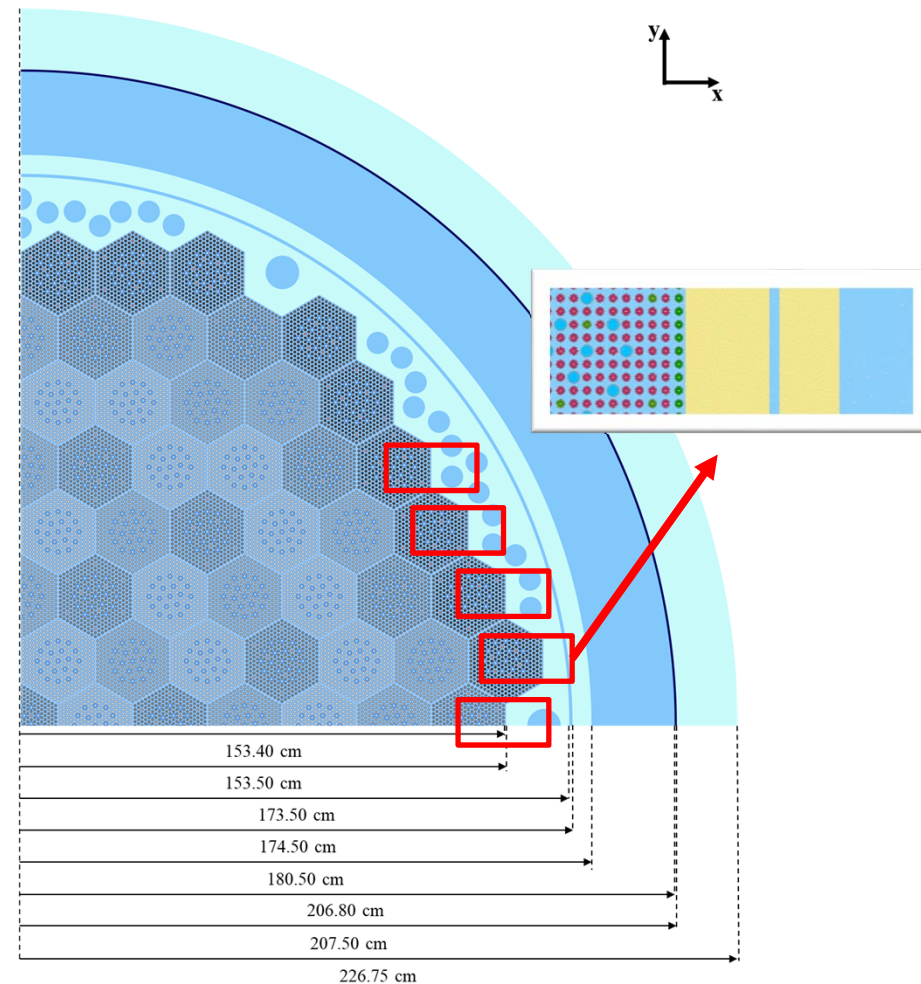


CASMO5 FA MODELS

- CASMO5 Figures of FAs Models respectively: U13, U22, U30Y9, U39A9, U39B6



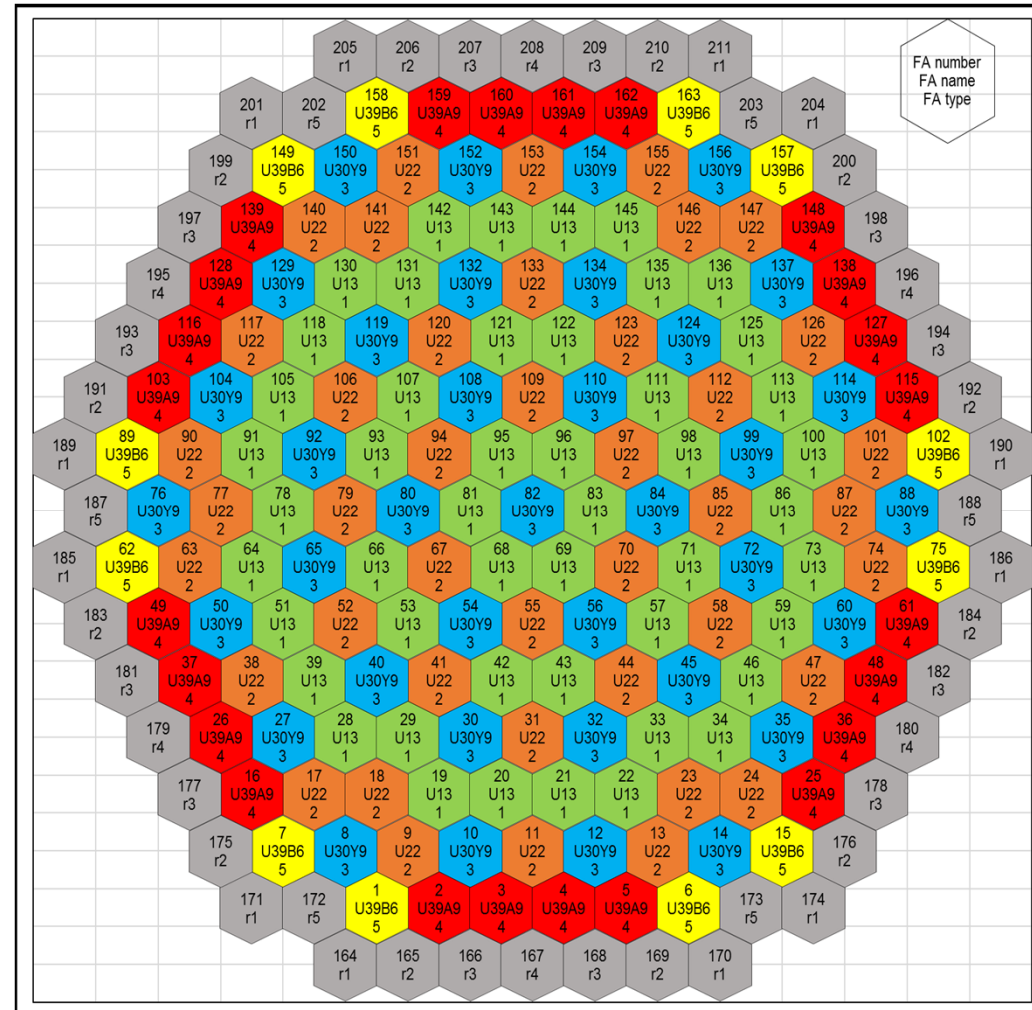
- 2D FAs Models, which were utilized to XS generation, were developed corresponds to the benchmark specification and SSS2 FAs models.



- 1D model for 5 radial reflector assemblies
- 1D model for top and bottom refl. assembl.

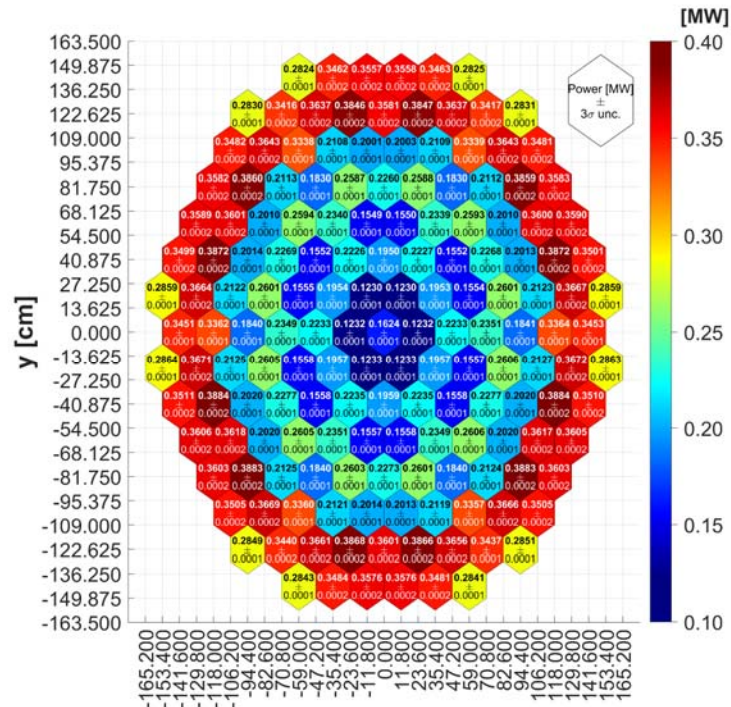
PARCS MODEL

- PARCS Version 3.3.1
- Internal TH feedback (Simple mass/energy solution)
- 2 energy groups
- 5 different FAs models
- 5 different radial and 2 top and 2 bottom reflector assemblies models
- 30 axial nodes

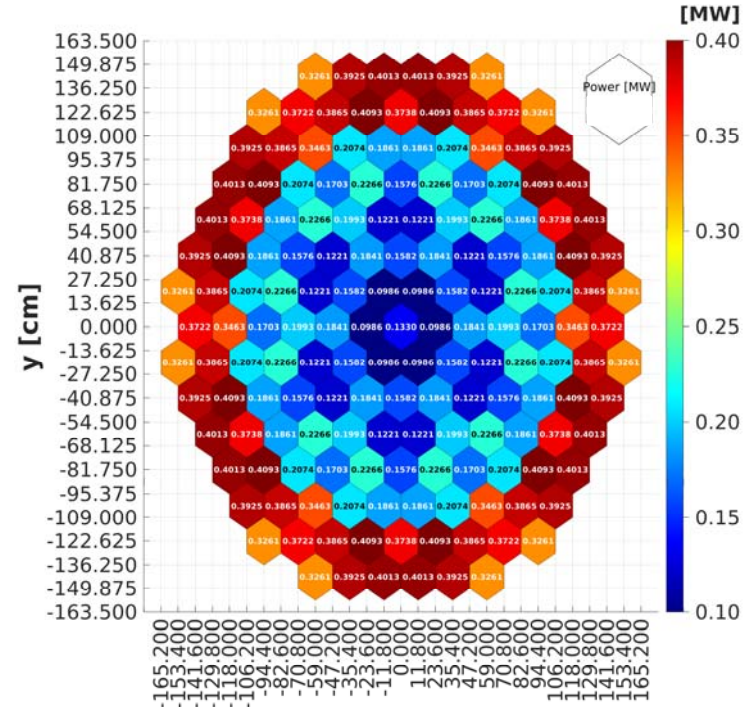


Comparison of SSS2/SCF and PARCS Results (1/2)

	$k_{\text{effective}}$
SSS2/SCF	0.997860 ± 0.0000029
PARCS standalone	0.997889
difference	2.9 pcm



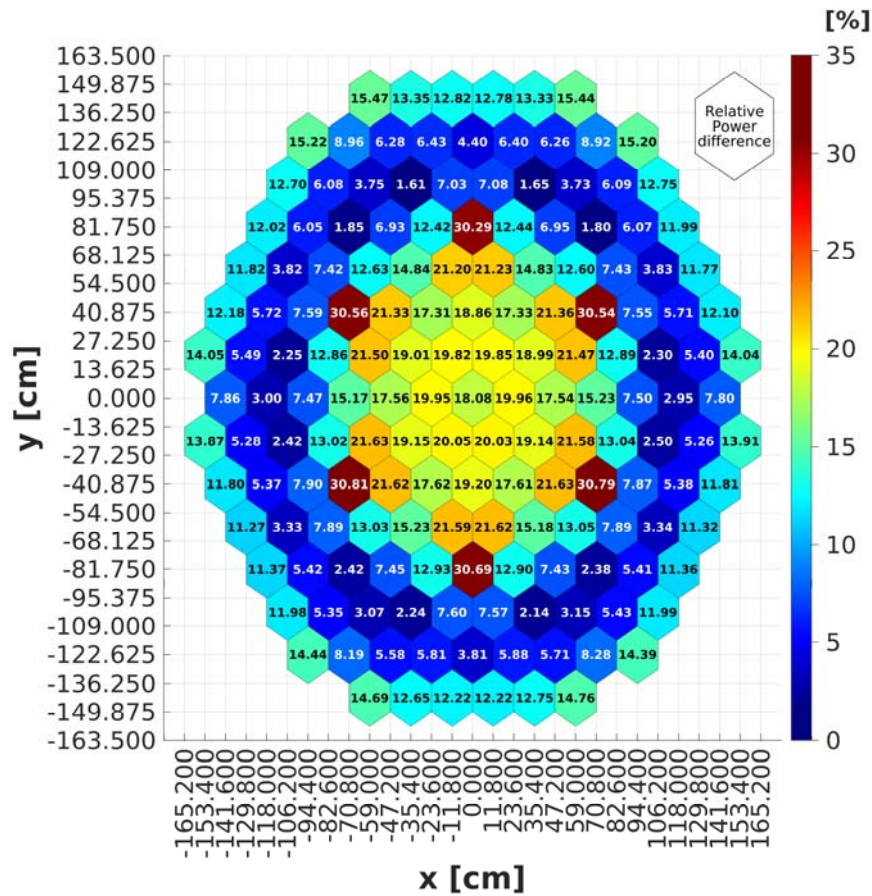
SSS2/SCF Radial view of FA level average power distribution



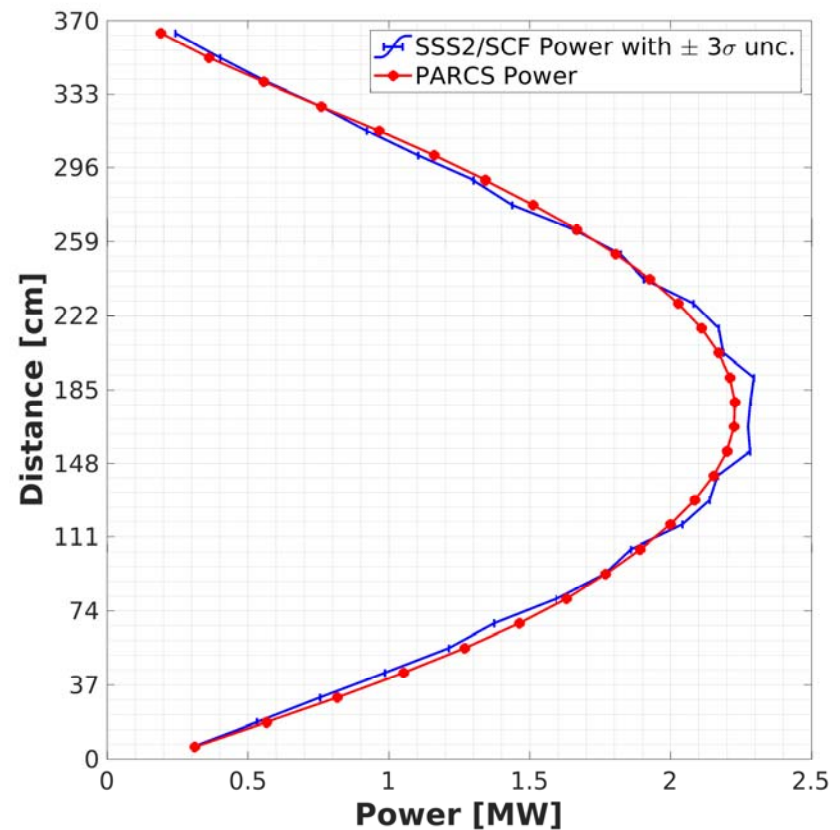
PARCS Radial view of FA level average power distribution

Comparison of SSS2/SCF and PARCS Results (2/2)

- SSS2/SCF Neutronic and TH results and preliminary PARCS standalone Neutronic and TH results



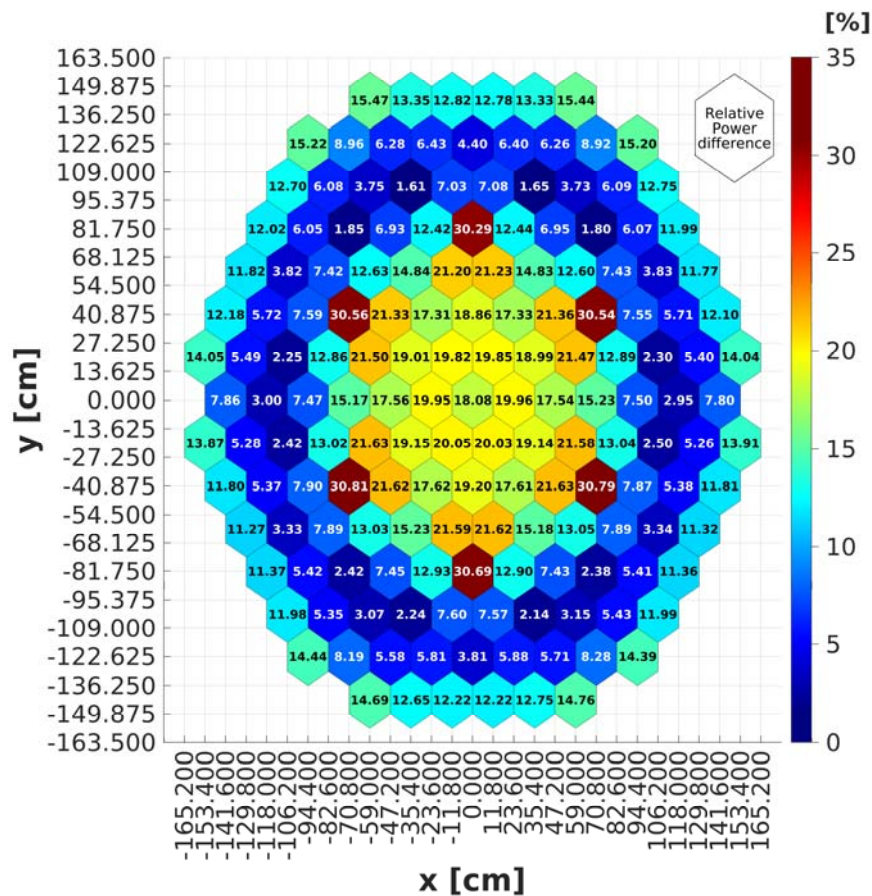
SSS2/SCF and PARCS FA level relative power difference



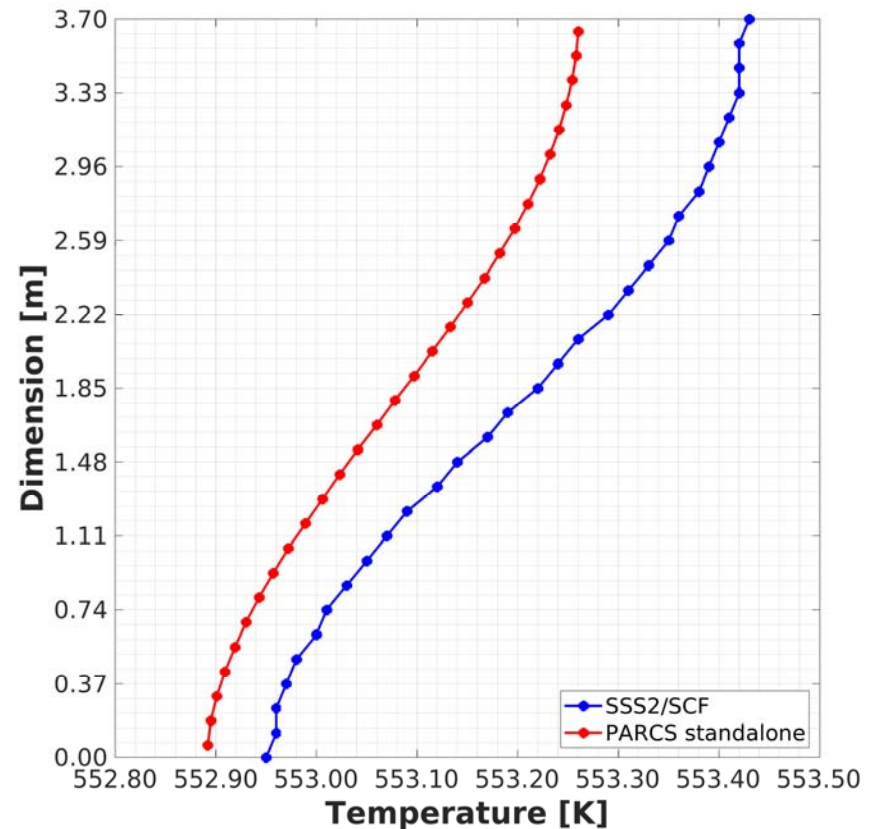
Core average axial power distribution

Comparison of SSS2/SCF and PARCS Results (2/2)

- SSS2/SCF Neutronic and TH results and preliminary PARCS standalone Neutronic and TH results



SSS2/SCF and PARCS FA level relative power difference



Core average axial coolant temperature distribution

Conclusion and Outlook

- Master-slave SSS2/SCF coupling works fine and stable.

- $k_{\text{effective}}$ results of the SSS2/SCF and PARCS standalone are compatible.
 - PARCS model will be improved to decrease the differences between SSS2/SCF and PARCS results.

- Next Steps:
 - Use of PARCS/SCF and TRACE/PARCS for 3D Nodal Core analysis
 - PARCS/SCF simulation will be carried out to analysis the BOC SS core condition and depletion of the core.

 - SSS2/SCF burnup simulation of Rostov-2 first cycle is still on going.

Thank you for your attention!