

3D modeling of stack-type superconducting magnetic bearings

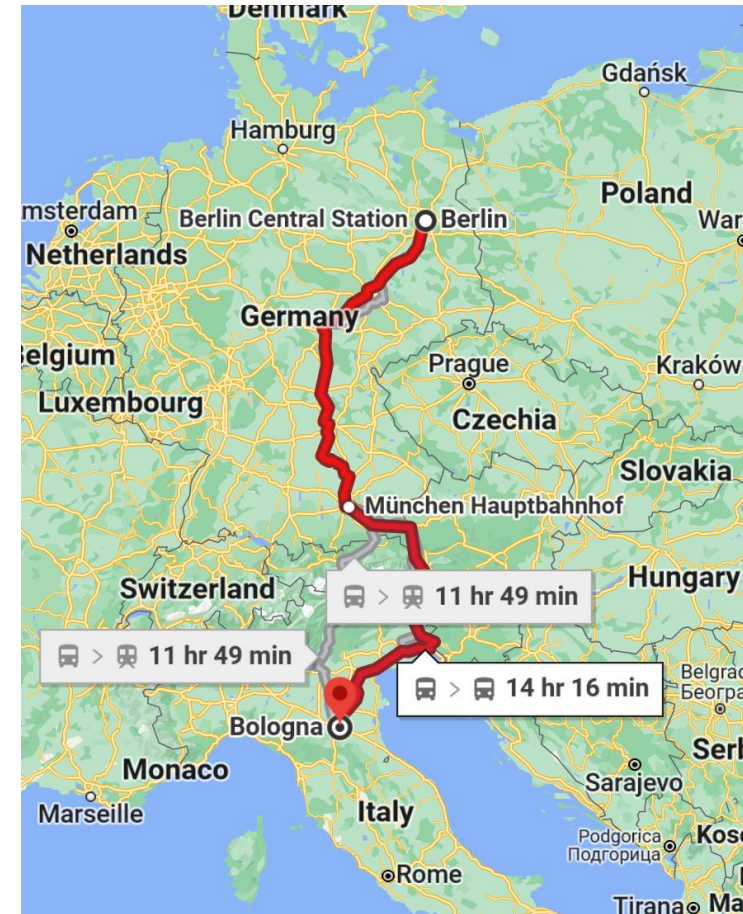
**Asef Ghabeli, Francesco Grilli, Jens Hänisch
Günter Fuchs, Oliver de Haas, Pengbo Zhou**

Maximum speed of 603 km/h!



Yamanashi: Japanese low- T_c superconducting maglev train

In 2 hours
instead of 12 hours!



Superconducting tape stack

Superconducting bulk



Advantages of tape stacks over bulks

- Better mechanical properties
- Better thermal conductivity
- Possibility of having more flexible configurations
- Higher engineering J_c and levitation force
- Possibility of increasing engineering J_c by reducing thickness of tape

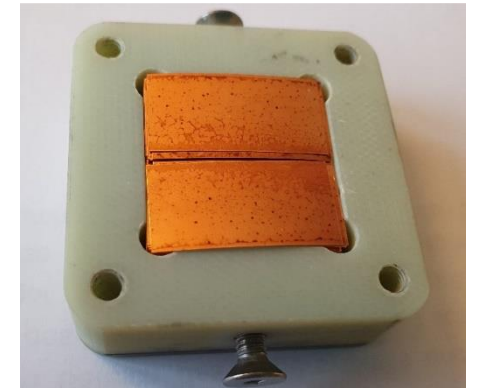


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■ Summary

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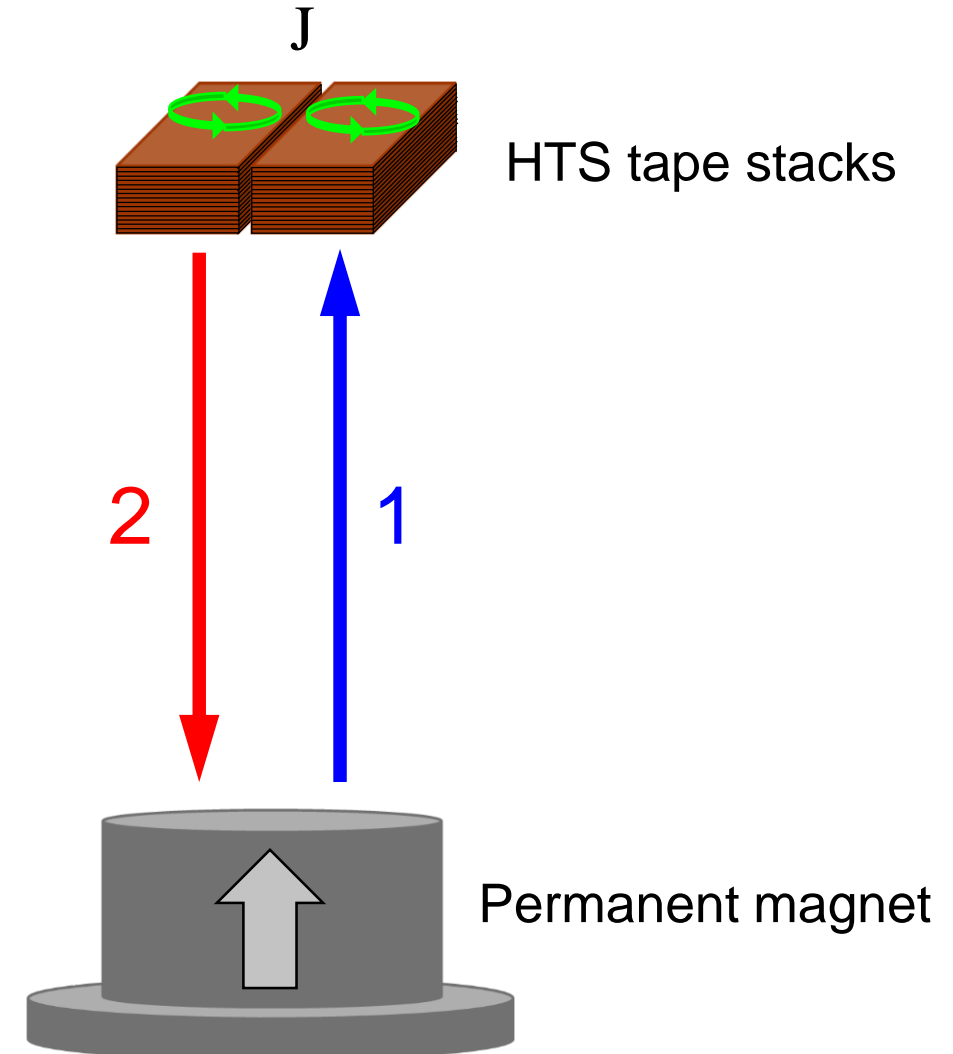
■ Summary

Calculation of levitation force

$$\mathbf{F} = \int_{\Omega} \mathbf{J} \times \mathbf{B} d\Omega$$

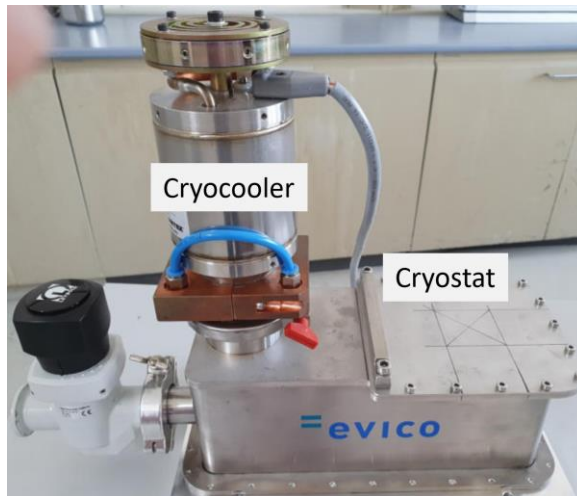
Lorentz force

between field of permanent magnet
& magnetization current in tape stacks



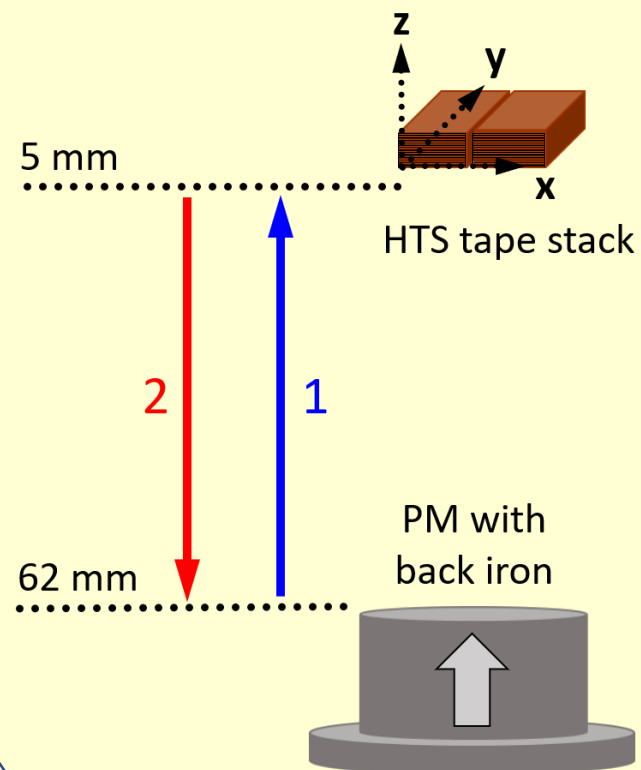
Studying different cases at different temperatures

$$\mathbf{F} = \int_{\Omega} \mathbf{J} \times \mathbf{B} d\Omega$$

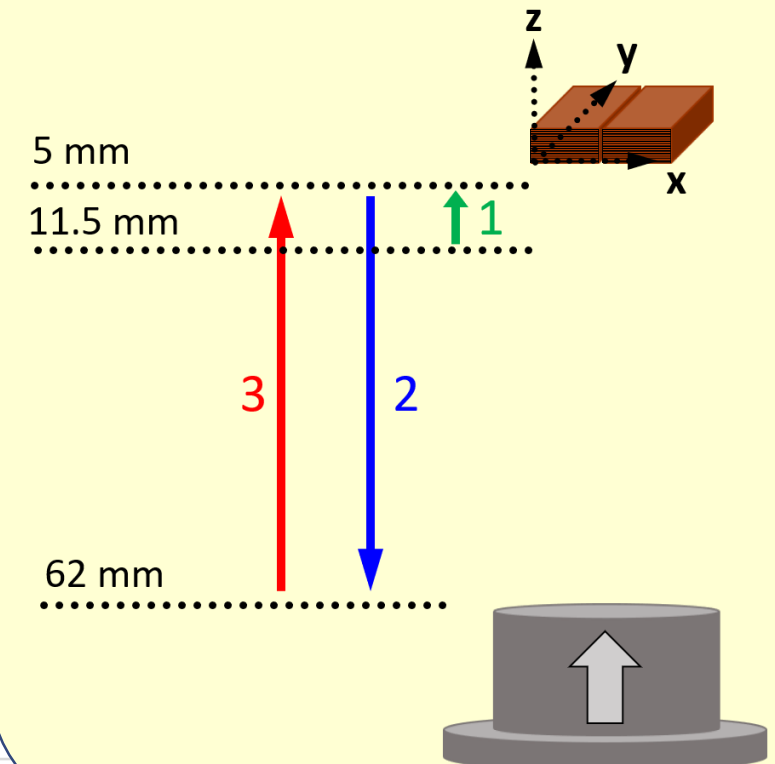


57 K < Temperatures < 77 K

Zero Field cooling

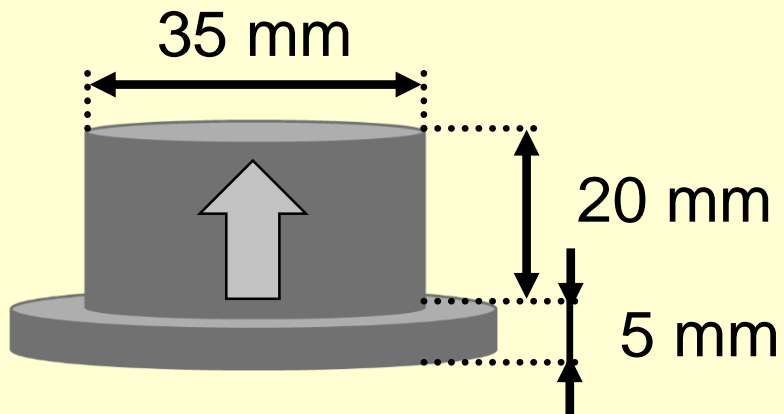


Field cooling



Input parameters

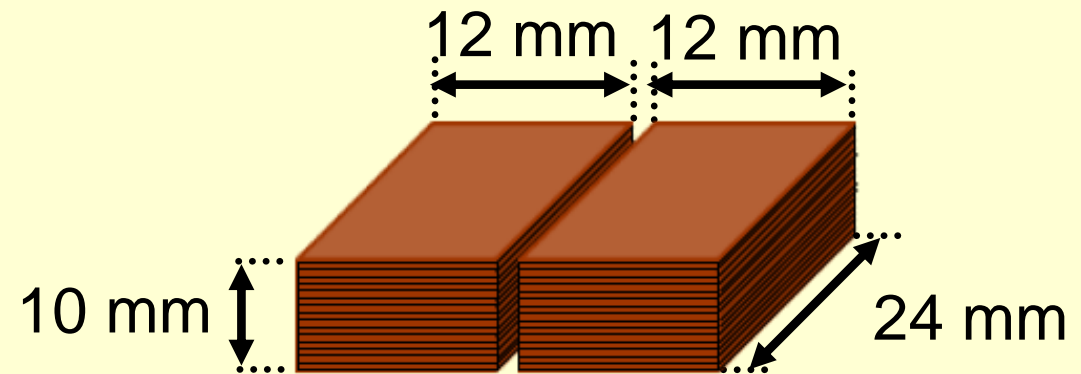
Cylindrical magnet with back iron



Remanent flux density (B_r) = 1.35 T

Magnet movement speed = 10 mm/s

HTS tape stacks



No. of tapes in each stack: 132

Self-field critical current = 400 A

n-value = 29

Minimum Electromagnetic Entropy Production method (MEMEP 3D)

Initially developed by **Milan Kapolka** and **Enric Pardo**
Institute of Electrical Engineering, Slovak Academy of Sciences



Variational method based on **T**-formulation

A vector potential \longrightarrow calculated analytically

$$\nabla \times \mathbf{T} = \mathbf{J}$$

\swarrow
effective magnetization

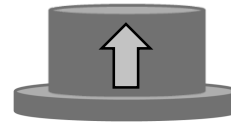
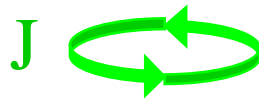
$$L = \int_V dv \left[\frac{1}{2} \frac{\Delta \mathbf{A}_J}{\Delta t} \cdot (\nabla \times \Delta \mathbf{T}) + \frac{\Delta \mathbf{A}_M}{\Delta t} \cdot (\nabla \times \Delta \mathbf{T}) + U(\nabla \times \mathbf{T}) \right]$$

known variables unknown variable

Minimum Electromagnetic Entropy Production method (MEMEP 3D)

\mathbf{A} vector potential \longrightarrow calculated analytically

$$\nabla \times \mathbf{T} = \mathbf{J}$$



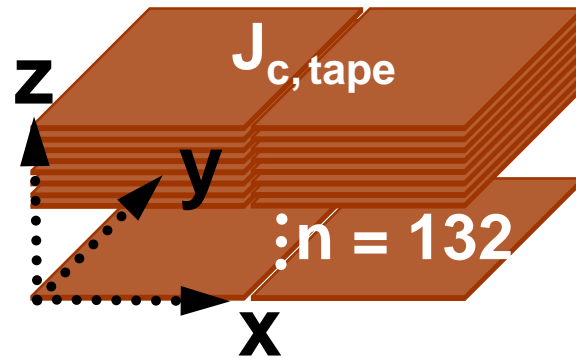
Dissipation factor
(E-J power law)

$$L = \int_V dv \left[\underbrace{\frac{1}{2} \frac{\Delta \mathbf{A}_J}{\Delta t} \cdot (\nabla \times \Delta \mathbf{T})}_{\text{Current term}} + \underbrace{\frac{\Delta \mathbf{A}_M}{\Delta t} \cdot (\nabla \times \Delta \mathbf{T})}_{\text{Magnetic field term}} + \underbrace{U(\nabla \times \mathbf{T})}_{\text{Dissipation factor (E-J power law)}} \right]$$

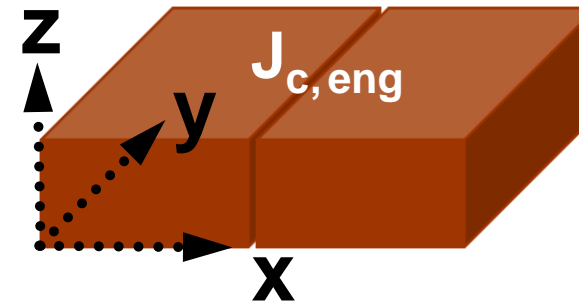
Minimum of this equation in each time step is
the unique solution of Maxwell differential equation

Homogenization process

HTS tape stacks



Homogenized Bulks



Current flows only in **x** and **y** directions

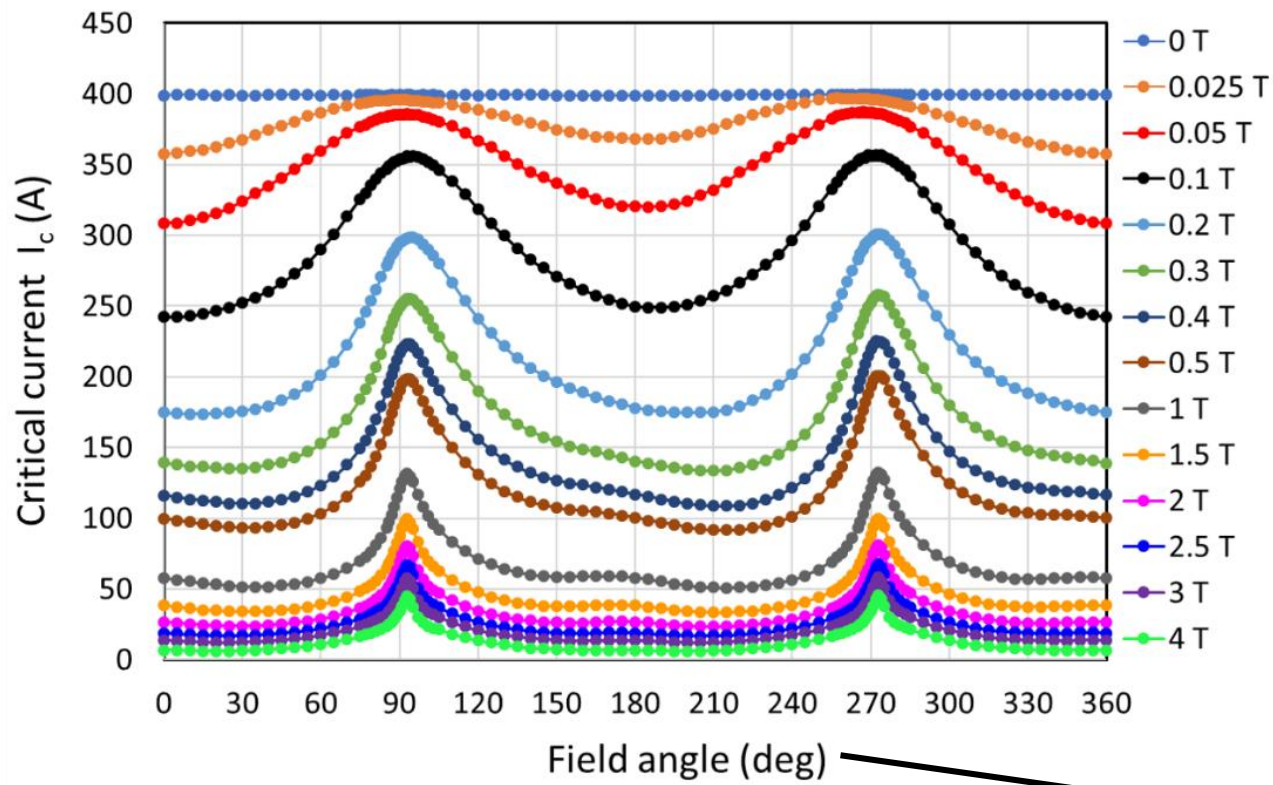
$$J_{c,eng} = n \times \frac{\delta}{\Delta_{bulk}} J_{c,tape}$$

Thickness of SC layer

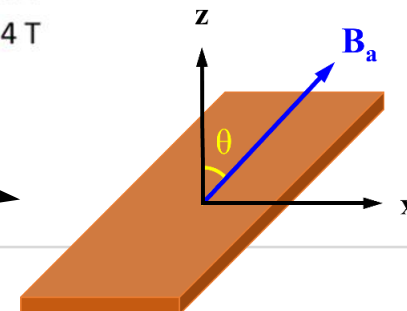
Height of bulk

SuperOx tape $I_c(B, \theta)$ measurement

$T = 77\text{ K}$

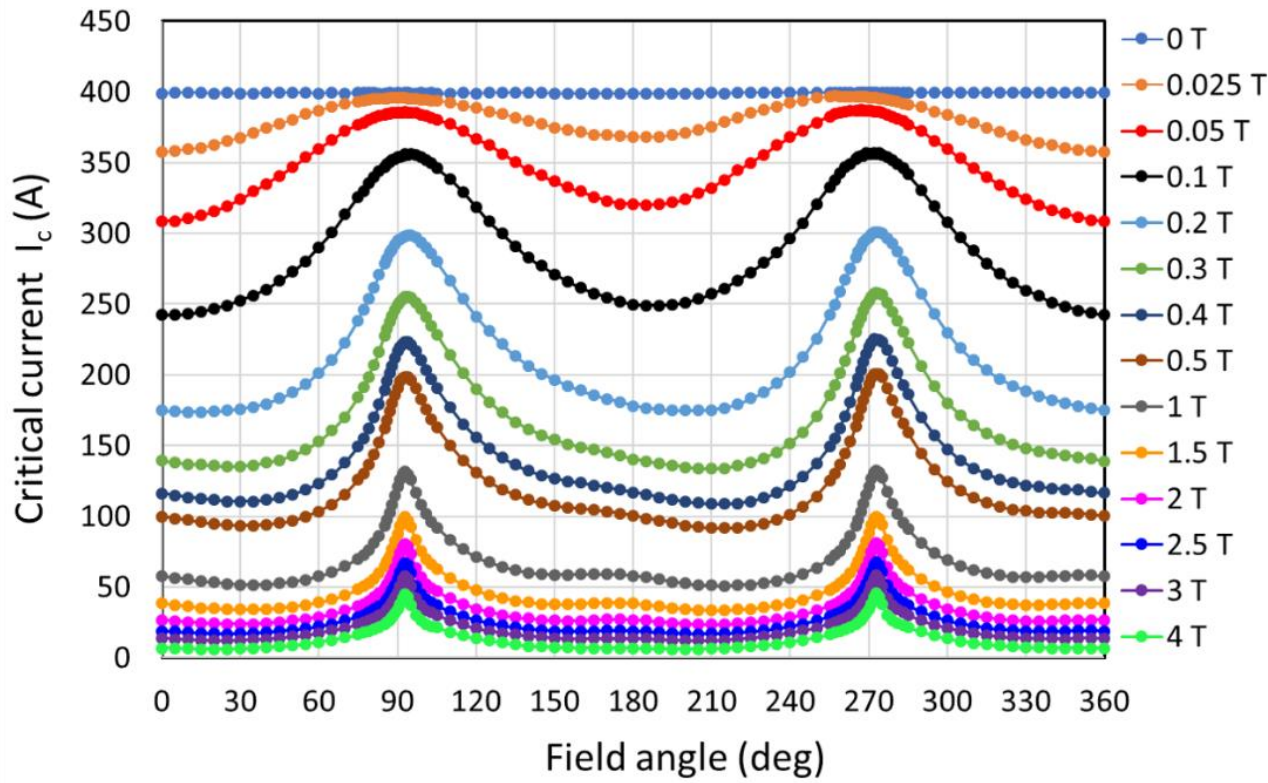


Data was measured by
SuperCurrent facility in



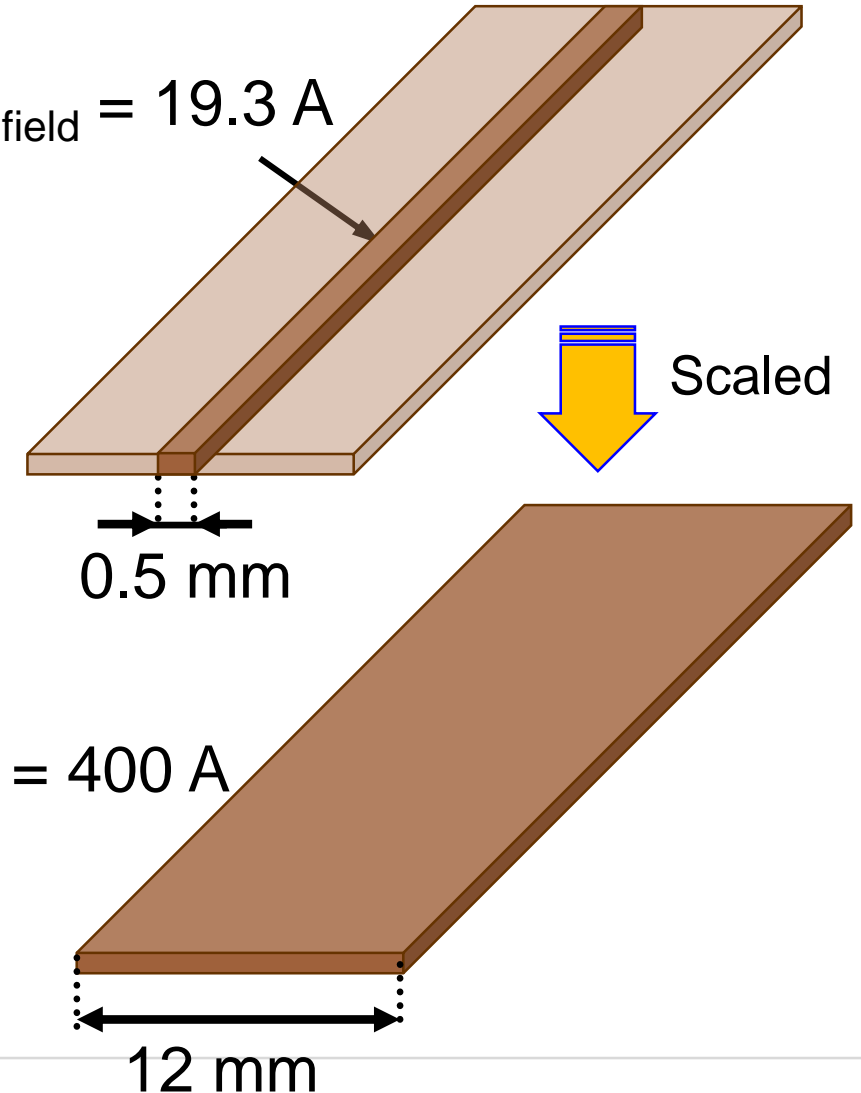
Scaling the data is necessary

Scaled data to a second measurement on whole 12 mm width of tape

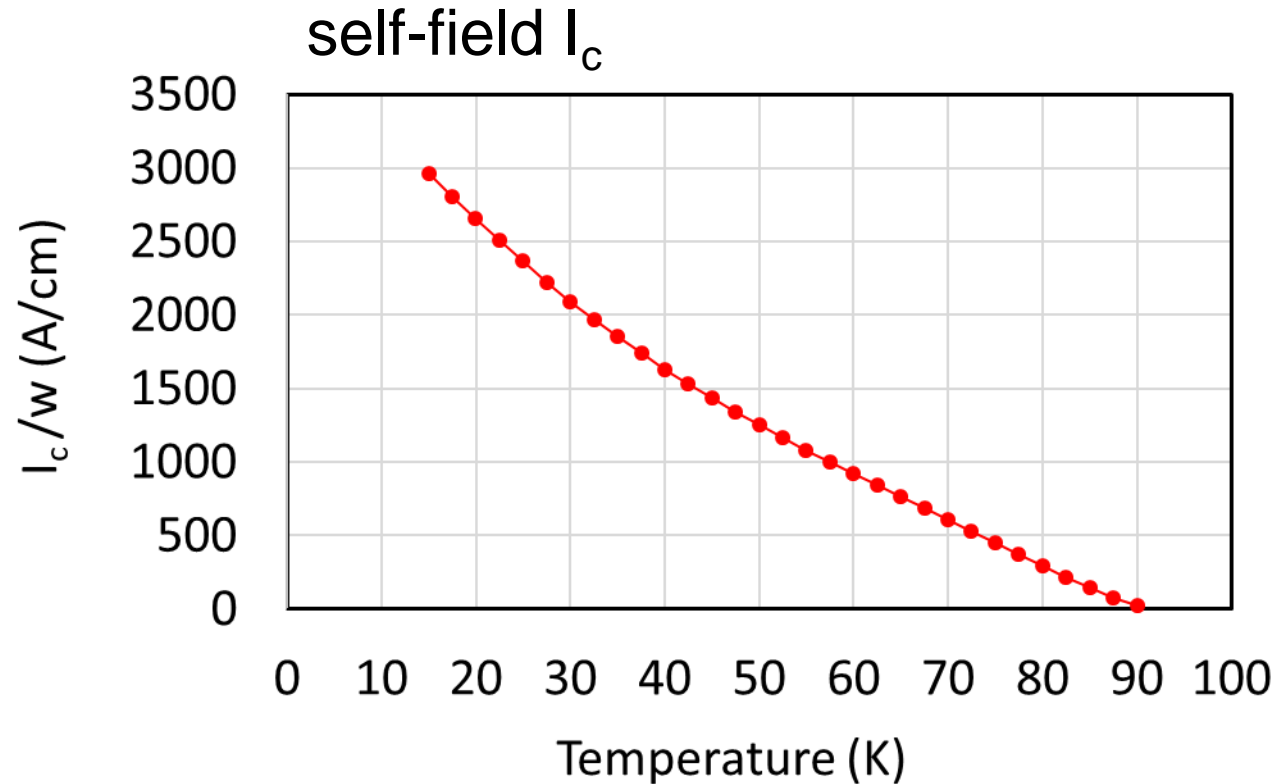


$T = 77 \text{ K}$

$I_{c, \text{self-field}} = 19.3 \text{ A}$

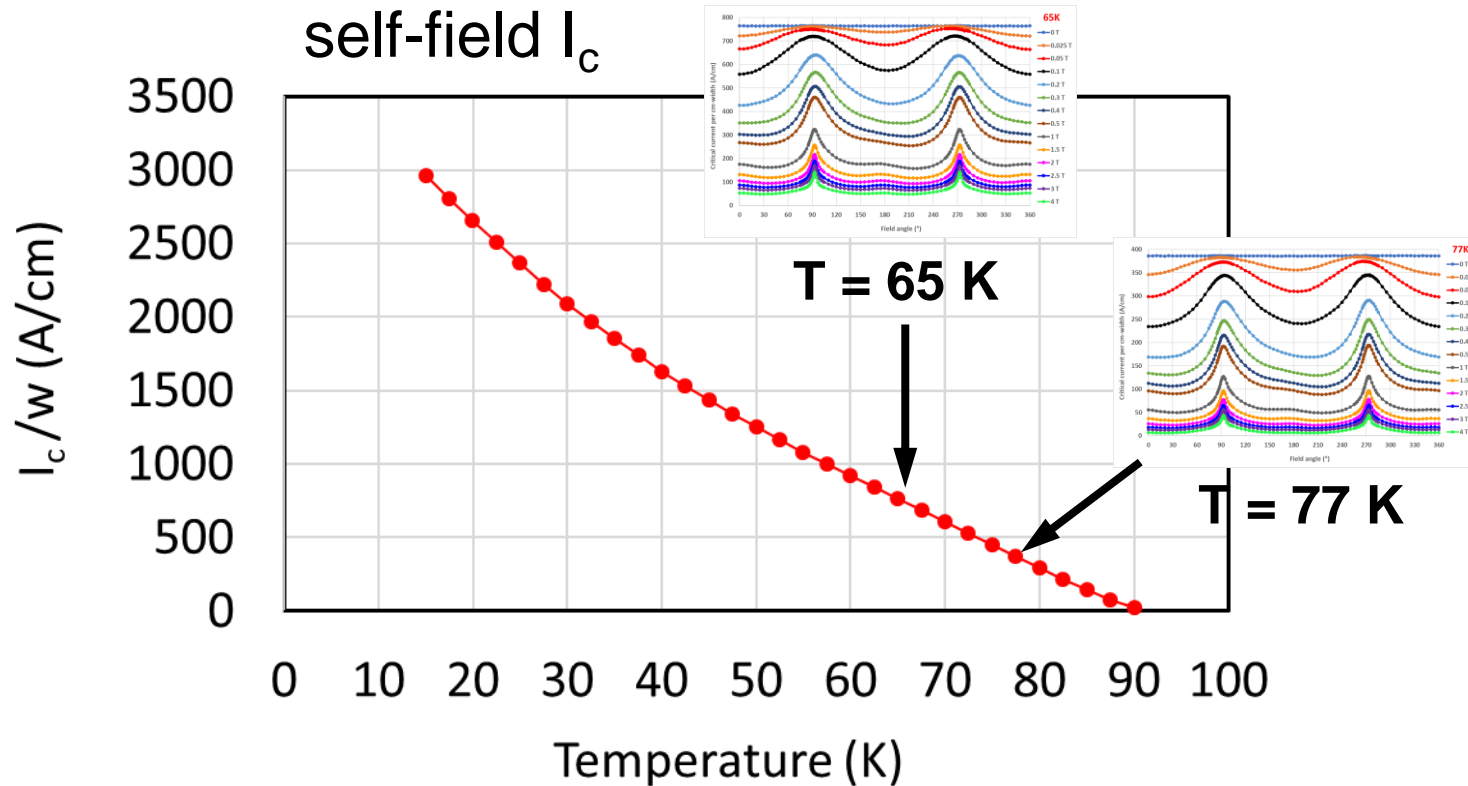


Calculating $I_c(B, \theta)$ at different temperatures



I_c changes almost linearly with temperature

Calculating $I_c(B, \theta)$ at different temperatures



I_c changes almost linearly with temperature

$$J_c = \left[\frac{J_{c2} - J_{c1}}{T_2 - T_1} (T - T_1) \right] + J_{c1}$$

Calculation time is around 17 hours

Element numbers $49 \times 49 \times 15 \approx 36000$

Time steps ≈ 110

Computer specification

AMD Ryzen Threadripper 3970x 32-core processor

128 GB RAM

Ubuntu 20.04.4 LTS operating system



**Calculation time
 ≈ 17 hours**

■ Modeling methodology

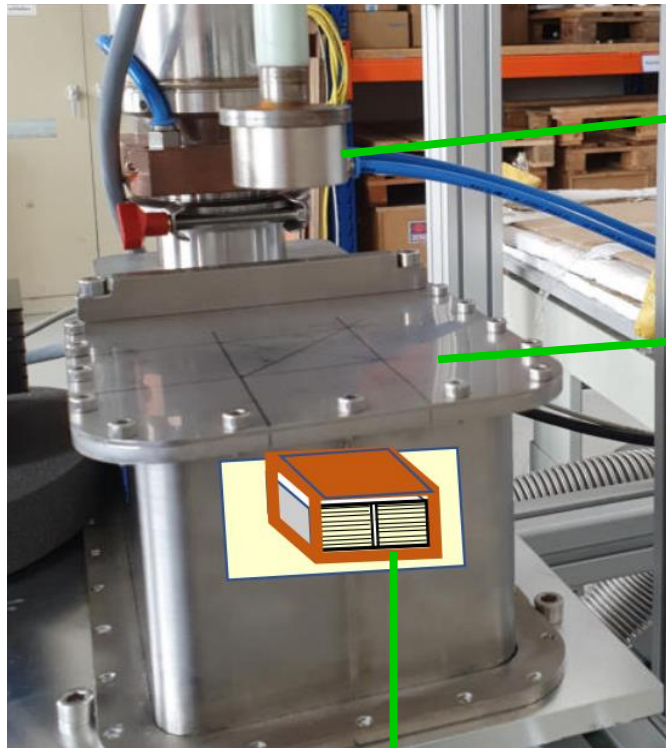
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- Homogenization
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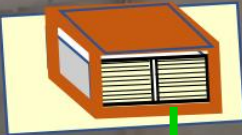
■ Summary

Zero field cooling case and measurement set-up

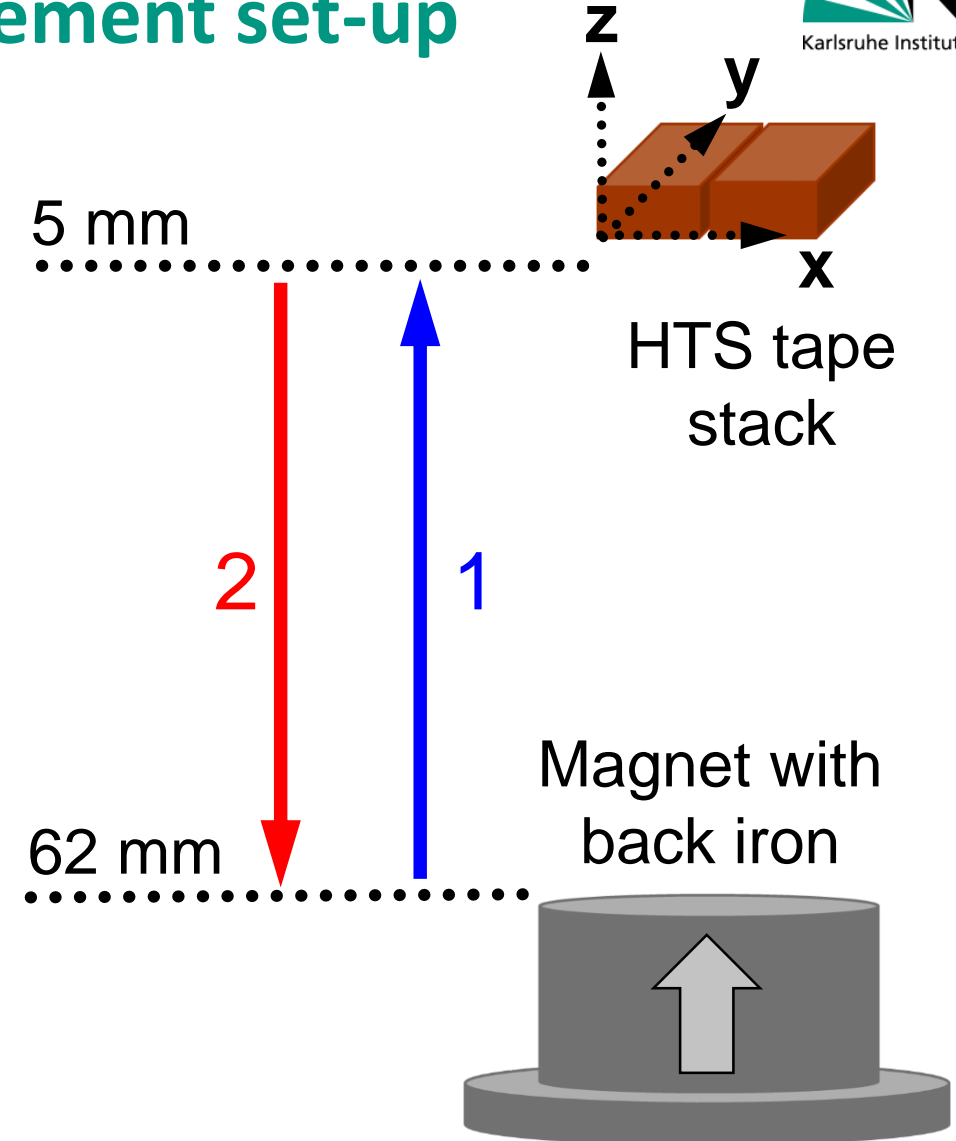
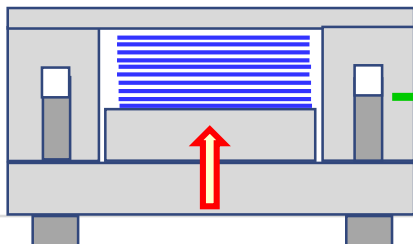


Magnet with
back iron

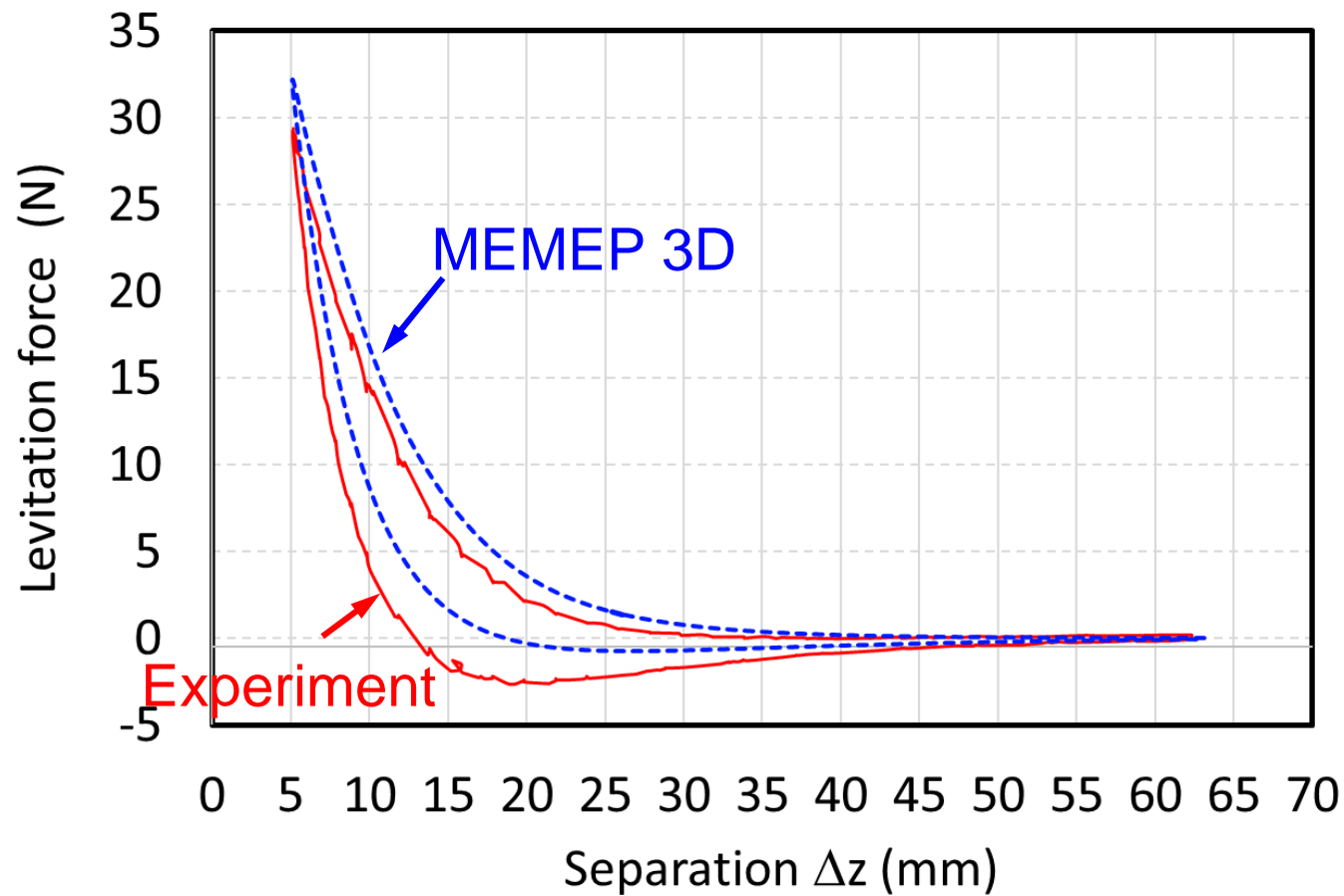
Cryostat



Tape stacks



Zero field cooling at 77 K



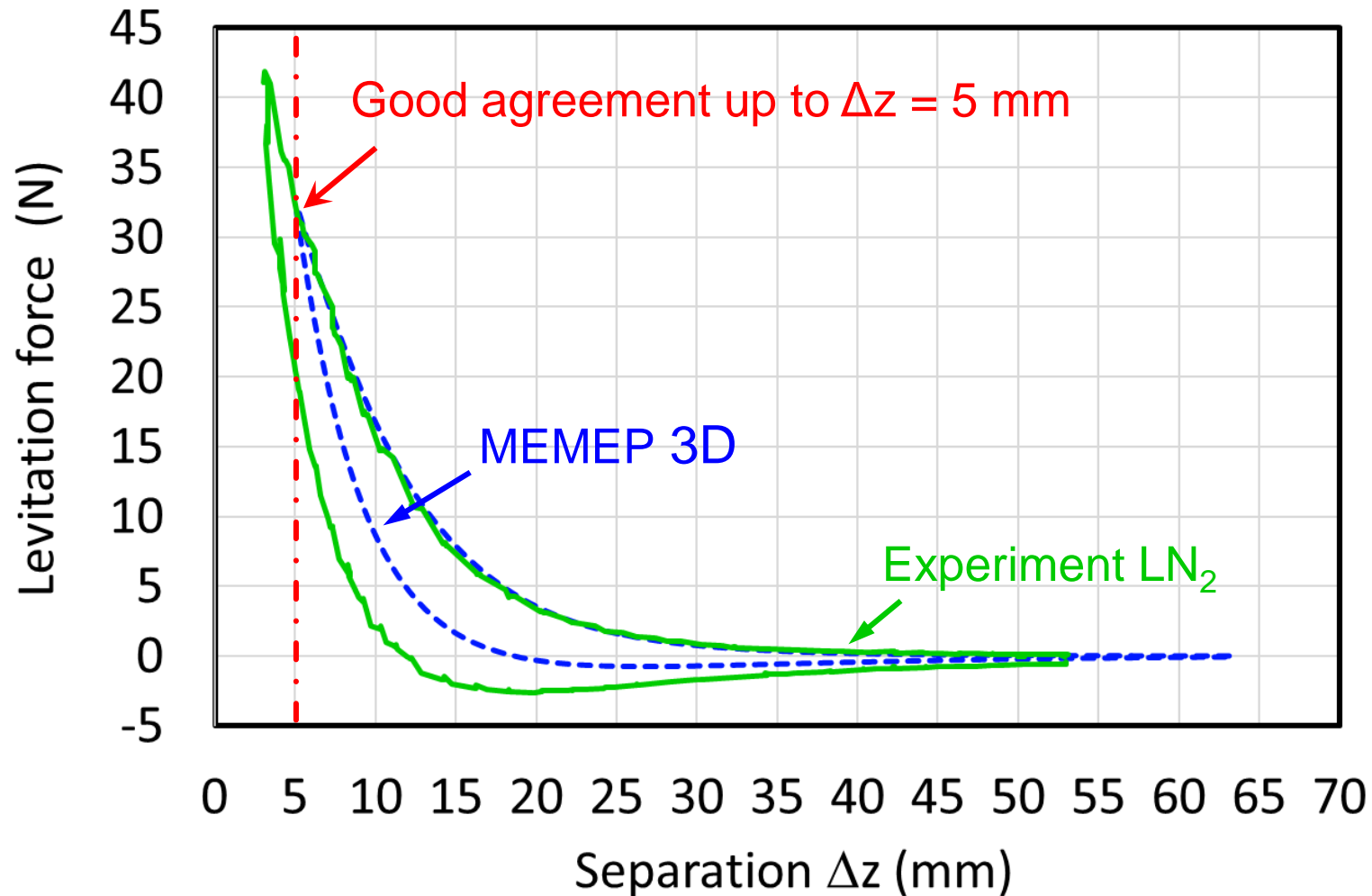
Maximum levitation force

Experiment : 29.4 N

Error: 9%

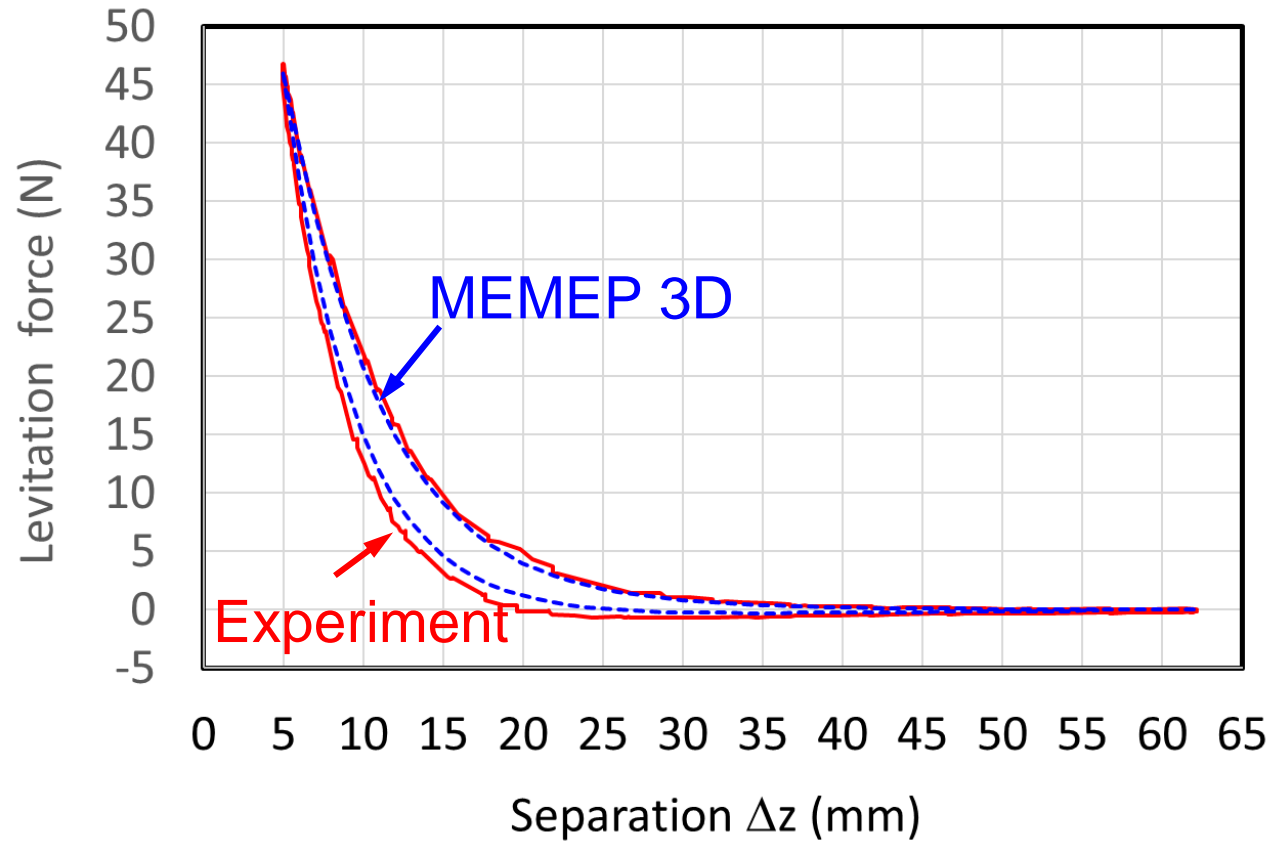
Model : 32.1 N

Zero field cooling at 77 K comparison with LN₂ measurement



**Measurement error in cryostat
at 77 K ?!**

Zero field cooling at 69 K



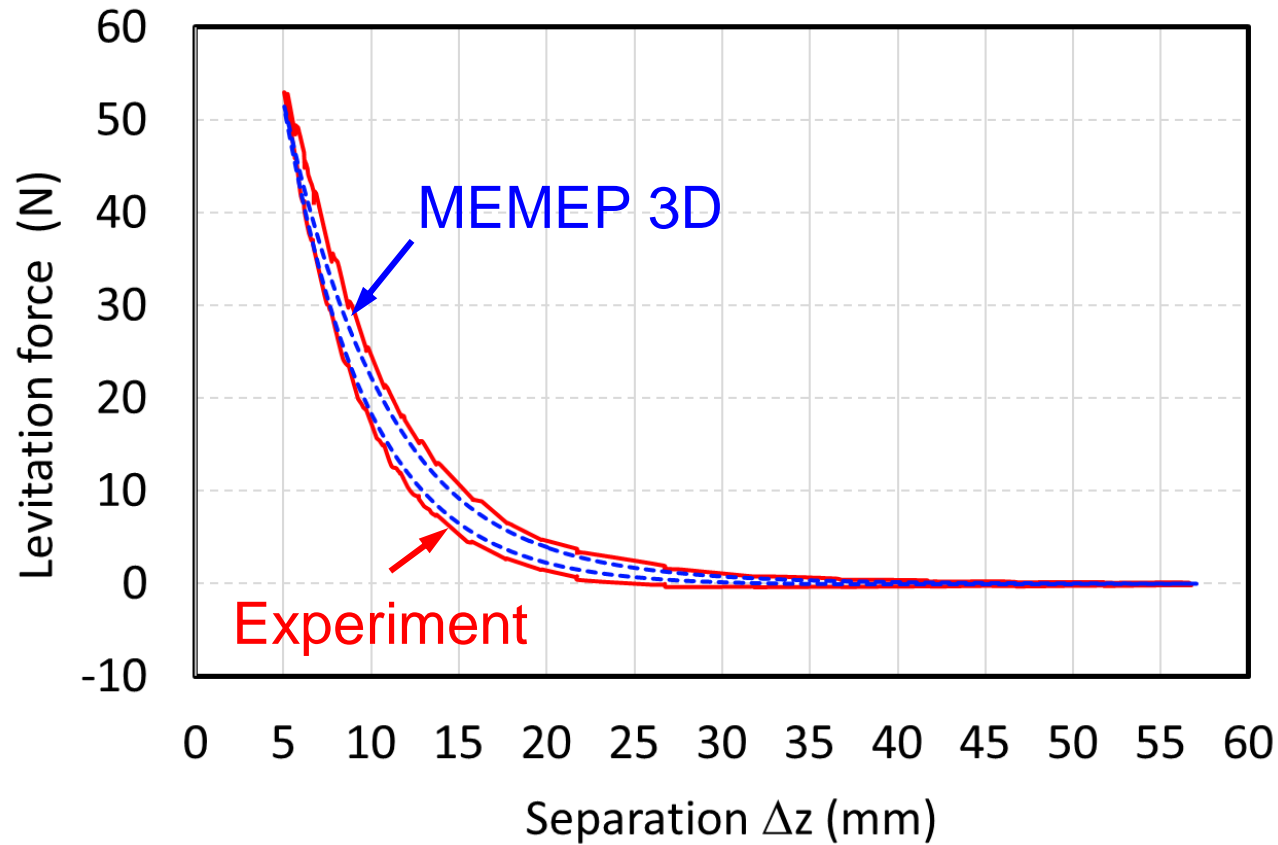
Maximum levitation force

Experiment : 46.8 N

Model : 46.2 N

Error: 1.3%

Zero field cooling at 57 K



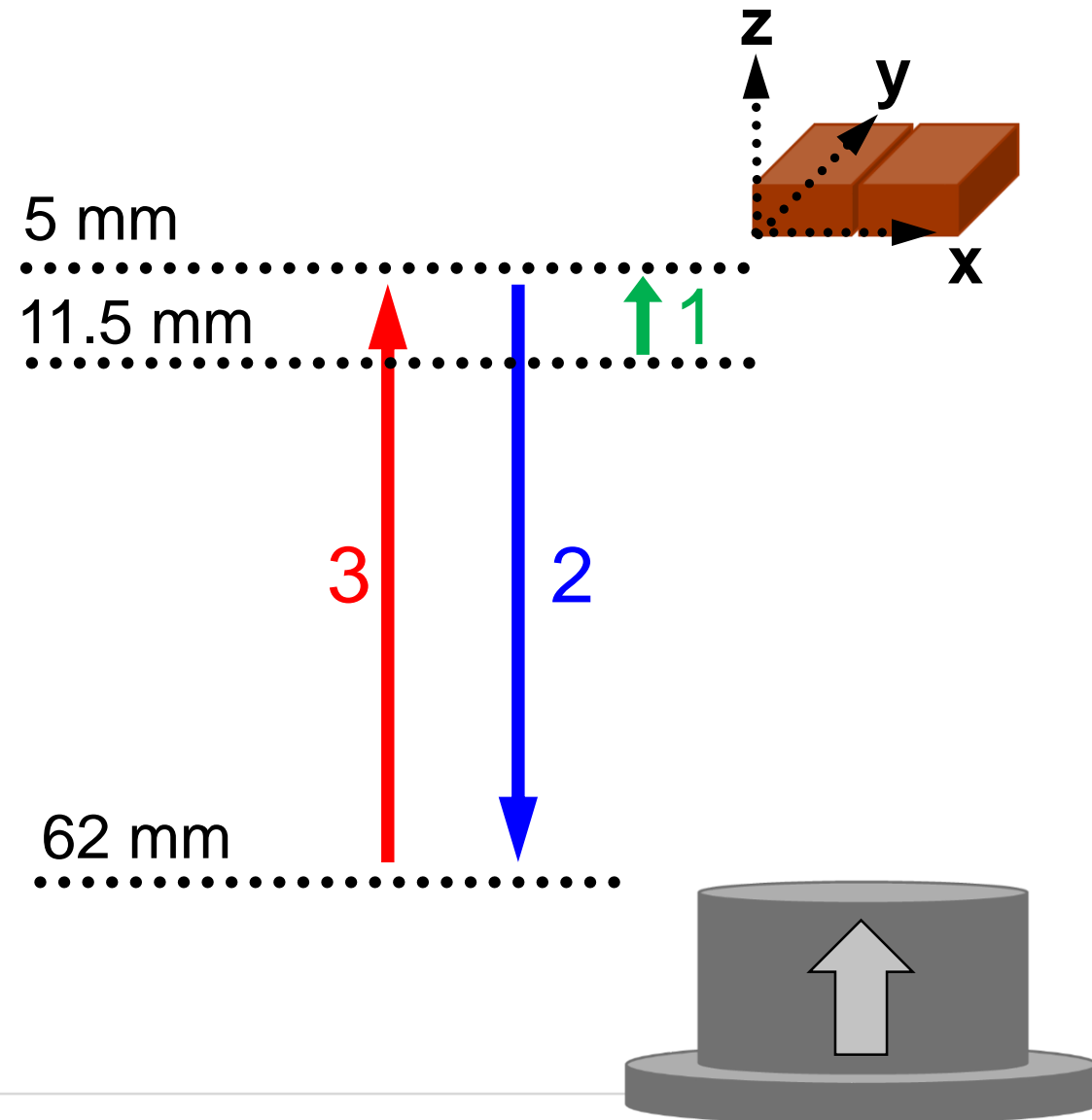
Maximum levitation force

Experiment : 53 N

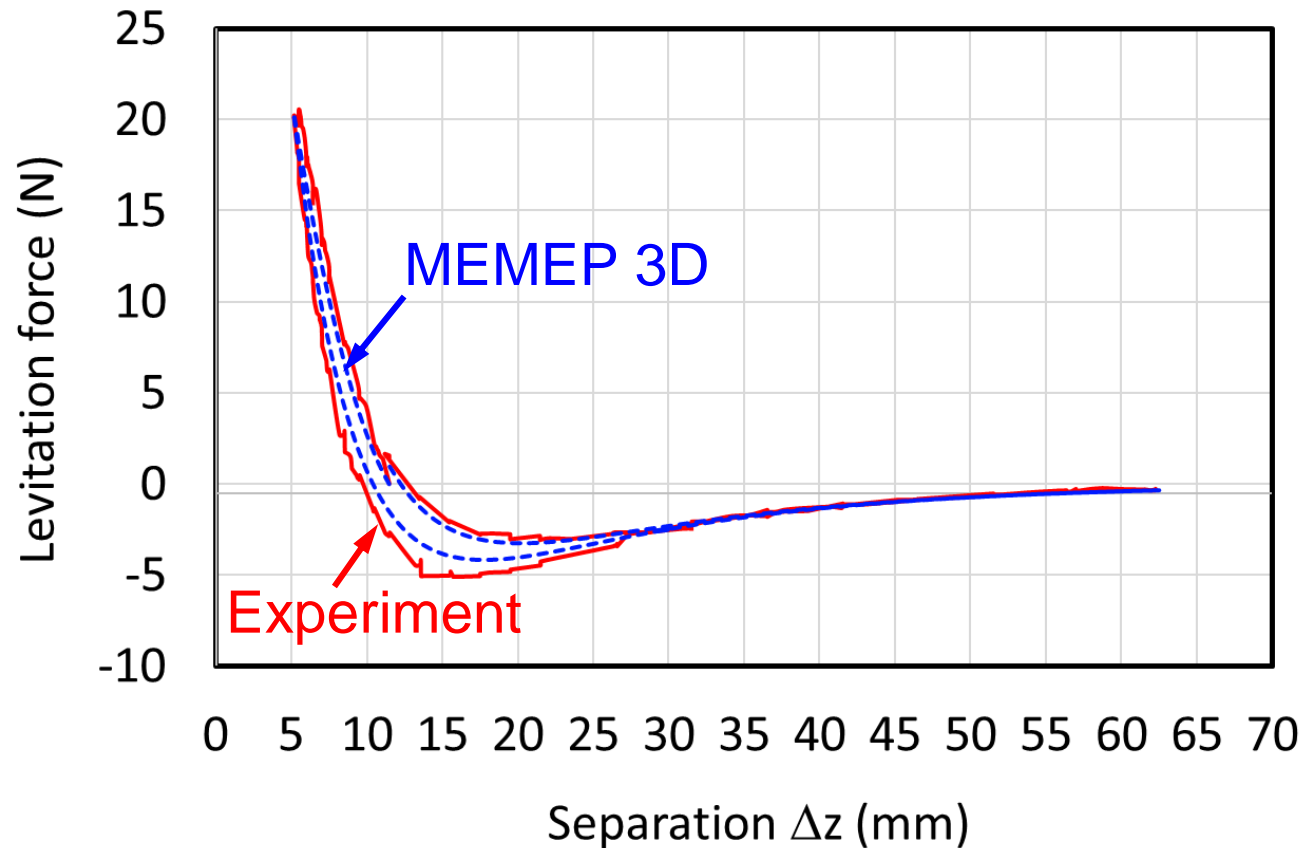
Error: 3%

Model : 51.5 N

Field cooling cases



Field cooling at 75 K



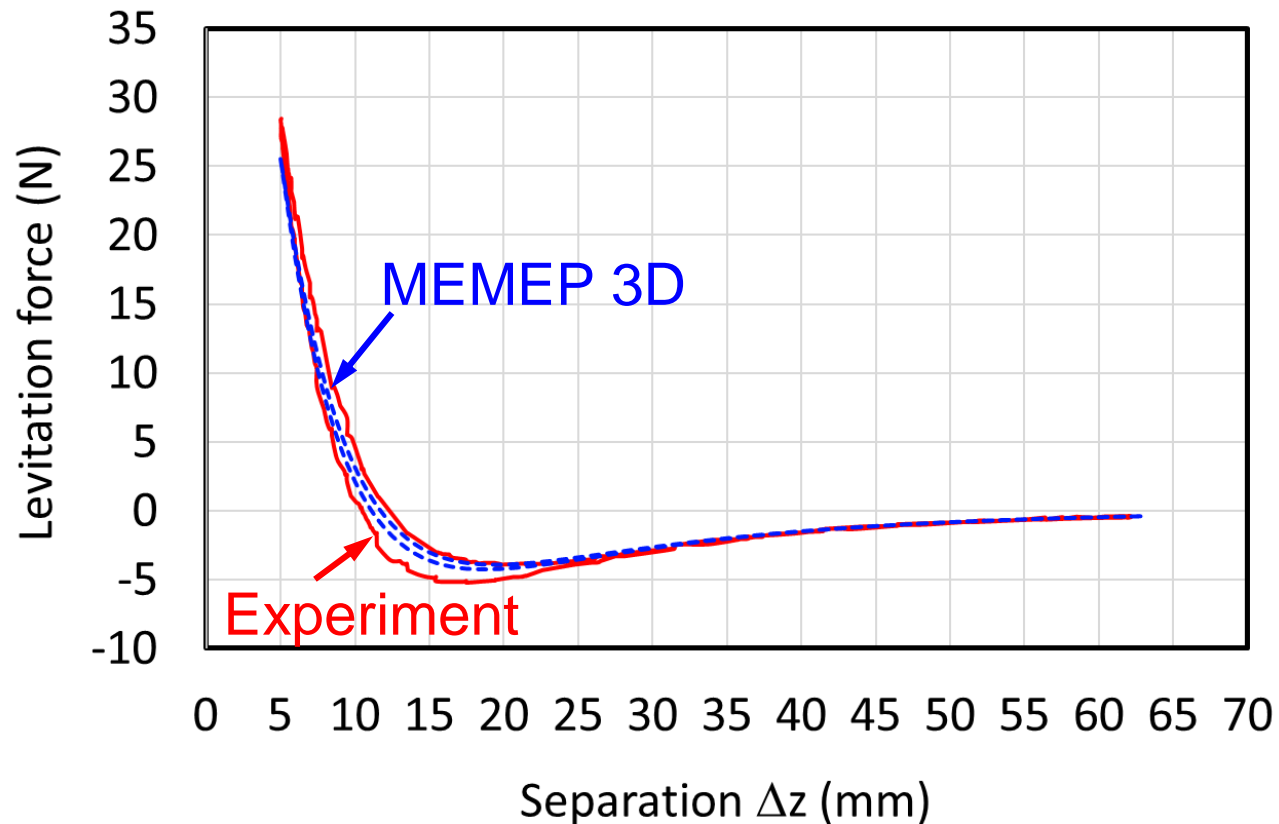
Maximum levitation force

Experiment : 20.5 N

Model : 20.2 N

Error: 1.5%

Field cooling at 57 K



Maximum levitation force

Experiment : 28.5 N

Model : 25.9 N

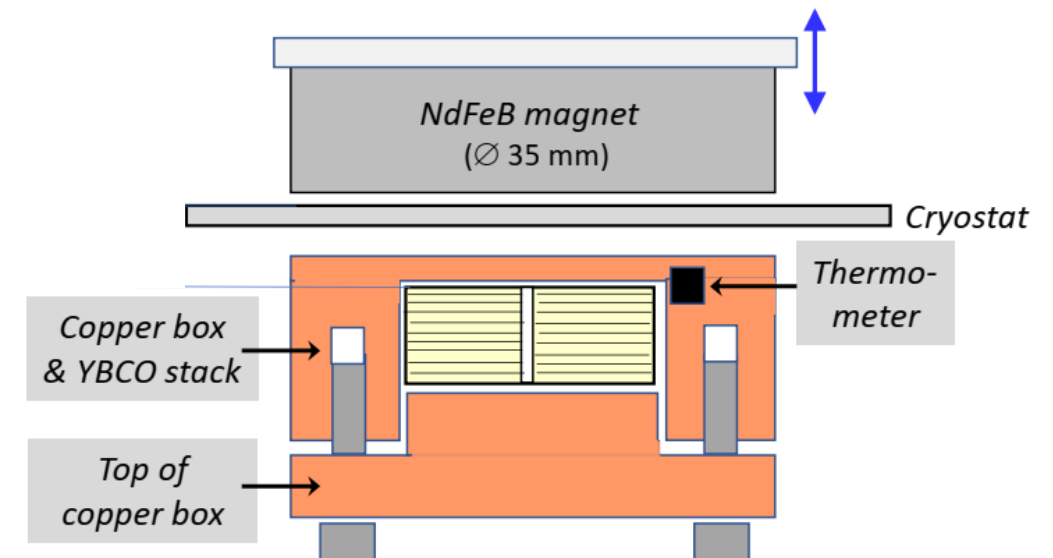
Error: 9%

Measurement error should not be neglected

Error is below 10% in all cases

Case	Temperature (K)	Error (%)
ZFC	77	9
	69	1.3
	57	3
FC	75	1.5
	57	9

- Separation (Δz) measuring error
- Temperature measuring error
- Force measuring error



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Summary and future work

- Developing full 3D simulation to model levitation force under various temperatures
- The first model to predict levitation force without manipulation of I_c with error $< 10\%$
- Other than modeling errors, measurement error is the cause of disagreement
- Implementing proper $I_c(B, \theta)$ is important to obtain a good agreement

Future work

- Impact of tape thickness reduction on levitation force with Halbach magnet as guideway

Thanks for your attention!