

# KIT Validation Activities of the ASTEC code against the QUENCH Bundle Experiments: Results and Outlook

F. Gabrielli, O. Murat, A. Mercan, A. Stakhanova, M. E. Cazado, Z. Jimenez Balbuena, V.H. Sanchez-Espinoza

Institute for Neutron Physics and Reactor Technology

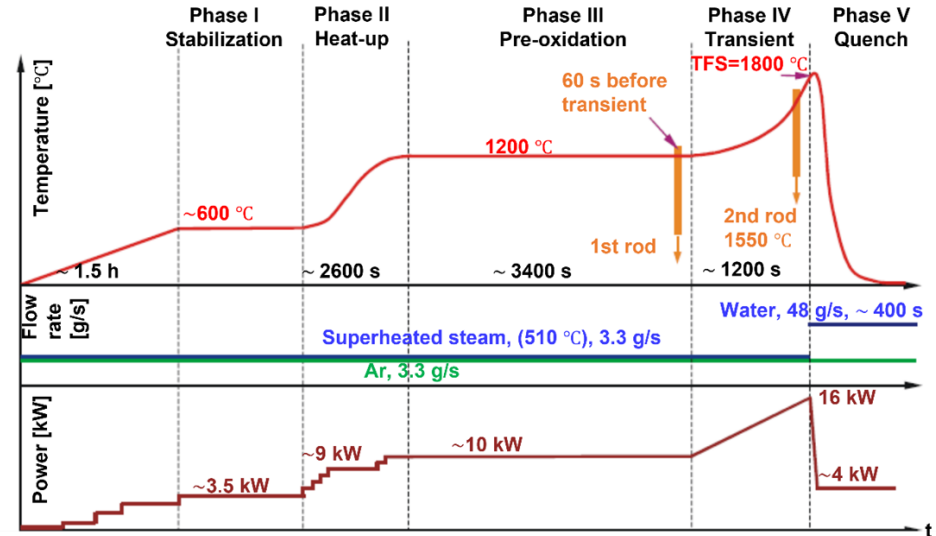
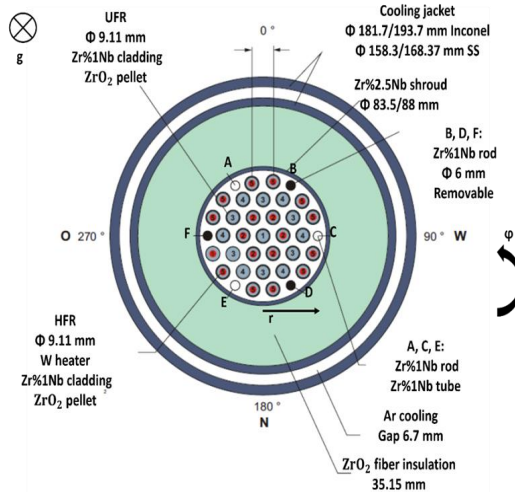


# Motivation

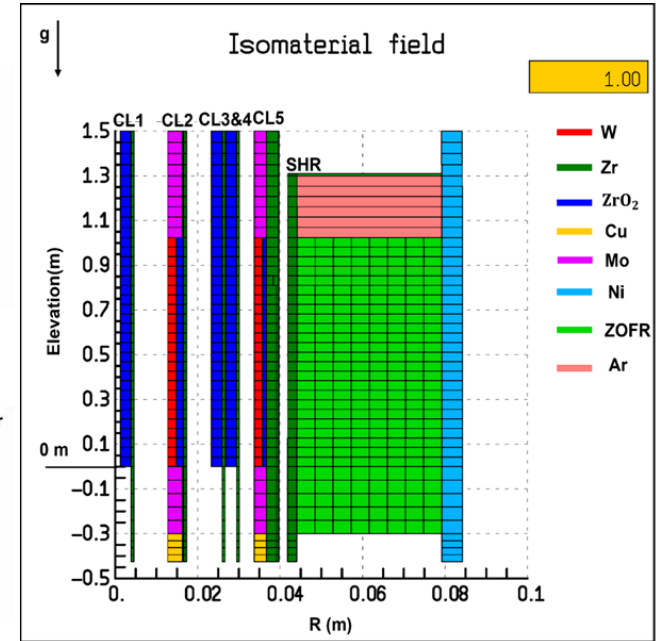
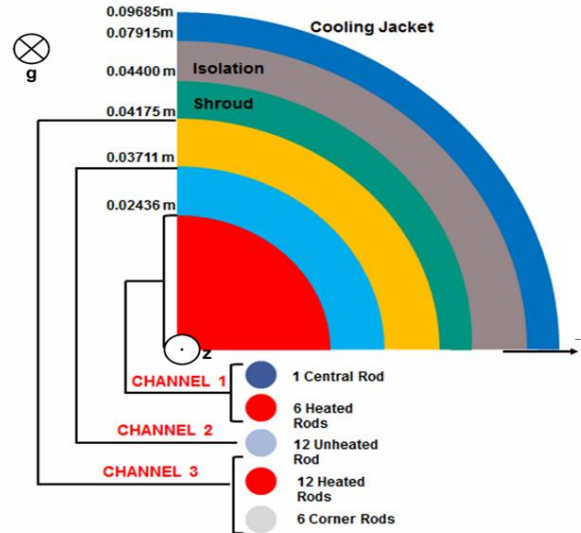
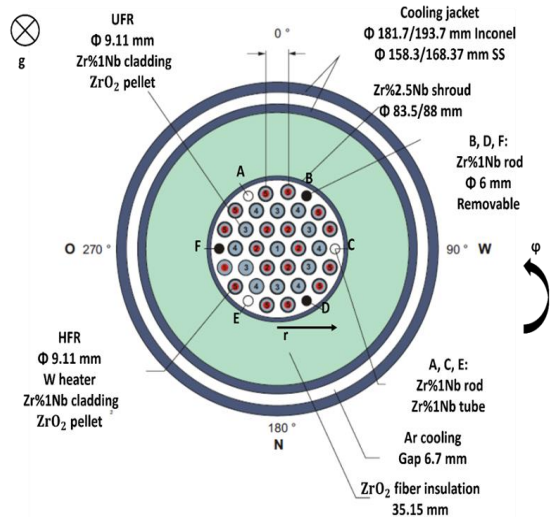
- KIT strategy for severe accident (SA) analyses → continuous improvement of the codes to evaluate the progression and the radiological consequences of SAs in current and innovative NPPs
- Validation of codes is a key step in the KIT strategy
- The ASTEC integral code, developed by IRSN, is extensively employed at KIT
- **ASTEC validation against QUENCH experiments is continuously going on since long at KIT → almost all the QUENCH bundle tests analyzed**
- Current priorities in the research activities:
  - Further widening the range of application of ASTEC, i.e., VVER (Q-12) and BWR (Q-20)
  - Enable the safety assessment of the innovative reactor concepts, i.e., SMRs, expected to employ ATF cladding materials

# ASTEC Validation against QUENCH-12

- **Framework: assessment of an ASTEC dataset of a generic VVER-1000 NPP**
- **QUENCH-12: VVER-type fuel assembly arrangement**
  - **Reflooding of pre-oxidized heated rods bundle**



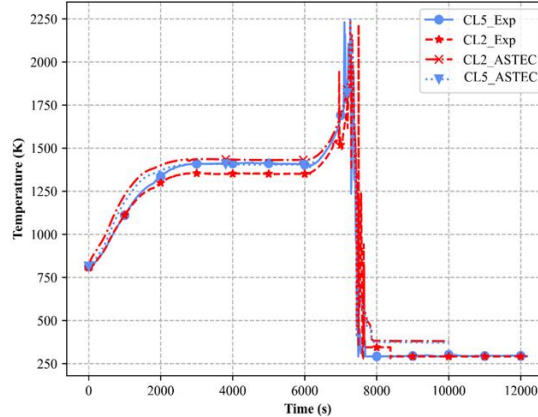
# ASTEC model of the QUENCH-12 Test



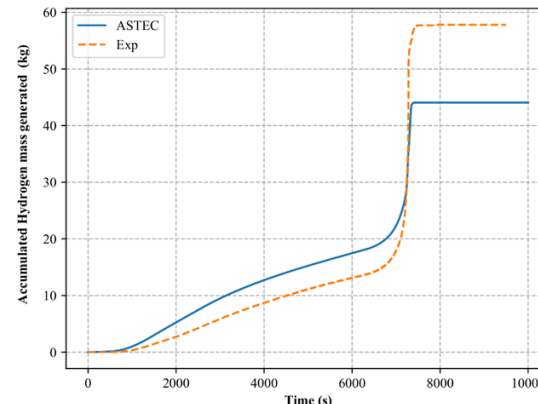
- All the ASTEC models activated
- Zr material data employed instead of Zr-1%Nb → work in progress at KIT

# ASTEC Results vs. QUENCH-12 Experiment

Heated rods @950 mm height



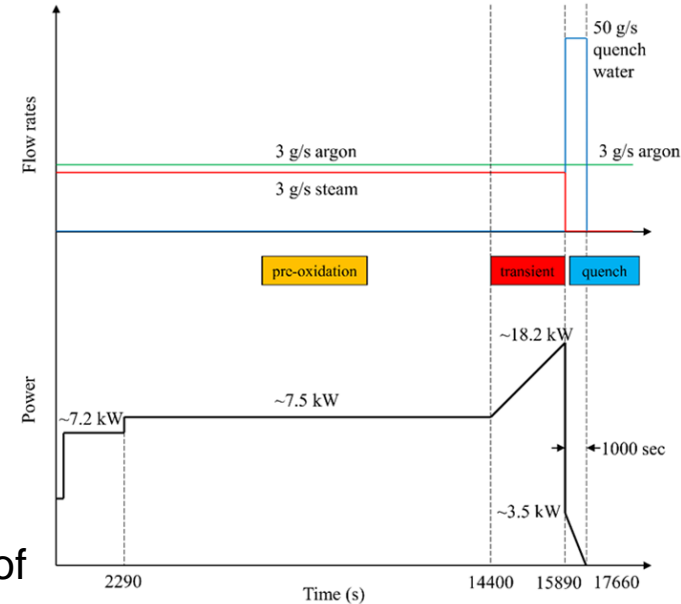
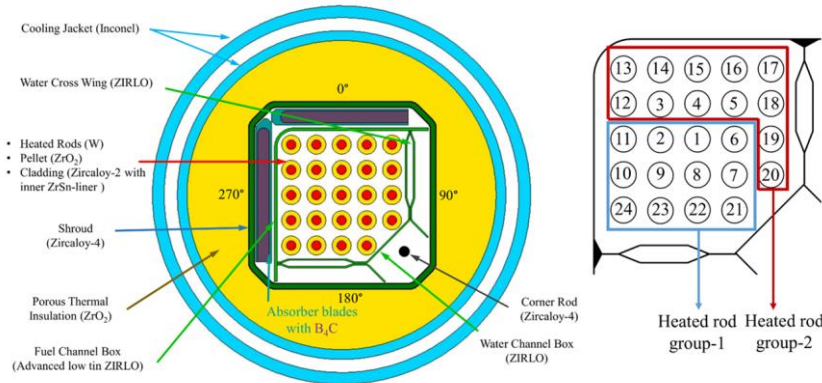
Hydrogen production



- **Good agreement on the temperatures of heated and un-heated rods**
- **Hydrogen production**
  - **Good agreement up to the beginning of the quenching phase: 34.2 g (ASTEC) vs. 34.7g (Exp.)**
  - **Underestimation during the quenching phase: 9.9 g (ASTEC) vs. 23.1 g (Exp.) → due to the use of Zr-4 instead of Zr-1%Nb**
  - **The code is able to catch the physical phenomena of the experiment**

# ASTEC Validation against QUENCH-20

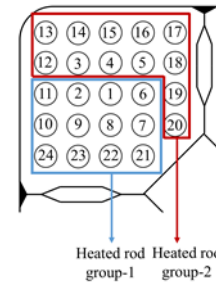
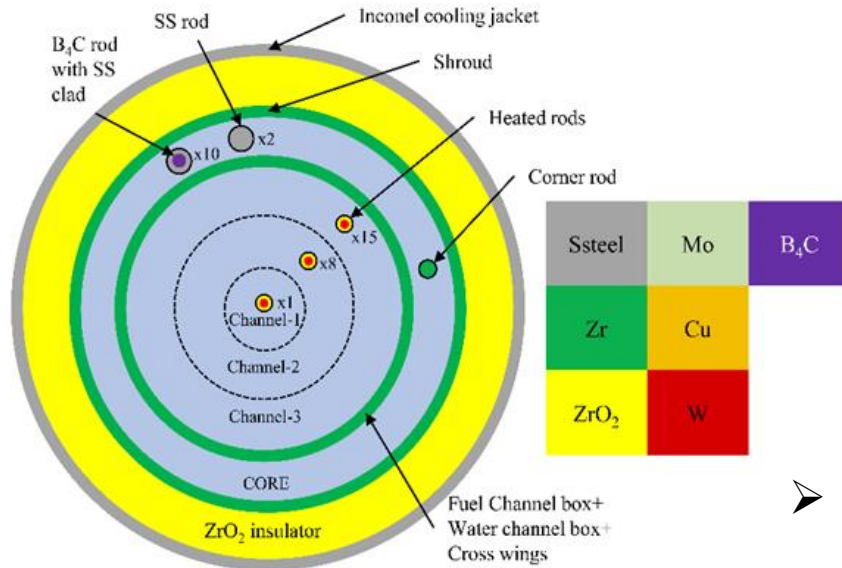
- **Framework: assessment of an ASTEC dataset of a generic model of the Peach Bottom BWR NPP (first-of-its-kind)**
- **QUENCH-20: Test Bundle Cross Section (1/4 SVEA 96 OPTIMA-2)**



1. Pre-oxidation phase: power at 7.5 kW, steam and Ar flows
2. Transient phase: Electric power increases up to 18.2 kW
3. Quench phase: 50 g/s quench water Injected at the end of the transient phase, steam flow off

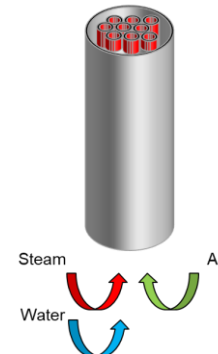
# ASTEC model of the QUENCH-20 Test

- Efforts to properly model the power distribution in the bundle



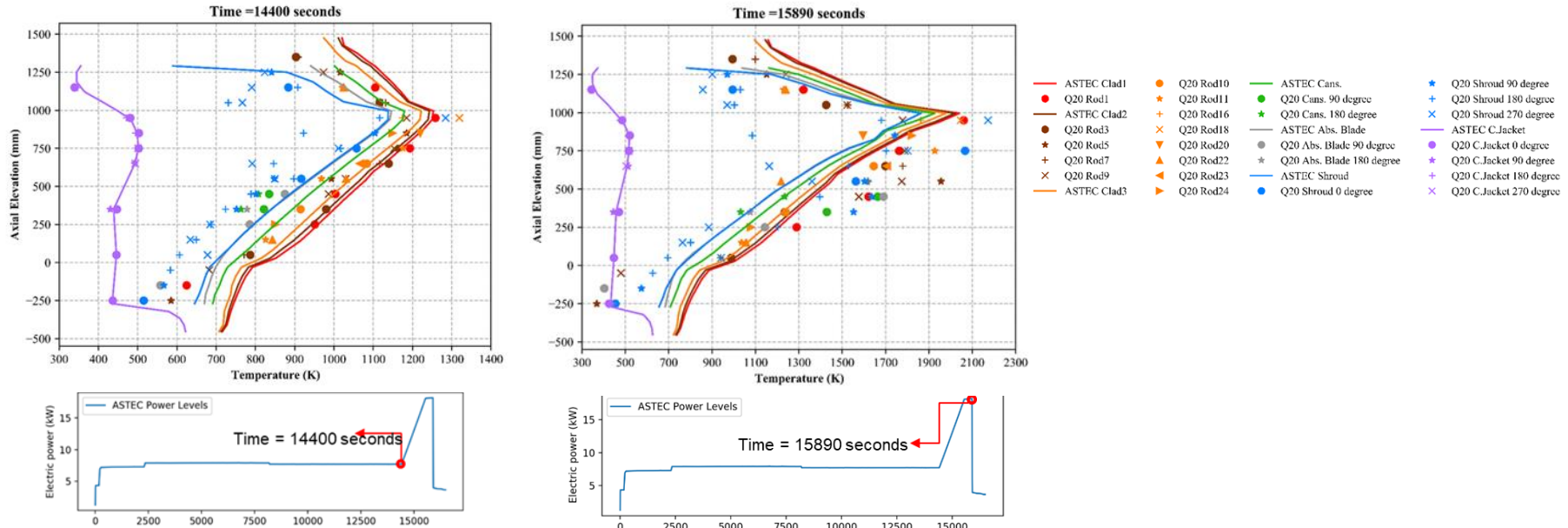
- The electrical power is not the same for each rod

- Boundary conditions from the experiment
- All ASTEC models activated





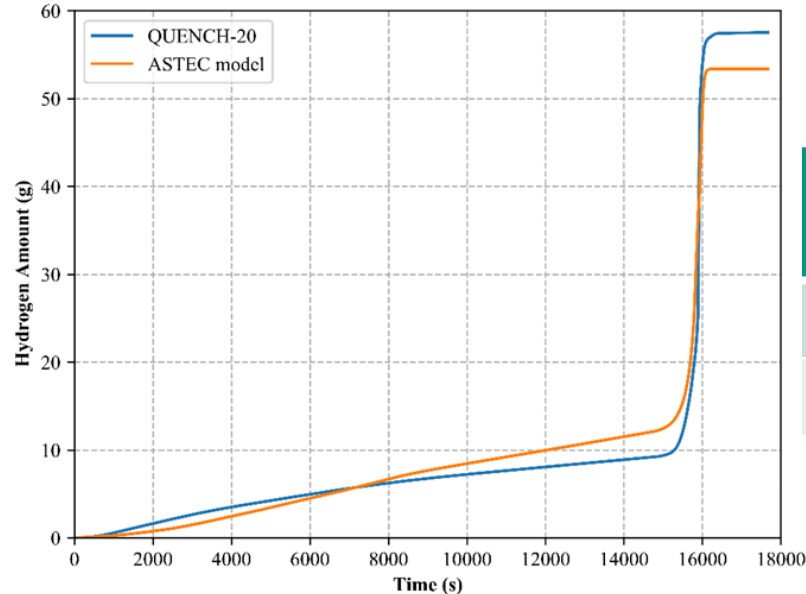
# ASTEC Results vs. QUENCH-20 Experiment



➤ **Considering the challenges in modelling the geometrical peculiarities of bundle, ASTEC reasonably well reproduces the temperature of the structures during the transient**



# ASTEC Results vs. QUENCH-20 Experiment



Contribution to H <sub>2</sub> production	Exp. [g]	ASTEC [g]
Total	<b>57.4</b>	<b>53.4</b>
B4C oxidation	<b>10.0</b>	<b>9.48</b>

➤ **ASTEC results on both the total and B4C contribution to the hydrogen production during the test are in good agreement with the experiment**

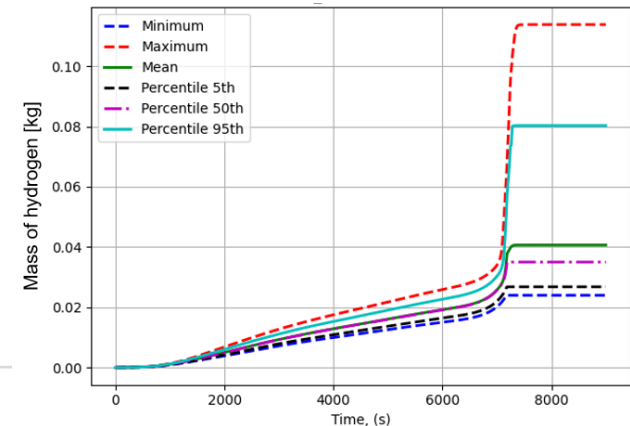
# Uncertainty and Sensitivity Analyses (U&Sa)

- U&Sa of the ASTEC results became part of the calculation route in the KIT strategy for SA analyses
- The application of U&Sa methods to the ASTEC results for the QUENCH tests play a key role in order to:
  - Testing the U&S methodologies
  - Identifying bottlenecks in the code, when developing/employing new models devoted to new materials, i.e. ATF
- The KARlsruhe Tool for Uncertainty and Sensitivity Analyses (KATUSA) has been developed at KIT
- The ASTEC/KATUSA has been used for the QUENCH-08 and QUENCH-06 analyses

# Uncertainty and Sensitivity Analyses (U&Sa)

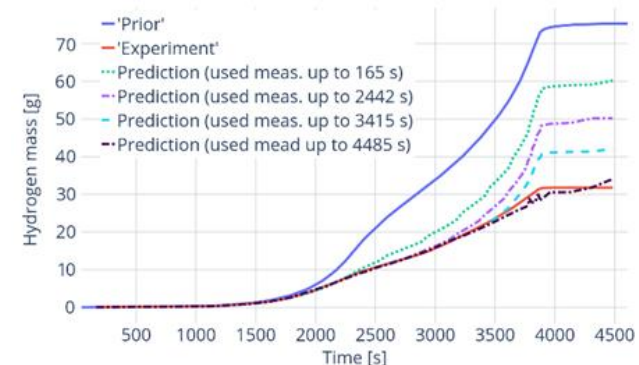
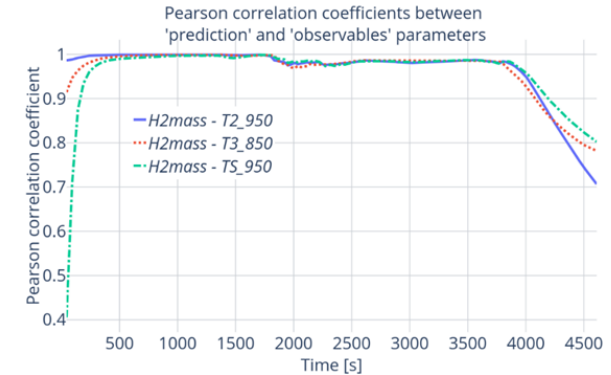
- The **U&Sa** of the results of integral codes for the **QUENCH-06** has been **selected as test case (Task 1)** in the IAEA CRP I31033 'Advancing the State-Of-Practice in Uncertainty and Sensitivity Methodologies for Severe Accident Analysis in Water Cooled Reactors' (2019-2024)
- Participants to the Task: KIT (coordination), ENEA, IBRAE, LEI
- 5 Figure-of-Merits selected ( $H_2$  production, temperatures, oxide scales)
- 23 uncertainty parameters selected and the corresponding PDFs characterized
- The TECDOC is in the publication process

## Simple statistics (ASTEC)



# U&Sa and Prediction of H<sub>2</sub> Production (QUENCH-08)

- Framework: Development of a tool for fast source term (ST) predictions based on a database of results from the ASTEC code (German WAME project, **accomplished**)
- Fast Source Term Code (FSTC) developed at KIT
  - U&Sa+Data Assimilation algorithm based on MOCABA (developed by Framatome GmbH)
  - Goal: iteratively use the measurements and previous predictions to construct the new one
- Before moving to NPPs applications, FSTC tested on the QUENCH-08 experiment
- An ASTEC database of 600 simulations assessed
- The ASTEC/FSTC allows predicting the hydrogen mass by using the TC measurements



# ASTEC Modelling of QUENCH ATF-Related tests

- Large efforts on the analysis of the QUENCH ATF-related bundle tests on-going
- Framework: OECD/NEA QUENCH-ATF and IAEA CRP ATF-TS
- Current approach in the ASTEC modelling: modifying the material database by including the correlations for such materials, i.e. FeCrAl

... .

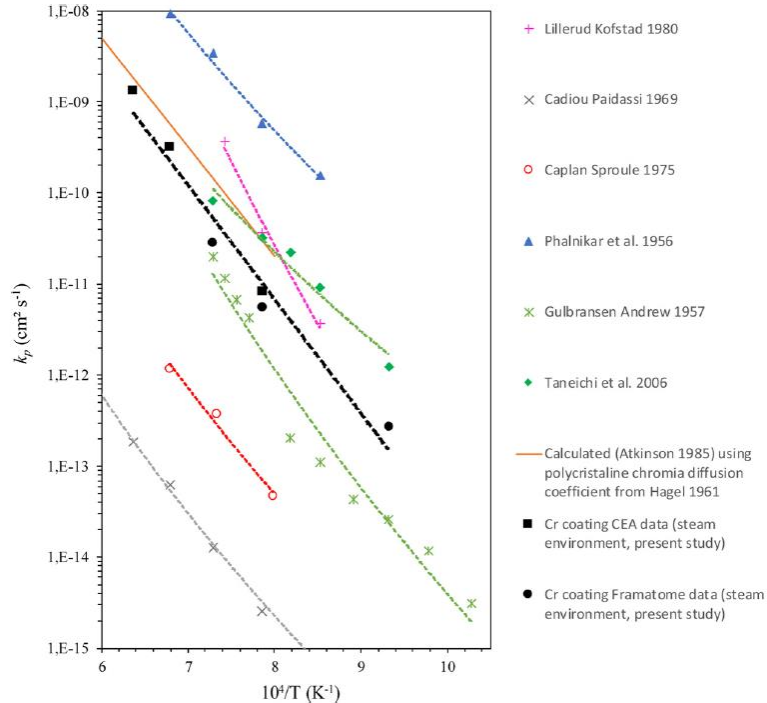
```
STRUCTURE MODEL NAME 'BEST-FIT' LAW 'COEFF' VARIABLE 'T' VUNIT 'K' RUNLOW 0. RUNUPP 5000.  
  SRG VALUE AGAIN 9.62D-10 BGAIN 0.0 ATHIC 2.252D-13 BTHIC 0.0 MODEL 0.5 TERM  
  X 1473.K  
  SRG VALUE AGAIN 3.0D+11 BGAIN 5.94354D5 ATHIC 3.371D3 BTHIC 5.94354D5 MODEL 0.5 TERM  
  X 1648.K  
  SRG VALUE AGAIN 2.4D+08 BGAIN 3.52513D5 ATHIC 0.008682D0 BTHIC 3.52513D5 MODEL 0.5 TERM  
END
```

- Mid-term approach: development and implementation in ASTEC of an oxidation model for new materials (currently efforts devoted to FeCrAl)





# Oxidation Model



➤ Brachet data

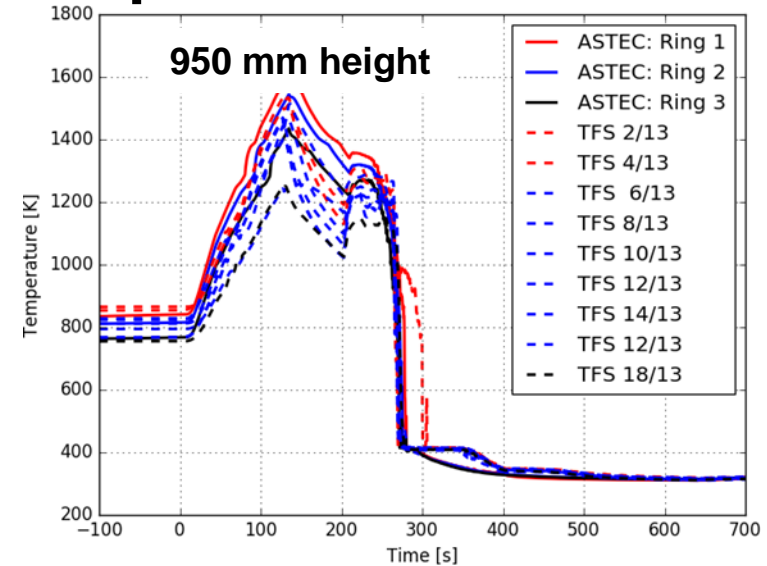
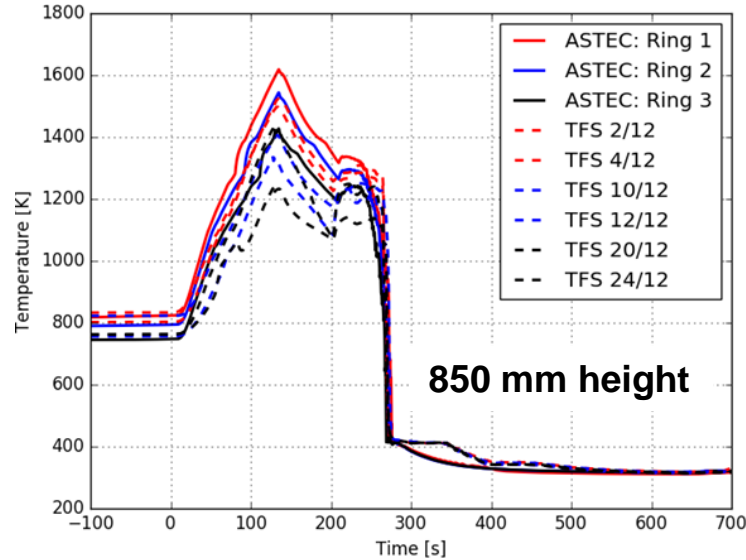
➤ Fitting functions for weight gain and thickness grown of the oxide layer provided by J. Stuckert

$$\delta = 0.00377 \cdot e^{-\frac{123783}{R \cdot T}} \cdot \sqrt{t}$$

$$\Delta m = 6.19 \cdot e^{-\frac{123783}{R \cdot T}} \cdot \sqrt{t}$$

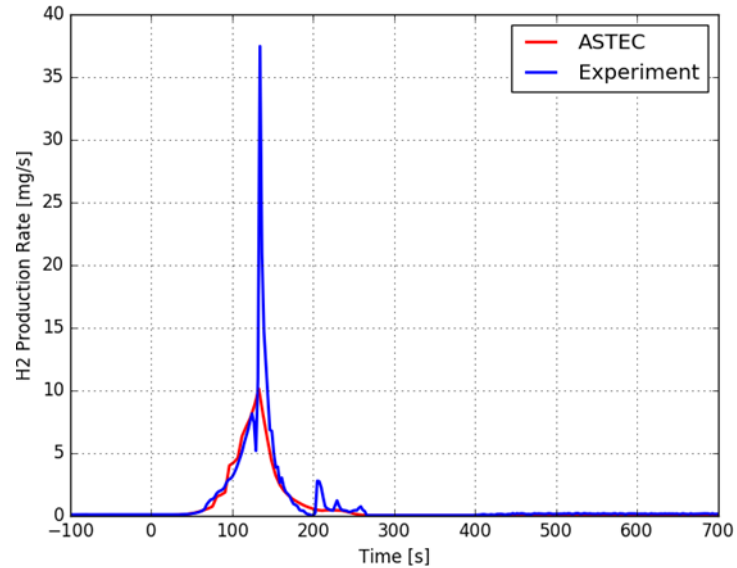
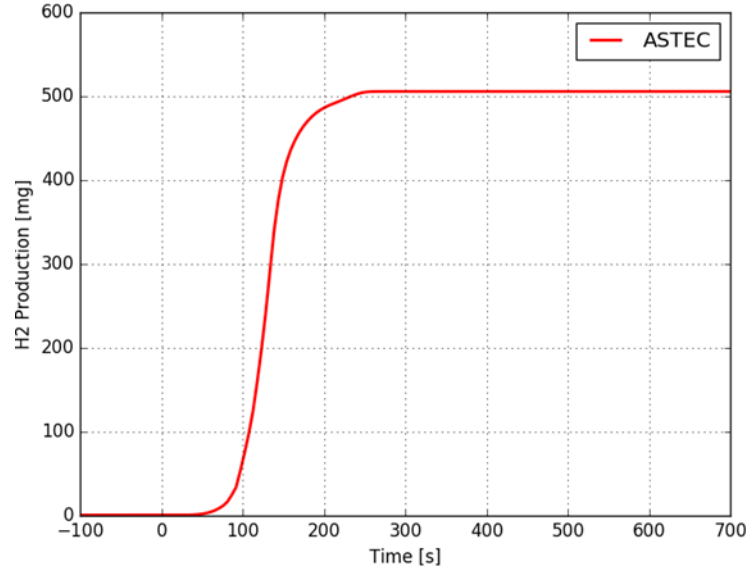
Brachet, J.-C., et al., 2020. High temperature steam oxidation of chromium-coated zirconium-based alloys: Kinetics and process, Corrosion Science 167 (2020) 108537..

# ASTEC Model: Results – Clad Temperature



- **Ring#1: reasonable agreement**
- **Ring#2: deviations @850 mm height (~200 degree), reasonable for some TCs @950 mm**
- **Ring#3: large deviations (up to~200 degree)**
- **Good agreement on the radial shape**

# ASTEC Model: Results – H<sub>2</sub> production

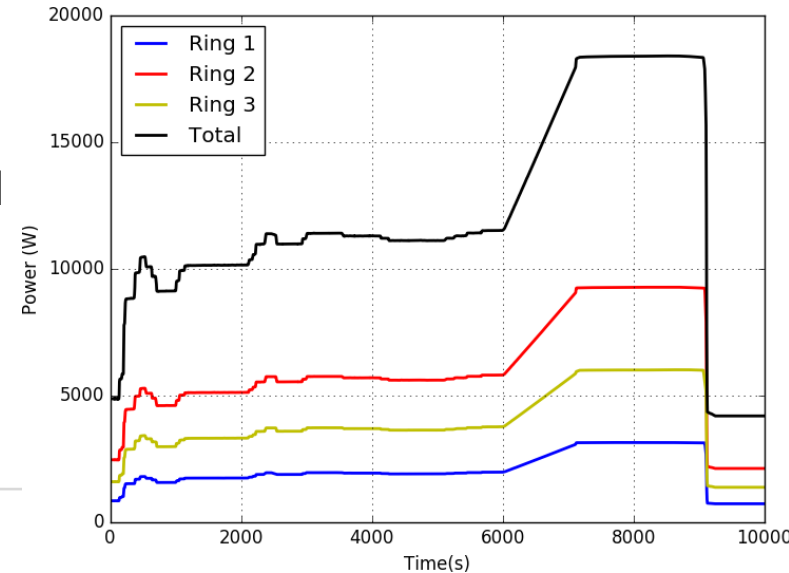
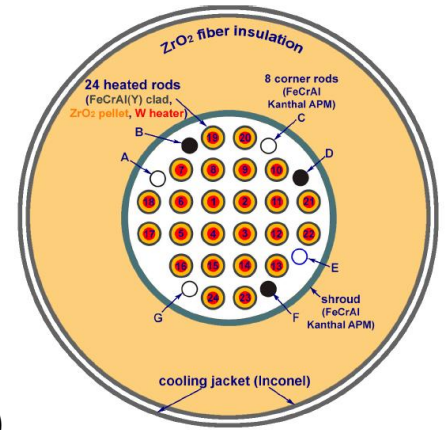


- Large deviation on the maximum H<sub>2</sub> production rate
- Very good agreement on the starting time of H<sub>2</sub> production and on the kinetics behavior

# QUENCH-19 Test

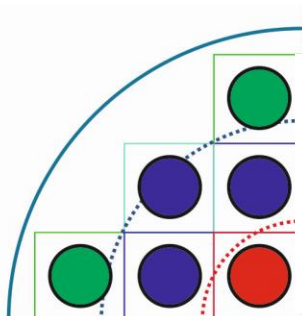
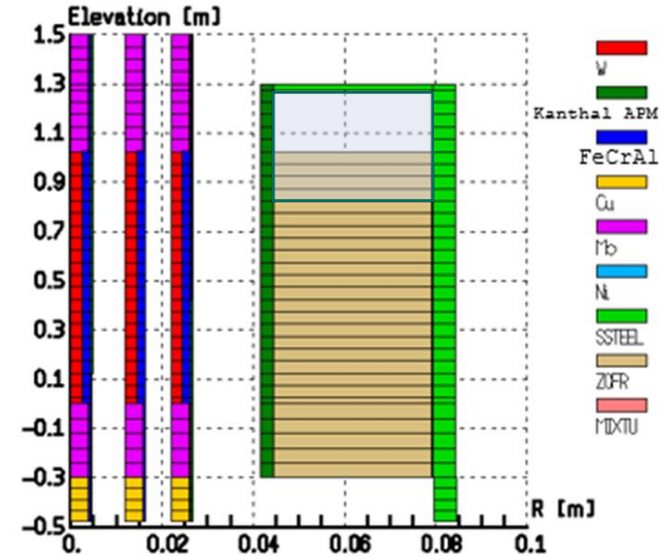
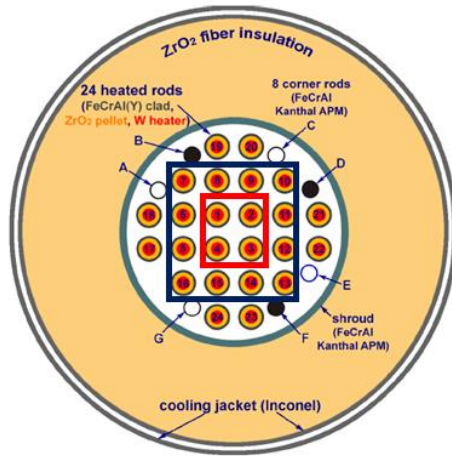
## ➤ IAEA ATF-TS Project

- Phase 1: heating up to  $\sim 600$  °C (4 kW)
- Phase 2: power increase up to 11.5 kW (pre-oxidation)
- Phase 3: power increased up to 18.12 kW (5 W/s)  
( $T_{\text{pct}} \sim 1500$  °C)
- Phase 4: power reduced to 4.1 kW
- Atmosphere of Ar (3.45 g/s) and superheated steam (3.6 g/s).
- Reflooding at  $\sim 9100$  s
  - Fast initial injection of 4 kg of water
  - Slow injection 48 ~ g/s of water



# ASTEC Model of the QUENCH-19 Test

## ➤ IAEA ATF-TS Project



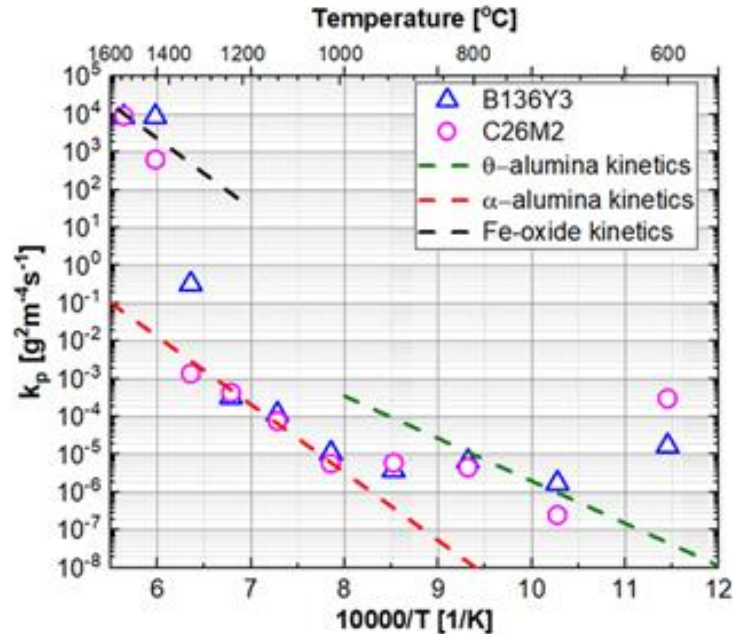
Ch. 3, 8 rods,  $r_{\text{ext}} = 41.5$  cm

Ch. 2, 12 rods,  $r_{\text{ext}} = 28.4$  cm

Ch. 1, 4 rods,  $r_{\text{ext}} = 14.2$  cm

- Accidental presence of 4 l water the gap between the shroud and the cooling jacket modelled

# ASTEC: FeCrAl Oxidation Model



➤ Fitting functions for weight gain provided by J. Stuckert

$$K = \begin{cases} 9.62 \times 10^{-12} [\text{g}^2/\text{cm}^4\text{s}], & T \leq 1473 \text{ K} \\ A_B \exp\left(\frac{-E_B}{RT}\right), & 1473 < T < 1648 \text{ K} \\ A_{Fe} \exp\left(\frac{-E_{Fe}}{RT}\right), & T \geq 1648 \text{ K (melting point of FeO)} \end{cases}$$

$$A_B = 3 \cdot 10^9 \text{ g}^2/\text{cm}^4 \text{ s}$$

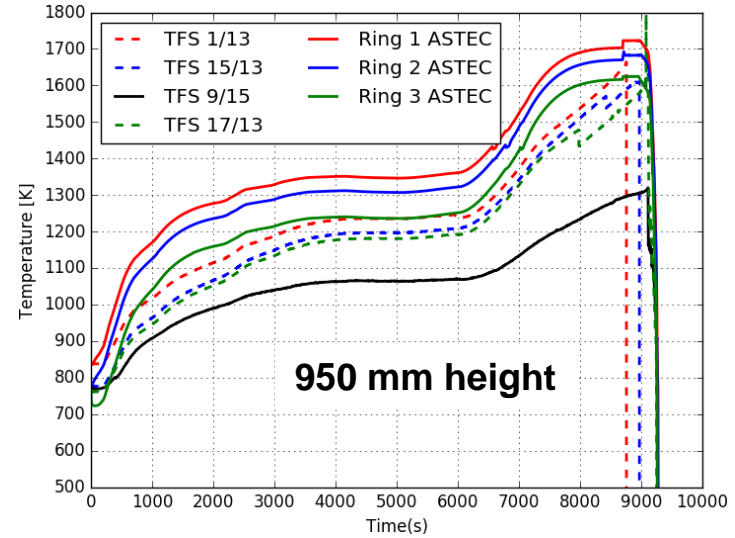
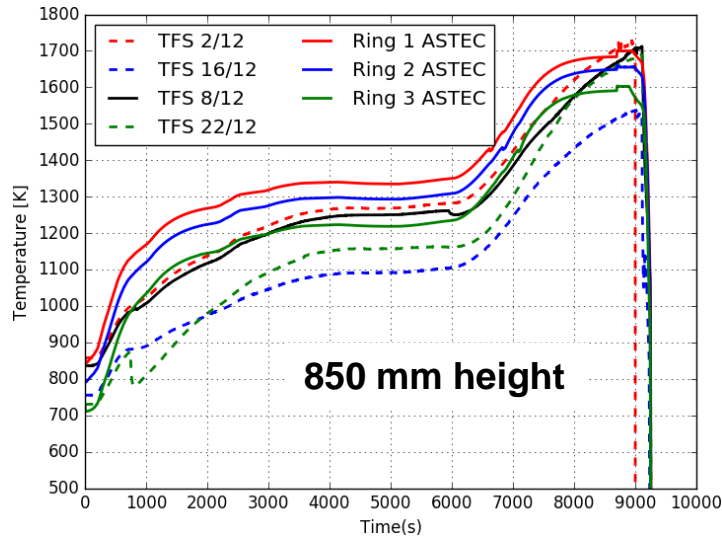
$$E_B = 594354 \text{ J/mol}$$

$$A_{Fe} = 2.4 \cdot 10^6 \text{ g}^2/\text{cm}^4 \text{ s}$$

$$E_{Fe} = 352513 \text{ J/mol}$$

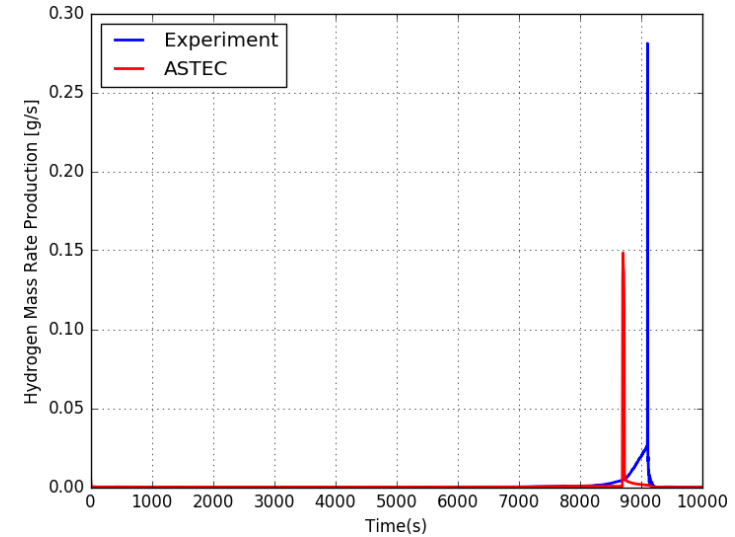
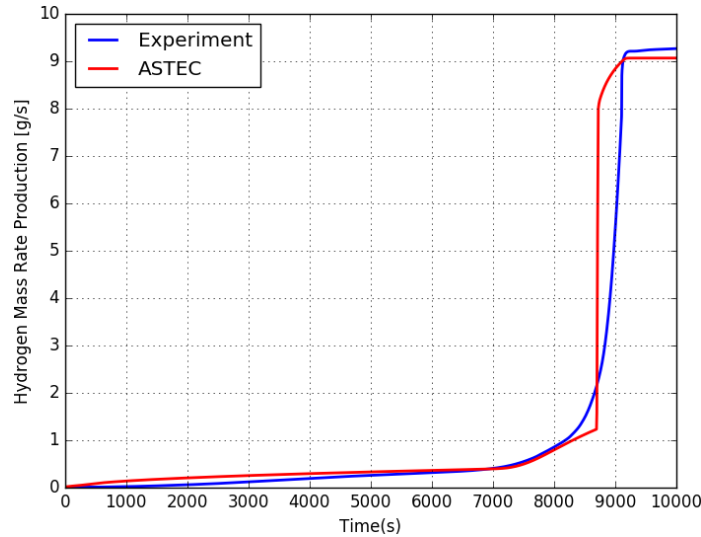


# ASTEC Results: Clad Temp. @850 and @950 mm Height



- Results exceed the exp. of about 100 degree in the pre-oxidation phase in Ring 1 (@850 mm) and in the Ring 1 and 2 (@950 mm height)
- Better agreement in Ring 2 and 3 (@850 mm) and Ring 3 (@950 mm)
- **Maximum temperatures reasonably well reproduced**

# ASTEC Results: Hydrogen Production



- **The final amount of H<sub>2</sub> is reasonably well reproduced**
- ASTEC results show a good agreement with exp. up about 8000 s
- Escalation is anticipated in time with about 50% of the mass rate compared with the experiment
- **'Smooth' kinetics behavior is not reproduced**

# Conclusion

- The validation activity of the ASTEC code against the QUENCH bundle tests is going on since long at KIT
- **The activity is a pillar of the KIT strategy on the analysis of hypothetical SAs in current and innovative NPPs**
- **ASTEC is able to properly reproduce the key phenomena and/or the experimental results of the QUENCH bundle tests**
- Efforts are currently devoted to analyze the QUENCH tests employing ATF materials in the frame of:
  - **The OECD/NEA QUENCH-ATF project**
  - **The IAEA T12032 CRP 'ATF-TS'**
  - **The development and the implementation in ASTEC of a physical model for the oxidation of FeCrAl cladding materials (tight connection with IRSN and the QUENCH team)**

# Acknowledgement

The authors wish to acknowledge the QUENCH team for the great support to the KIT/INR computation team

**Special thank to J. Stuckert, M. Steinbrück, and M. Große for their continuous support, suggestions, and availability**