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Influence of the macropore structure on heat and mass transfer inside catalytic washcoats

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Motivation

Results

The performance of catalytic coated monolith reactors, technically used in the reduction of pollutants and greenhouse gases, is strongly limited by heat and mass transport within the porous washcoat. Spatially resolved multiscale modelling improves the understanding of the processes inside the reactor and allows to optimize the catalyst design. In this contribution an approach to model the fluid flow inside an overflowed macroscopic pore structure coupled with transport and reaction within the mesoporous catalyst is presented. The simulations are used to study the impact of the macroscopic pore structure on transport phenomena and catalytic reaction.

Methodology

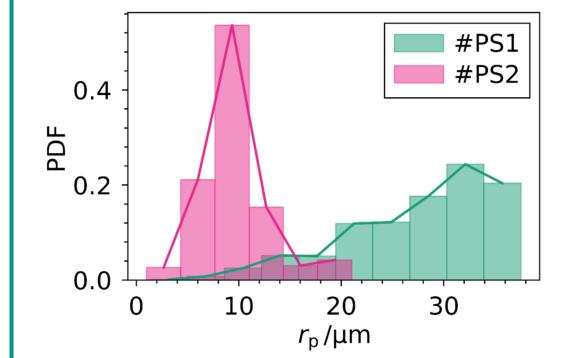
Domain and simulation setup

The pore structure (PS) is synthetically generated with a defined porosity using the Python package PoreSpy [1]. The resulting TIFF stack is converted into a surface mesh with the open-source software Blender and inplemented into the following geometry:

Symmetry wall (adiabatic,

impermeable, slip)

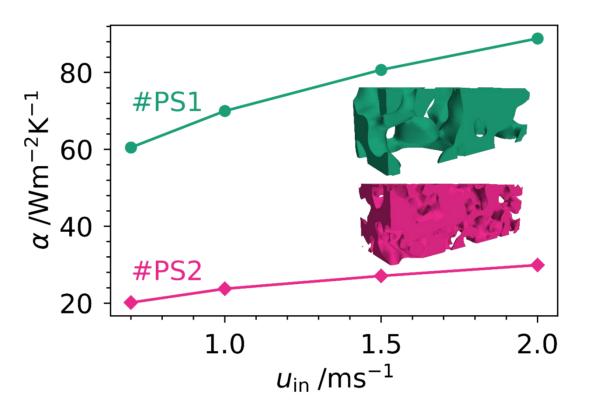
Pore-structure



	Е	A/mm^2	$ au_{\chi}$	$ au_{\mathcal{Y}}$	$ au_{Z}$
#PS1	0.5	0.10	1.73	1.37	1.62
#PS2	0.5	0.22	1.71	1.66	1.59

Tortuosity τ calculated with the method presented by Cooper et al. [5]

Heat transfer between pore-wall and fluid



- Pore structure with smaller pores and higher surface area (#PS2) results in a decreased heat transfer coefficient α due to less convective transport
- Optimal pore structure is a trade-off between surface area and convective transport

mesoporous catalyst decreases

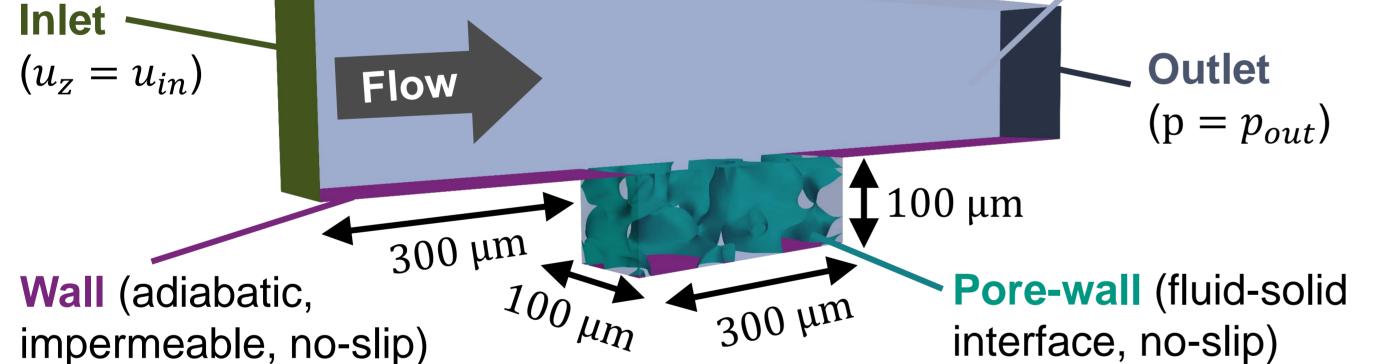
with increasing inlet velocity.

Inlet velocity has a small impact

on the catalyst efficiency η_{meso}

Catalytic reaction within the pore-structure

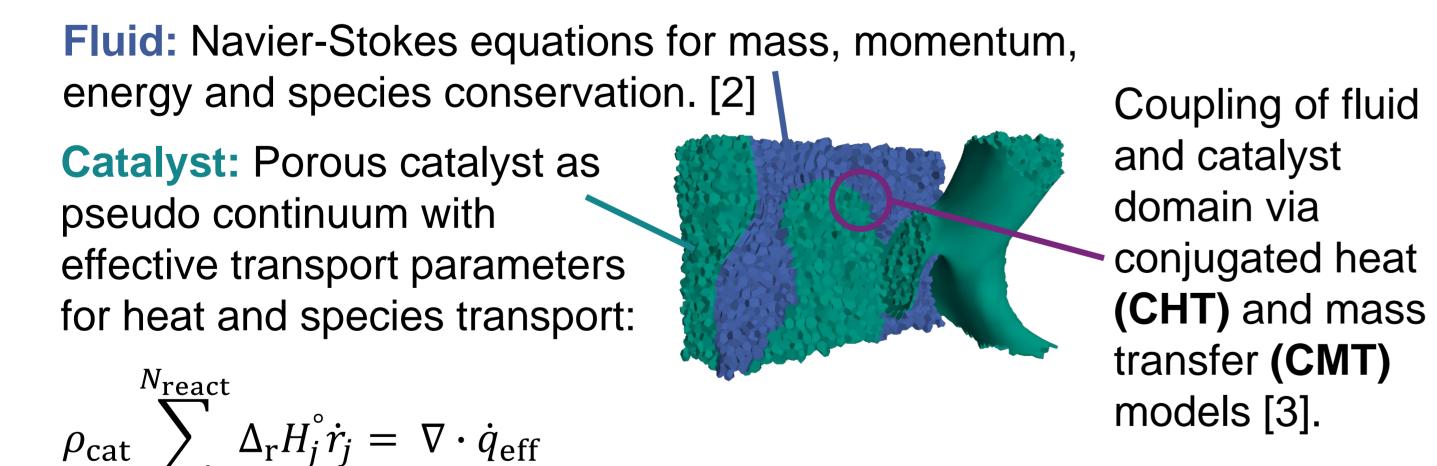
Pore-structure: #PS1; **Boundary conditions**: $T_{in} = 500 K$, $x_{in,CO} = 0.075$, $x_{in,O_2} = 0.039$, $x_{in,CO_2} = 0$, $x_{in,Ar} = 0.886$, $p_{out} = 1$ atm.



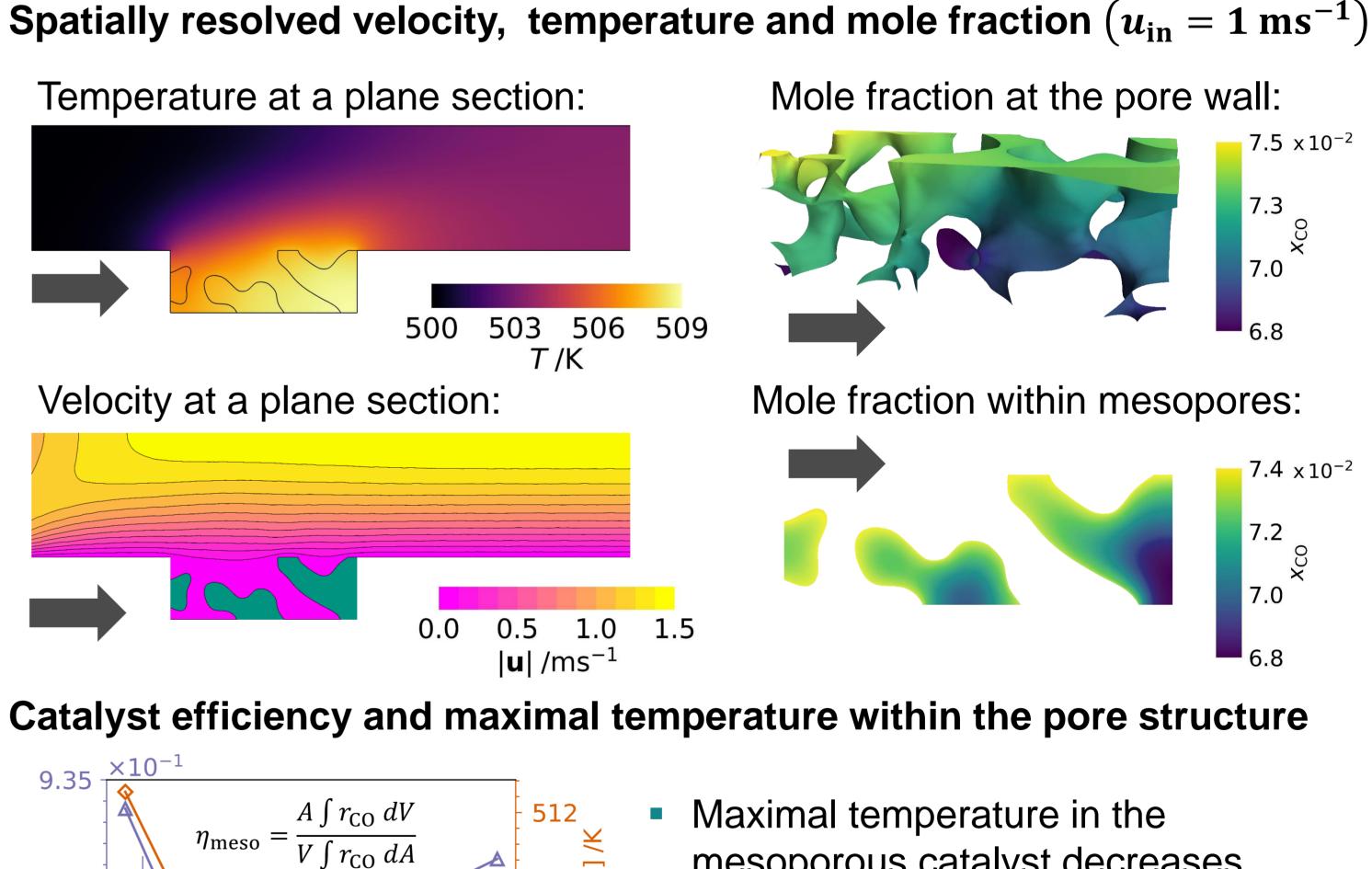
1100 µm

The entire domain is discretized using polyhedral volume cells to solve the governing equations with the finite volume method.

Pore-resolved CFD coupled with catalytic reaction



Fickian approach for diffusive fluxes *J*.



 $Mw_i\rho_{\text{cat}}\sum_{j=1}^{N_{\text{react}}}v_{i,j}\dot{r}_j = \nabla \cdot \dot{J}_{\text{eff},i}$

Considering Knudsen diffusion within the mesoporous catalyst phase by the Wilke-Bosanquet approximation.

As a model reaction, the oxidation of CO to CO_2 over a platinum catalyst is implemented using the reaction rate according to Shishu et al. [4].

References

[1] J.Gostick et al., J. Open Source Softwa., 2019, 4 (37), 1296 DOI:10.21105/joss.01296. [2] Jakobsen, Chemical reactor modeling, Springer, 2014, DOI: <u>10.1007/978-3-319-05092-8</u>. [3] Kutscherauer et al., Eng. Appl. Comput. Fluid Mech. 18 (1), 2024, DOI: 10.1080/19942060.2023.2292100. [4] Shishu et al., Johns. Matthey technol. rev., 1974, 18, 58-64, DOI: <u>10.1595/003214074X1825864</u>. [5] Cooper et al., J. Power Sources, 2014, 247, 1033-1039, DOI: <u>10.1016/j.jpowsour.2013.04.156</u>.

Conclusion and outlook

 $u_{\rm in}/{\rm ms}^{-1}$

1.5

1.0

စ္တ **9.34**

9.33

0.5

ηm

This work demonstrates how pore-resolved simulations of catalytic washcoats can contribute to a better understanding of the interplay between transport and reaction. In the future, the non-reactive phase of the macroporous washcoat will be included and the more accurate Maxwell-Stefan diffusion approach will be implemented.

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