EUROfusion

Design advancements of the HCPB BB and TER system for DEMO

Guangming Zhou[1], David Alonso[2], Ion Cristescu[1], Christophe Garnier[3], Francisco A. Hernández[1,4], Béla Kiss[5], Christina Koehly[1], Luis Maqueda[2], Carlos Moreno[6], Iole Palermo[7], Jin Hun Park[1], Volker Pasler[1], Anoop Retheesh[1], Álvaro Yáñez[2]

[1] Karlsruhe Institute of Technology, Germany
[2] ESTEYCO, Spain
[3] CEA, France
[4] EUROfusion PMU, Germany
[5] Budapest University of Technology and Economics, Hungary
[6] Heffen Technologies, Spain
[7] CIEMAT, Spain

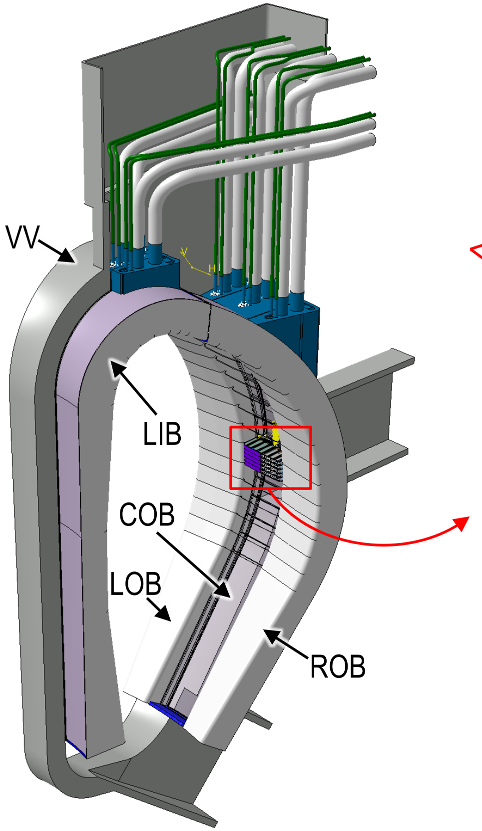
Breeding Blanket Project in EUROfusion

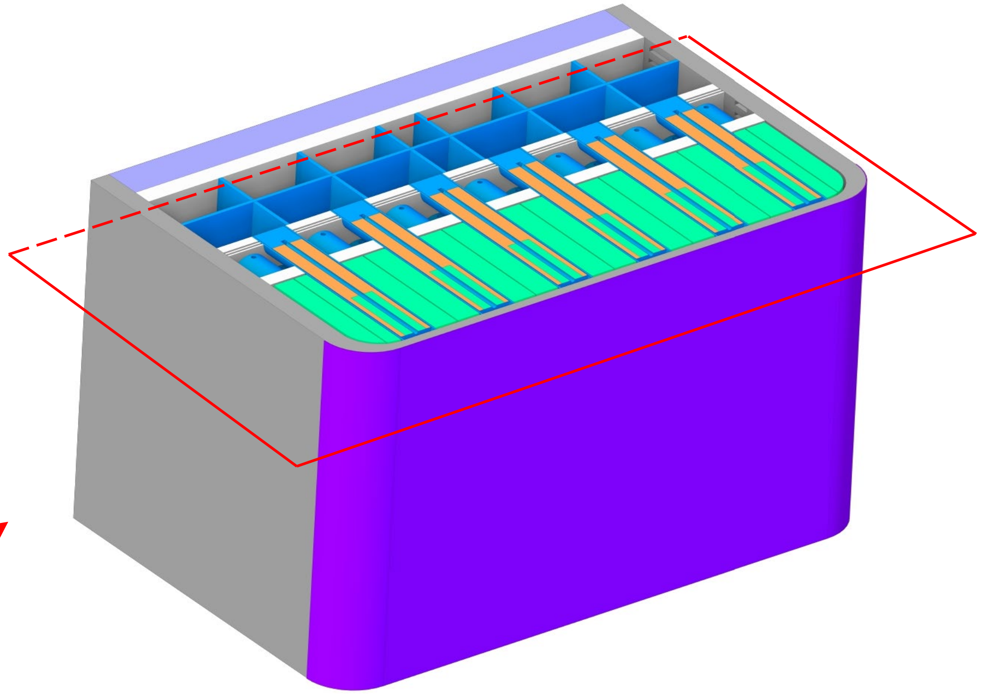
This work has been carried out within the framework of the EUROfusion Consortium, funded by the European Union via the Euratom Research and Training Programme (Grant Agreement No 101052200 — EUROfusion). Views and opinions expressed are however those of the author(s) only and do not necessarily reflect those of the European Union or the European Commission.

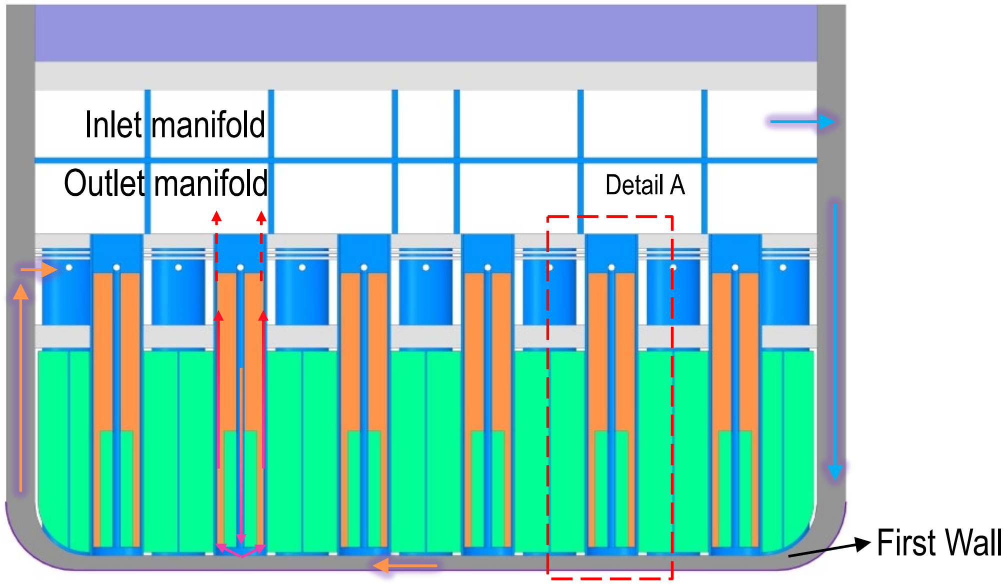
Outline

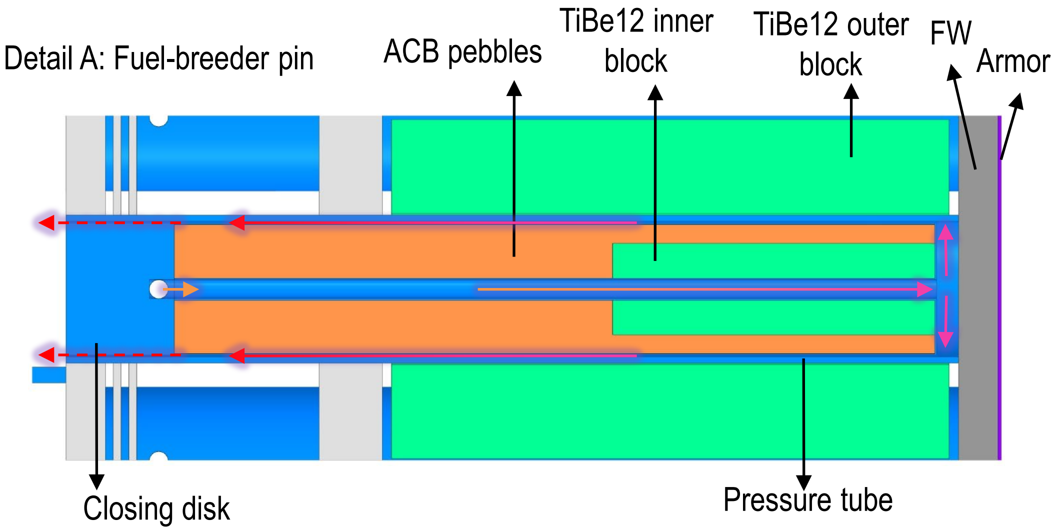
1. Current design of HCPB Breeding Blanket
2. Neutronics analysis
3. Thermal hydraulics analysis
4. Structural analysis
5. Design of HCPB Tritium Extraction and Recovery System
6. Conclusions

Design of high pressure purge gas HCPB (HCPB-BL2017-HP-v1)



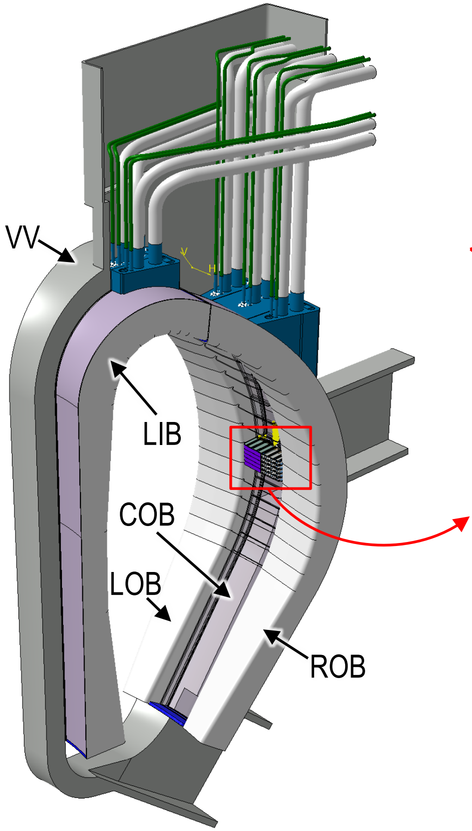


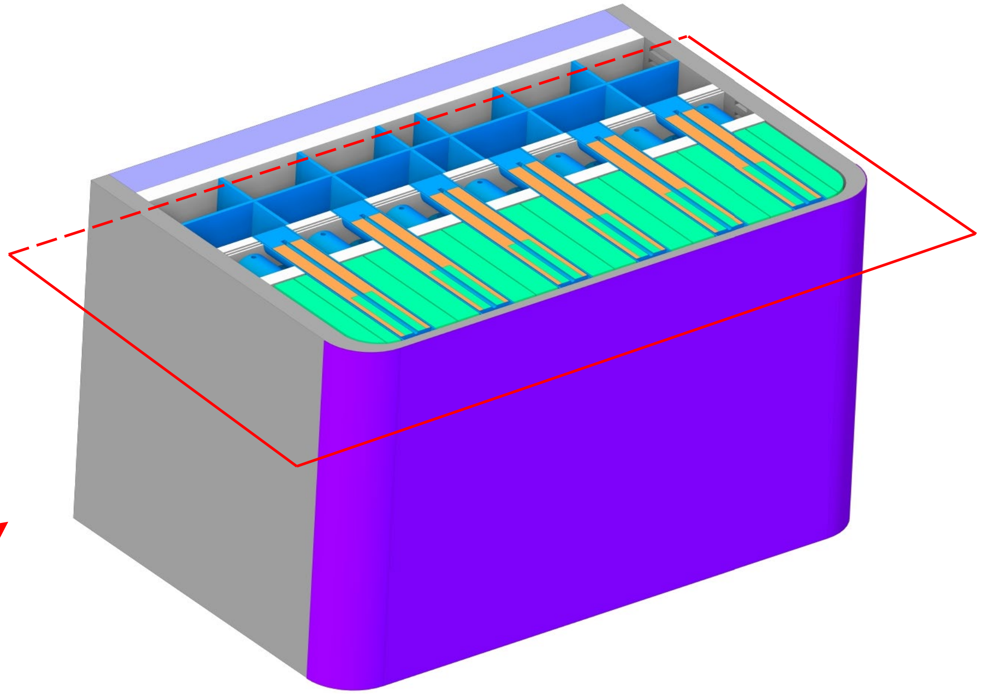


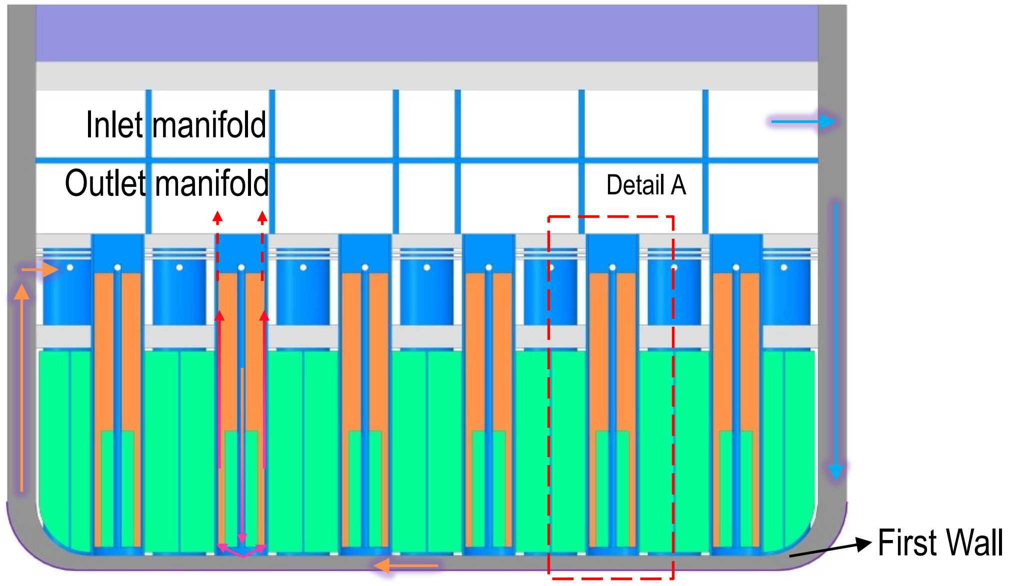


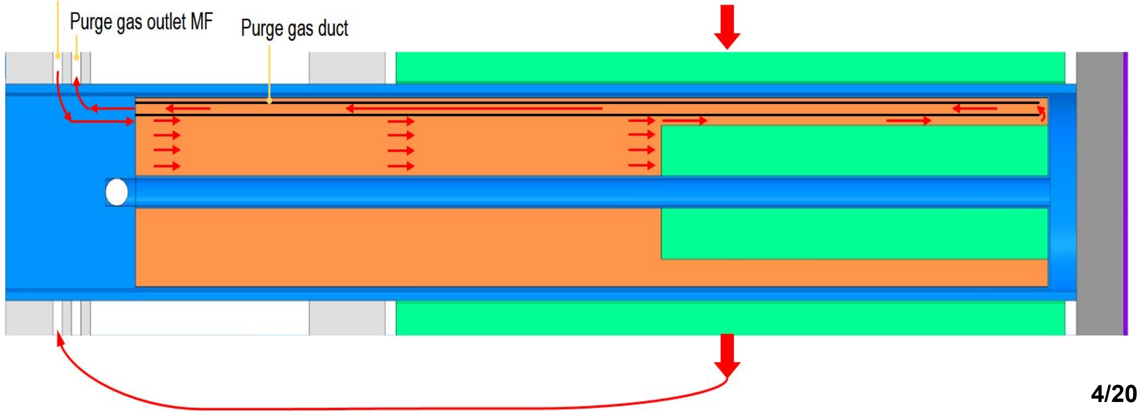
- Coolant: He @80 bar, 300-520°C
- Structural steel: Eurofer97
- Fuel-breeder pins contain advanced ceramic breeder (ACB) pebble
- T-extraction: He + 100 Pa H_2 @80 bar
- Inner beryllide block inside ACB pebble

Design of high pressure purge gas HCPB (HCPB-BL2017-HP-v1)









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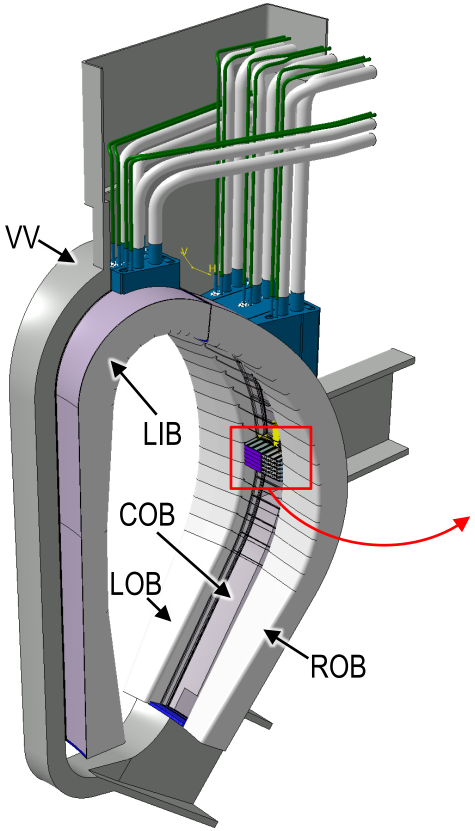
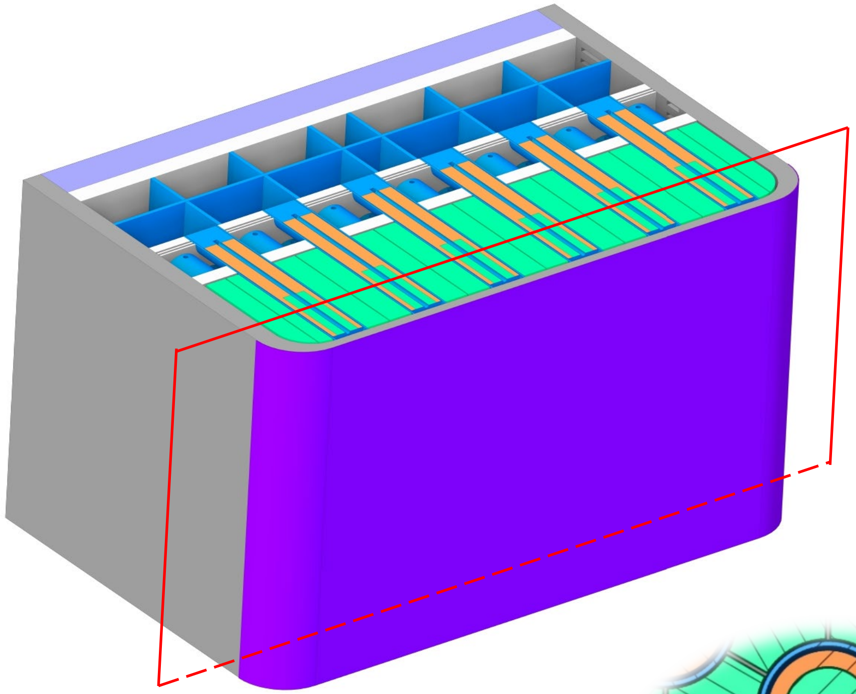
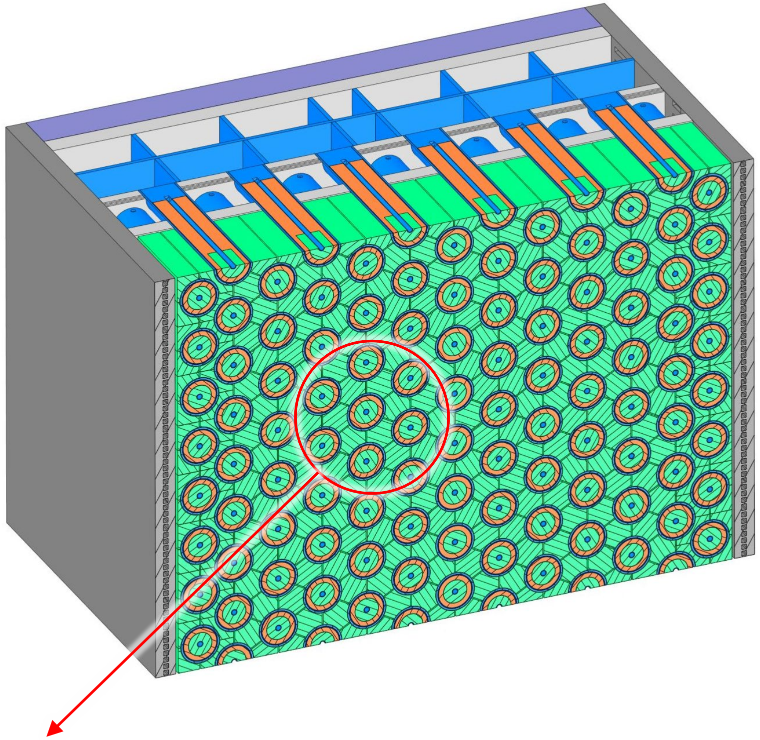
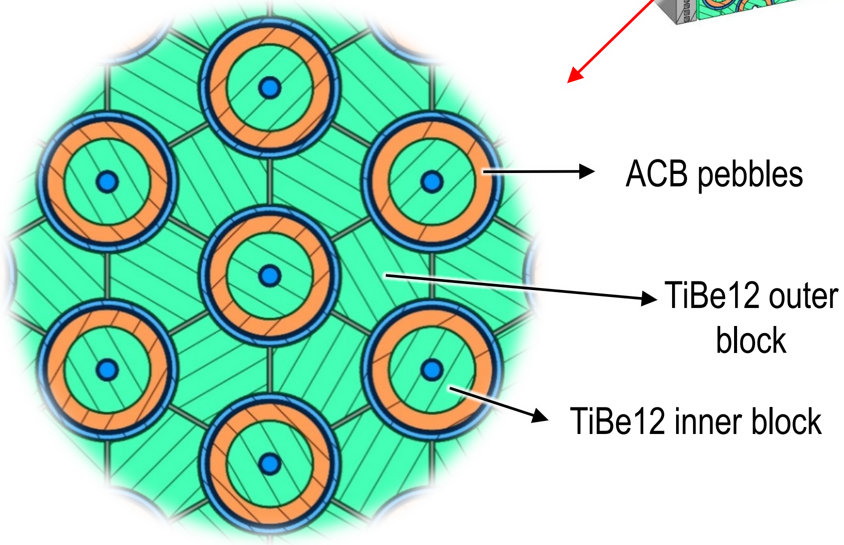




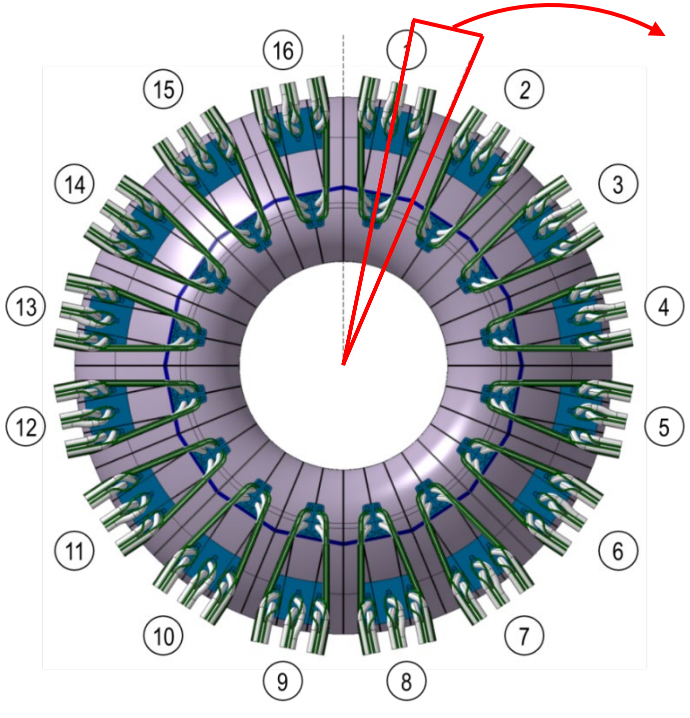




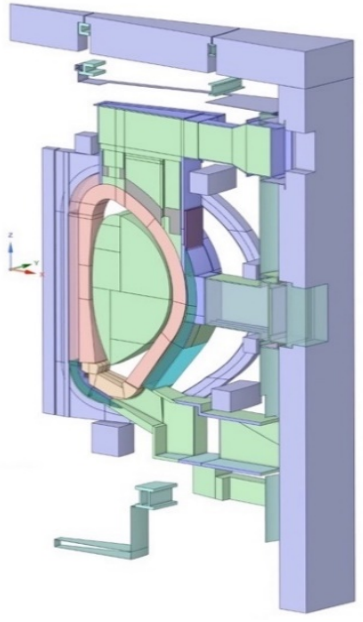
- Fuel-breeder pins arranged in triangular arrangement
- Beryllide neutron multiplier of triangular prism with lateral edges filleted

Tritium breeding assessment

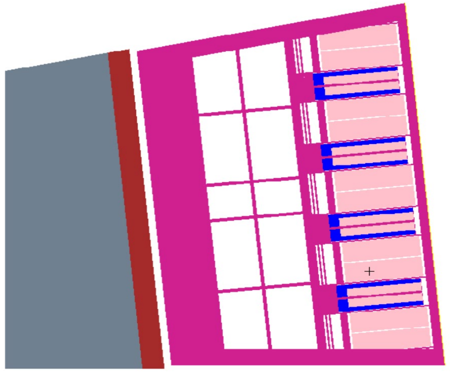
- **Without considering cut-outs**
  - 3D heterogenous model calculated using MCNP6.2 and JEFF-3.3
  - 11.25°: half of a sector of reactor



360° Model

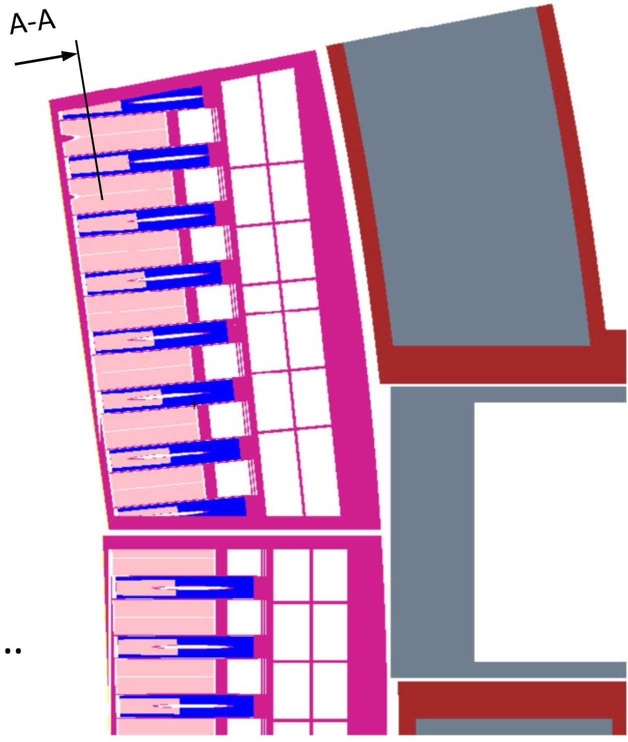


11.25° Model

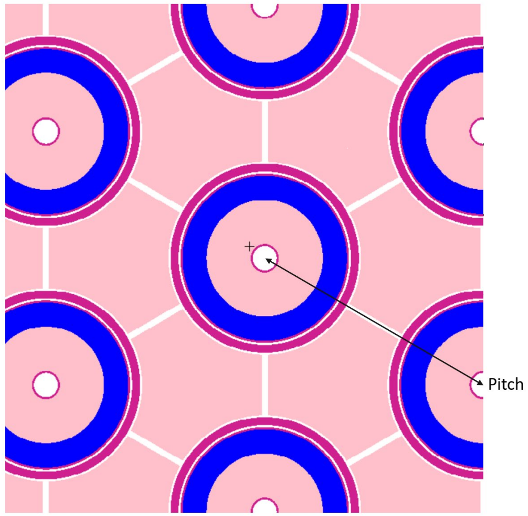


Radial-toroidal cut view - inboard

...



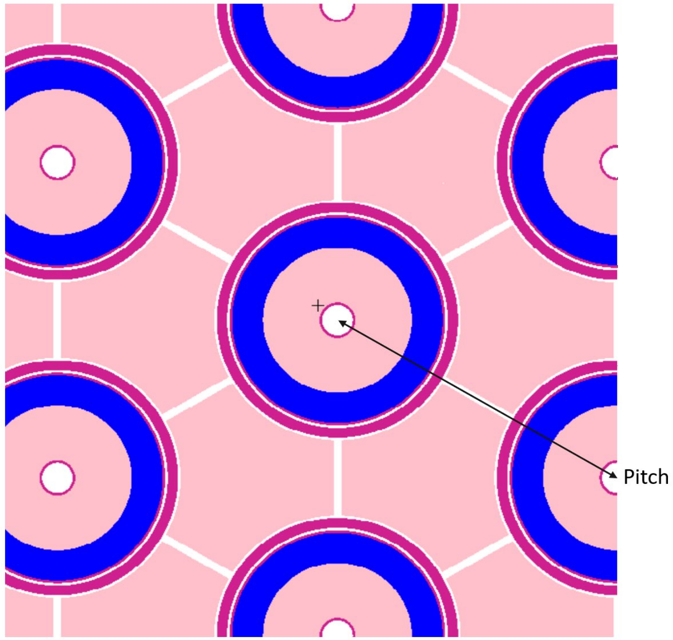
Radial-toroidal cut view - outboard



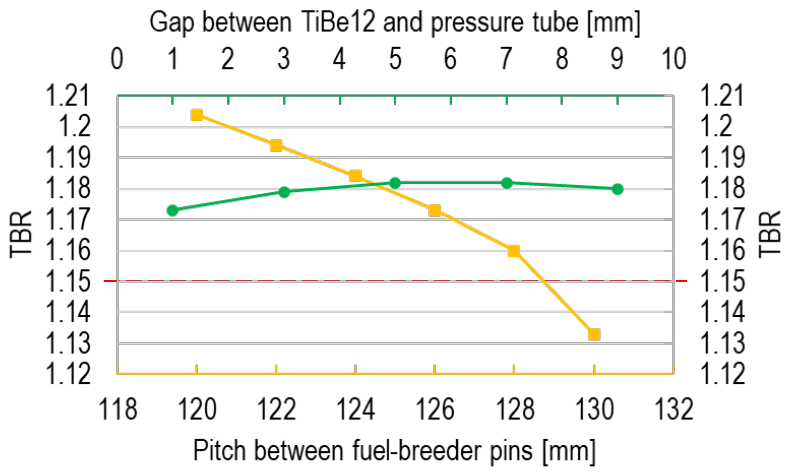
A-A: Poloidal-toroidal view

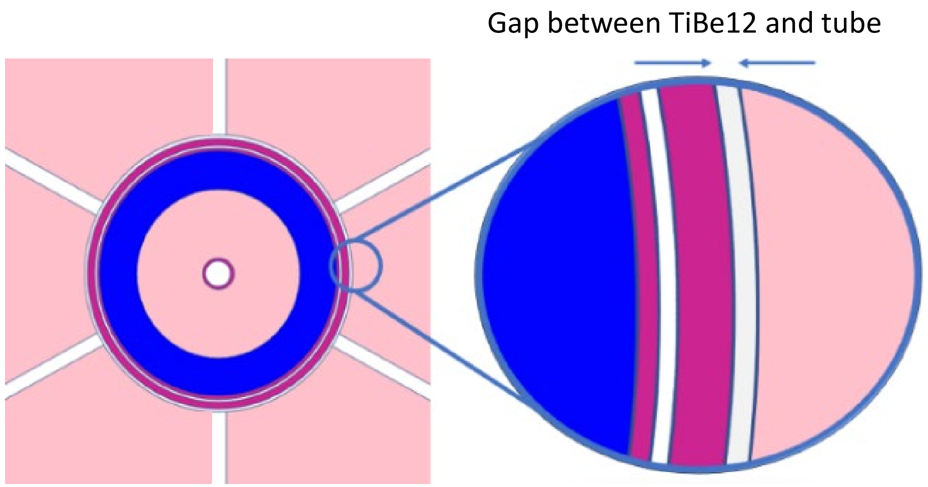
Tritium breeding assessment

- **Without considering cut-outs**
  - The smaller the pitch, the higher TBR (TBR=1.16~1.20 ±0.01%)
  - Larger gap facilitates neutron streaming, saturates at 5 mm



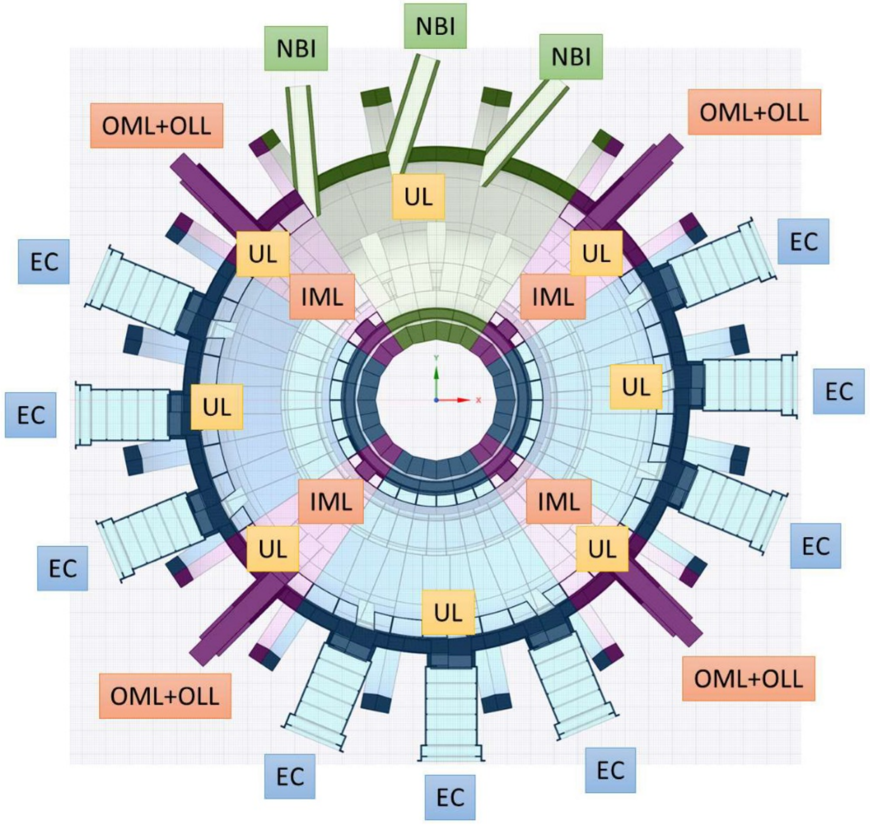
Pitch between two pins

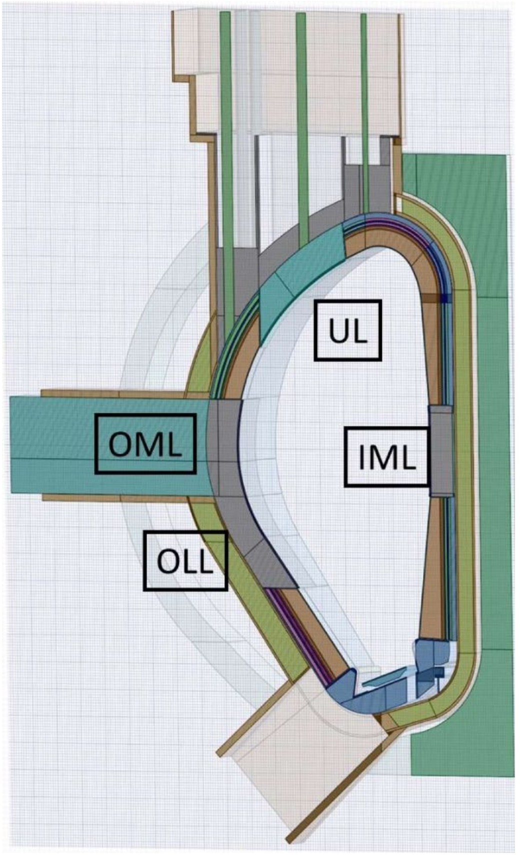




Without considering cut-out, TBR=1.16~1.20

Global tritium breeding assessment considering heating systems & limiters





Systems that cut breeding blanket

	ΔTBR Single IVC	Amount of systems in whole reactor	ΔTBR 360° Reactor
EC	0.22%	9	1.97%
NBI	0.22%	3	0.66%
UL	0.52%	8	4.14%
IML	0.19%	4	0.77%
OML	0.37%	4	1.49%
OLL	0.37%	4	1.49%
Total TBR reduction			**10.51%**

TBR=1.16~1.20 (Without cut-out)

TBR=1.04~1.07 (With cut-out)

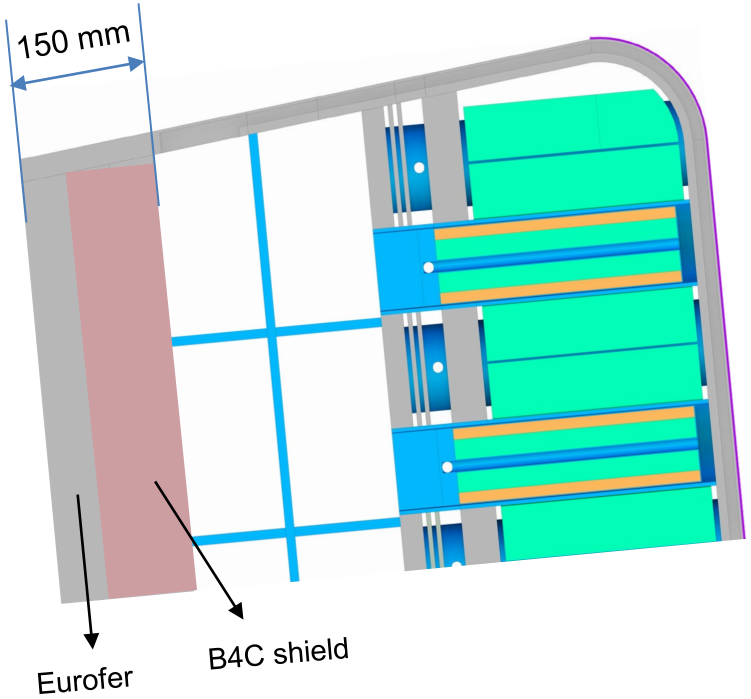
Shielding assessment

- Parametric neutronics analysis

Shield materials: B4C, WC, WB and hydrides

- ***Baseline***: 150 mm Eurofer
- ***v1***: 10 mm B_4C, 140 mm Eurofer
- ***v2***: 20 mm B_4C, 130 mm Eurofer
- ***v3:*** 30 mm B_4C, 120 mm Eurofer
- …
- ***v10***: 100 mm B_4C, 50 mm Eurofer

Shoshin A et al., 2021 *Fusion Eng Des* 168, 112426



HCPB inboard blanket

- Tritium and helium production in B_4C

$$^{10}_{5}B + ^{1}_{0}n \rightarrow ^{3}_{1}T + 2^{4}_{2}He$$

Shielding assessment

- Results

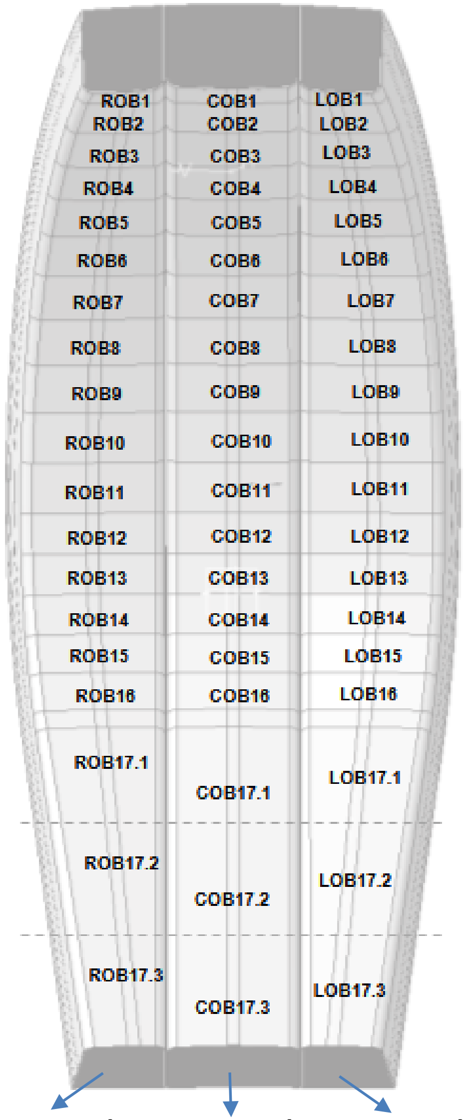
Cases	Nuclear heating at 1st cm of TFC (limit: 5e-5)	Neutron flux at 1st cm of TFC (limit: 1e9)	dpa/fpy at 1st cm of TFC (limit: 1.6e-5)	dpa/fpy at 1st cm of VV (limit: 4.5e-1)	He product. at 1st cm of VV (limit: 0.16)
	W/cm^3	$n/cm^2/s$	appm/fpy	appm/fpy	appm/fpy
Baseline	8.69e-5	2.21e9	1.81e-5	1.53e-1	0.56
v1	7.36e-5	2.07e9	1.69e-5	1.28e-1	0.42
v2	6.83e-5	2.29e9	1.24e-5	9.27e-2	0.35
v3	5.37e-5	1.82e9	1.42e-5	9.43e-2	0.29
v4	5.16e-5	1.74e9	1.50e-5	8.58e-2	0.27
v5	4.72e-5	1.66e9	1.40e-5	7.70e-2	0.24
v6	4.16e-5	1.57e9	1.41e-5	6.94e-2	0.22
v7	3.69e-5	1.47e9	1.41e-5	6.29e-2	0.18
v8	3.32e-5	1.43e9	1.24e-5	5.76e-2	0.17
v9	3.30e-5	1.41e9	1.27e-5	5.52e-2	0.16
v10	3.24e-5	1.40e9	1.24e-5	5.27e-2	0.15
v5_inverted	4.06e-5	1.65e9	1.28e-5	7.46e-2	0.19
v10_inverted	2.81e-5	1.33e9	1.16e-5	5.07e-2	0.14

- Maximum T and He production is in v10: 1.84 mol (5.52 g) T per FPY, 500 mol (2 kg) Helium per FPY in EU-DEMO

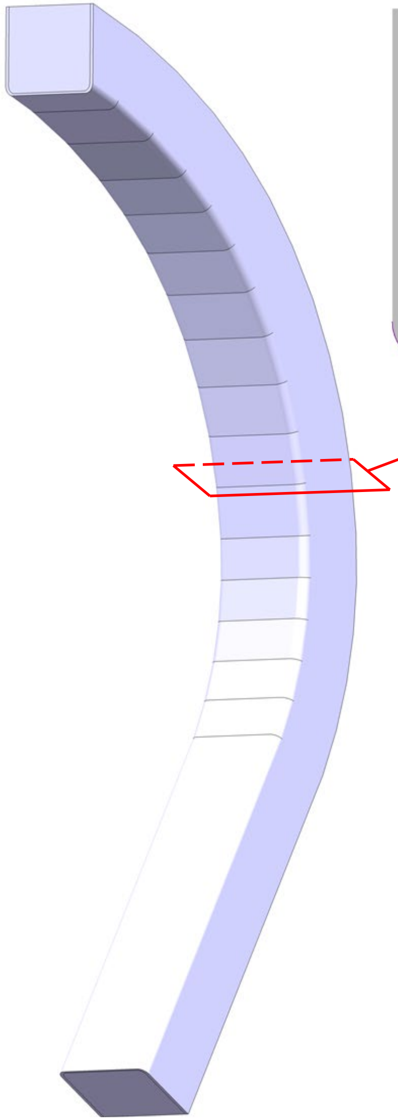
  Negligible, 117 kg T/fpy in EU-DEMO → 1e-28 [Pa·m³/(s·m²)] << Outgassing limit 1e-11

- 90 mm B_4C is needed for meeting all the requirements
- ITER-like solution seems feasible

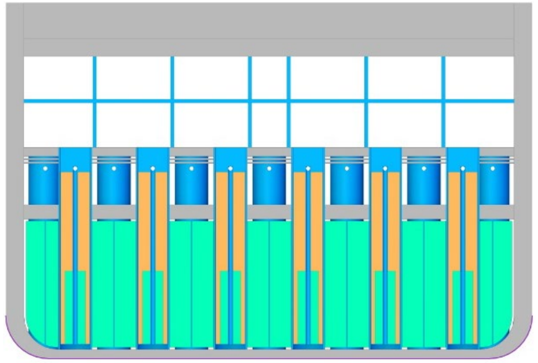
Geometry difference between central outboard and lateral outboard



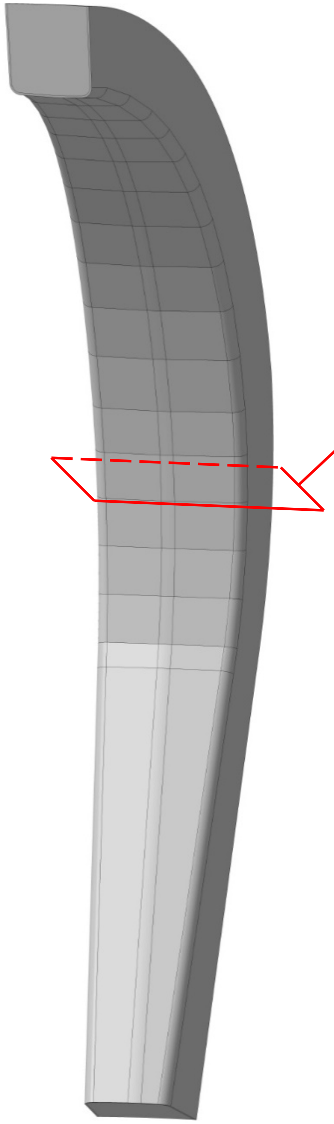
Lateral Central Lateral



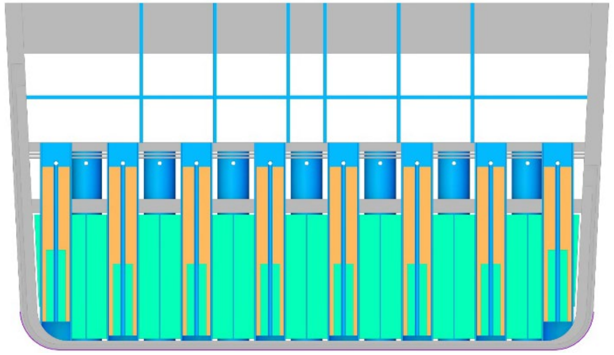
Central OB



Central OB at midplane

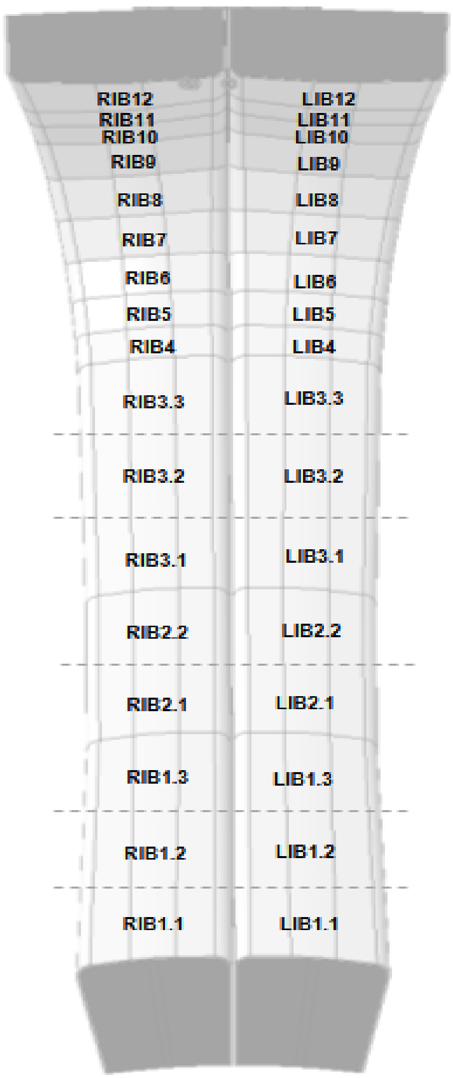


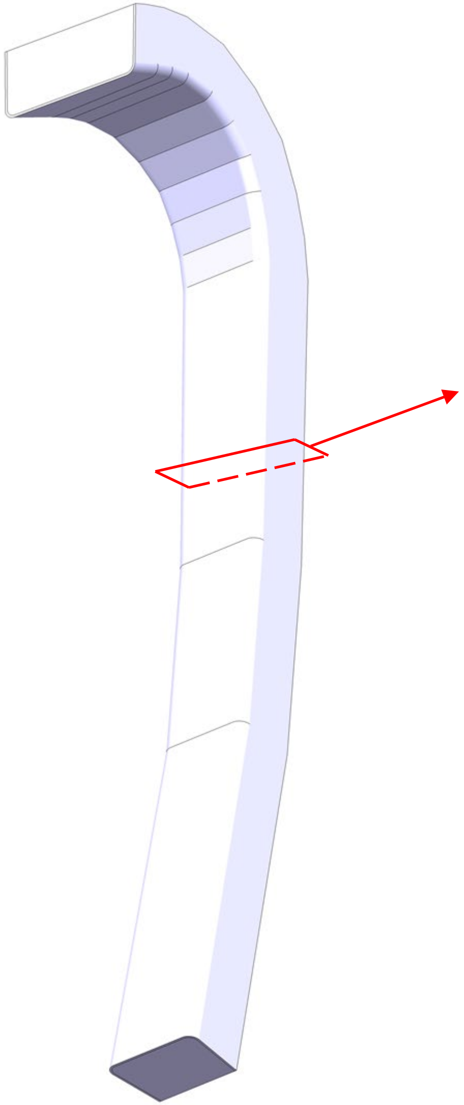
Lateral OB

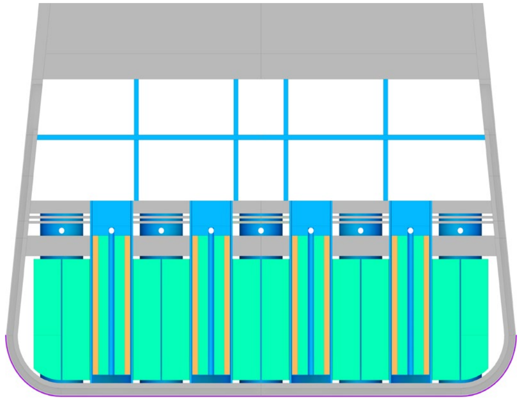


Lateral OB at midplane

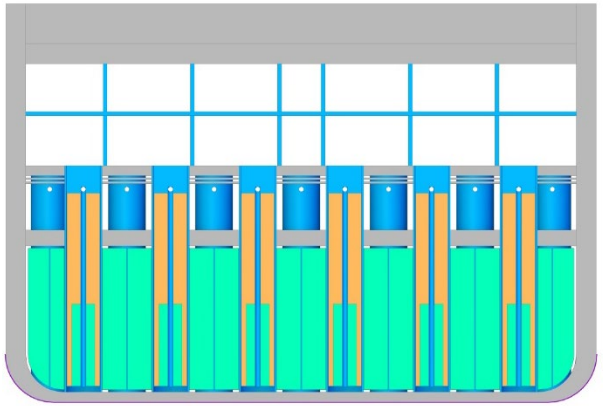
Geometry difference between central outboard and inboard





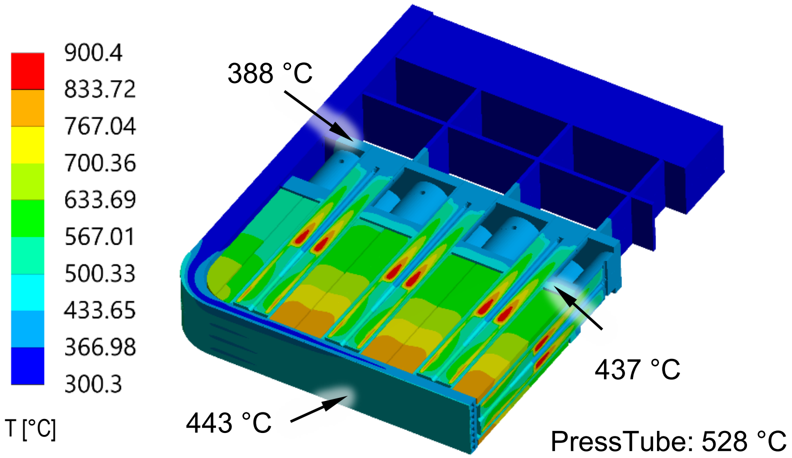


IB at midplane

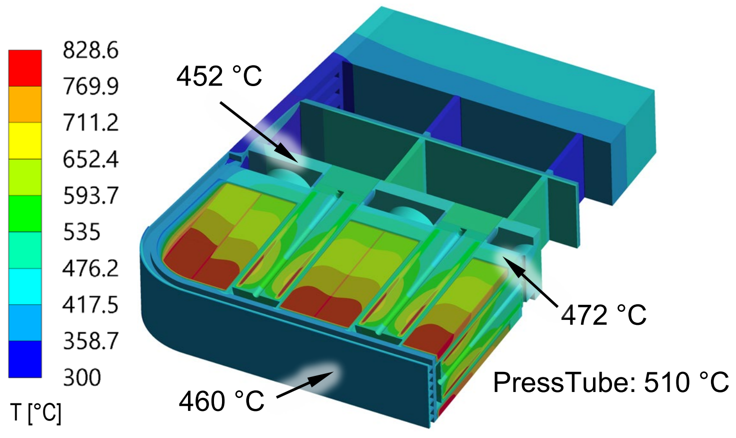


Central OB at midplane

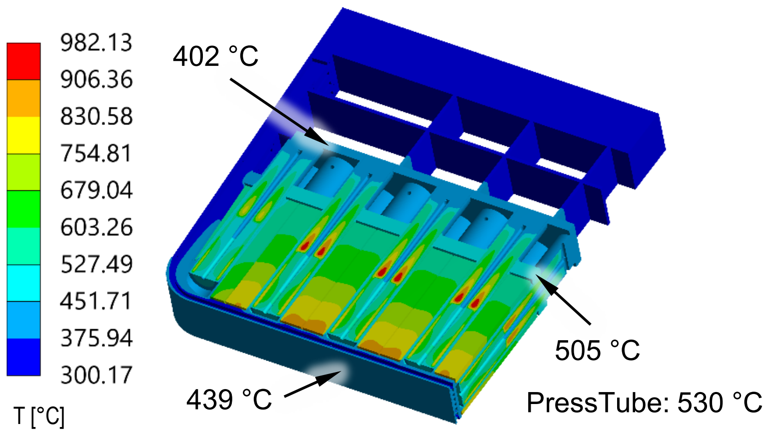
Thermal hydraulics: Temperature



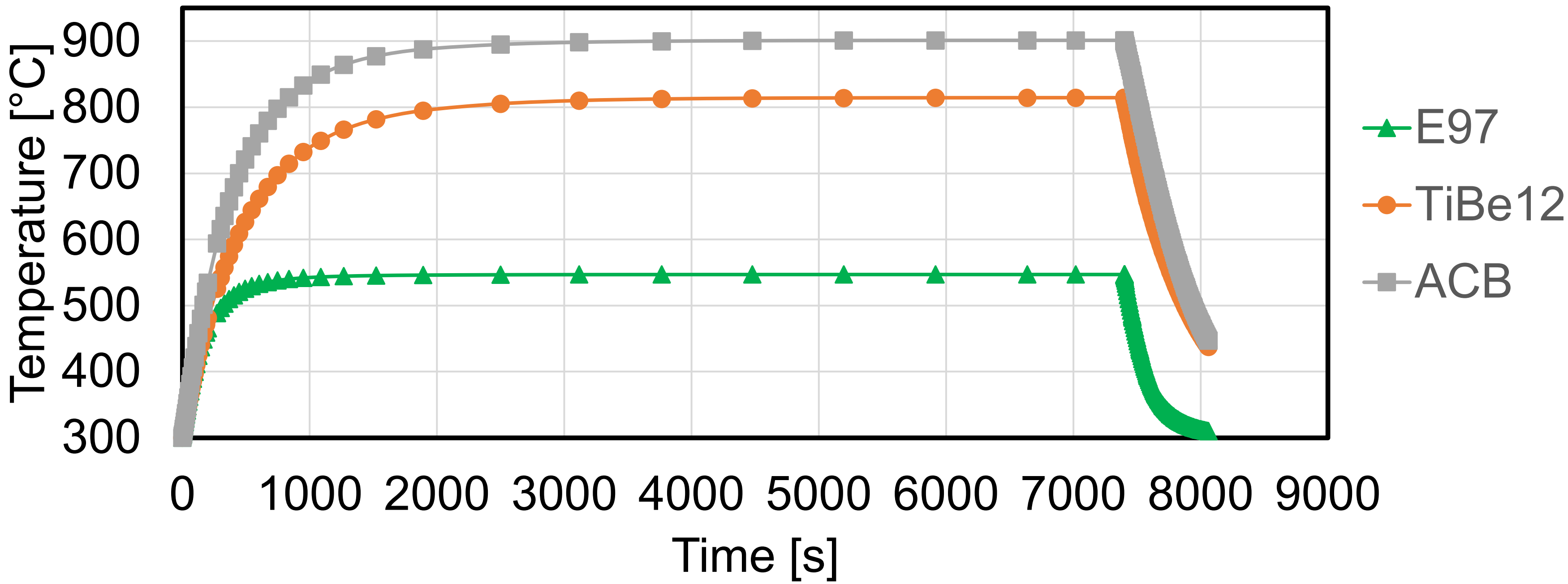
Temp. field of half unit-slice of COB



Temp. field of half unit-slice of LIB



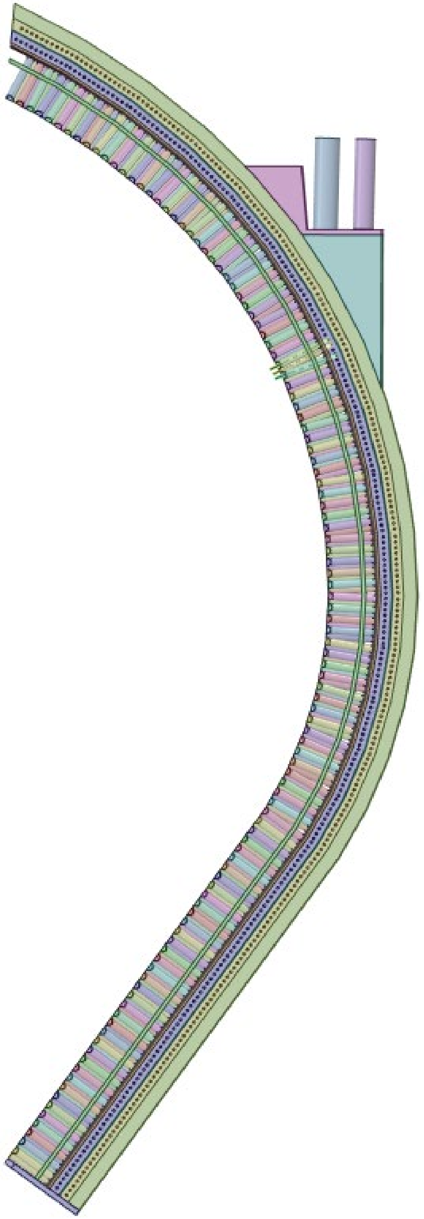
Temp. field of half unit-slice of LOB



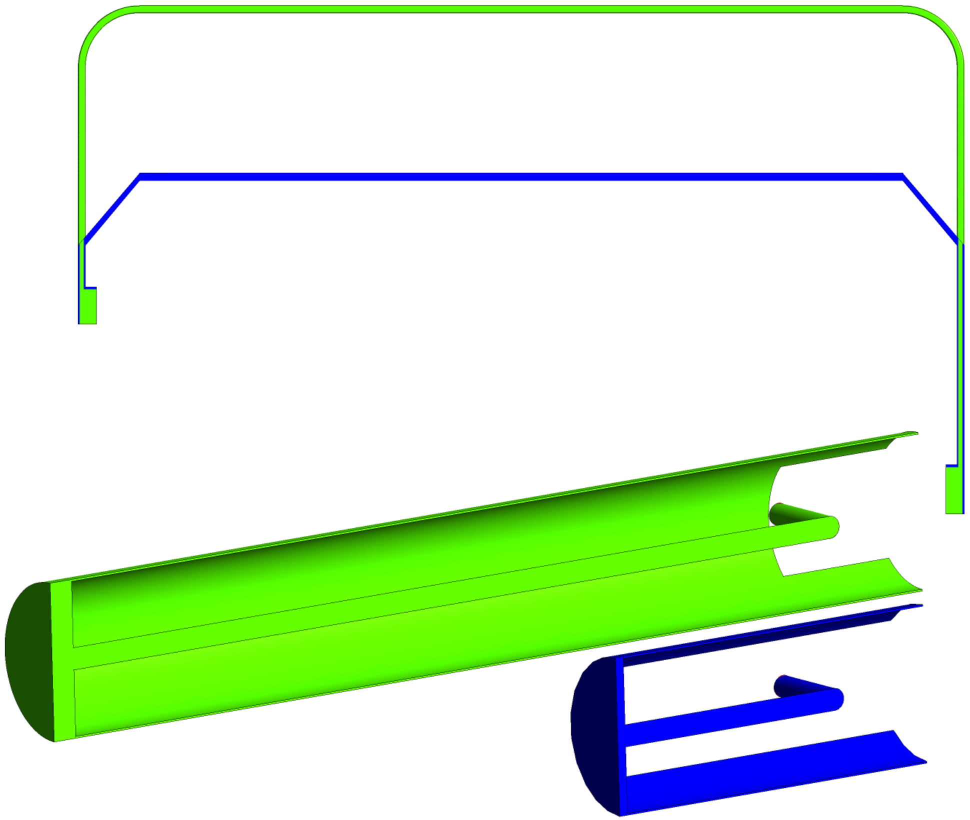
Temperatures of three unit slice within design limits

Transient thermal analysis shows that there is a thermal inertial in the blanket, especially in functional materials.

Thermal hydraulics: Flow distribution

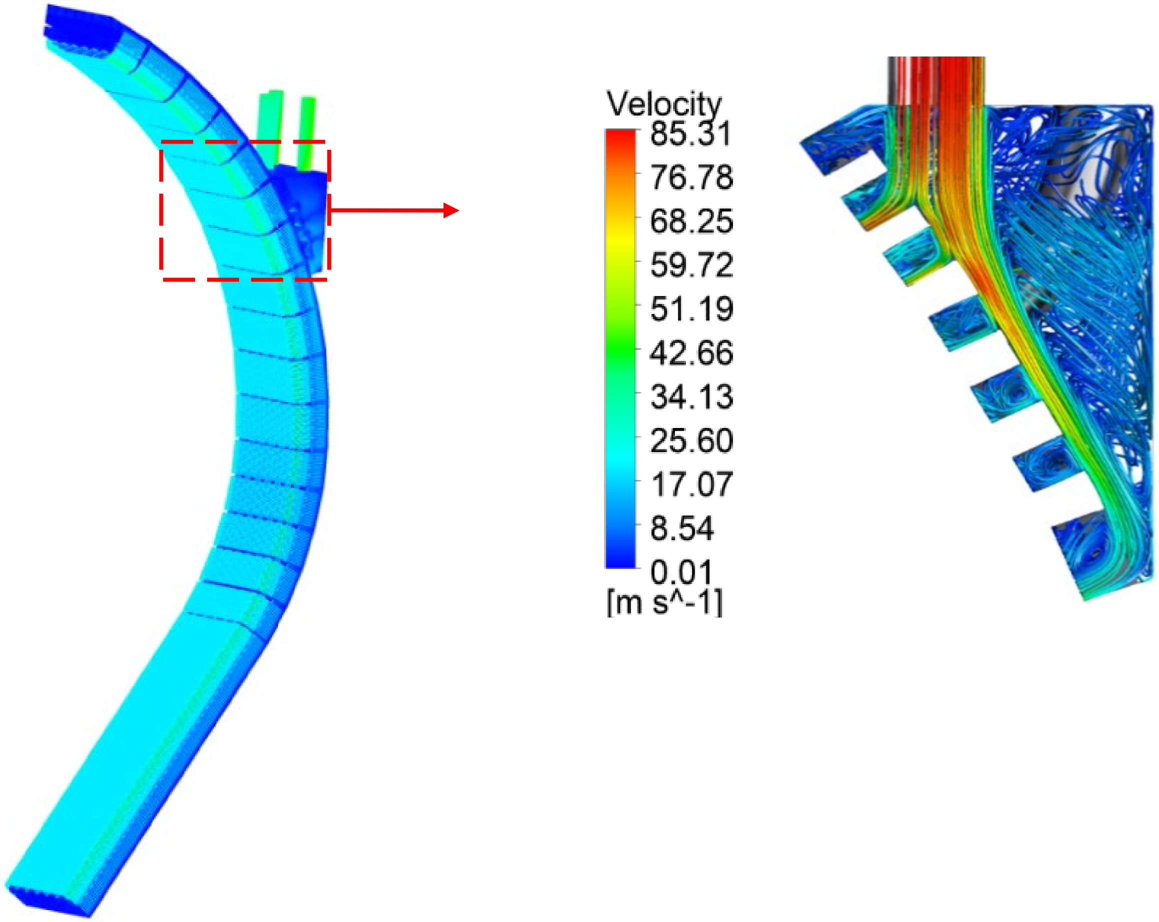


Porous media approach to reduce meshing and computing time

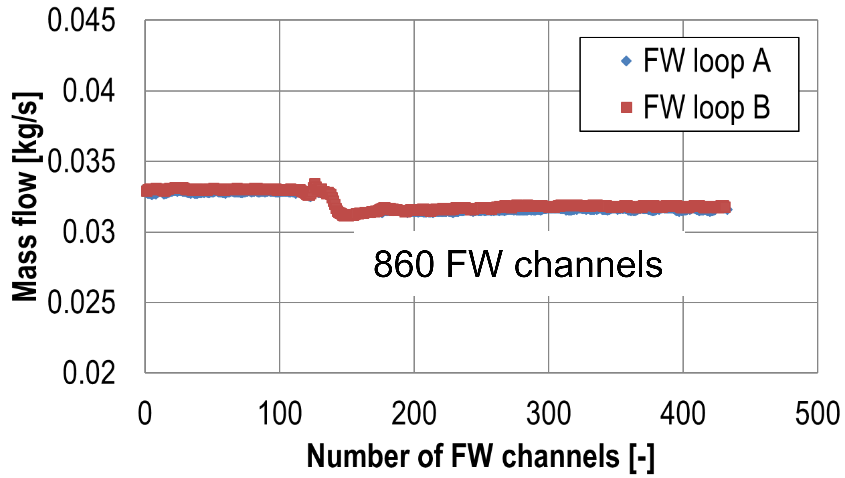


Novel method: Zhou G et al., 2020 *Nucl Fusion* 60, 096008.

Thermal hydraulics: Flow distribution

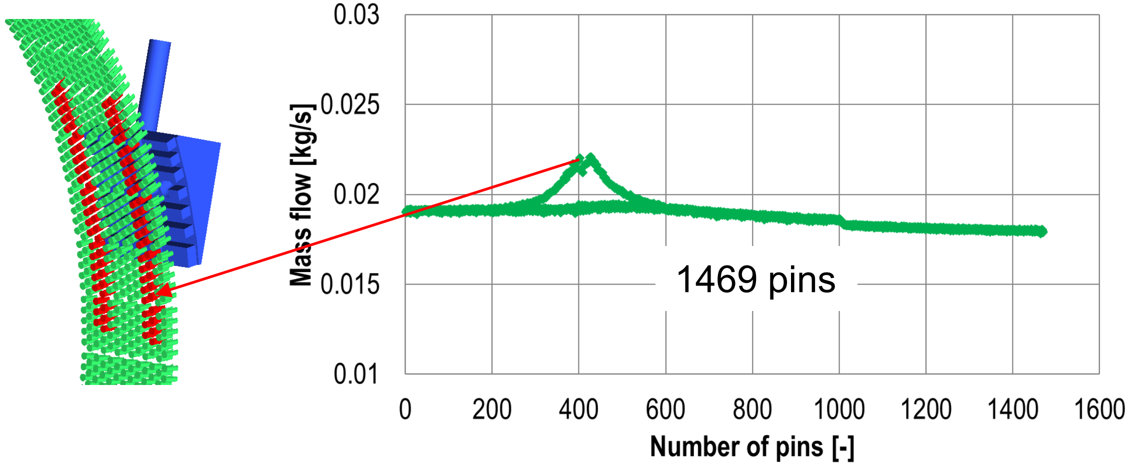


Flow streamline of blanket segment



Mass flow rate distribution in FW

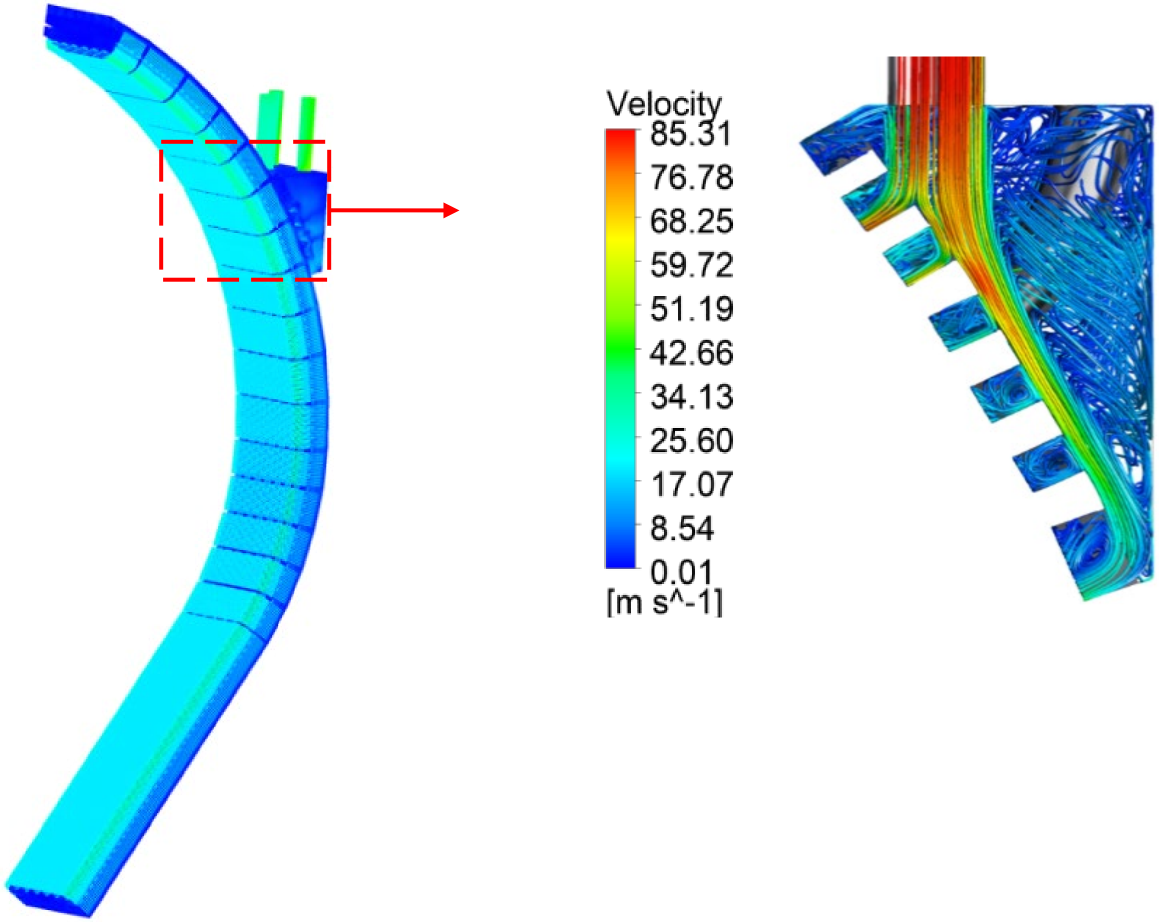
- Max deviation from target value: 4.4%



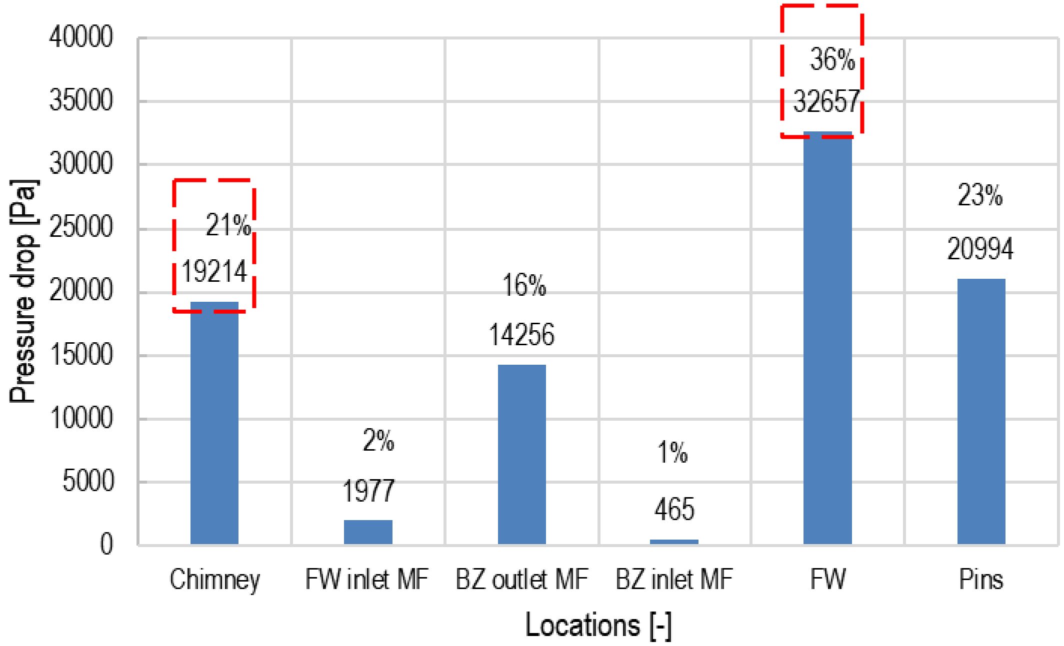
Mass flow rate distribution in pins

- Max deviation from target value: 17.3%

Thermal hydraulics: Pressure drop



Flow streamline of blanket segment

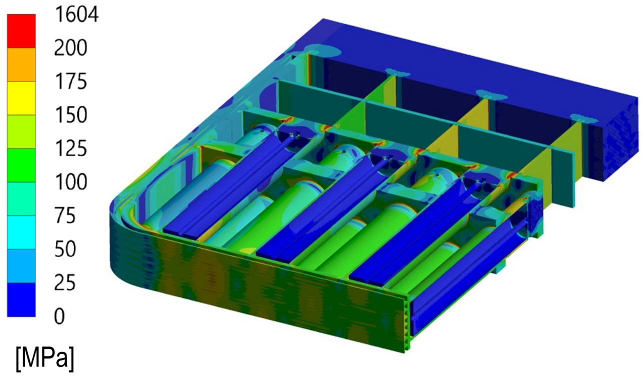


Pressure drop distribution

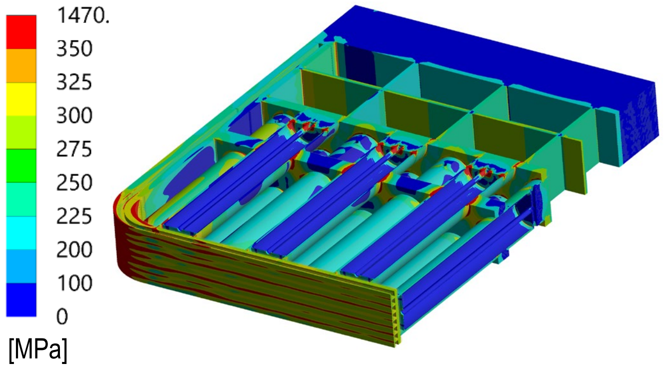
- Total pressure drop: 0.89 bar

Thermal mechanical assessment

- **Stress assessment using generalized plane strain**

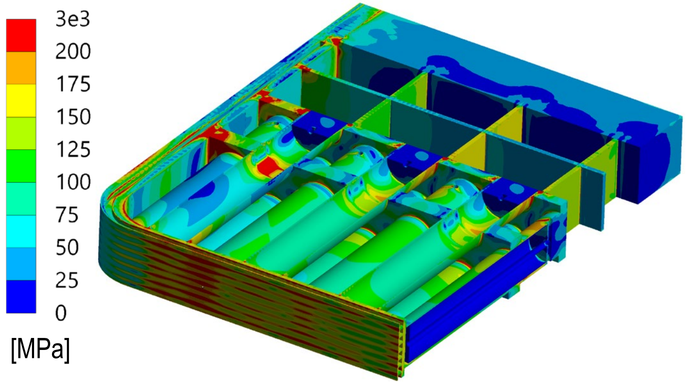


Primary stress of COB

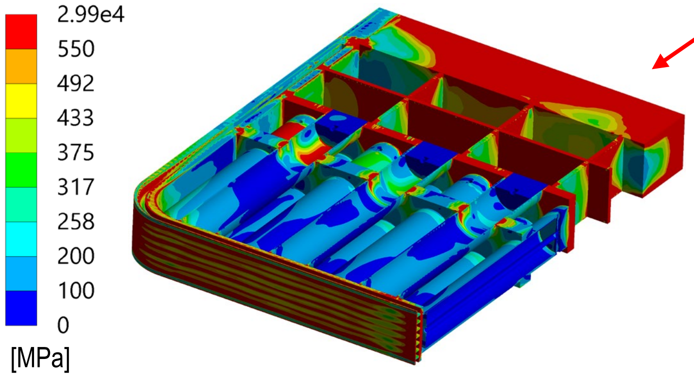


Primary+Secodary stress of COB

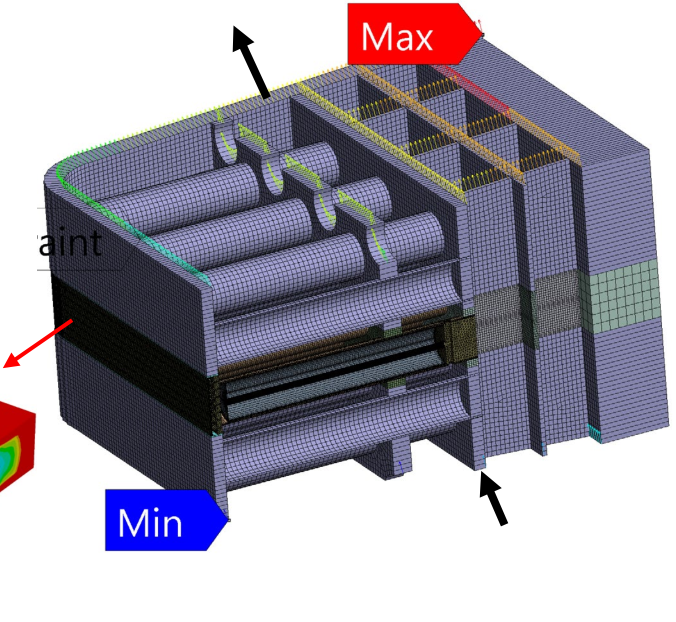
- **Stress assessment using submodelling technique**



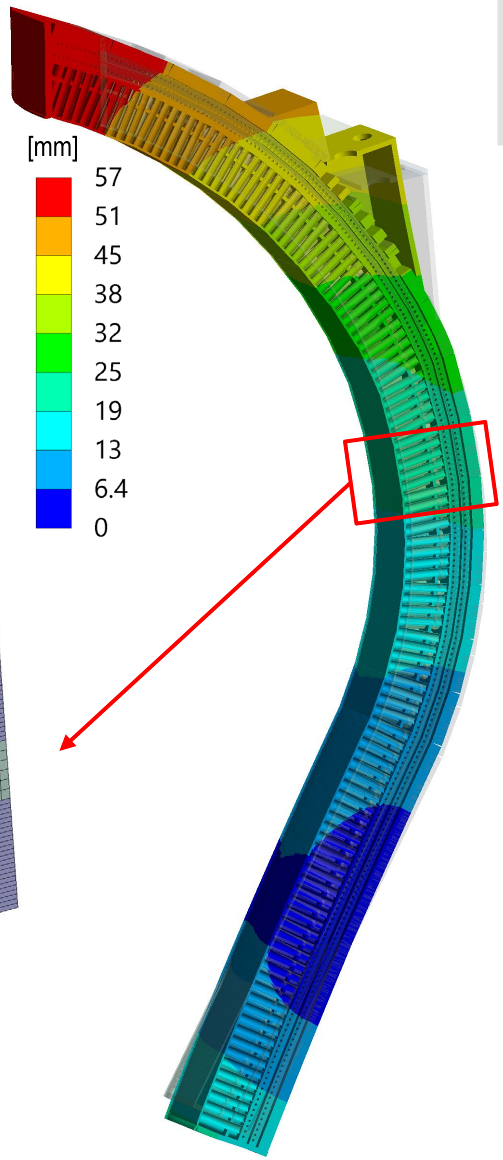
Primary stress of COB



Primary+Secodary stress of COB



Submodel



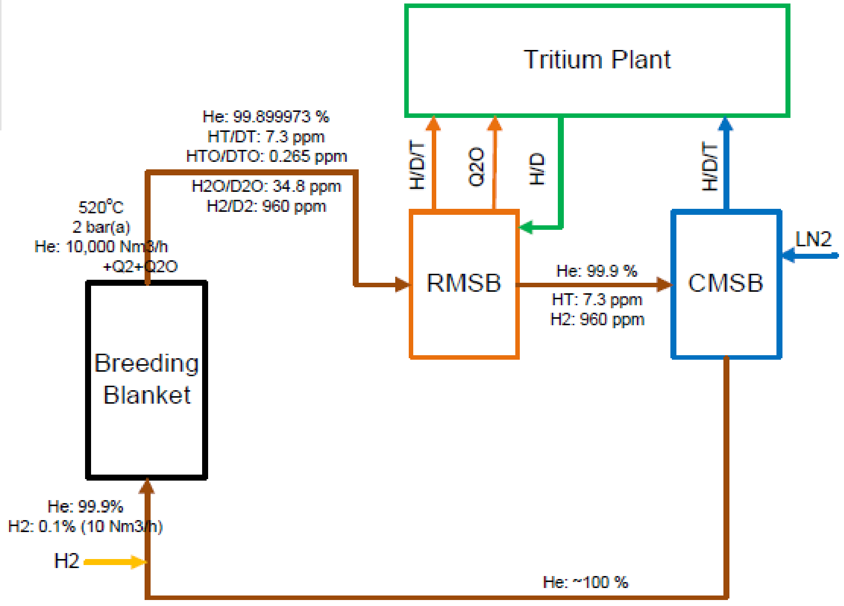
Displacement of global model

- Developed a sub-modelling technique to transfer the global displacement to submodel
- Generalized or plane strain boundary conditions not conservative
- Most critical regions met the immediate plastic instability, plastic collapse and thermal creep damage modes

Tritium Extraction and Recovery (TER) system

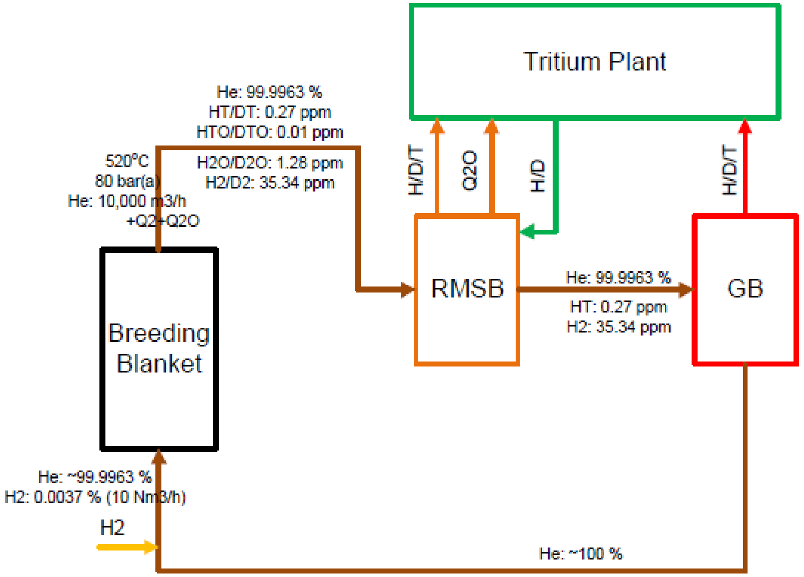
- Previous design
  - Two stages in series, first the adsorption of Q2O on the Reactive Molecular Sieve Bed (RMSB), thereafter the adsorption of Q2 on the Cryogenic Molecular Sieve Bed (CMSB) at 77 K

    Q = H, D, T
  - Tritium recovered via isotope exchange on RMSB and by heating-up of the CMSB
  - Extrapolated to DEMO scale is realizable, high Tech. Readiness Level



2 bar purge gas

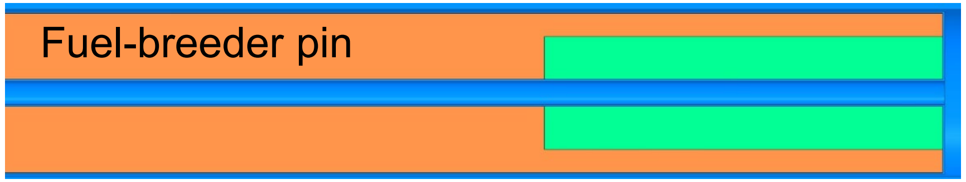
- Proposed design
  - 80 bar purge gas, introduced to improve reliability of BB
  - CMSB requires large amount of liquid N2, getter bed is explored as alternative
  - Getter bed, in particular ZAO + ZrCo, shows to be a viable option to replace CMSB in TER configuration for Q2 recovery from the purge gas



80 bar purge gas

Tritium permeation analysis

- 3D component level solver
  - Developed based on the OpenFOAM and benchmarked with TMAP 7

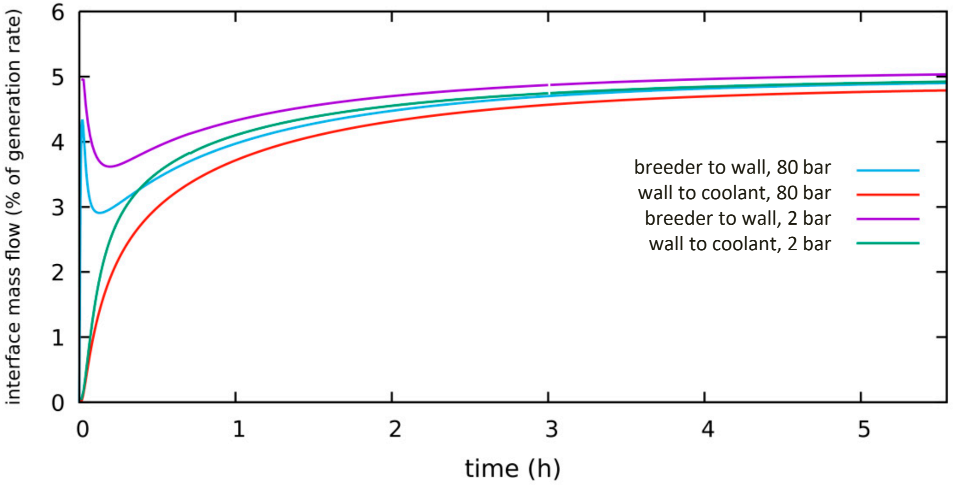


OpenFOAM

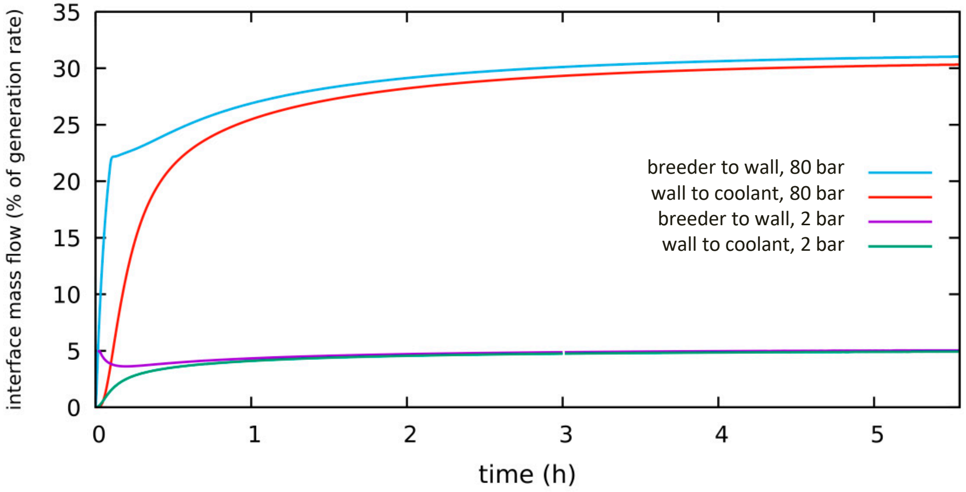
The Open Source CFD Toolbox

- Tritium permeation analysis
  - Tritium permeation analysis under 2 bar pressure purge gas vs 80 bar pressure purge gas, with same H2 partial pressure
  - Wet purge gas vs dry purge gas

Purge gas	Permeation to coolant	Wall T inventory
200Pa H2, no H2O	0.077% of T generation	65 ng
200Pa H2 + 200Pa H2O	0.022% of T generation 3.5 times less	19.2 ng



Permeation under equal volumetric flow



Permeation under equal mass flow

Conclusions

- Nuclear, thermal hydraulics and thermal mechanics assessments confirms the soundness of high pressure purge gas HCPB concept
- Global neutronics analysis recommends a large TBR for counting uncertainity
- Tritium Extraction and Recovery system can cope with high pressure purge gas

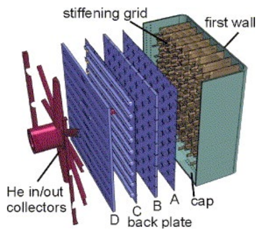
Contact: Guangming Zhou
Email: guangming.zhou@kit.edu

Backup slides

Solid breeding blanket in Europe: HCPB Design evolution

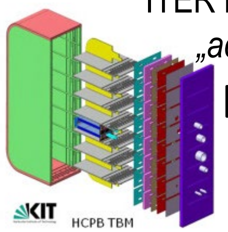
- HCPB and WCLL are two reference blanket concepts for EU DEMO

Pre-Concept Design Phase (FP8)



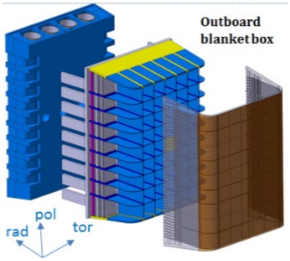
PPCS Model B (HCPB)

ITER HCPB TBM „act-alike“



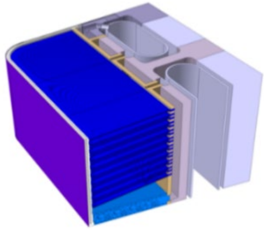
- Coolant: He @80 bar, 300-520°C
- Structural steel: Eurofer97
- T-breeder: Li-ceramics
- n-multiplier: Beryllide
- T-extraction: purge gas

2014 — "Beer-box" DEMO baseline 2014



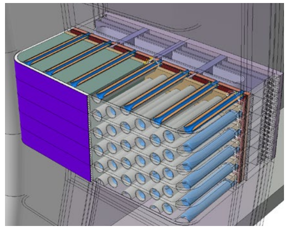
- \+ ↑↑ Robustness (in-box LOCA)
- – ↓↓ TBR (1.06)
- – ↑↑ Fabrication & assembly complexity
- – ↑↑ Δp (P_{pump}≈250MW, low TRL BoP)

2015, 2016 — DEMO baseline 2015 "Sandwich"



- \+ ↑ Robustness (in-box LOCA)
- \+ ↑ TBR (1.15)
- – ↑ Fabrication & assembly complexity
- – ↑ Δp (P_{pump}≈150MW, low TRL BoP)

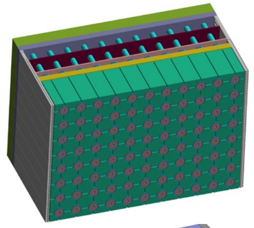
2017, 2018, 2019, 2020 — DEMO baseline 2017 "Fuel-breeder pin"



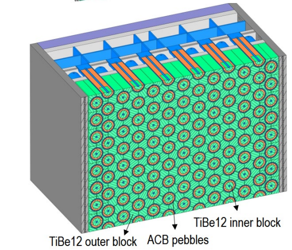
- \+ ↑ Robustness (in-box LOCA)
- \+ ↑ TBR (1.20)
- \+ ↓ Fabrication & assembly complexity
- \+ ↓ Δp (P_{pump}≈ 90MW, high TRL BoP)
- – RAMI

Concept Design Phase (FP9)

2021
2022
2023
2024

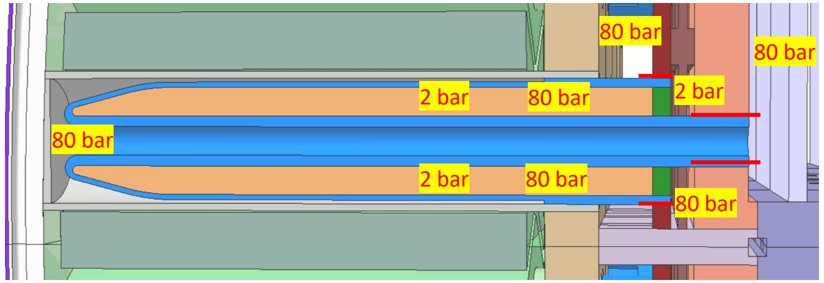


G. Zhou et al. 2022. TOFE 2022



G. Zhou et al. 2023. ISFNT-15

- \+ ↑ Robustness (in-box LOCA)
- \+ ↑ TBR (1.20)
- \+ ↓ Fabrication & assembly complexity
- \+ ↓ Δp (P_{pump}≈ 90MW, high TRL BoP)
- \+ ↑ High reliability



Assessment of lifetime due to pebble-Eurofer interaction

- Acc. to [1], the fatigue lifetime reduced due to interaction between pebbles and Eurofer97

Li_4SiO_4+
30 mol% Li_2TiO_3
1 mm pebbles

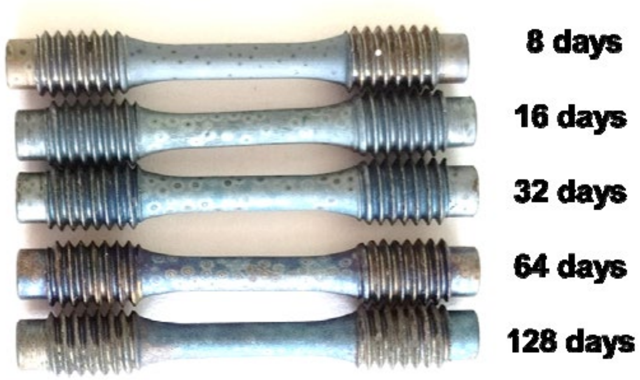
EUROFER97-2
low-cycle fatigue (LCF)
specimens Ø2 mm

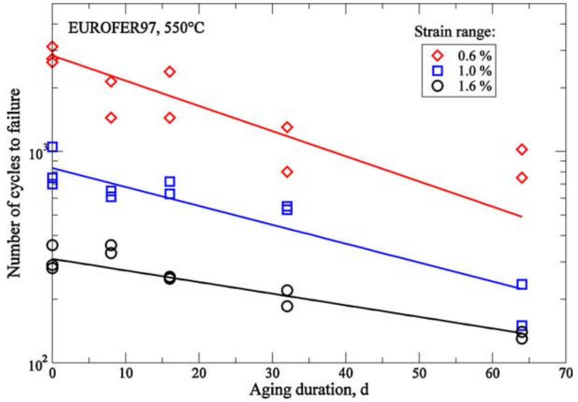
Interaction conditions:

T=550°C

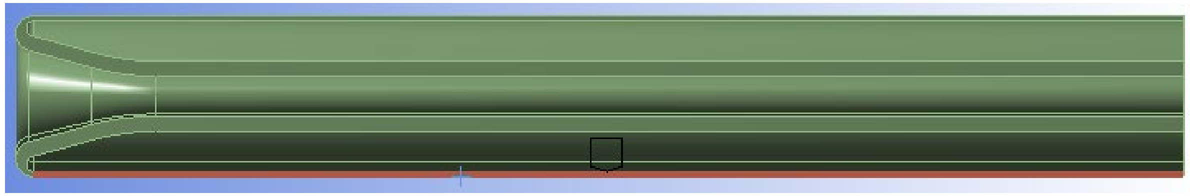
Atmosphere: purge gas flow (He+0.1%H_2)

Duration: 8, 16, 32, 64, 128 days



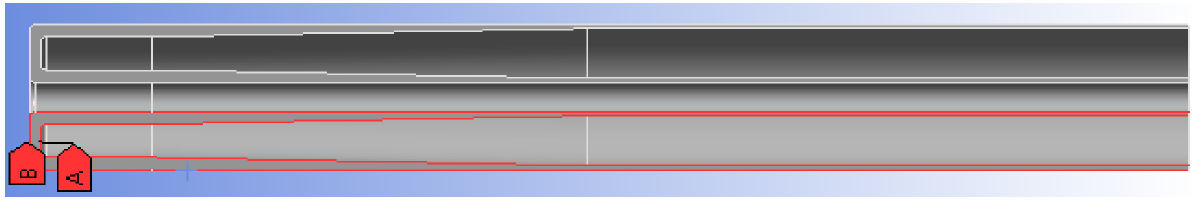


- Creep-Fatigue-Assessment tool [2] used to assess different design options (2 bar vs 80 bar purge gas)



2 bar purge gas

- Along the indicated paths, most regions failed to withstand the required 7787 cycles



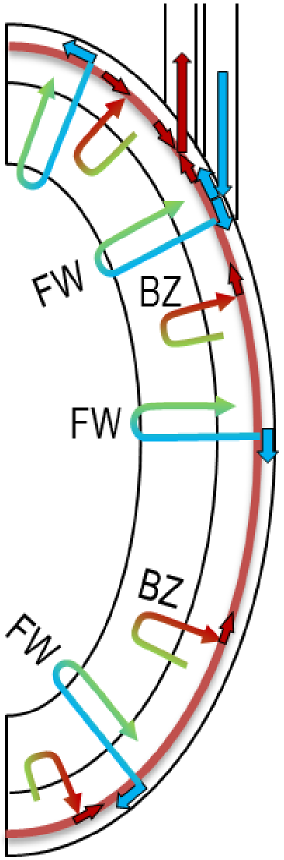
80 bar purge gas

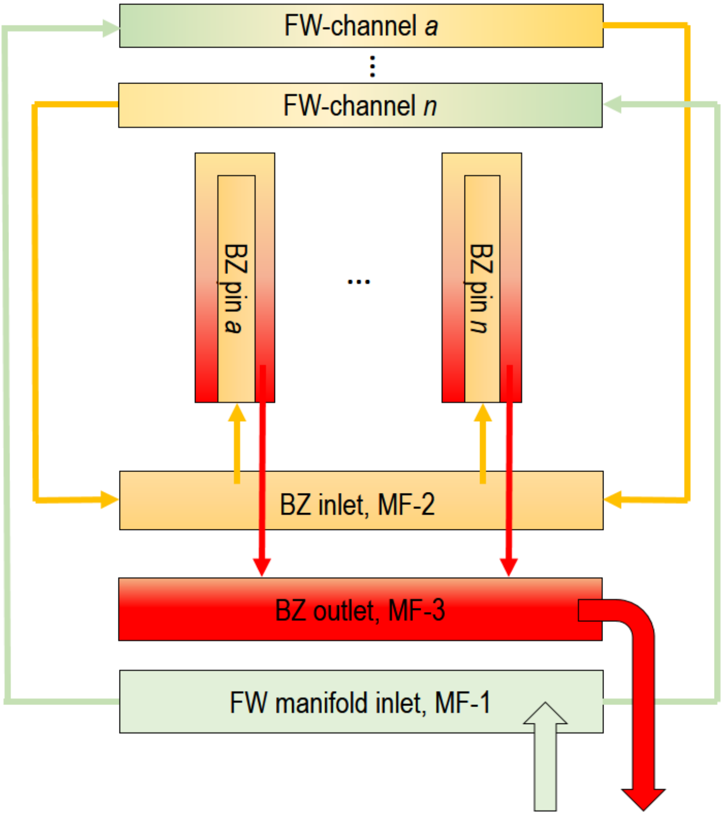
- Along the indicated paths, most regions succeeded to withstand the required 7787 cycles

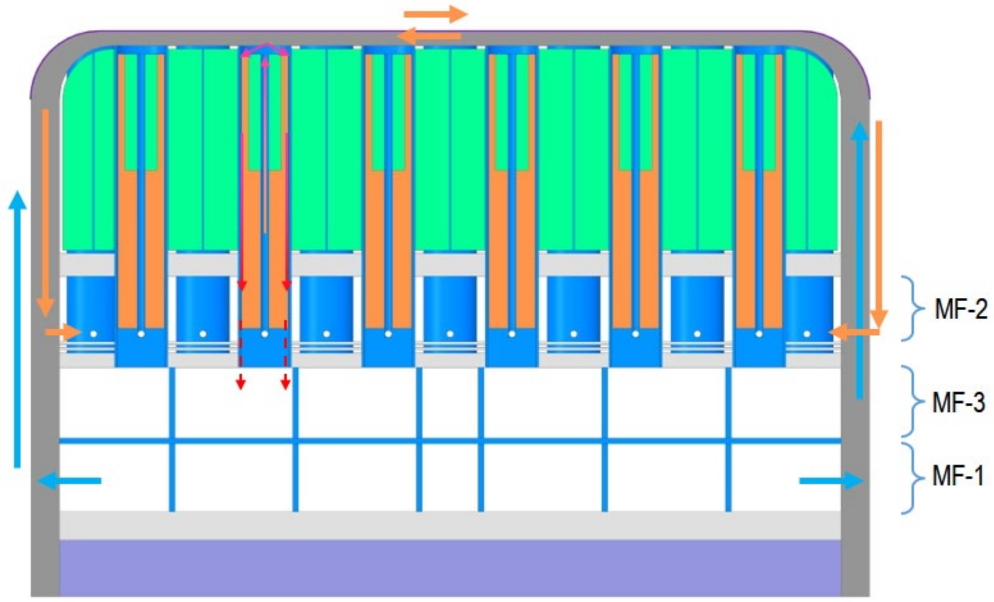
- New design able to improve lifetime

[1] Aktaa J et al., 2020 *Fusion Eng Des* 157, 111732.
[2] Mahler M, Aktaa J, 2018 *Nucl Mat Energ* 15, 85-91.

Flow scheme


FW
BZ
FW
BZ
FW


FW-channel a
FW-channel n
BZ pin a
...
BZ pin n
BZ inlet, MF-2
BZ outlet, MF-3
FW manifold inlet, MF-1


MF-2
MF-3
MF-1

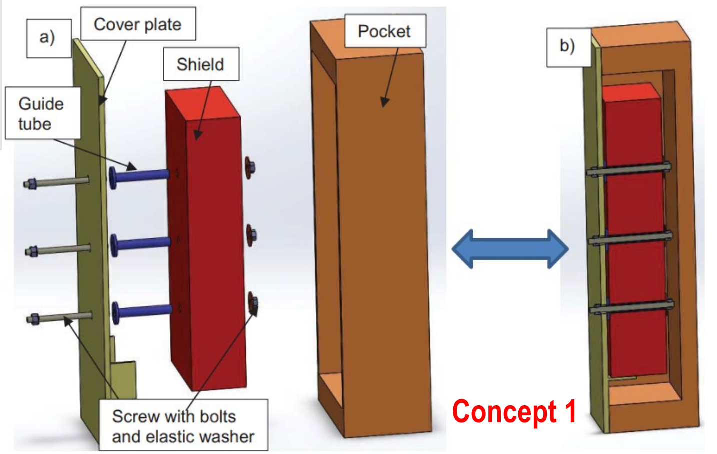
Shield design: Structural design and analysis

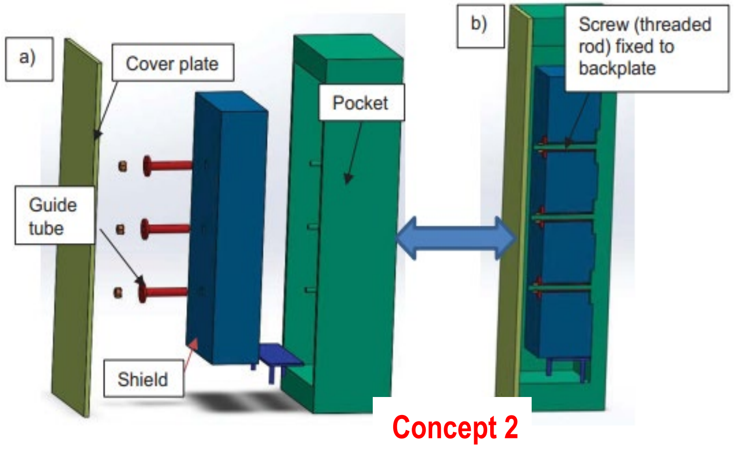
To confine the fragmentation, B_4C shield is designed to be contained

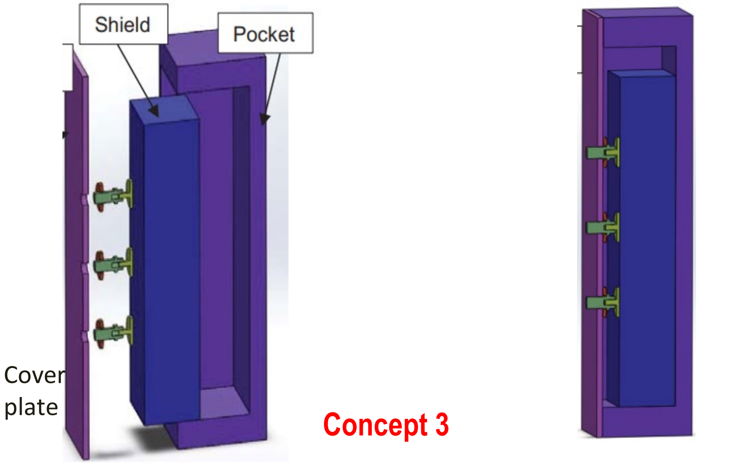
- Concept 1: Radiation, shield fixed to cover plate
- Concept 2: Contact, shield fixed to BSS backplate
- Concept 3: Contact, shield fixed to BSS backplate with external clamping

			Cover plate	Shield	BSS
Concept 1	Tmax	°C	795 > 450°C → **significant creep**	950°C	364 < 375°C → negligible creep
	Tmoy ΔT	°C	791 5	935 54	343 48
	Max($\bar{\sigma}$)	MPa	9	124	89
	$\overline{Q_m + Q_b} = \overline{\Delta Q}$	MPa	8 → low value	-	109
	Applied design criteria		Simplified analysis with negligible creep: Ratcheting $\overline{P_m + P_b} + \overline{\Delta Q} < 3\,Sm$	Max($\bar{\sigma}$)<155 MPa (B_4C Yield strength at 980°C)	Ratcheting, negligible creep $\overline{\Delta Q} < 1.5\,Sm$=275 MPa (350°C)
	Validation		**No analysis (low stress), should be validated**	**Validated**	**Validated**

			Cover plate	Shield	BSS
Concepts 2 & 3	Tmax	°C	426 < 450°C → negligible creep	467	382 > 375°C → **significant creep**
	Tmoy ΔT	°C	425 1	443 85	353 62
	Max($\bar{\sigma}$)	MPa	2	156	113
	$\overline{Q_m + Q_b} = \overline{\Delta Q}$	MPa	2 → low value	-	132
	Applied design criteria		Ratcheting: $\overline{P_m + P_b} + \overline{\Delta Q} < 3\,Sm$	Max($\bar{\sigma}$)<155 MPa (B_4C Yield strength at 980°C)	Simplified analysis with negligible creep: Ratcheting $\overline{\Delta Q} < 1.5\,Sm$=275 MPa (350°C)
	Criteria		**No analysis, should be validated**	**Validated**	**Validated**







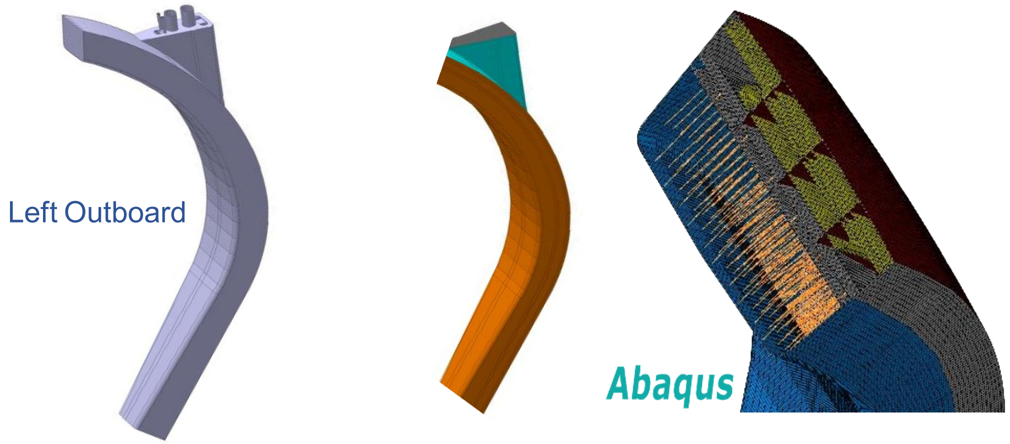
Shield of ITER diagnostic port-plug

Shoshin A et al., 2021 *Fusion Eng Des* 168, 112426

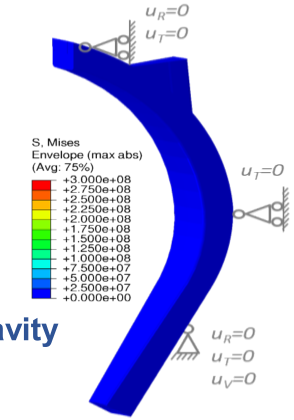
Optioneering of blanket attachment (1/2)

- Attachment: accomodate gravity, thermal, pressure and EM loads, conform remote handling

Equivalent shell and beam elements used to get quick feedback

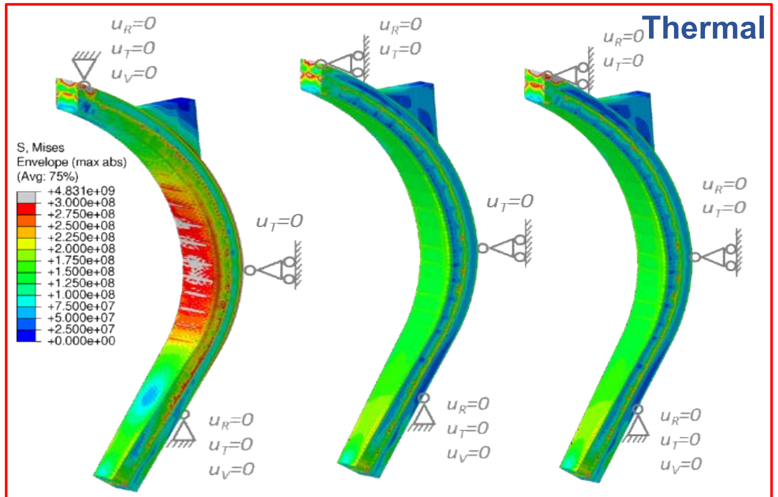


Solid geometry | Surface bodies | Shell and beam elements



Gravity

Gravity loads do not cause a large global stress, thus not critical. However, it is important that the segments are fully supported before any thermal expansion occurs.

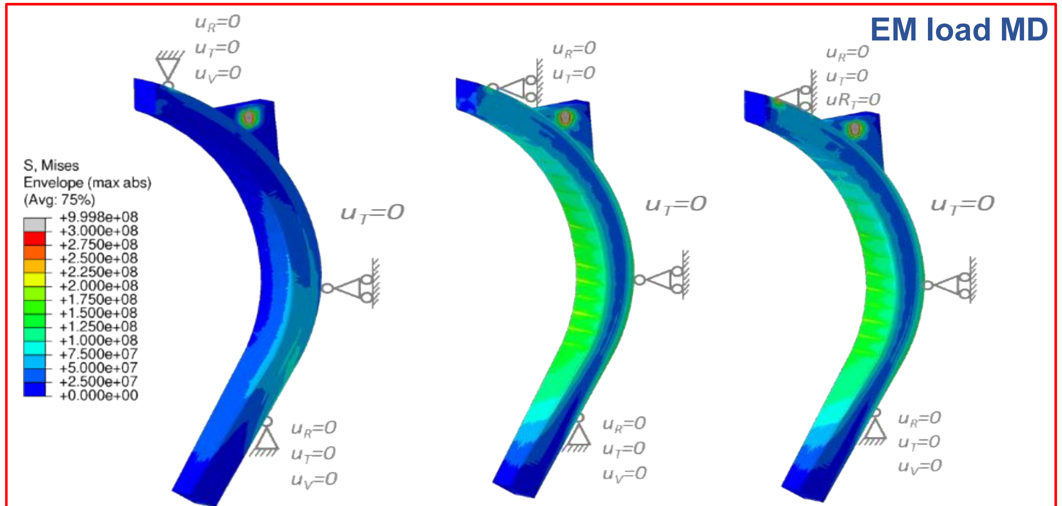


Constrained vertically | Free vertical expansion | Free vertical expansion

When fully constrained, causing a large global stress on the First Wall.

When free to expand vertically, the stress level at the FW is almost negligible.

A slightly larger stress level is reached at the FW when a radial support is included.



Constrained vertically | Free vert. expan. | Constrained tor. rotation

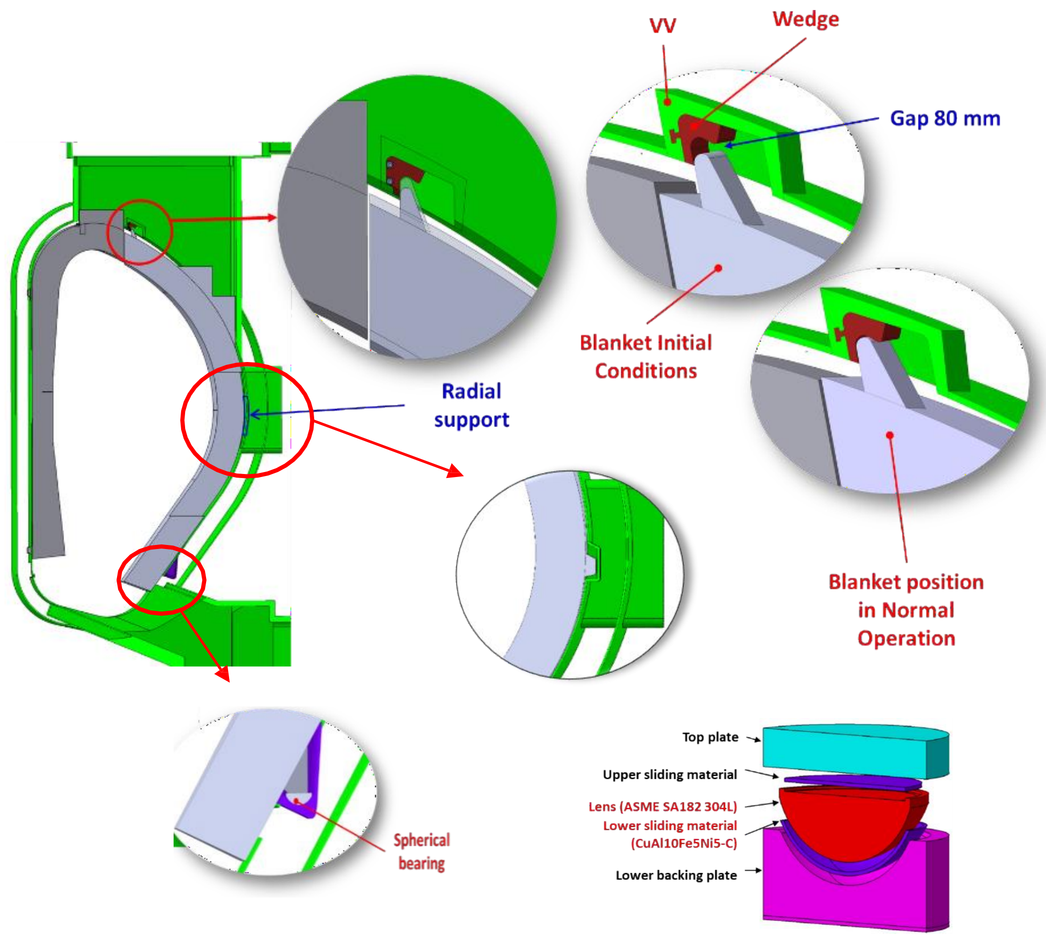
When fully constrained, the stress on FW is negligible, but stresses become large if the segment is free to expand vertically.

An important requirement derived: sufficient supporting conditions to withstand EM and seismic loads during operation

Optioneering of blanket attachment (2/2)

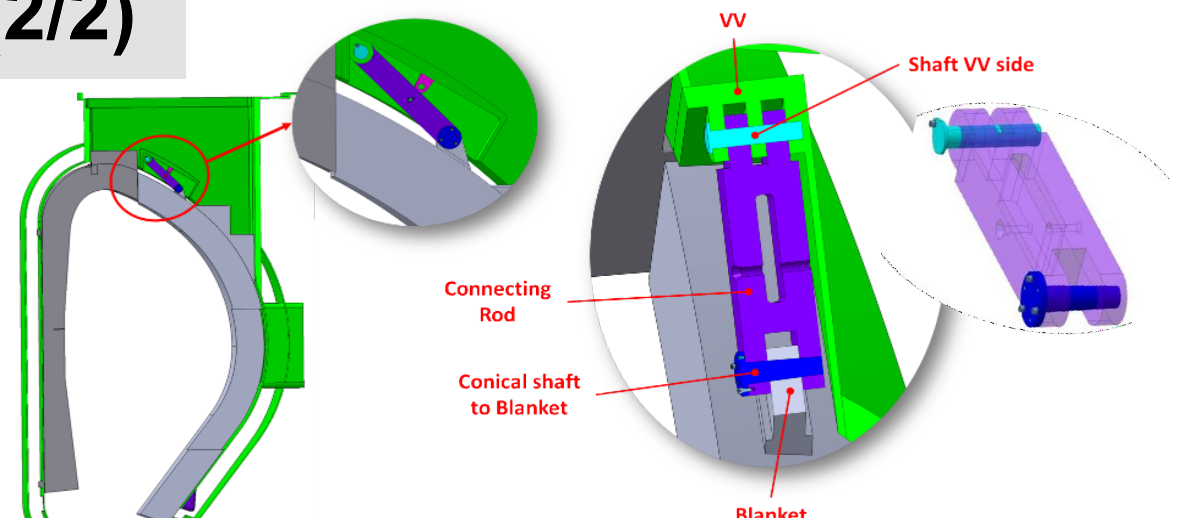
- Proposed concepts of BB-to-VV attachment

Bottom, middle and top supporting structures



ITER Cryostat Support Bearings to take 1100 tonnes

Proposal 1



Proposal 2

At bottom, spherical bearing similar to ITER Cryostat Support Bearings

At midplane, toroidal key is proposed. The toroidal key has a toroidal gap to facilitate assembly by RH tools. The pocket at the VV allows sufficient vertical displacement (124 mm) of the segment for the assembly process.

At top, two proposals are being considered. Wedge (Proposal 1) and Conical shaft (Proposal 2).