

## Introduction

- The HCPB blanket concept for EU-DEMO fusion reactors employs **high-pressure (8 MPa) helium gas** as coolant for the plasma facing first wall. Up-to-date estimations for the total maximum of **heat flux go up to 0.73 MW/m<sup>2</sup>**. **60°-V-shaped rectangular ribs** show high heat transfer and are thus the subject of the presented studies.
- Challenges in Turbulence Modelling:** LES provides high-fidelity results but is computationally expensive, RANS models are efficient, but struggle to predict complex flow features and underestimate the heat transfer up to 22 %.

## Long Term Objectives

- Long term objectives of the qualification work for numerical simulations for the helium cooled First Wall channels of DEMO are to provide a consistent, fully validated and practically feasible (in terms of computing resources) **numerical approach** to provide simulations of **complete rib enhanced FW channels/ full-size blanket components**.

## Approach: Generalized k-omega (GEKO) Model

- The **generalized k-omega (GEKO) turbulence model** offers higher accuracy predicting **heat transfer and pressure drop** compared to other RANS and Reynolds Stress Models (RSM).
- High-fidelity **Large Eddy Simulations (LES)** as **target data** are used to **optimize GEKO parameters** in Ansys Fluent.

### Model Equations for Turbulent Kinetic Energy $k$ and Dissipation $\omega$ :

$$\frac{\partial(\rho k)}{\partial t} + \frac{\partial(\rho u_j k)}{\partial x_j} = P_k - C_{\mu} \rho k \omega + \frac{\partial}{\partial x_j} \left[ \left( \mu + \frac{\mu_t}{\sigma_k} \right) \frac{\partial k}{\partial x_j} \right] \quad P_k = -\tau_{ij} \frac{\partial u_i}{\partial x_j}$$

$$\frac{\partial(\rho \omega)}{\partial t} + \frac{\partial(\rho u_j \omega)}{\partial x_j} = C_{\omega 1} F_1 \frac{\omega}{k} P_k + C_{\omega 2} F_2 \rho \omega^2 + \rho F_3 CD + \frac{\partial}{\partial x_j} \left[ \left( \mu + \frac{\mu_t}{\sigma_\omega} \right) \frac{\partial \omega}{\partial x_j} \right]$$

$$CD = \frac{2}{\sigma_\omega} \frac{1}{\omega} \frac{\partial \omega}{\partial x_j} \frac{\partial \omega}{\partial x_j} \quad P_k = -\tau_{ij} \frac{\partial u_i}{\partial x_j}$$

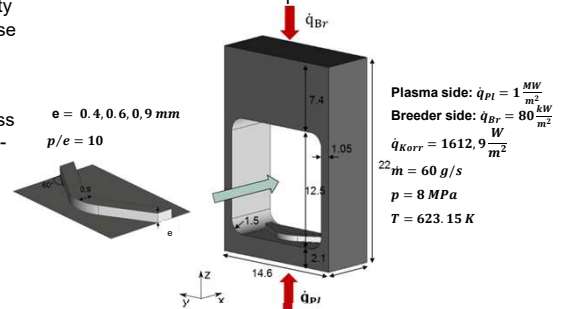
$$\tau_{ij} = \tau_{ij}^{EV} - C_{CORNER} \frac{1.2 \mu_t}{\max(0.3\omega, \sqrt{0.5}(S_2 + \Omega_2))} (S_{ik}\Omega_{kj} - \Omega_{ik}S_{kj})$$

### Free coefficients

- $C_{sep}$ : reduces eddy-viscosity of entire flow field > increase flow separation
- $C_{nw}$ : affects only inner part of wall boundary layers, >increases wall shear stress
- $C_{CORNER}$ : Non-linear stress-strain term to account for secondary flows
- $C_{mix}$ : increase spreading rates of free shear flows

embedded in  $F_1, F_2, F_3$

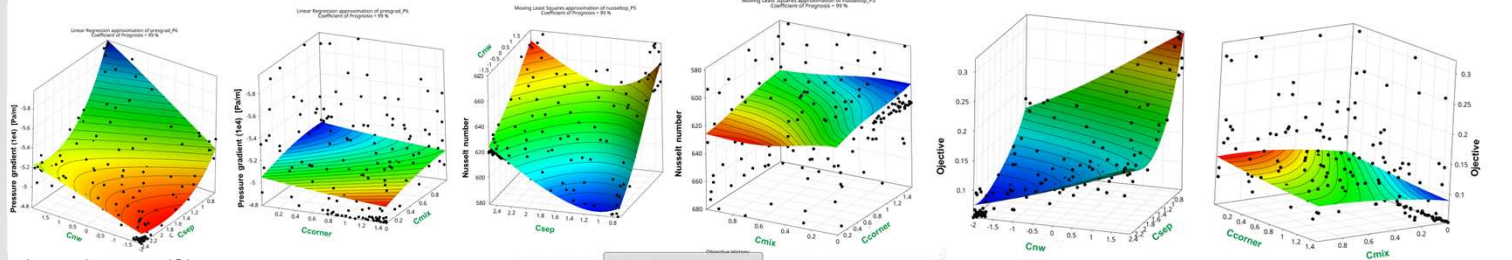
**Target Data:** Time averaged velocity and temperature fields of LES for FW test section with periodic heat transfer conditions



**Focus** on main parameters: Nusselt number  $Nu$  plasma side wall and pressure gradient

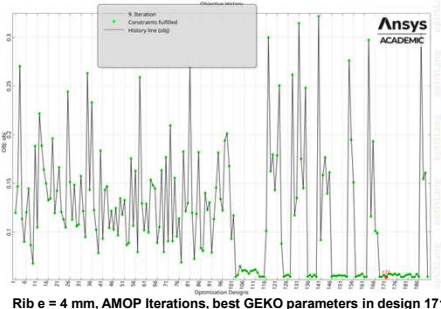
$Pgrad >$  Minimize for both difference between results for GEKO and LES

$$\text{Objective} = \sqrt{\left( \frac{Nu_{Geko}}{Nu_{LES}} - 1 \right)^2 + \left( \frac{Pgrad_{Geko}}{Pgrad_{LES}} + 1 \right)^2}$$



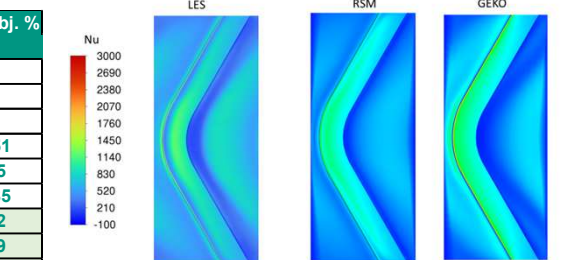
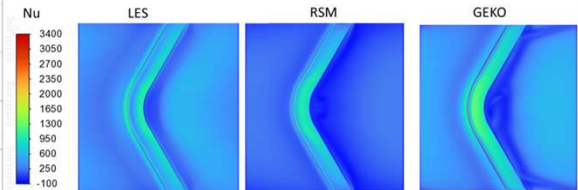
## Ansys Ansys optiSlang:

- Input parameter: GEKO parameters  $C_{sep}$ ,  $C_{nw}$ ,  $C_{CORNER}$ ,  $C_{CORNER}$
- Output parameter: pressure gradient  $Pgrad$ , Nusselt number  $Nu$ , objective function  $Objektive$
- Adaptive Meta Model of Optimal Prognosis (AMOP) identifies with sensitivity analysis influence of GEKO parameters on the simulation's results (responses) and measurement of forecast quality of the response variation



	Nu	Nu/ Nu <sub>o</sub>	dev. Nu to Nu LES %	P grad. [Pa/m]	dev. P grad. to P grad. LES %	Darcy fric. factor $f$	$f/f_0$	dev. Obj. %
LES $e = 0.4 \text{ mm}$	626	2.58		-46866		0.050	3.04	
LES $e = 0.6 \text{ mm}$	595	2.45		-66889		0.071	4.34	
LES $e = 0.9 \text{ mm}$	573	2.36		-80771		0.086	5.24	
RSM $e = 0.4 \text{ mm}$	549	2.26	-12.35	-57860	23.46	0.062	3.76	26.51
RSM $e = 0.6 \text{ mm}$	554	2.28	-6.82	-68539	2.47	0.073	4.45	7.25
RSM $e = 0.9 \text{ mm}$	443	1.82	-22.63	-78175	-3.21	0.083	5.07	22.85
Geko $e = 0.4 \text{ mm}$	620	2.55	-1.03	-47946	2.30	0.051	3.11	2.52
Geko $e = 0.6 \text{ mm}$	611	2.52	2.72	-70233.7	5.00	0.075	4.56	5.69
Geko $e = 0.9 \text{ mm}$	589	0.00	2.84	-78049	-3.37	0.083	5.07	4.41

Table 1: Comparison Results for RSM and GEKO for different rib heights



## Conclusion

- RSM shows lower values of the heat transfer vs. the LES in all cases. The under-estimation of heat transfer was up to 22 %.
- But RSM shows a good match of the values for the friction factor for the higher ribs 0.6 and 0.9 (here max difference 3 %), capture flow features better.
- GEKO (best parameter set was used in each case) match heat transfer and friction factor vs. the LES with a maximal difference of 5 %.
- Baseline (BSL) Reynolds Stress Model (RSM) with the GEKO options seems promising capturing flow features and with the tuneable GEKO able to solve challenges regarding turbulent heat transfer.