

# Experimental study on the impact of H<sub>2</sub>S and H<sub>2</sub>SO<sub>4</sub> in CO<sub>2</sub> on five different sealant compositions under conditions relevant for geological CO<sub>2</sub>-storage

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## ABSTRACT

The integrity of well sealants is a key challenge to secure geological storage of CO<sub>2</sub>. While it has been well-established through experimental research that the exposure of such sealants to CO<sub>2</sub>-bearing fluids can lead to carbonation, and potentially degradation during prolonged exposure or flow, the impact of impurities present in injected CO<sub>2</sub> has not received much consideration.

This paper reports exposure of five different sealants to simulated well conditions with supercritical CO<sub>2</sub> containing H<sub>2</sub>S or H<sub>2</sub>SO<sub>4</sub> as impurities. Three of these sealants are based on Portland Cement, while the other two are based on Calcium Aluminate Cement, and a rock-based geopolymer specifically developed for Geological CO<sub>2</sub> Storage (GCS). The impact of the impurities on these sealants was assessed through scanning electron microscopy with energy-dispersive X-ray spectroscopy, computed tomography scanning, and fluid chemical analysis, and compared to previous research where the same five sealants were exposed to clean CO<sub>2</sub> under otherwise identical conditions.

The results show that during exposure to CO<sub>2</sub>-saturated water, the presence of H<sub>2</sub>S mostly resulted in enhanced sealant alteration depths, and reduced carbonate precipitation. During exposure to wet supercritical CO<sub>2</sub>, the presence of H<sub>2</sub>S or H<sub>2</sub>SO<sub>4</sub> resulted in reduced carbonate precipitation, and enhanced alteration depths in some (H<sub>2</sub>S) or all (H<sub>2</sub>SO<sub>4</sub>) sealants. Additionally, relatively minor degradation was observed in the outer 100–200 μm of samples exposed in the presence of H<sub>2</sub>SO<sub>4</sub>. Overall, the impacts of impurities were more pronounced for sealants that were more affected by exposure to clean CO<sub>2</sub>.

## 1. Introduction

CO<sub>2</sub> captured from a power plant or industrial process is likely to contain a range of additional components that are often referred to as impurities. While many impurities, such as N<sub>2</sub> or Ar, are chemically inert, some impurities may react and form products that potentially have deleterious effects on the transportation, injection and storage systems. While corrosion of steel pipes, tanks and other components is the key concern, potential reactions between the CO<sub>2</sub>-stream and fluids, rocks and other solids in the storage reservoir also need to be considered.

Once an impure CO<sub>2</sub>-stream is injected into a geological reservoir, the injected CO<sub>2</sub> will displace most of the pore fluid present in the reservoir (i.e., saline water or brine in case of injection into a saline aquifer), while also interacting with this fluid. CO<sub>2</sub> and certain impurities will dissolve into the reservoir fluid, and may react with other solutes present in this fluid. In return, components present in the reservoir (such as water, hydrocarbons, H<sub>2</sub>S, etc.) may dissolve into the CO<sub>2</sub>-phase. The partitioning of these various components between the water- and CO<sub>2</sub>-phases will then lead to a chromatographic fractionation

as components that preferentially partition into the water phase dissolve into pore water close to the injection zone, while components that prefer the CO<sub>2</sub>-phase will concentrate at the leading edge of the migrating plume (Bachu and Bennion, 2009; Talman, 2015; Wolf et al., 2017; Xu et al., 2007). Consequently, components with much higher solubility in the water phase than in the CO<sub>2</sub> phase will accumulate in the hydrous reservoir pore fluid. Key impurities with higher affinity for water than CO<sub>2</sub> include reactive impurities such as SO<sub>x</sub>, H<sub>2</sub>S, and NH<sub>3</sub>. These compounds are thus expected to accumulate in hydrous fluids near the injection point, for example in trapped pockets of water left within the CO<sub>2</sub>-plume.

Within a CO<sub>2</sub>-storage reservoir, the hydraulic sealants used as annular seals and plugs in the various wells provide some of the most reactive, and hence vulnerable materials. While the impact of CO<sub>2</sub>-saturated water and wet supercritical CO<sub>2</sub> on wellbore cements has been investigated extensively in laboratory experiments (e.g., (Abid et al., 2015; Barlet-Gouédard et al., 2006; Bjørge et al., 2019; Chavez Panduro et al., 2017; Duguid, 2009; Duguid and Scherer, 2010; Gu et al., 2017; Jacquemet et al., 2012; Jacquemet et al., 2008; Kutchko et al., 2015;

This article is part of a special issue entitled: CCUS Geoenergy Frontiers published in Geoenergy Science and Engineering.

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<https://doi.org/10.1016/j.geoen.2025.214005>

Received 19 January 2025; Received in revised form 5 May 2025; Accepted 25 May 2025

Available online 28 May 2025

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Kutchko et al., 2007; Kutchko et al., 2011; Kutchko et al., 2009; Kutchko et al., 2008; Laudet et al., 2011; Lende et al., 2021; Lende et al., 2024; Lesti et al., 2013; Liteanu and Spiers, 2011; Matteo and Scherer, 2012; Omosebi et al., 2015; Sterpenich et al., 2014; Todorovic et al., 2020; Wigand et al., 2009; Zhang et al., 2014a; Zhang et al., 2014b; Zhang and Talman, 2014)), field samples (e.g., (Carey et al., 2007; Crow et al., 2009)), and numerical modelling (e.g., (Brunet et al., 2013; Hernández-Rodríguez et al., 2017; Jacquemet et al., 2012; Walsh et al., 2014; Xiao et al., 2017)), the impact of impurities within a CO<sub>2</sub>-phase has not received as much attention. Most of that attention has been focused on H<sub>2</sub>S, either by itself, or in combination with CO<sub>2</sub>, as sealants may be exposed to H<sub>2</sub>S in sour gas systems as well as in Geological CO<sub>2</sub> Storage (GCS) (cf. (Jacquemet et al., 2012; Jacquemet et al., 2008; Kutchko et al., 2011; Lende et al., 2021)). Experimental research addressing the potential impact of other impurities on cement integrity in a CO<sub>2</sub>-storage reservoir appears to be lacking from the open literature.

While the maximum concentrations of impurities in published CO<sub>2</sub>-specifications are very low (e.g., (Equinor, 2019; NorthernLights, 2024)), the preferential partitioning of key reactive impurities into the water phase can still lead to high concentrations of these impurities in the near-wellbore area. When further considering the mass of the cement seals compared to the mass of injected CO<sub>2</sub>, the total quantities of injected impurities are very high. Thus, even low concentrations of impurities could potentially affect significant parts of the wellbore seals. It has been shown that common impurities, like H<sub>2</sub>S, SO<sub>2</sub>, NO<sub>2</sub> and O<sub>2</sub> may react and create nitric acid, sulphuric acid and elemental sulphur (Morland et al., 2019a,b). Considering these impurities and their reaction products, as well as the presence of water within the reservoir and seals, it is expected that SO<sub>2</sub> is the most deleterious single impurity, especially when this can react with water and a source of O<sub>2</sub> to form H<sub>2</sub>SO<sub>4</sub> (Morland et al., 2022). Equilibrium calculations with thermodynamic software at pressure and temperature representative for storage reservoirs (80 °C and 10 MPa) show that even when H<sub>2</sub>SO<sub>4</sub>-concentrations in the CO<sub>2</sub> phase are very low (0-10 ppm-mol), most of the H<sub>2</sub>SO<sub>4</sub> will partition to the hydrous phase, leading to severe acidification by up to 2 orders of magnitude (i.e., a decrease in pH by up to 2 units).

Therefore, the potential impact of impurities co-injected with CO<sub>2</sub> for storage in geological reservoirs on the cementitious materials used to seal wells remains a key knowledge gap in published research. To address this knowledge gap, we have performed experimental research exposing samples of five different sealant compositions to water and either clean CO<sub>2</sub> (van Noort et al., 2025), a CO<sub>2</sub>-phase containing 1.6 mol% H<sub>2</sub>S, or CO<sub>2</sub> in equilibrium with concentrated H<sub>2</sub>SO<sub>4</sub>. Next, the exposed samples as well as aqueous exposure solutions were analysed using a series of analysis techniques, including optical observations, sample mass measurements, Inductively Coupled Plasma Optical Emission Spectroscopy (ICP-OES), and Scanning Electron Microscopy (SEM) with Energy Dispersive X-ray Spectroscopy (EDS) to study how exposure affected the different materials. Then, the impacts of H<sub>2</sub>S and H<sub>2</sub>SO<sub>4</sub> as impurities in CO<sub>2</sub> on sealant integrity were assessed through comparison of the obtained results.

## 2. Materials and methods

### 2.1. Sealant compositions and samples

As part of the ACT-funded CEMENTTEGRITY project, five different sealant compositions were extensively tested under conditions relevant for CO<sub>2</sub>-injection and -storage (see Table 1). Three of these sealants (S1, S2 and S3) were based on Portland Cement (PC) with various additives, while one sealant (S4) was based on Calcium Aluminate Cement (CAC), and one sealant (S5) was a rock-based geopolymer being tailored for GCS-applications as part of the project. All samples used in this study were prepared by Halliburton in Norway, in accordance with API Recommended Practice 10B-2 (API, 2013), which included curing for 28

**Table 1**

Description of the different sealants that were studied.

Sealant	Description	Specific gravity
S1	Reference cement consisting of Class G cement plus 35 % BWOC <sup>a</sup> silica flour.	1.90
S2	Very low permeability composition based on Class G cement plus 35 % BWOC <sup>a</sup> silica flour, adding silica fume and MgO.	1.90
S3	Composition based on S2, replacing 28.5 % of the binder with RePlug™ (olivine-based CO <sub>2</sub> -sequestering agent).	1.90
S4	CAC-based sealant composition.	1.80
S5	Geopolymer based on powdered granite with GGBFS <sup>b</sup> and micro-silica.	1.90

<sup>a</sup> By Weight of Cement.

<sup>b</sup> Ground Granulated Blast-Furnace Slag.

days at 150 °C and 30 MPa. After curing, the 12 mm diameter cylinders (still in the Teflon moulds) were cut to lengths of 30 mm and stored submerged in their curing water.

### 2.2. Sample exposure

Sample exposures were carried out in 400 ml titanium autoclaves. Titanium was used as material for the autoclaves because of its excellent chemical resistance under the selected conditions. For the H<sub>2</sub>S tests, the autoclaves were half filled with water and half filled with H<sub>2</sub>S-containing CO<sub>2</sub>. For the H<sub>2</sub>SO<sub>4</sub> tests, the autoclaves contained only CO<sub>2</sub> and a small quantity of acid. All exposure tests were carried out at 80 °C and 10 MPa.

The autoclaves had sample holders that allowed for the simultaneous exposure of multiple samples to either CO<sub>2</sub>-saturated water (bottom), or wet supercritical CO<sub>2</sub> (top). The autoclaves were pressurised with CO<sub>2</sub> from a piston cylinder with nitrogen back-pressure. The test system and start-up/termination procedure have been described in a previous paper (van Noort et al., 2025). Demineralised water was used as the water phase, while the CO<sub>2</sub>-phase was either pure CO<sub>2</sub> or CO<sub>2</sub> with 2.2 mol% H<sub>2</sub>S (which resulted in 1.6 mol% H<sub>2</sub>S in the CO<sub>2</sub> phase after equilibration with the water phase).

The CO<sub>2</sub>-H<sub>2</sub>S mixture was prepared directly in the piston cylinder using a high-precision balance. The required quantity of H<sub>2</sub>S was first injected into the pressure-less piston cylinder (ambient pressure), followed by injection of high-pressure CO<sub>2</sub> using a booster pump, while accurately registering the mass added of both components. The exact H<sub>2</sub>S concentration could then be calculated based on the measured masses of H<sub>2</sub>S and CO<sub>2</sub> in the cylinder.

A different procedure was used to expose samples to CO<sub>2</sub> with H<sub>2</sub>SO<sub>4</sub> (where H<sub>2</sub>SO<sub>4</sub> was used as this represents the most chemically aggressive reaction product of SO<sub>2</sub>). As the solubility of H<sub>2</sub>SO<sub>4</sub> in CO<sub>2</sub> is very low (Morland et al., 2019a,b), practically all added H<sub>2</sub>SO<sub>4</sub> (or SO<sub>3</sub>) would quickly partition into the water-phase, where it would be significantly diluted and would only have a minor impact, if the same method to add H<sub>2</sub>SO<sub>4</sub> was used as described above for H<sub>2</sub>S. Furthermore, when using realistic H<sub>2</sub>SO<sub>4</sub> concentrations in the CO<sub>2</sub>-phase (for example 1-2 ppm-mol), the total quantity of H<sub>2</sub>SO<sub>4</sub> in the system would be very small, and therefore rapidly depleted. Adding a significant quantity of H<sub>2</sub>SO<sub>4</sub> to the water phase would likewise not be representative of how sealants might be exposed in a rising CO<sub>2</sub>-plume. Thus, in an attempt to expose sealant samples directly to a supercritical CO<sub>2</sub>-phase with realistically low H<sub>2</sub>SO<sub>4</sub>-concentration (saturation) while at the same time maintaining replenishment of any sulphuric acid that was consumed, the water phase was replaced by small vials with concentrated sulphuric acid (total 4–5 g of 96 wt.% sulphuric acid per experimental run). These vials with acid were placed on the lower shelf of the sample holder while the sealant samples were placed on the top shelf (about 10 cm distance between them). The sealant samples were water-saturated before exposure, but water was not added directly to the



system. The autoclaves were closed and then pressurised using pure CO<sub>2</sub>, and exposures were otherwise carried out using the same procedures as the other tests. It was hypothesised that H<sub>2</sub>SO<sub>4</sub> would dissolve from the vials into the CO<sub>2</sub>-phase, and then partition into the pore fluid within the sealant samples, thus exposing these samples to a low concentration but buffered quantity of H<sub>2</sub>SO<sub>4</sub> in CO<sub>2</sub>. While pore water from the sealant samples would likewise dissolve in the CO<sub>2</sub> phase and then dissolve in the acid, some water would remain in the samples, adsorbed at gel surface and in narrow pores.

### 2.3. Chemical equilibrium calculations

Chemical equilibrium calculations were performed with the OLI-Studio software (v/12.0 and the MSE database with redox turned off), see Table 2. When pure water is equilibrated with clean CO<sub>2</sub>, at 80 °C and 10 MPa, this leads to a hydrous liquid containing 1.5 mol% CO<sub>2</sub> (mostly as H<sub>2</sub>CO<sub>3</sub>) at a pH of 3.1, and a CO<sub>2</sub>-phase that contains 1.0 mol % H<sub>2</sub>O.

Addition of 2.2 mol% H<sub>2</sub>S to the CO<sub>2</sub> phase (CO<sub>2</sub> feed) in this system then results in a hydrous liquid containing 1.5 mol% CO<sub>2</sub> (mostly as H<sub>2</sub>CO<sub>3</sub>) and 0.087 mol% H<sub>2</sub>S (mostly as H<sub>2</sub>S, with very minor HS<sup>-</sup> and S<sup>2-</sup> –equivalent to 1508 mg/kg total S in the hydrous phase), at a pH of 3.1. Upon equilibration, the CO<sub>2</sub>-phase in this system then contains 1.0 mol% H<sub>2</sub>O, and 1.6 mol% H<sub>2</sub>S (less H<sub>2</sub>S than in the CO<sub>2</sub> feed, as some H<sub>2</sub>S partitioned to the water phase). Finally, when dry supercritical CO<sub>2</sub> is equilibrated with a small volume of concentrated sulphuric acid, this leads to a CO<sub>2</sub>-phase containing  $0.24 \times 10^{-3}$  mol% H<sub>2</sub>O and  $0.091 \times 10^{-3}$  mol% H<sub>2</sub>SO<sub>4</sub> (mostly as H<sub>2</sub>SO<sub>4</sub>, but with traces of SO<sub>3</sub>).

### 2.4. Analytical methods

Polished, resin-impregnated cross-sections of exposed and unexposed samples were photographed using a regular office scanning machine at 600 dpi. Next, these samples were investigated with SEM and EDS, using carbon coating to prevent charge-buildup. The SEM instrument was operated with 15 kV acceleration voltage. Most pictures were acquired using the backscatter electron detector, configured to maximise atomic number contrast. EDS maps (of elemental composition) were acquired using the AZtec v/6.1 software from Oxford Instruments. Each map was taken over a 800 µm × 550 µm area, with a 1024 × 704 pixels grid, giving a pixel density (resolution) of 0.8 µm × 0.8 µm (van Noort et al., 2025).

Fluids retrieved from the autoclaves after exposure were analysed by ICP-OES, on an Agilent 5800 ICP-OES, using the same methods as described previously (van Noort et al., 2025).

CT-scanning was performed on an X-ray micro-tomography (micro-CT) scanner (model CoreTOM, TESCAN), with a spatial resolution (voxel size) of about 13.5 µm. Panthera software (version 1.4, TESCAN) was then used to post-process the images, again using the same procedures as before (van Noort et al., 2025). CT-scanning was performed on the

cut-off half cylinders, except for the S2 sample exposed to CO<sub>2</sub> with H<sub>2</sub>SO<sub>4</sub>. As this sample cracked during saw-cutting, a full sample was CT-scanned instead.

## 3. Results

The impact of exposure of cores of sealants S1-S5 to wet supercritical CO<sub>2</sub> and CO<sub>2</sub>-saturated water, without impurities, was previously reported in (van Noort et al., 2025). The present work focuses on how the presence of H<sub>2</sub>S (1.6 mol% in the CO<sub>2</sub>-phase) and H<sub>2</sub>SO<sub>4</sub> (vials of saturated solution placed in the autoclave, separate from the samples) affected these sealants.

### 3.1. Scanned sample cross-sections

Optical scans of the resin-impregnated sample cross-sections, shown in Fig. 1, display clear differences depending on exposure condition as well as sealant composition. In general, exposure to clean CO<sub>2</sub> and CO<sub>2</sub> with H<sub>2</sub>SO<sub>4</sub> led to limited discolouration for sealants S2-S5 (Fig. 1b–e), while in sealant S1 (Fig. 1a) it caused a strong khaki-brownish discolouration. Exposure to CO<sub>2</sub> with H<sub>2</sub>S led to more blue-grey, darker colours, which is assumed to be due to the differences in oxidation state between the different exposure conditions, as well as the formation of sulphide minerals in these samples. This could be ascertained through additional analyses, for example using XRD on powders recovered from exposed samples at different distances from the sample surface.

Here, it should also be noted that all S1 and S2 samples exposed to CO<sub>2</sub> in the presence of H<sub>2</sub>SO<sub>4</sub> fractured during cross-sectioning. The three S1 samples cracked ahead of the sawcut, while the S2 samples not only cracked ahead of the sawcut, but also fractured parallel to the sample axis.

### 3.2. Mass and chemical changes

Fig. 2 shows relative sample mass changes as a function of exposure time, for all five sealants, and under all exposure conditions. Comparing the mass changes for S1 with and without H<sub>2</sub>S shows that while the presence of H<sub>2</sub>S had a negligible effect on mass changes due to direct exposure to wet supercritical CO<sub>2</sub>, exposure to CO<sub>2</sub>-saturated water with H<sub>2</sub>S resulted in a lower increase in mass after 4 weeks, and a larger decrease after 16 weeks (leading to an overall decrease in mass by 4.6 % after 16 weeks while exposure to clean CO<sub>2</sub> led to an overall increase by 0.5 %). For sample S3, exposure to CO<sub>2</sub>-saturated water with H<sub>2</sub>S did not result in a decrease in mass at 16 weeks (relative to 4 or 8 weeks) as was observed for the sample exposed to CO<sub>2</sub>-saturated water without H<sub>2</sub>S. For the other samples, the impact of H<sub>2</sub>S on mass changes due to exposure to CO<sub>2</sub>-saturated water or wet supercritical CO<sub>2</sub> was negligible.

For the samples exposed to supercritical CO<sub>2</sub> in the presence of H<sub>2</sub>SO<sub>4</sub>, sample masses consistently decreased. This is most likely due to the removal of free water from these samples, as the CO<sub>2</sub> was not pre-saturated with water (to prevent dilution of the H<sub>2</sub>SO<sub>4</sub> solution). It was hypothesised that the samples would maintain sufficient water in narrow (gel) pores, and adsorbed on surfaces to allow for chemical reactions requiring dissolution to proceed locally. To determine the initial water content of the sealants before exposure, sample cylinders of all five sealants were dried in an oven at 60 °C until stable mass was achieved (see Table 3).

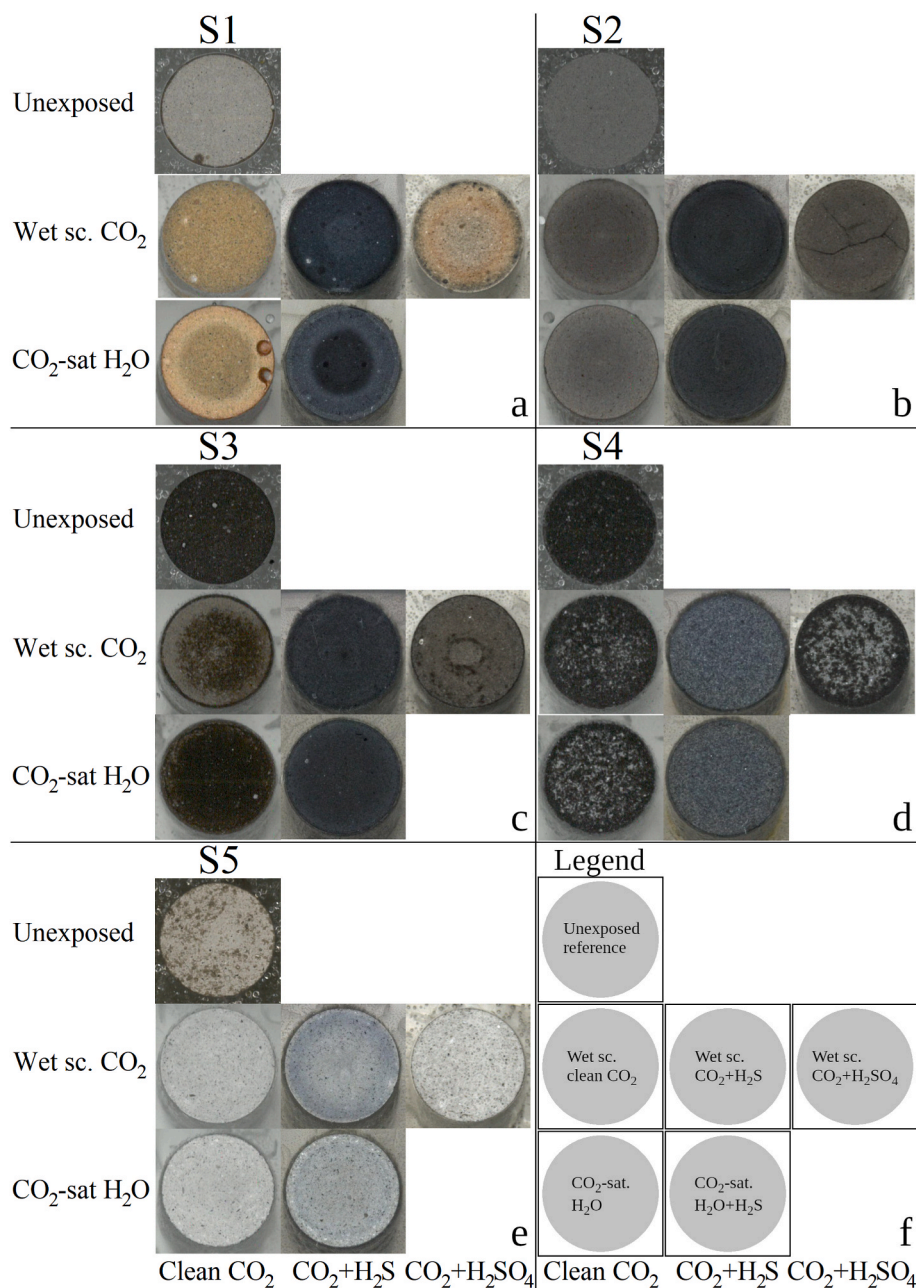
### 3.3. Fluid chemical compositions

Fig. 3 shows plots of fluid composition, measured using ICP-OES, against time for the exposure water samples of the clean CO<sub>2</sub> and CO<sub>2</sub> with H<sub>2</sub>S experiments. The composition at 0 weeks is the composition of the fluid the samples were cured, transported and stored in, and assumed equivalent to the initial pore fluid composition. For the experiments with H<sub>2</sub>S, fluid samples were only taken after 16 weeks,

**Table 2**

Calculated equilibrium compositions of the hydrous liquids and CO<sub>2</sub>-phases at 80 °C and 10 MPa.

	Water and CO <sub>2</sub> (mol%)	Water and CO <sub>2</sub> with H <sub>2</sub> S (mol%)	CO <sub>2</sub> with H <sub>2</sub> SO <sub>4</sub> (mol%)
Water in CO <sub>2</sub> phase	1.0	1.0	$0.24 \times 10^{-3}$
H <sub>2</sub> S in CO <sub>2</sub> phase	–	1.6	–
H <sub>2</sub> SO <sub>4</sub> in CO <sub>2</sub> phase	–	–	$0.091 \times 10^{-3}$
Total CO <sub>2</sub> in water	1.5	1.5	–
Total H <sub>2</sub> S in water	–	0.087	–
pH	3.1	3.1	–



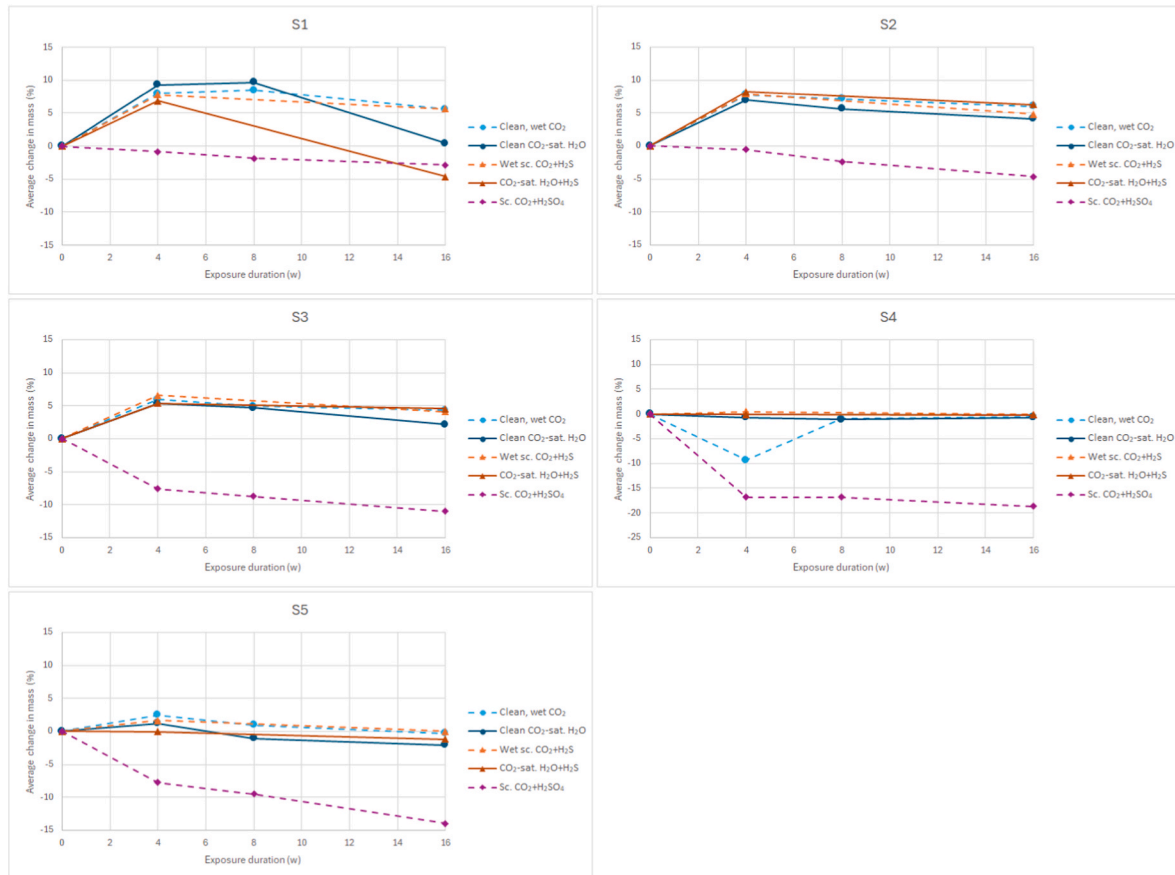
**Fig. 1.** Optical scans of resin-impregnated cross-sections of samples of S1 (a), S2 (b), S3 (c), S4 (d), and S5 (e), showing unexposed reference samples, as well as samples exposed for 16 weeks to CO<sub>2</sub>-saturated water or directly to the supercritical CO<sub>2</sub> phase, using clean CO<sub>2</sub>, CO<sub>2</sub> with 1.6 mol% H<sub>2</sub>S, or CO<sub>2</sub> equilibrated with concentrated H<sub>2</sub>SO<sub>4</sub>. A legend mapping exposure conditions to optical scans is given in (f).

because of health and safety risks related to the toxicity of the H<sub>2</sub>S. Comparing the fluid compositions after 16 weeks, most element contents in the fluids do not differ significantly in the presence of H<sub>2</sub>S, though some key differences were observed. Firstly, while without H<sub>2</sub>S the fluid Si-content for the S1 exposures was constant from 8 to 16 weeks at about 86–88 mg/kg, with H<sub>2</sub>S, the fluid Si-content after 16 weeks was considerably higher at 458 mg/kg. Mg, K, and Ca contents were also elevated at 245 vs 71 mg/kg, 590 vs 65 mg/kg and 217 vs 131 mg/kg, respectively. For S2, fluid Na- and Mg-contents after 16 weeks exposure in the presence of H<sub>2</sub>S were elevated at 161 vs 74 mg/kg and 494 vs 283 mg/kg, respectively. For S3, exposure in the presence of H<sub>2</sub>S led to a considerably higher Mg-content in the fluid at 1646 vs 790 mg/kg, as well as relatively minor increases in Na- and K-contents. For S4, exposure in the presence of H<sub>2</sub>S led to minor increases in fluid Mg- and Ca-contents. Finally, for S5, exposure to CO<sub>2</sub> with H<sub>2</sub>S led to a lower Ca-

content in the fluid, at 8 vs 35 mg/kg.

Interestingly, sulphur contents in the initial pore fluids are much higher than in the fluid samples taken after exposure. However, for sealants S1, S2 and S3, S-contents in the exposure fluids after exposure to CO<sub>2</sub> with H<sub>2</sub>S are significantly higher than after exposure to clean CO<sub>2</sub> (263, 130 and 317 mg/kg vs. 84, 48 and 121 mg/kg, respectively). In contrast, S-contents of exposure fluids for sealants S4 and S5 are very low for both clean CO<sub>2</sub> (2.6 and < 0.01 mg/kg, respectively) and CO<sub>2</sub> with H<sub>2</sub>S (19 and 7.0 mg/kg, respectively). Note that the equilibrium concentration of H<sub>2</sub>S in water calculated for our experimental conditions, 0.087 mol%, equals ~1547 mg/kg S.

As in the H<sub>2</sub>SO<sub>4</sub> experiments, samples were not directly exposed to the concentrated H<sub>2</sub>SO<sub>4</sub>, these liquids were not analysed. However, optical observations showed colour changes in many of the vials, to various levels of brown to near-black, indicating that the chemical



**Fig. 2.** Average changes in sample mass (mass %) relative to average initial sample mass (before exposure), plotted against exposure time for all five sealants, and under all exposure conditions. Relative sample mass changes of samples exposed to clean CO<sub>2</sub> were previously reported by (van Noort et al., 2025).

**Table 3**

Changes in sample mass upon drying at 60 °C. The wt.% of evaporable water is calculated as the total change in mass compared to the initial surface-dry, water-saturated mass.

Sealant	Surface-dry, water-saturated mass (g)	Dry mass (g)	Evaporable water (wt. %)
S1	6.184	4.756	23.1
S2	6.185	4.775	22.8
S3	6.157	4.641	24.6
S4	6.136	4.838	21.2
S5	6.140	4.760	22.5

compositions of these fluids did change.

### 3.4. Microstructural changes

Changes in sample microstructure were assessed based on SEM imaging with EDS mapping, as well as CT scans. Unfortunately, while the greyscale values in these CT scans are indicative of relative density, they are not absolute meaning individual scans cannot be compared to each other. As SEM and EDS analyses of the samples exposed to clean CO<sub>2</sub> already have been presented (van Noort et al., 2025), only the samples exposed to CO<sub>2</sub> with impurities will be presented here. When discussing changes in sample microstructure and composition, as seen in SEM micrographs with EDS mapping, ratios of key elements, such as the Ca/Si-ratio (or Ca/Al for S4), were used as indicators of chemical change. Ca is a mobile element here, while Si is expected to be more stationary. Likewise, the ratio of S/Si was used as indicator for penetration of sulphur into the exposed sealant samples. Element ratios, rather than element concentrations themselves, were used to eliminate

variations in the analyses due to, for example, differences in porosity.

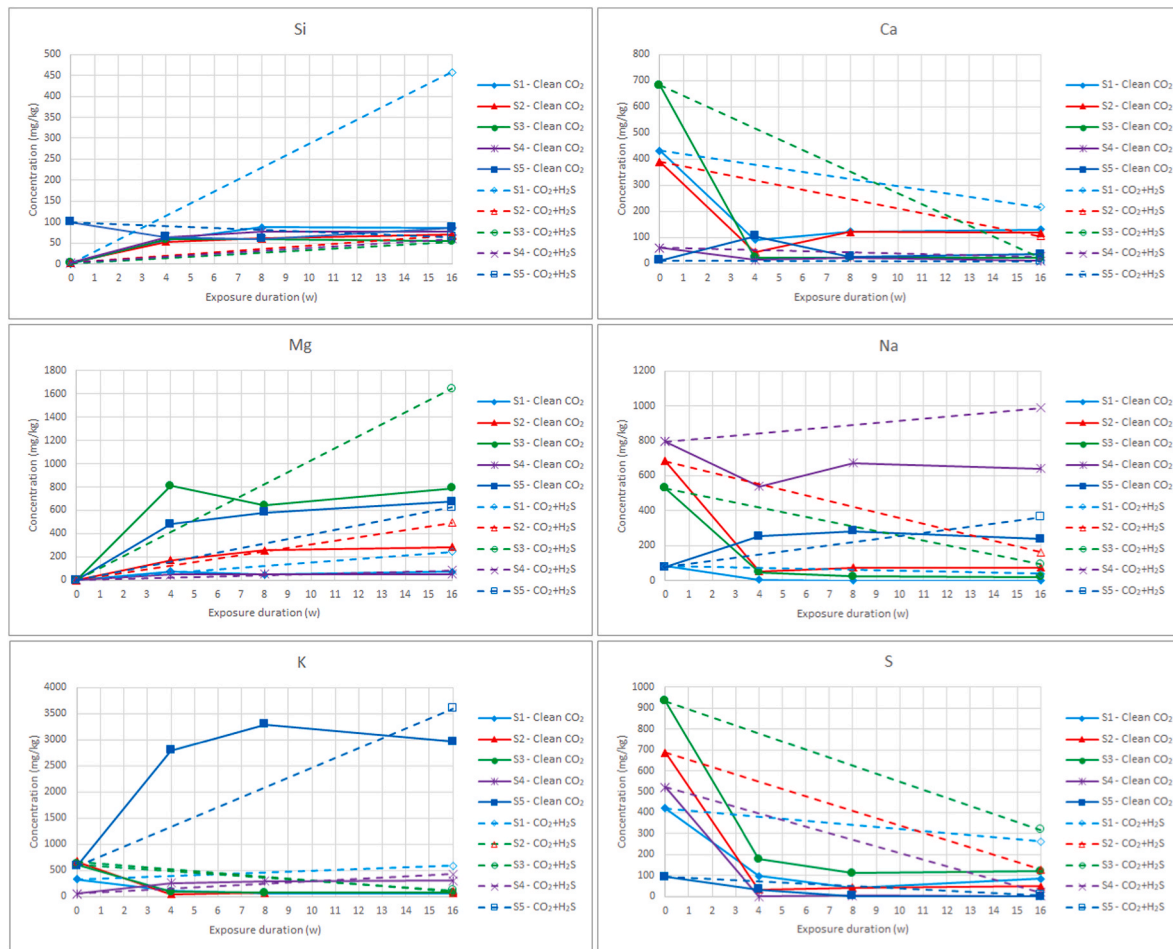
#### 3.4.1. Sealant S1

CT scans of an unexposed sample of sealant S1, and samples exposed for 16 weeks are shown in Fig. 4. The larger dark and light spots visible in the unexposed reference sample (Fig. 4a) as well as some exposed samples are air bubbles (dark) that may be filled with carbonate (light). Irregular light particles are unreacted clinker particles. Comparison of the scans shows that exposure to CO<sub>2</sub>-saturated water (with no H<sub>2</sub>S – Fig. 4c) resulted in concentric reaction zones with (from inside to outside) a diffuse transition from normal to low density starting at about ~2000 µm from the sample surface, followed by an irregular transition to zone of elevated density between ~400 and ~1000 µm from the sample surface, and an outer zone of roughly ~110 µm wide with lowered density. The sample exposed to CO<sub>2</sub>-saturated water with H<sub>2</sub>S (Fig. 4e) shows a similar diffuse transition from unaffected density to a lower density starting at ~2600 µm from the sample surface, then a very irregular transition to areas with somewhat elevated density between ~600 and ~2000 µm. An outer zone with more reduced density was not observed.

In contrast, samples exposed to wet supercritical CO<sub>2</sub> show an elevated density in a thin zone (~240 µm) near the sample surface (Fig. 4b). The same trend was observed in the presence of H<sub>2</sub>S (Fig. 4c). In the presence of H<sub>2</sub>SO<sub>4</sub>, the increase in density was more diffuse, and reached deeper into the sample. Furthermore, in the sample exposed to H<sub>2</sub>SO<sub>4</sub>, some inhomogeneity in density was observed in the outer ~100 µm (Fig. 4d).

Fig. 5 shows SEM cross-sections and element ratio curves of sealant S1 samples exposed to CO<sub>2</sub>-saturated water, with the CO<sub>2</sub>-phase containing 1.6 mol% H<sub>2</sub>S, for 4 and 16 weeks. As can be seen in Fig. 5a, a 4-





**Fig. 3.** Element concentrations in sampled fluids, measured using ICP-OES. Fluid compositions for the clean CO<sub>2</sub> exposures were previously reported by (van Noort et al., 2025).

week exposure to CO<sub>2</sub>-saturated water led to an outer zone of up to ~80  $\mu$ m thickness where dissolution and leaching led to a degradation of sample integrity. Inwards of that zone, a second zone was observed (700–800  $\mu$ m wide), where the sample density was reduced while the integrity was mostly maintained. Within this zone, some localised areas of higher density were seen, representing more concentrated carbonate precipitation. Inwards of this zone, from ~900 to 1200  $\mu$ m from the sample surface, the matrix porosity was somewhat reduced. Further inwards, the microstructure becomes relatively homogeneous and consistent to the sample core. The differences in microstructure correspond with a strong reduction of the Ca/Si-ratio in the outer 100  $\mu$ m (somewhat increasing from the surface inwards), then a slight decrease in Ca/Si-ratio over the following ~140  $\mu$ m to a minimum at about ~240  $\mu$ m from the sample surface, and then a gradual increase to reference values, reached at about 900–1000  $\mu$ m from the sample surface. S/Si-ratios are elevated throughout this sample compared to the reference value (0.076), but in particular in the outer ~150  $\mu$ m, and somewhat less between about 150 and 500  $\mu$ m from the surface.

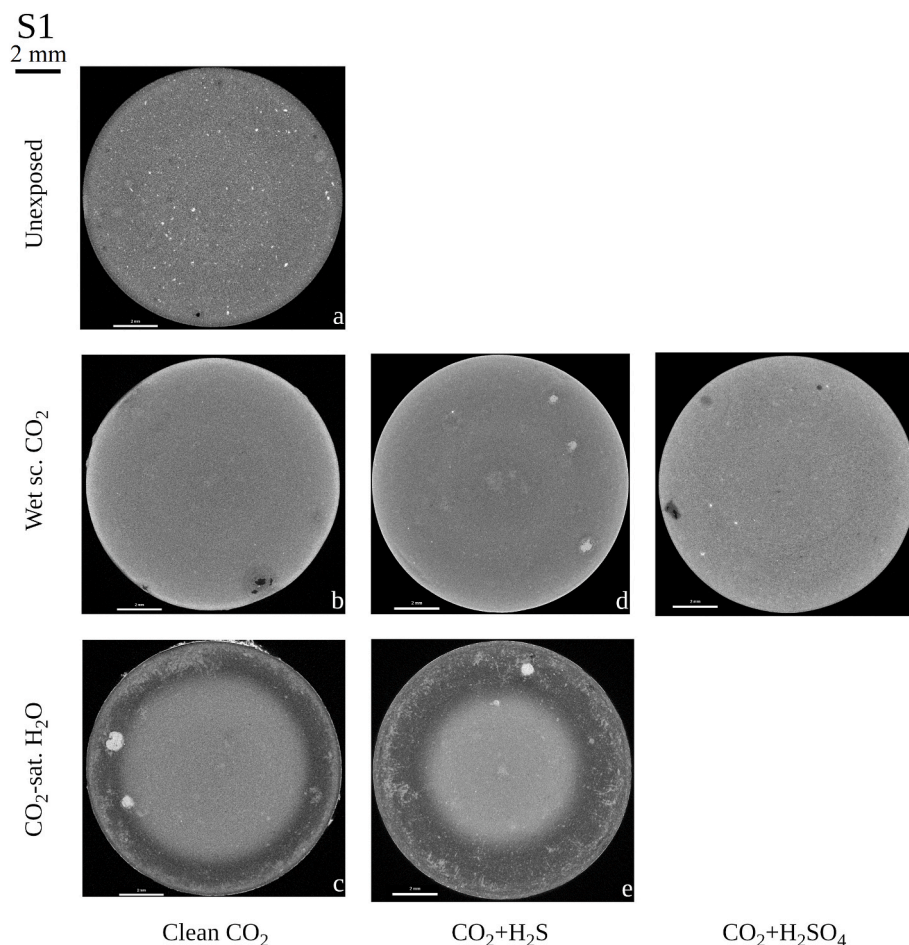
In the sample exposed for 16 weeks, a strongly depleted outer zone where the integrity was degraded was similarly observed. A combination of increased porosity and carbonate precipitation was observed between 50 and 200  $\mu$ m from the sample surface, while the Ca/Si-ratio was largely constant at considerably reduced values. Inwards of this zone, the Ca/Si-ratio dropped (to below 0.1), and the microstructure shows signs of being strongly depleted, leading to increased porosity and reduced gel density, though overall cohesion of the material was mostly maintained. Within this zone, the Ca/Si-ratio stays mostly constant to about ~1800  $\mu$ m from the surface, though elevated Ca/ratios between

~300 and 900  $\mu$ m from the surface correspond to areas of higher density due to Ca-carbonate precipitation. Ca/Si-ratios then increase gradually up to reference values at about 2900–3000  $\mu$ m from the surface, while the microstructure changes gradually, becoming less porous as density and integrity increase, becoming relatively homogeneous and comparable to the sample centre at about ~2700  $\mu$ m from the sample surface. As with the sample exposed for 4 weeks, S/Si-ratios are increased throughout the sample, though they are relatively low between 250 and 2700  $\mu$ m, i.e., where Ca/Si-ratios are likewise depleted.

Very fine (mostly sub-micron) high-density (white) particles are observed in SEM images of both samples exposed to CO<sub>2</sub>-saturated water with H<sub>2</sub>S. Closer inspection of the sample exposed for 16 weeks shows that these particles are found throughout the sample. EDS analysis of a number of these particles indicated that they consist mainly Fe and S, with about 1.5–2.0 S per Fe, though accurate quantitative analysis was prevented by the small particle size.

Fig. 6 shows sample cross-sections and element ratios for samples exposed directly to the H<sub>2</sub>S-bearing CO<sub>2</sub>-phase. After 4 weeks exposure, a thin outer precipitate layer was formed of a few  $\mu$ m thick. Inwards of this, the sample was partly dissolved, leading to a degradation of integrity and then gradually increasing integrity (decreasing porosity) inwards over ~150–200  $\mu$ m. This is correlated to a minimum Ca/Si-ratio at the sample surface, gradually increasing to reference values 280–290  $\mu$ m from the sample surface. Sample porosity is relatively reduced between 250  $\mu$ m and ~700  $\mu$ m from the sample surface. Inwards from there the sample microstructure appears relatively homogeneous through to the centre. The S/Si-ratio is elevated throughout the sample, but more so in the outer ~100–150  $\mu$ m, indicating that H<sub>2</sub>S fully





**Fig. 4.** CT-scans of sealant S1; a) unexposed, b) exposed to wet supercritical  $\text{CO}_2$ , c) exposed to  $\text{CO}_2$ -saturated water, d) exposed to wet supercritical  $\text{CO}_2$  with 1.6 mol %  $\text{H}_2\text{S}$ , e) exposed to  $\text{CO}_2$ -saturated water with  $\text{H}_2\text{S}$ , and f) exposed to supercritical  $\text{CO}_2$  equilibrated with concentrated  $\text{H}_2\text{SO}_4$ . The scalebars shown with the scans are 2 mm. All exposure durations were 16 weeks. CT scans of the unexposed reference sample and samples exposed to clean  $\text{CO}_2$  taken from (van Noort et al., 2025).

penetrated the sample, but was also being bound in the outer part of the exposed sample.

In the sample exposed for 16 weeks, the outer zone contains relatively thick carbonate precipitates, though with some areas with higher porosity between the carbonates in the outer  $\sim 200\ \mu\text{m}$ . Between  $\sim 200$  and  $\sim 600\ \mu\text{m}$  from the sample surface, this porosity is greatly reduced, while further inwards the microstructure looks quite homogeneous. The Ca/Si-ratio is somewhat elevated in the outer  $\sim 200\ \mu\text{m}$  of the sample, decreasing gradually to reference values going inwards from the surface. The S/Si-ratio is elevated relatively constantly from surface to core, but somewhat more elevated in the outer  $\sim 400\ \mu\text{m}$ . In these samples exposed to wet supercritical  $\text{CO}_2$  with  $\text{H}_2\text{S}$ , very fine (sub-micron), high-density particles, similar to those identified as iron sulphides in the samples exposed to  $\text{CO}_2$ -saturated water, are likewise observed throughout the samples.

Fig. 7 shows samples exposed to supercritical  $\text{CO}_2$  in the presence of  $\text{H}_2\text{SO}_4$  for 4, 8 and 16 weeks. In all three samples, a thin (few  $\mu\text{m}$  thick) outer skin is observed, while inwards of that the sample has very high porosity, due to dissolution of material, with the sealant then gradually becoming more consistent moving inwards. In the sample exposed for 4 weeks, this degraded outer zone is  $\sim 150\text{--}200\ \mu\text{m}$  wide and correlated to a depleted Ca/Si-ratio at the sample surface that increases moving inwards to reference values at  $\sim 150\text{--}200\ \mu\text{m}$ . Between 200 and  $800\ \mu\text{m}$  from the surface, the sample has a relatively low porosity due to carbonate precipitation. From  $\sim 800\ \mu\text{m}$  inwards, porosity increases gradually, until the sample becomes relatively homogeneous from  $\sim 1300\ \mu\text{m}$  inwards. The S/Si-ratio is somewhat higher than reference values,

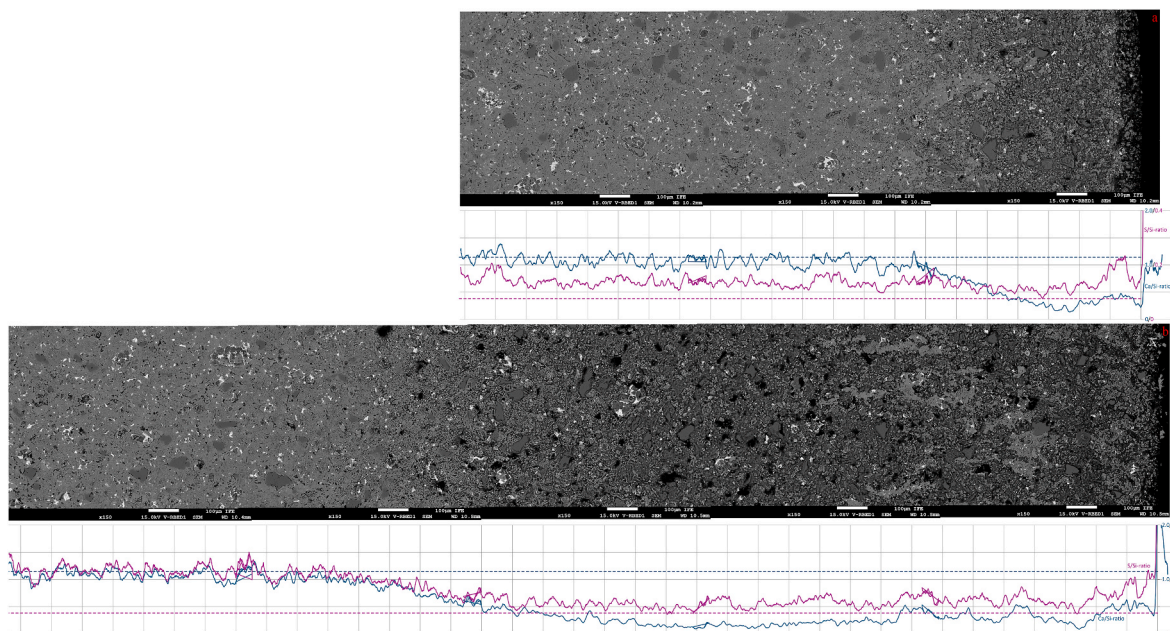
and relatively constant from the surface inwards.

In the sample exposed for 8 weeks, similar zones are observed as described above. Here, the degraded outer zone is about  $100\text{--}200\ \mu\text{m}$  wide, and correlated to a depleted Ca/Si-ratio in the outer  $100\ \mu\text{m}$  only. Reduced porosities are observed down to  $\sim 900\text{--}1000\ \mu\text{m}$  from the surface. S/Si-ratios are also somewhat elevated throughout the sample.

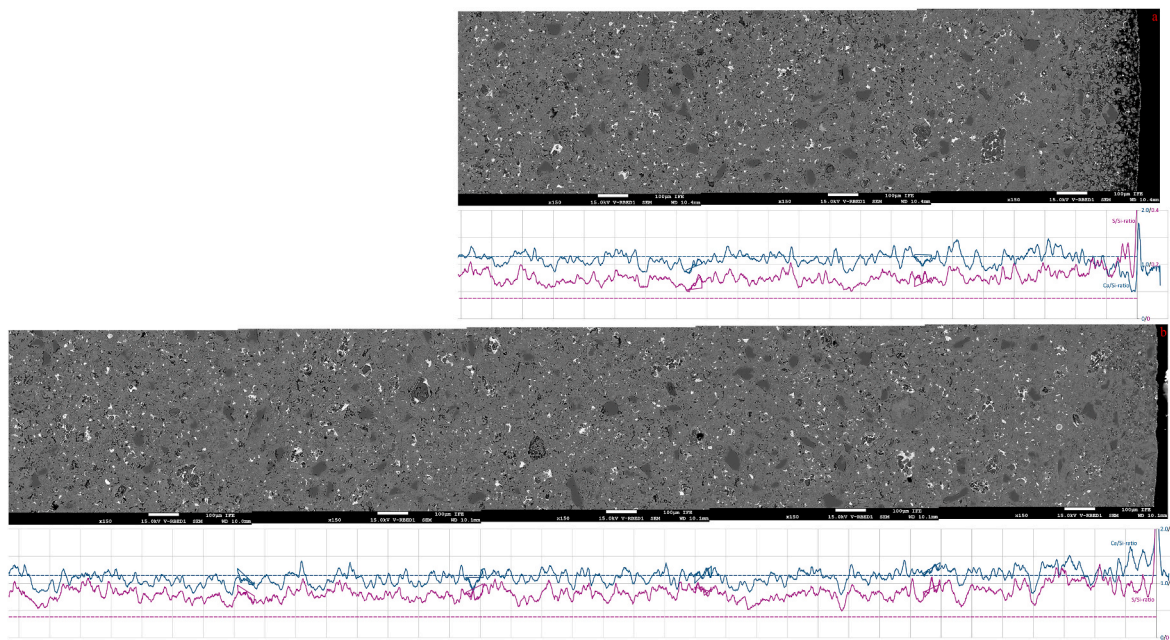
Finally, in the sample exposed for 16 weeks, degradation is observed in the outer  $\sim 100\text{--}200\ \mu\text{m}$ , and correlated to a depleted Ca/Si-ratio in the outer  $\sim 80\ \mu\text{m}$ , which then increases steeply to reference values between  $\sim 80$  and  $100\ \mu\text{m}$  from the sample surface. Between  $\sim 200\ \mu\text{m}$  and  $\sim 1000\ \mu\text{m}$  from the sample surface, the porosity is relatively low, while from  $\sim 1000\ \mu\text{m}$  inwards, the sample microstructure is relatively homogeneous. As with the other samples, S/Si-ratios are somewhat elevated, and constant throughout the sample.

#### 3.4.2. Sealant S2

All CT scans of samples of sealant S2 are shown in Fig. 8. Similar to S1, exposure of S2 to  $\text{CO}_2$ -saturated water (Fig. 8c) led to concentric zones, with a relatively unaffected core surrounded by a lower density zone ( $\sim 1020\ \mu\text{m}$  wide), in turn bound by a zone with somewhat higher density than seen at the core ( $\sim 800\ \mu\text{m}$  wide), and a narrow outer zone of about  $60\ \mu\text{m}$  with reduced density. Here, the sample exposed to  $\text{CO}_2$  containing  $\text{H}_2\text{S}$  (Fig. 8e) shows somewhat deeper penetration of these reaction zones, with enhanced density observed to about  $\sim 1040\ \mu\text{m}$  from the sample surface, and subsequent depleted densities observed down to  $\sim 2030\ \mu\text{m}$  from the sample surface. Exposure to supercritical  $\text{CO}_2$  led to a minor increase in density in the outer zone of all samples,



**Fig. 5.** SEM Micrographs of S1 samples exposed to water saturated with CO<sub>2</sub> containing 1.6 mol% H<sub>2</sub>S for 4 (a) and 16 (b) weeks. The graphs underneath each micrograph show the Ca/Si (blue, on the 0–2.0 axis) and S/Si (purple, on the 0–0.4 axis) elemental ratios (atom %/atom %) measured along the micrograph using EDS. The dashed lines are reference values (average values) measured at the centre of an unexposed sample. Scalebars shown with the micrographs and gridline spacing for the graphs are 100  $\mu$ m.



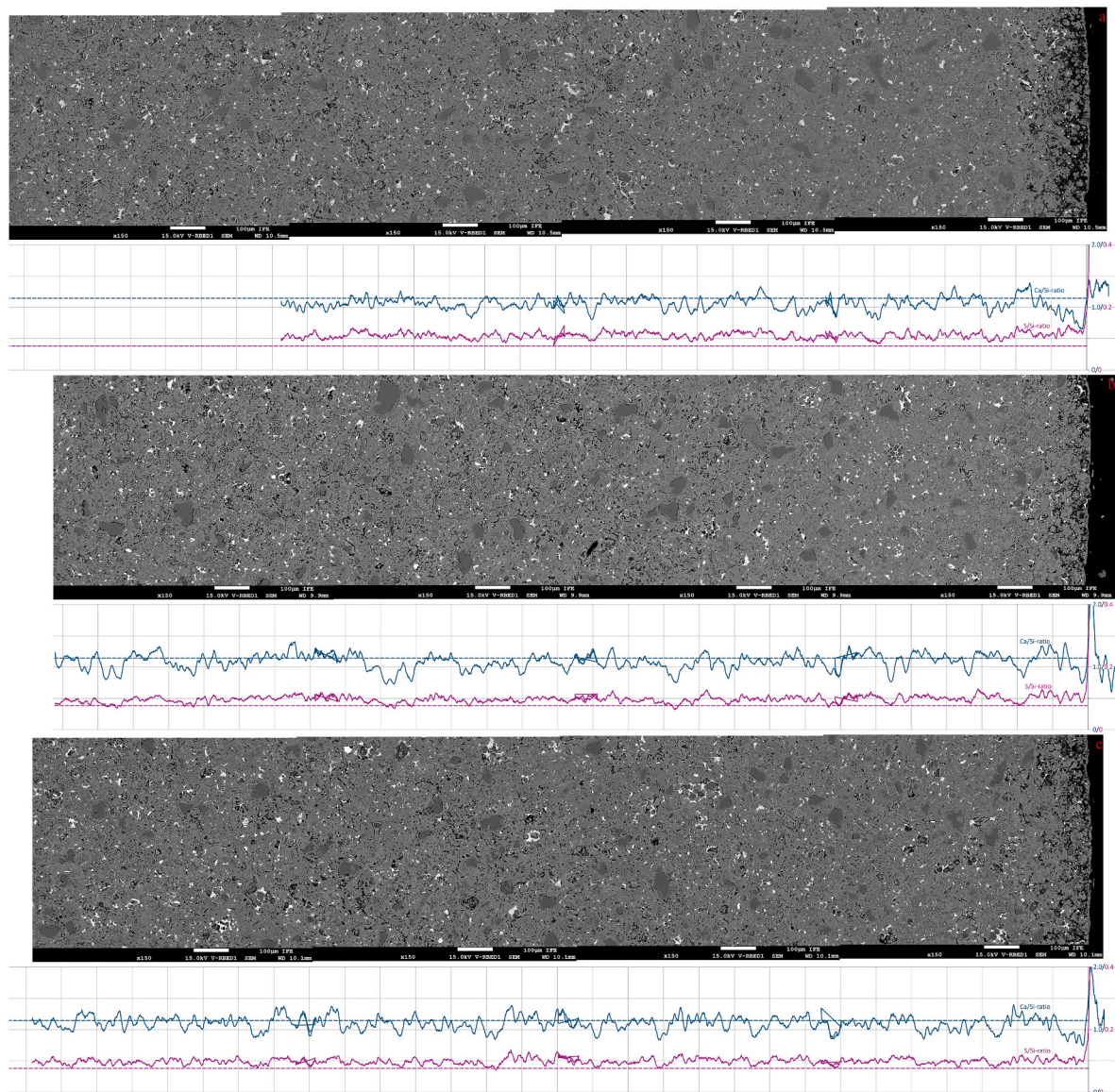
**Fig. 6.** SEM Micrographs of S1 samples exposed to wet supercritical CO<sub>2</sub> with 1.6 mol% H<sub>2</sub>S for 4 (a) and 16 (b) weeks. The graphs underneath each micrograph show the Ca/Si (blue, on the 0–2.0 axis) and S/Si (purple, on the 0–0.4 axis) elemental ratios (atom %/atom %) measured along the micrograph using EDS. The dashed lines are reference values (average values) measured at the centre of an unexposed sample. Scalebars shown with the micrographs and gridline spacing for the graphs are 100  $\mu$ m.

and compared to clean CO<sub>2</sub> (Fig. 8b) this alteration penetrated deeper into the sample in the presence of H<sub>2</sub>S (Fig. 8d) and (to a lesser extent) H<sub>2</sub>SO<sub>4</sub> (Fig. 8f).

Fig. 9 shows SEM cross-sections and element ratio curves of sealant S2 samples exposed to CO<sub>2</sub>-saturated water, with the CO<sub>2</sub>-phase containing 1.6 mol% H<sub>2</sub>S, for 4 and 16 weeks. As can be seen in Fig. 9a, a 4-week exposure led to the formation of a thin (a few  $\mu$ m thick) precipitate layer on the outer surface of the exposed sample. Behind this precipitate

layer, the material is partly dissolved and quite strongly degraded in a 10–20  $\mu$ m wide zone, and then gradually increases in integrity. In the outer 200–400  $\mu$ m of the sample, this correlates to a depleted Ca/Si-ratio, that increases gradually up to the reference value. Between ~400 and ~800  $\mu$ m from the surface, the sample is somewhat less porous, indicating carbonate precipitation. Inwards from this, the sample is relatively homogeneous. On the surface of the sample exposed for 16 weeks, a similar thin precipitate layer is observed, behind which the



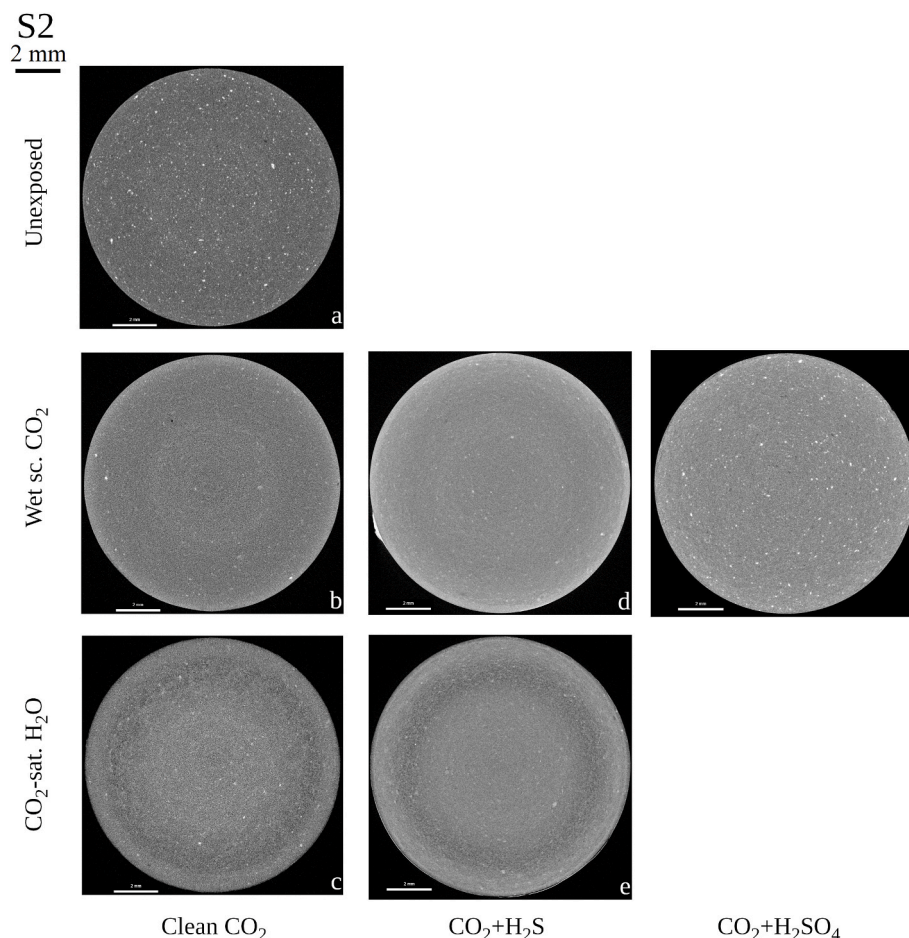


**Fig. 7.** SEM Micrographs of S1 samples exposed to wet supercritical  $\text{CO}_2$  equilibrated with concentrated  $\text{H}_2\text{SO}_4$  for 4 (a), 8 (b), and 16 (c) weeks. The graphs underneath each micrograph show the Ca/Si (blue, on the 0–2.0 axis) and S/Si (purple, on the 0–0.4 axis) elemental ratios (atom %/atom %) measured along the micrograph using EDS. The dashed lines are reference values (average values) measured at the centre of an unexposed sample. Scalebars shown with the micrographs and gridline spacing for the graphs are 100  $\mu\text{m}$ .

sample is strongly degraded for  $\sim 100\ \mu\text{m}$ . Inwards from that, over a  $\sim 150\ \mu\text{m}$  wide zone, dense precipitation fills much of the porosity. This transitions abruptly into a zone with finer-grained precipitates and somewhat higher porosity. These microstructural zones are associated with a strongly depleted Ca/Si-ratio near the sample surface, that then increases inwards, reaching reference values at about 400–500  $\mu\text{m}$  from the surface. Moving further inwards, the porosity increases again, and from  $\sim 700\ \mu\text{m}$  from the surface the Ca/Si-ratio decreases below reference values. Between  $\sim 1100\ \mu\text{m}$  and  $\sim 2100\ \mu\text{m}$  from the surface, a zone of relatively high porosity is correlated with a depleted Ca/Si-ratio. Around  $\sim 2100\ \mu\text{m}$ , this ratio increases to (near-)reference values, and then remains relatively constant, while the microstructure appears homogeneous from here. After both 4 and 16 weeks, the S/Si-ratio is elevated throughout the sample compared to the reference value (0.069), and relatively constant between surface and core. In these samples sub-micron high-density particles, similar to those identified as iron sulphides in the S1 samples exposed to  $\text{CO}_2$ -saturated water, are also observed. In the 4-week exposed sample, these are observed in the

outer  $\sim 1500\ \mu\text{m}$ , while in the 16-week exposed sample they were found throughout, though mostly in the outer  $\sim 1500\ \mu\text{m}$  (and especially in the outer  $\sim 100\ \mu\text{m}$ ).

Fig. 10 shows sample cross-sections and element ratios for S2 samples exposed directly to the wet supercritical  $\text{CO}_2$ -phase, containing 1.6 mol%  $\text{H}_2\text{S}$ . The sample exposed for 4 weeks has a very thin precipitate layer on its outer surface, behind which the sample is somewhat degraded to  $\sim 20$ – $30\ \mu\text{m}$  from the sample surface, at which point a dense precipitate appears that fills up most pore space around silica particles. This dense precipitate is observed to about  $\sim 300\ \mu\text{m}$  from the surface, where it sharply transitions into a finer-grained precipitate with higher intergranular porosity. From about  $\sim 700\ \mu\text{m}$  inwards, the sample microstructure is mostly homogeneous. These microstructures are correlated with a somewhat decreased Ca/Si-ratio in the outer 150–200  $\mu\text{m}$  of the sample. On the sample exposed for 16 weeks, the outer precipitate layer is slightly thicker, and more consistent. Behind it, the degraded zone is  $\sim 50\ \mu\text{m}$  wide, before coarse precipitates fill up most porosity. At about 300  $\mu\text{m}$  from the sample surface, the coarse



**Fig. 8.** CT-scans of sealant S2; a) unexposed, b) exposed to wet supercritical  $\text{CO}_2$ , c) exposed to  $\text{CO}_2$ -saturated water, d) exposed to wet supercritical  $\text{CO}_2$  with 1.6 mol %  $\text{H}_2\text{S}$ , e) exposed to  $\text{CO}_2$ -saturated water with  $\text{H}_2\text{S}$ , and f) exposed to supercritical  $\text{CO}_2$  equilibrated with concentrated  $\text{H}_2\text{SO}_4$ . The scalebars shown with the scans are 2 mm. All exposure durations were 16 weeks. CT scans of the unexposed reference sample and samples exposed to clean  $\text{CO}_2$  taken from (van Noort et al., 2025).

precipitates sharply transition to finer precipitates, coarsening inwards between 300 and 650  $\mu\text{m}$ , while from there inwards the microstructure is mostly homogeneous. While the Ca/Si-ratio is somewhat depleted in the outer  $\sim 80\text{--}100\text{ }\mu\text{m}$ , it is mostly constant (and around the reference value) in the rest of the sample. Both 4 and 16 weeks exposure led to an increase in S/Si-ratio throughout each sample. In these samples sub-micron high-density particles, similar to those identified as iron sulphides in the S1 samples exposed to  $\text{CO}_2$ -saturated water, are also observed. In the 4-week exposed sample, these are only found in the outer  $\sim 1000\text{ }\mu\text{m}$ , while in the 16-week exposed sample they were found throughout, though mostly in the outer  $\sim 600\text{ }\mu\text{m}$ .

Fig. 11 shows cross-sections through S2 samples exposed to supercritical  $\text{CO}_2$  in the presence of  $\text{H}_2\text{SO}_4$  for 4, 8 and 16 weeks. All three samples show an outer zone where carbonation has led to a relatively coarse microstructure, with large pores and massive precipitates. Inwards, this microstructure transitions quite sharply to a zone with very fine, grainy matrix structure, that then gradually coarsens and becomes homogeneous. In the samples exposed for 4 and 8 weeks, the coarse outer zone is  $\sim 100\text{--}130\text{ }\mu\text{m}$  wide, while the finer microstructure coarsens and becomes homogeneous between  $\sim 600$  and  $800\text{ }\mu\text{m}$  from the sample surface. While in the sample exposed for 4 weeks, the Ca/Si-ratio is mostly constant, in the sample exposed for 8 weeks, this ratio is somewhat depleted up to  $500\text{ }\mu\text{m}$  from the sample surface. In the sample exposed for 16 weeks, the coarse outer zone is between 100 and  $150\text{ }\mu\text{m}$  wide. Here, the zone with very fine microstructure transitions to a coarser, homogeneous microstructure between  $\sim 500$  and  $800\text{ }\mu\text{m}$  from the sample surface. While the Ca/Si-ratio is depleted in the outer  $\sim 50$

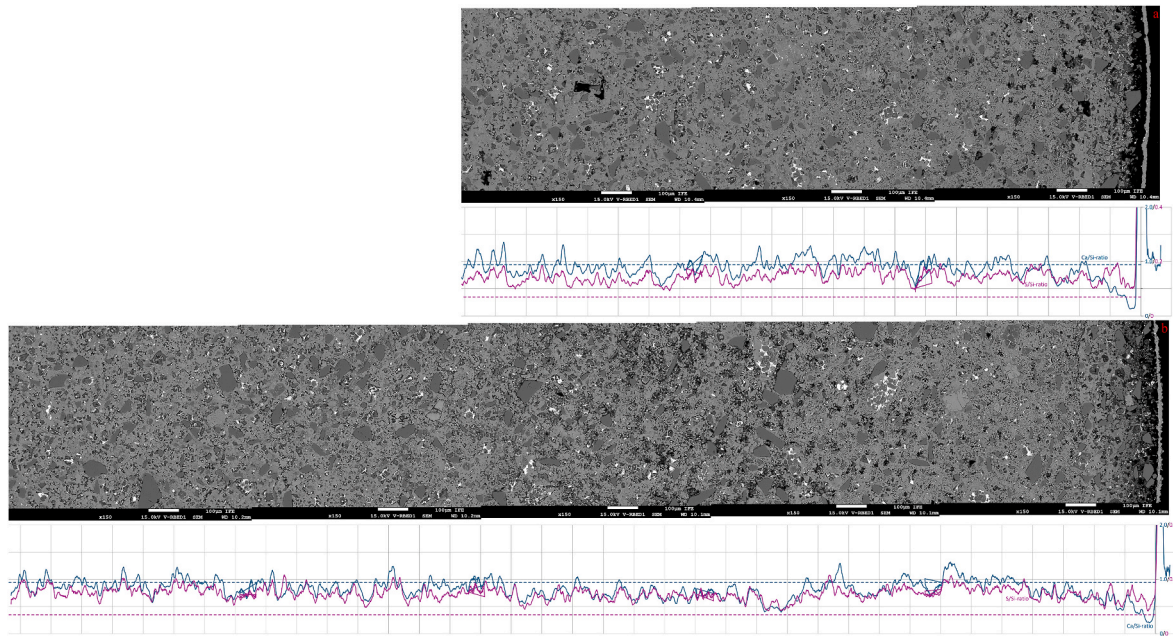
$\mu\text{m}$ , it is slightly elevated further inwards to  $1280\text{ }\mu\text{m}$  from the surface, where it drops sharply to reference values. In all three samples, the S/Si-ratio is somewhat increased over reference values, but does not vary much between surface and centre.

#### 3.4.3. Sealant S3

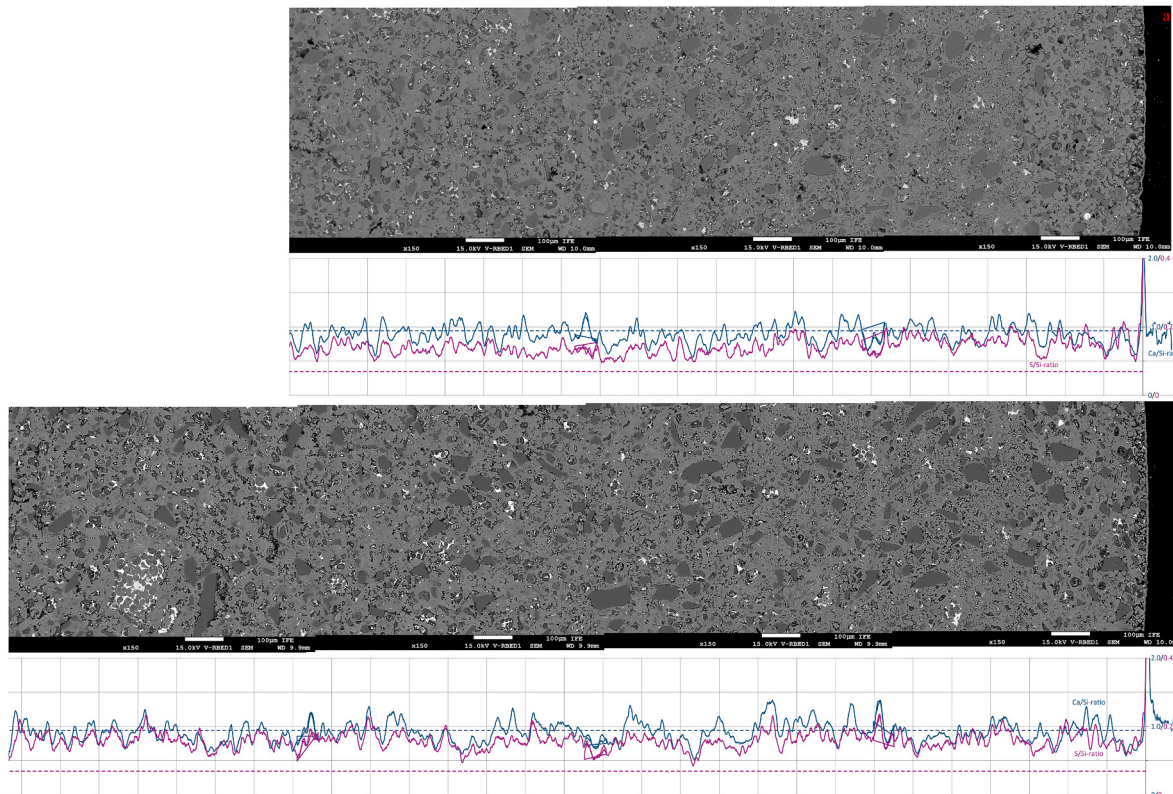
All CT scans of samples of sealant S3 are shown in Fig. 12. The sample exposed to water saturated with clean  $\text{CO}_2$  (Fig. 12c) shows relatively little change in density, except for localised areas of density loss within the outer  $\sim 200\text{ }\mu\text{m}$  of the sample. In contrast, the sample exposed to water saturated with  $\text{CO}_2$  containing  $\text{H}_2\text{S}$  (Fig. 12e) shows a sharply bound outer zone of  $\sim 265\text{ }\mu\text{m}$  where its density is increased. Inwards of that zone, the density is somewhat reduced for about  $\sim 280\text{ }\mu\text{m}$ , gradually increasing to a constant value (assumed to be unaffected). In the sample exposed to clean, wet supercritical  $\text{CO}_2$  (Fig. 12b), the outer rim ( $\sim 250\text{ }\mu\text{m}$  wide) is somewhat elevated in density, while there are also localised areas of reduced density. Within that, the sample density is somewhat enhanced to  $\sim 1100\text{ }\mu\text{m}$  from the sample surface. In the sample exposed to wet supercritical  $\text{CO}_2$  with  $\text{H}_2\text{S}$  (Fig. 12d), the outer zone ( $\sim 310\text{--}320\text{ }\mu\text{m}$  wide) is likewise somewhat elevated in density. In the sample exposed to  $\text{CO}_2$  with  $\text{H}_2\text{SO}_4$  (Fig. 12f), a minor increase in density is observed in a relatively wide outer zone, but especially in the outer  $\sim 400\text{ }\mu\text{m}$  of the sample.

Fig. 13 shows SEM cross-sections and element ratio curves of sealant S3 samples exposed to  $\text{CO}_2$ -saturated water, with the  $\text{CO}_2$ -phase containing 1.6 mol%  $\text{H}_2\text{S}$ , for 4 and 16 weeks. The sample exposed for 4 weeks, shown in Fig. 13a, has a thin outer precipitate layer behind



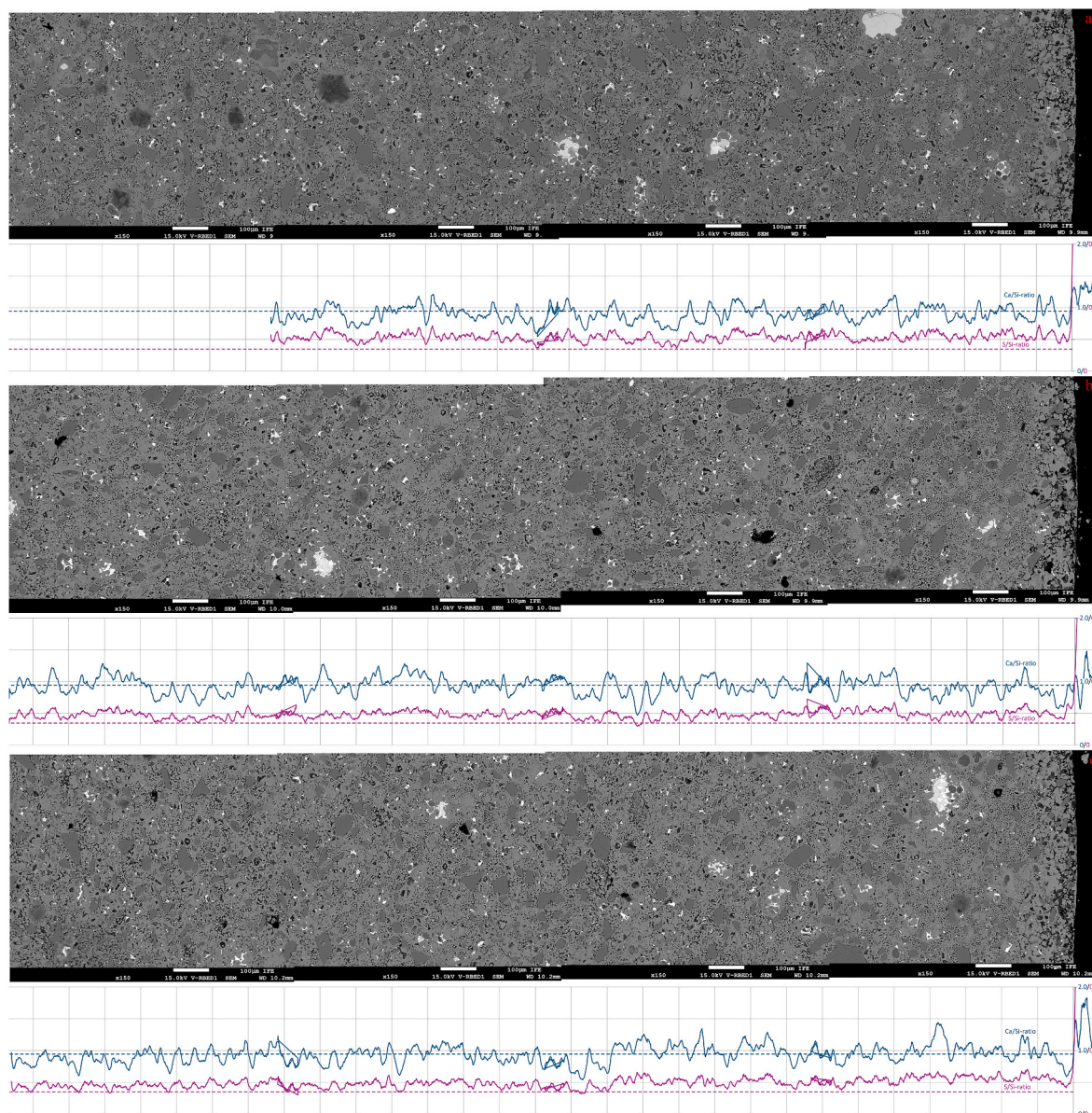


**Fig. 9.** SEM Micrographs of S2 samples exposed to water saturated with  $\text{CO}_2$  containing 1.6 mol%  $\text{H}_2\text{S}$  for 4 (a) and 16 (b) weeks. The graphs underneath each micrograph show the Ca/Si (blue, on the 0–2.0 axis) and S/Si (purple, on the 0–0.4 axis) elemental ratios (atom %/atom %) measured along the micrograph using EDS. The dashed lines are reference values (average values) measured at the centre of an unexposed sample. Scalebars shown with the micrographs and gridline spacing for the graphs are 100  $\mu\text{m}$ .



**Fig. 10.** SEM Micrographs of S2 samples exposed to wet supercritical  $\text{CO}_2$  with 1.6 mol%  $\text{H}_2\text{S}$  for 4 (a) and 16 (b) weeks. The graphs underneath each micrograph show the Ca/Si (blue, on the 0–2.0 axis) and S/Si (purple, on the 0–0.4 axis) elemental ratios (atom %/atom %) measured along the micrograph using EDS. The dashed lines are reference values (average values) measured at the centre of an unexposed sample. Scalebars shown with the micrographs and gridline spacing for the graphs are 100  $\mu\text{m}$ .



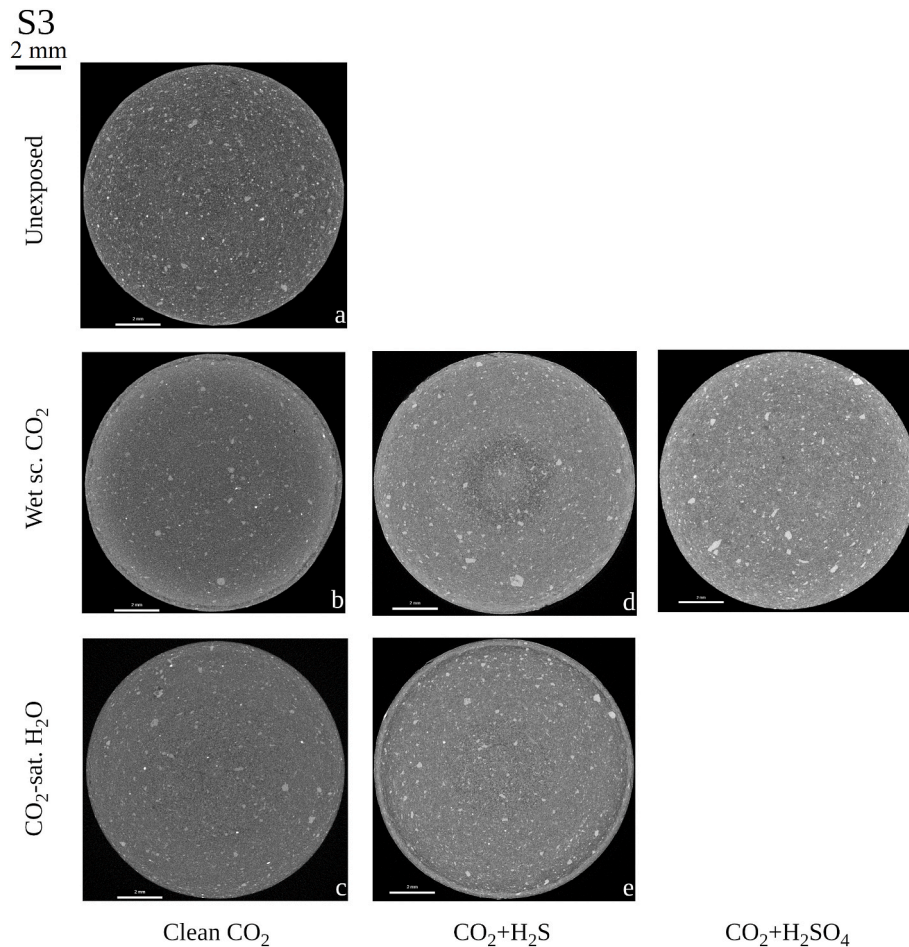


**Fig. 11.** SEM Micrographs of S2 samples exposed to wet supercritical  $\text{CO}_2$  equilibrated with concentrated  $\text{H}_2\text{SO}_4$  for 4 (a), 8 (b), and 16 (c) weeks. The graphs underneath each micrograph show the Ca/Si (blue, on the 0–2.0 axis) and S/Si (purple, on the 0–0.4 axis) elemental ratios (atom %/atom %) measured along the micrograph using EDS. The dashed lines are reference values (average values) measured at the centre of an unexposed sample. Scalebars shown with the micrographs and gridline spacing for the graphs are 100  $\mu\text{m}$ .

which, over  $\sim 50 \mu\text{m}$ , the sealant is degraded due to dissolution and leaching. Inwards from this, the open pore space is filled with relatively small ( $< 10 \mu\text{m}$ ), spherical precipitates. From  $\sim 120 \mu\text{m}$ , moving inwards this precipitated microstructure coarsens gradually, leading to a relatively coarse, homogeneous microstructure from  $\sim 450 \mu\text{m}$  from the sample surface. In the outer  $\sim 100$ – $120 \mu\text{m}$ , these microstructures are correlated with a somewhat depleted Ca/Si-ratio, and elevated Mg/Ca-ratio. The sample exposed for 16 weeks shows some precipitation on the outer surface. Behind this, the outer  $\sim 50$ – $100 \mu\text{m}$  of the sample is quite degraded. Between  $\sim 50$  and  $400 \mu\text{m}$ , the pores between larger silicate grains are filled with fine spherical, insular precipitates ( $< \sim 10 \mu\text{m}$  in diameter). From  $\sim 400 \mu\text{m}$  inwards, these precipitate grains have relatively dark (i.e., lower in density) cores, and gradually increase in size. From about  $1200 \mu\text{m}$  from the sample surface, the sample microstructure becomes relatively homogeneous, with precipitate rims around larger silicate grains and relatively coarse precipitates in the pore space between these grains. In the outer  $\sim 150 \mu\text{m}$ , the Ca/Si-ratio is depleted

(and the Mg/Ca-ratio relatively enriched). From  $150$  to  $\sim 600 \mu\text{m}$  from the sample surface, the Ca/Si-ratio increases gradually up to reference values. S/Si-ratios are elevated throughout both samples compared to the reference value (0.078), independent of exposure duration (or distance from the sample surface). In these samples sub-micron high-density particles, similar to those identified as iron sulphides in the S1 samples exposed to  $\text{CO}_2$ -saturated water, are also observed. In the 4-week exposed sample, these are found throughout the exposed sample, but are somewhat more prevalent near the sample surface, while in the 16-week exposed sample they were found throughout, but are considerably more prevalent in a few mm wide zone from  $\sim 300 \mu\text{m}$  from the sample surface.

Fig. 14 shows cross-sections through the S3 samples exposed directly to the  $\text{H}_2\text{S}$ -bearing supercritical  $\text{CO}_2$ -phase. In the sample exposed for 4 weeks, exposure led to an outer zone with very fine, insular precipitates surrounding the larger silicate grains, with these precipitates coarsening from about  $\sim 300$ – $400 \mu\text{m}$  from the sample surface. Over the outer



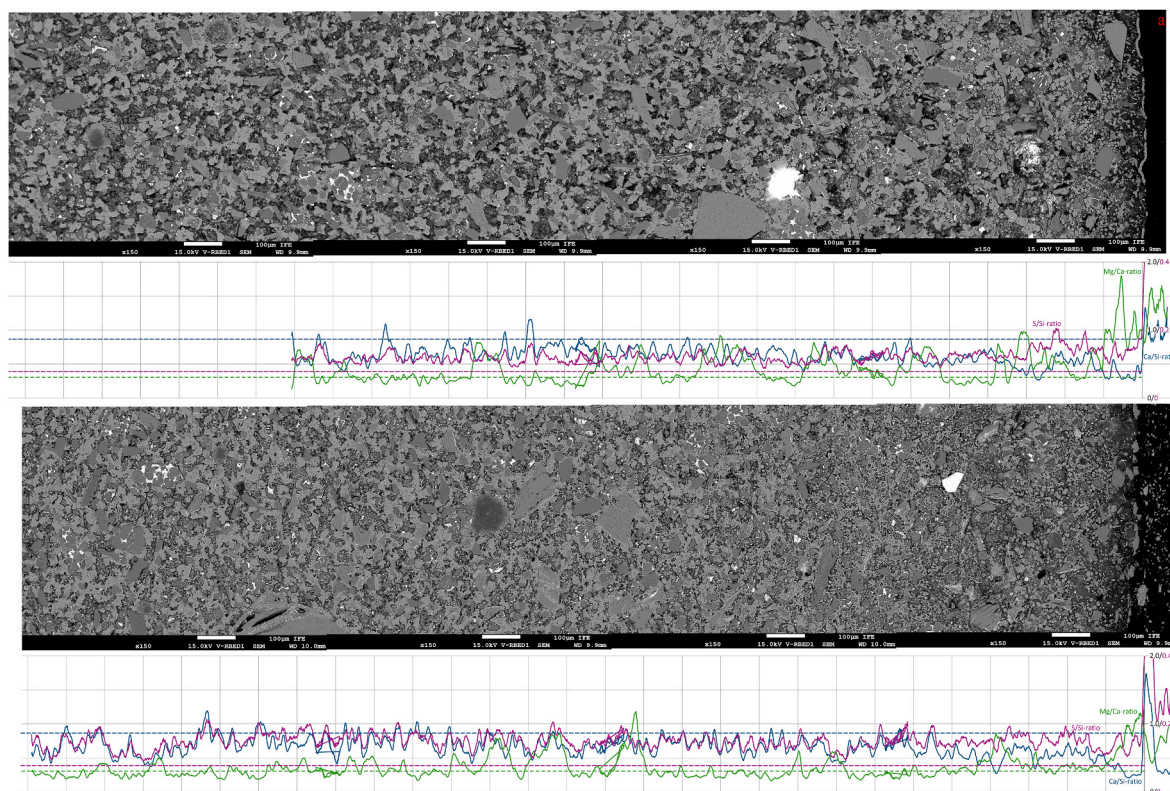
**Fig. 12.** CT-scans of sealant S3; a) unexposed, b) exposed to wet supercritical  $\text{CO}_2$ , c) exposed to  $\text{CO}_2$ -saturated water, d) exposed to wet supercritical  $\text{CO}_2$  with 1.6 mol%  $\text{H}_2\text{S}$ , e) exposed to  $\text{CO}_2$ -saturated water with  $\text{H}_2\text{S}$ , and f) exposed to supercritical  $\text{CO}_2$  equilibrated with concentrated  $\text{H}_2\text{SO}_4$ . The scalebars shown with the scans are 2 mm. All exposure durations were 16 weeks. CT scans of the unexposed reference sample and samples exposed to clean  $\text{CO}_2$  taken from (van Noort et al., 2025).

$\sim 400 \mu\text{m}$ , the Ca/Si-ratio shows a minor depletion towards the sample surface, while the Mg/Ca-ratio is somewhat elevated. In the sample exposed for 16 weeks, the finer precipitates in the outer zone are considerably less fine than in the sample exposed for 4 weeks (though still  $<10 \mu\text{m}$ ). Between 200 and 700  $\mu\text{m}$  from the sample surface, these finer precipitates gradually coarsen and become less spherical in shape, leading to a homogeneous microstructure into the sample core. In this sample, the Ca/Si-ratio is significantly depleted in the outer  $\sim 100 \mu\text{m}$ , and somewhat depleted between  $\sim 100$  and 700  $\mu\text{m}$ , while the Mg/Ca-ratio is somewhat enriched. Furthermore, S/Si-ratios are enriched throughout the samples after both 4- and 16-week exposures. In these samples sub-micron high-density particles, similar to those identified as iron sulphides in the S1 samples exposed to  $\text{CO}_2$ -saturated water, are also observed. In the 4-week exposed sample, these are found throughout but are somewhat more prevalent in the outer  $\sim 2 \text{ mm}$ , while in the 16-week exposed sample they were found throughout, but are considerably more prevalent in a few mm wide zone from  $\sim 400 \mu\text{m}$  from the surface.

Fig. 15 shows cross-sections through the S3 samples exposed to supercritical  $\text{CO}_2$  containing  $\text{H}_2\text{SO}_4$ , for 4, 8 and 16 weeks. In these samples, exposure resulted in a microstructure in which the larger pre-existing silicate grains (mostly quartz and olivine) are surrounded by a porosity filled with mostly insular precipitate grains (as well as some more continuous precipitates around or between larger grains). The grain-size of the insular precipitates varies in various zones between sample surface and core. In the sample exposed for 4 weeks, in an outer

zone of about  $\sim 250 \mu\text{m}$  wide, the precipitate particles are medium in size ( $\sim 10 \mu\text{m}$  in diameter), and the open porosity appears somewhat higher than elsewhere in the sample. In this zone, the Ca/Si-ratio is depleted, and then increases sharply to reference values around  $\sim 140\text{--}150 \mu\text{m}$  from the sample surface. Inwards of this outer zone, the precipitation found in the pore space is a combination of very fine insular precipitates (typically  $\sim 5 \mu\text{m}$  across) with more massive precipitates around and between the larger silicate grains. However, between  $\sim 1600$  and  $\sim 2100 \mu\text{m}$  from the sample surface, the finer precipitate is more prevalent, resulting in an apparent lower porosity than in the other parts of the sample. In the sample exposed for 8 weeks, a similar outer zone with relatively high porosity and medium-sized precipitates,  $\sim 300 \mu\text{m}$  wide, is correlated with a somewhat depleted Ca/Si-ratio between  $\sim 50 \mu\text{m}$  and  $\sim 200 \mu\text{m}$  from the sample surface. Inwards of this zone, the precipitates are again a combination of finer, insular grains as well as larger, more massive precipitates mostly around the larger silicate grains. A zone with somewhat decreased porosity due to increased precipitation of fine carbonates, similar to the sample exposed for 4 weeks but less intense, is seen between  $\sim 1800$  and  $\sim 2400 \mu\text{m}$  from the sample surface. Finally, in the sample exposed for 16 weeks, a similar outer zone of about  $\sim 300 \mu\text{m}$  wide coincides with a somewhat depleted Ca/Si-ratio over the outer  $\sim 300 \mu\text{m}$ . A zone with increased very fine precipitation is observed between  $\sim 2200$  and  $2700 \mu\text{m}$  from the sample surface. Between these two distinct zones, the sample microstructure is mostly homogeneous. Note that S/Si-ratios are elevated throughout all samples exposed to  $\text{CO}_2$  with  $\text{H}_2\text{SO}_4$ .





**Fig. 13.** SEM Micrographs of S3 samples exposed to water saturated with CO<sub>2</sub> containing 1.6 mol% H<sub>2</sub>S for 4 (a) and 16 (b) weeks. The graphs underneath each micrograph show the Ca/Si and Mg/Ca (blue and green, respectively, both on the 0–2.0 axis), and S/Si (purple, on the 0–0.4 axis) elemental ratios (atom %/atom %) measured along the micrograph using EDS. The dashed lines are reference values (average values) measured at the centre of an unexposed sample. Scalebars shown with the micrographs and gridline spacing for the graphs are 100  $\mu$ m.

#### 3.4.4. Sealant S4

All CT scans of samples of sealant S4 are shown in Fig. 16. Here, it is clearly seen that none of the exposures led to significant changes in density, and the samples were not significantly affected by the presence of either H<sub>2</sub>S or H<sub>2</sub>SO<sub>4</sub>.

Similarly to the CT-scans, the SEM cross-sections of S4 samples exposed to CO<sub>2</sub> with H<sub>2</sub>S (Figs. 17 and 18) and CO<sub>2</sub> with H<sub>2</sub>SO<sub>4</sub> (Fig. 19) show that this exposure resulted in only little change in microstructure or composition. No significant microstructural changes are seen in the samples exposed for 4 or 16 weeks to water saturated with CO<sub>2</sub> with H<sub>2</sub>S. In the sample exposed for 4 weeks, the Ca/Al- and Si/Al-ratios are somewhat depleted at the sample surface, and rise gradually moving inwards over  $\sim$ 200  $\mu$ m. In the sample exposed for 16 weeks, such minor depletion is not observed. Though the Si/Al-ratio is somewhat elevated compared to reference values between  $\sim$ 100  $\mu$ m and  $\sim$ 700  $\mu$ m from the sample surface, this is also seen in the unexposed samples (van Noort et al., 2025). S/Al-ratios are somewhat elevated compared to the reference value (0.10), notably in the outer  $\sim$ 700  $\mu$ m of the sample exposed for 16 weeks, but the change is relatively limited.

Direct exposure to wet supercritical CO<sub>2</sub> with H<sub>2</sub>S likewise led to limited change in sample microstructure or integrity. However, in the S4 sample exposed thus for 4 weeks, an apparent increase in porosity is observed up to  $\sim$ 600–700  $\mu$ m from the surface. While this may actually be due to sample preparation differences, this increase in porosity is associated with an elevated Si/Al-ratio peaking at  $\sim$ 200  $\mu$ m from the sample surface and decreasing gradually to reference values between 200 and 700  $\mu$ m from the sample surface, as well as an enriched Ca/Al-ratio in the outer  $\sim$ 700  $\mu$ m of the sample. Note that in the outer 40–50  $\mu$ m of this sample, the Ca/Al-ratio increases strongly towards the surface, while the Si/Al-ratio decreases. The S/Al-ratio is somewhat enhanced in the outer  $\sim$ 700  $\mu$ m of this sample. The sample exposed for 16 weeks does not show the somewhat enhanced porosity near the

sample surface seen in the sample exposed for 4 weeks. Here, the Si/Al- and Ca/Al-ratios increase strongly in the outer 80–100  $\mu$ m, to a peak in these ratios, and then decrease gradually going inwards over about 600–700  $\mu$ m. The S/Al-ratio is somewhat elevated compared to the reference value (0.10), mostly in the outer  $\sim$ 1000  $\mu$ m.

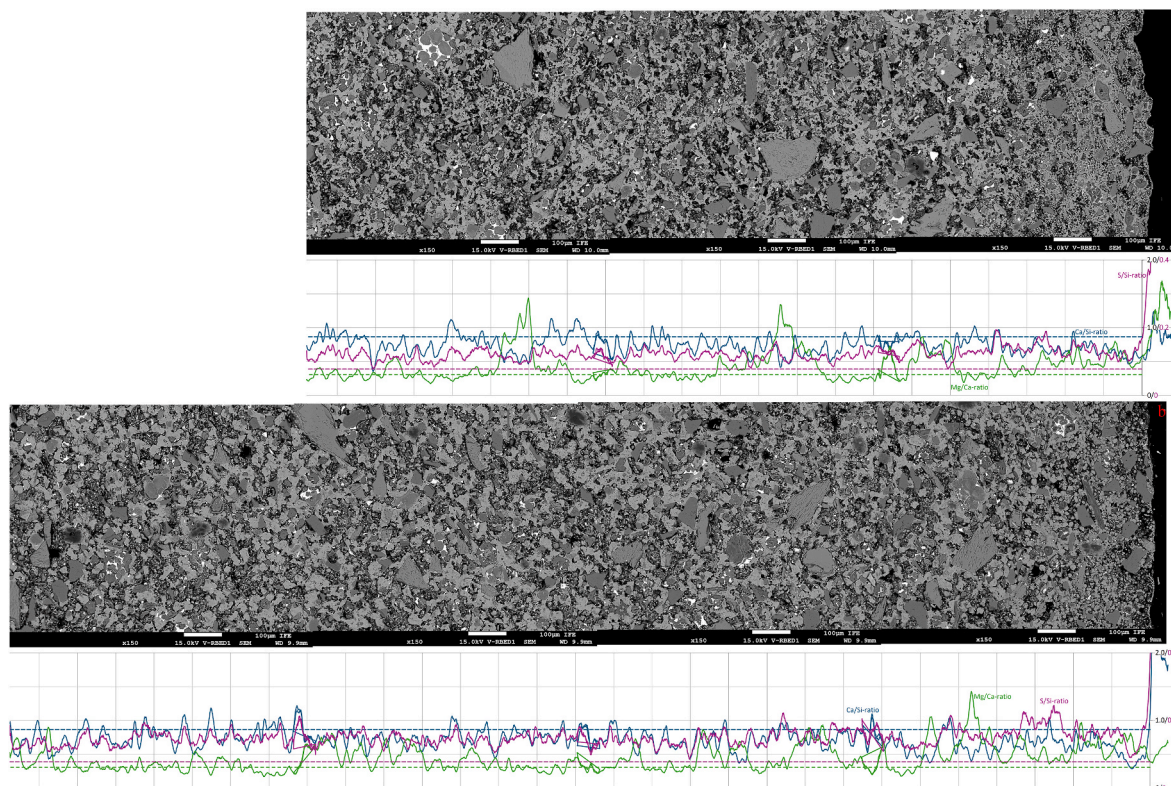
While some very fine (submicron), high-density particles were observed in S4 samples exposed to CO<sub>2</sub> with H<sub>2</sub>S, similar particles were also found in unexposed S4 samples, and samples exposed to clean CO<sub>2</sub>, and there was no significant change in quantity of distribution of such particles. The chemical composition of these particles has not been investigated further.

In the samples exposed to supercritical CO<sub>2</sub> with H<sub>2</sub>SO<sub>4</sub>, likewise no significant changes in sample integrity of microstructure due to exposure are observed. Here, similar, relatively minor variations in Si/Al- and Ca/Al-ratios are observed in the outer  $\sim$ 1000  $\mu$ m of the samples. S/Al-ratios are somewhat elevated in the outer  $\sim$ 600  $\mu$ m of the sample exposed for 8 weeks, and the outer  $\sim$ 900–1000  $\mu$ m of the sample exposed for 16 weeks, while in the sample exposed for 4 weeks, the S/Al-ratios are not affected significantly.

#### 3.4.5. Sealant S5

All CT scans of samples of sealant S5 are shown in Fig. 20. The large irregular holes seen in the unexposed reference sample (Fig. 20a), and in samples of S5 exposed directly to a CO<sub>2</sub>-phase most likely formed by the dissolution of activator particles during curing. As noted previously (van Noort et al., 2025), exposure to water saturated with clean CO<sub>2</sub> (Fig. 20c) led to a  $\sim$ 1300–1400  $\mu$ m wide outer zone with somewhat reduced density, plus a  $\sim$ 1200  $\mu$ m wide transition to an inner zone with relatively high density. However, density differences between these zones are very minor. Exposure to CO<sub>2</sub>-saturated water with H<sub>2</sub>S (Fig. 20e) led to a similar outer zone with somewhat reduced density of about 900–1000  $\mu$ m wide, followed by a  $\sim$ 1900–2000  $\mu$ m wide irregular





**Fig. 14.** SEM Micrographs of S3 samples exposed to wet supercritical  $\text{CO}_2$  with 1.6 mol%  $\text{H}_2\text{S}$  for 4 (a) and 16 (b) weeks. The graphs underneath each micrograph show the Ca/Si and Mg/Ca (blue and green, respectively, both on the 0–2.0 axis), and S/Si (purple, on the 0–0.4 axis) elemental ratios (atom %/atom %) measured along the micrograph using EDS. The dashed lines are reference values (average values) measured at the centre of an unexposed sample. Scalebars shown with the micrographs and gridline spacing for the graphs are 100  $\mu\text{m}$ .

transition zone. Exposure to wet supercritical  $\text{CO}_2$  (Fig. 20b) led to a sharply delineated zone with somewhat enhanced density between  $\sim 170 \mu\text{m}$  and  $510 \mu\text{m}$  from the sample surface, and within that, a diffuse zone with somewhat reduced density. Outside of that zone, near the sample surface, some areas of reduced density are observed. Exposure to wet supercritical  $\text{CO}_2$  with  $\text{H}_2\text{S}$  (Fig. 20d) similarly led to enhanced densities in an outer zone  $\sim 140$ – $400 \mu\text{m}$  wide, and within that a slightly reduced density. However, some areas of reduced density are also observed near the sample surface. Exposure to  $\text{CO}_2$  with  $\text{H}_2\text{SO}_4$  (Fig. 20f), however, only resulted in a  $\sim 250 \mu\text{m}$  wide outer rim with slightly enhanced density.

SEM cross-sections of samples exposed to  $\text{CO}_2$  with  $\text{H}_2\text{S}$  are presented in Figs. 21 and 22. Considering first the samples exposed to  $\text{CO}_2$ -saturated water (Fig. 21), in the sample exposed for 4 weeks, in an outer zone of  $\sim 100 \mu\text{m}$ , the matrix is darker, indicating potential degradation. EDS analyses show that in the outer  $\sim 650 \mu\text{m}$ , the Ca/Si-ratio is depleted strongly, then increasing gradually to approximately the reference value at  $\sim 1400 \mu\text{m}$  from the sample surface. The Mg/Si-ratio is likewise somewhat depleted in the outer  $\sim 500 \mu\text{m}$  of the sample. The S/Si-ratio is somewhat elevated near the sample surface compared to the reference value (0.035), decreasing gradually to reference values at  $\sim 80 \mu\text{m}$  from the surface, and then increases somewhat from 600 to  $700 \mu\text{m}$  from the sample surface to remain somewhat elevated further inwards. The sample exposed for 16 weeks has a somewhat dark matrix in the outer  $\sim 400 \mu\text{m}$ . While the Ca/Si-ratio is depleted along the full  $\sim 3200 \mu\text{m}$  analysed, it is most strongly depleted in the outer  $\sim 800$ – $900 \mu\text{m}$ , and increases relatively sharply to near-reference values between 2000 and  $2200 \mu\text{m}$ . The Mg/Si-ratio is likewise depleted somewhat along the full section analysed, though mostly in the outer  $\sim 600$ – $700 \mu\text{m}$  of the sample. The S/Si-ratio is somewhat elevated near the sample surface, decreasing gradually to reference values at  $\sim 200 \mu\text{m}$  from the surface, and then increases somewhat from 900 to  $1100 \mu\text{m}$  from the sample

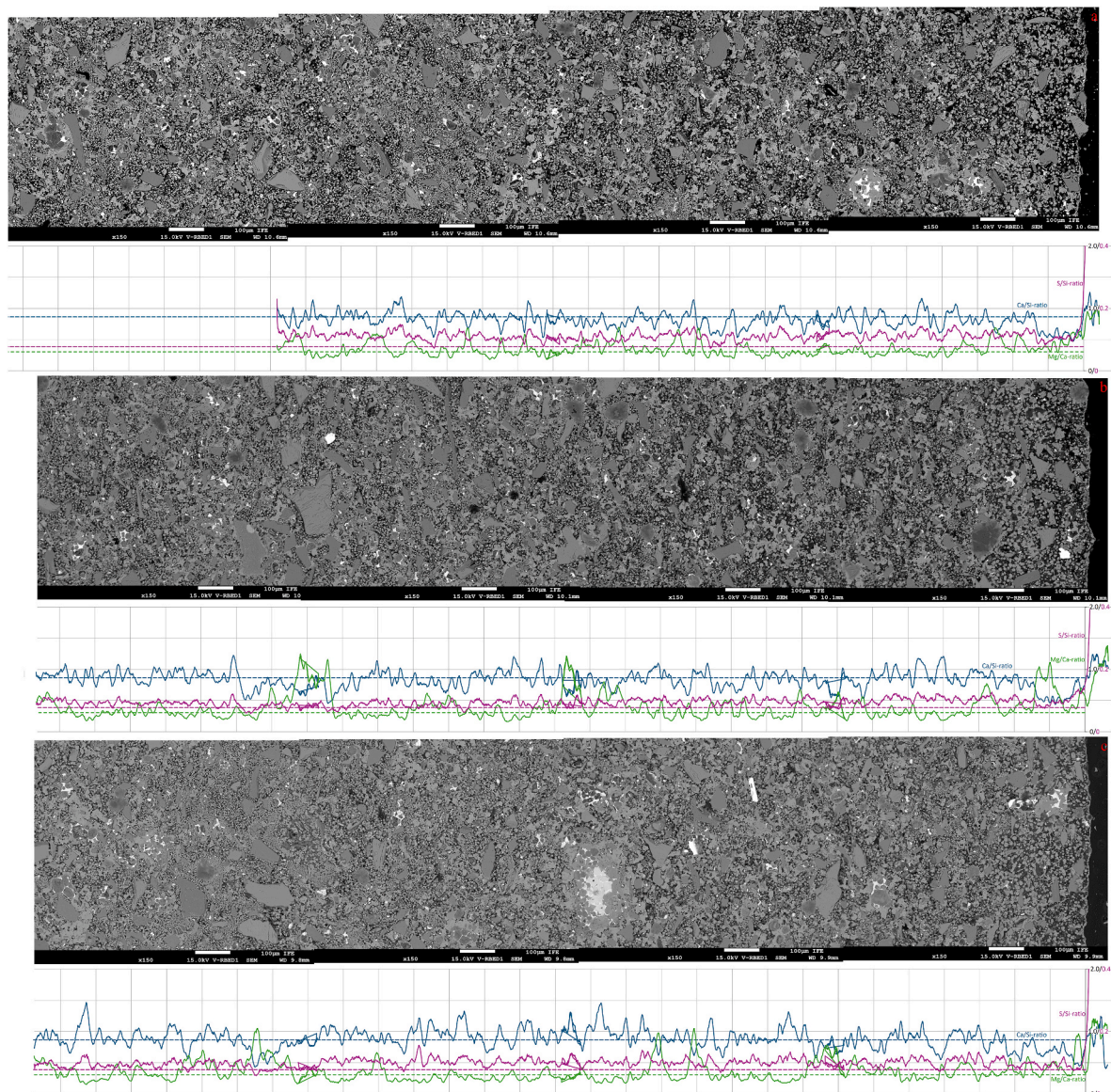
surface to then be consistently elevated further inwards.

In the samples exposed to wet supercritical  $\text{CO}_2$  with  $\text{H}_2\text{S}$  (see Fig. 22), after 4 weeks exposure, some precipitation is observed on the sample surface, while in the outer  $\sim 100 \mu\text{m}$  the sample matrix is somewhat darker (i.e., degraded). Furthermore, the Ca/Si-ratio is depleted in the outer  $\sim 1000$ – $1100 \mu\text{m}$  of the sample, as well as from  $\sim 1700 \mu\text{m}$  inwards. The S/Si-ratio is elevated throughout the sample. In the sample exposed for 16 weeks, in the outer  $\sim 100 \mu\text{m}$  the matrix likewise appears somewhat degraded, while between  $\sim 100$  and  $\sim 250 \mu\text{m}$  from the sample surface, matrix density is enhanced due to carbonate precipitation. The Ca/Si-ratio is somewhat depleted in the outer  $\sim 80 \mu\text{m}$ , but increases rapidly between 60 and  $140 \mu\text{m}$  from the sample surface, and then drops relatively steeply again between 140 and  $280 \mu\text{m}$ . While between  $\sim 400 \mu\text{m}$  and  $\sim 1400 \mu\text{m}$  from the sample surface, the Ca/Si-ratio is somewhat depleted, it then becomes relatively stable inwards at approximately the reference value. The S/Si-ratio is somewhat elevated compared to reference values throughout this sample, in particular in the outer  $\sim 200 \mu\text{m}$ .

Small quantities of very fine (submicron), high-density particles were observed in samples of S5 exposed to  $\text{CO}_2$  with  $\text{H}_2\text{S}$ . While these particles appear similar to those identified as Fe-sulphides in samples of S1, S2, and S3 exposed to  $\text{CO}_2$  with  $\text{H}_2\text{S}$ , similar particles were also observed in S5 samples exposed to clean  $\text{CO}_2$  and the S5 reference sample, and significant differences in quantity or distribution of such particles correlated to exposure fluid composition were not observed.

In the samples exposed to  $\text{CO}_2$  in the presence of  $\text{H}_2\text{SO}_4$  (see Fig. 23) after 4, 8 and 16 weeks, the sample matrixes are somewhat darker in the outer  $\sim 100 \mu\text{m}$ , while Ca/Si-ratios are somewhat depleted there, suggesting minor degradation in this zone. Moving inwards from that, matrix porosities appear somewhat reduced due to carbonate precipitation to  $\sim 1200 \mu\text{m}$  from the sample surfaces. While some precipitation is observed within the matrix inwards from this outer zone, this is not





**Fig. 15.** SEM Micrographs of S3 samples exposed to wet supercritical  $\text{CO}_2$  equilibrated with concentrated  $\text{H}_2\text{SO}_4$  for 4 (a), 8 (b), and 16 (c) weeks. The graphs underneath each micrograph show the Ca/Si and Mg/Ca (blue and green, respectively, both on the 0–2.0 axis), and S/Si (purple, on the 0–0.4 axis) elemental ratios (atom %/atom %) measured along the micrograph using EDS. The dashed lines are reference values (average values) measured at the centre of an unexposed sample. Scalebars shown with the micrographs and gridline spacing for the graphs are 100  $\mu\text{m}$ .

associated with any clear trends in elemental composition. In all three samples, the S/Si-ratio is somewhat elevated, especially in the outer  $\sim 200\text{--}300\ \mu\text{m}$ .

## 4. Discussion

### 4.1. Alteration and degradation of exposed sealants

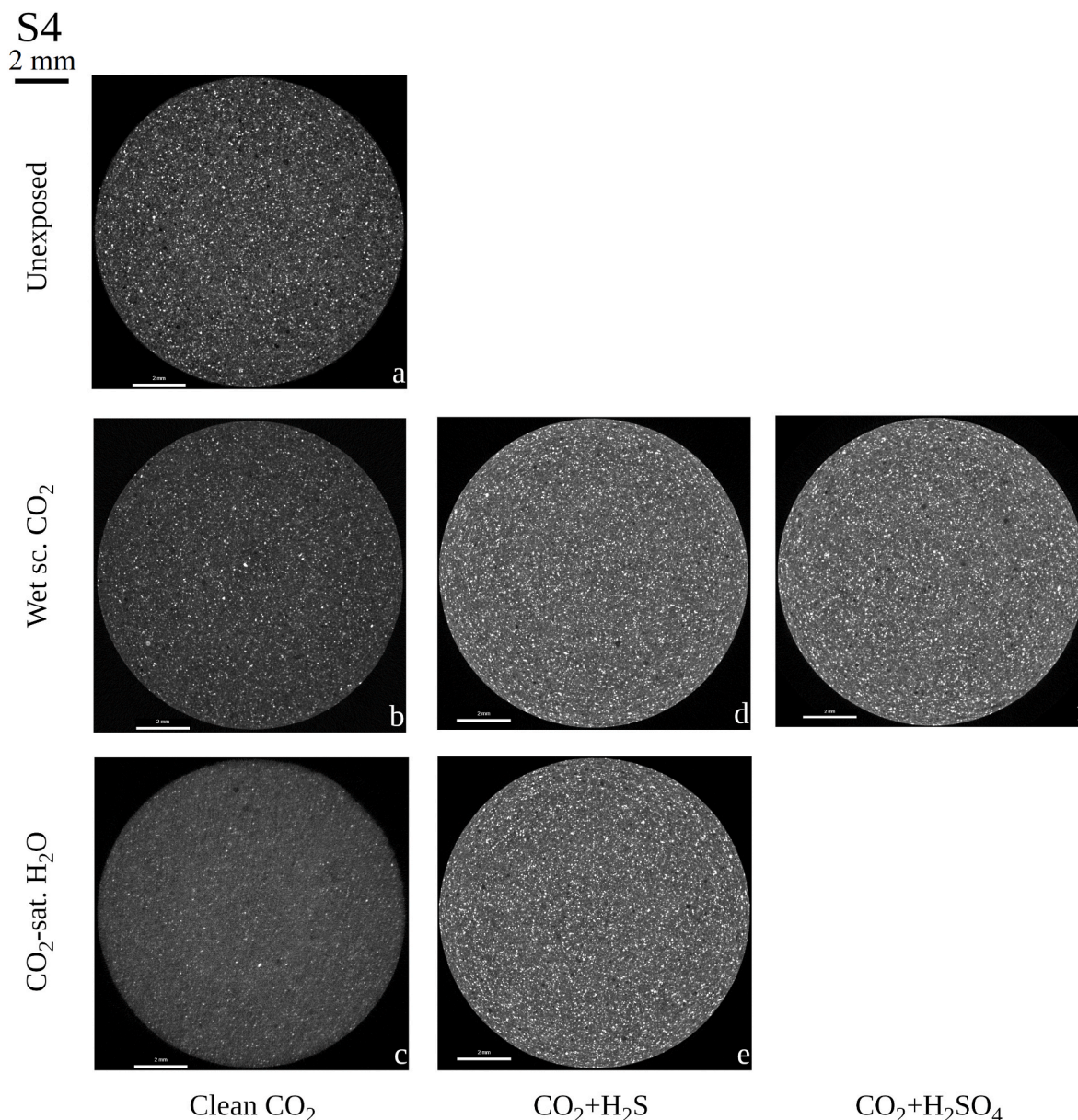
Based on testing with phenolphthalein on the samples exposed to clean  $\text{CO}_2$ , free  $\text{Ca}(\text{OH})_2$  in all tested samples was fully carbonated after only 4 weeks exposure (see also (van Noort et al., 2025)). However, more significant impacts leading to chemical and microstructural alteration and degradation were observed using CT scans (density changes) and SEM/EDS investigation (microstructural changes and significant changes in chemical composition as tracked through elemental ratios). The observed extents of alteration and degradation are displayed in bar diagrams in Figs. 24 and 25.

### 4.2. Impact of $\text{H}_2\text{S}$ as impurity in $\text{CO}_2$

While low contents of  $\text{H}_2\text{S}$  in (e.g.,)  $\text{N}_2$  are known to impact cement-based sealants quite strongly (cf. (Todorovic et al., 2023)), when exposing sealants to  $\text{CO}_2$ -saturated water containing  $\text{H}_2\text{S}$  ( $\sim 0.087\ \text{mol}\%$ ), the overall changes in sealant microstructure and composition are dominated by the impact of  $\text{CO}_2$ . The most notable impact of  $\text{H}_2\text{S}$  in the experiments reported here was the difference in exposed sample colours, with the presence of  $\text{H}_2\text{S}$  leading to dark blueish colours, whereas exposure to clean  $\text{CO}_2$  resulted in more brownish sample colours. Brownish colourations are known to be due to the formation of various (hydr)oxides of (in particular) iron.  $\text{H}_2\text{S}$  is known to react with iron and form black iron sulphides. The difference in exposed sample colours were interpreted as a result of differences in oxidation state during exposure, and the formation of Fe-sulphides and other phases when  $\text{H}_2\text{S}$  was present.

In addition, in sealant S1, the impact of exposure to  $\text{CO}_2$ -saturated water was enhanced with the addition of  $\text{H}_2\text{S}$ , as seen in the loss of





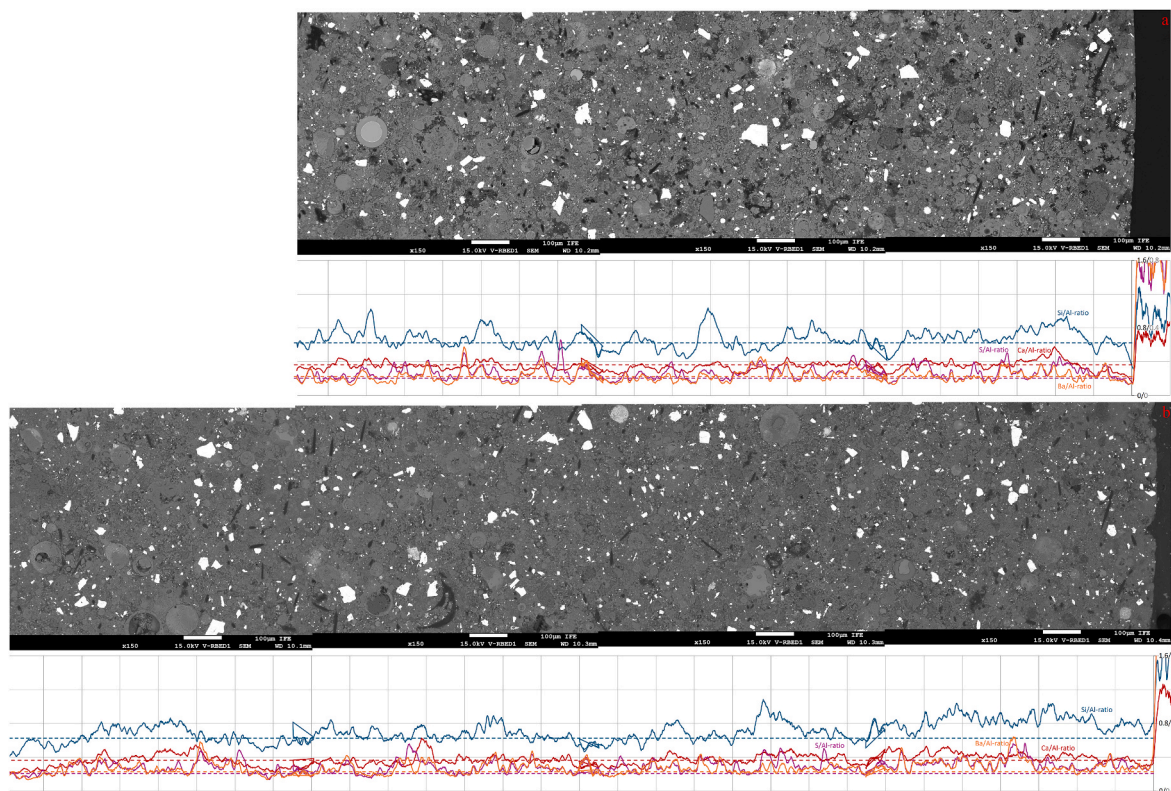
**Fig. 16.** CT-scans of sealant S4; a) unexposed, b) exposed to wet supercritical  $\text{CO}_2$ , c) exposed to  $\text{CO}_2$ -saturated water, d) exposed to wet supercritical  $\text{CO}_2$  with 1.6 mol%  $\text{H}_2\text{S}$ , e) exposed to  $\text{CO}_2$ -saturated water with  $\text{H}_2\text{S}$ , and f) exposed to supercritical  $\text{CO}_2$  equilibrated with concentrated  $\text{H}_2\text{SO}_4$ . The scalebars shown with the scans are 2 mm. All exposure durations were 16 weeks. CT scans of the unexposed reference sample and samples exposed to clean  $\text{CO}_2$  taken from (van Noort et al., 2025).

sample mass after 16 weeks. This corresponds with increased Ca and Si in solution at the end of the experiment, while with clean  $\text{CO}_2$ , Ca and Si contents remained constant after 8 weeks, suggesting equilibrium values were maintained. Microstructurally and compositionally, after 16 weeks of exposure, the added impact of  $\text{H}_2\text{S}$  is reflected in a  $\sim 1.5$  times deeper affected zone where Ca/Si-ratios are depleted more strongly in the presence of  $\text{H}_2\text{S}$  compared to clean  $\text{CO}_2$ , as seen in both SEM-micrographs and CT-scans.

In sealant S2, the presence of  $\text{H}_2\text{S}$  caused a minor increase in sample mass compared to samples exposed to water saturated with clean  $\text{CO}_2$ , as well as in fluid Mg-contents (and Na-contents) that are significantly higher. While the microstructural and compositional changes in samples exposed with and without  $\text{H}_2\text{S}$  are similar, based on CT-scanning and SEM analyses, alteration caused by exposure penetrated deeper with  $\text{H}_2\text{S}$  than without  $\text{H}_2\text{S}$  (2100–2200  $\mu\text{m}$  vs. 1800–1900  $\mu\text{m}$  after 16 weeks).

In sealant S3, whereas the sample mass decreased between 8 and 16

weeks exposure times with clean  $\text{CO}_2$ , it remained relatively constant between 4 and 16 weeks exposure time in the presence of  $\text{H}_2\text{S}$ . Furthermore, fluid Mg-contents after 16 weeks of exposure were much higher in the presence of  $\text{H}_2\text{S}$ , while they remained relatively constant between 4 and 16 weeks without  $\text{H}_2\text{S}$ . Microstructurally, CT-scans show that the presence of  $\text{H}_2\text{S}$  resulted in precipitation and densification in the outer  $\sim 265 \mu\text{m}$  of the sample, as well as some leaching (and reduction of density) just ahead of that enhanced carbonation front. SEM images show that the presence of  $\text{H}_2\text{S}$  resulted in a wider outer zone of degradation and (Ca-)depletion ( $\sim 100$  vs  $\sim 50 \mu\text{m}$ ), but also show the higher density of the alteration zone. The total depth of penetration of alteration effects with  $\text{H}_2\text{S}$  was  $\sim 1200 \mu\text{m}$ , while this was estimated to be  $\sim 1400 \mu\text{m}$  for water saturated for clean  $\text{CO}_2$ . However, it should be noted that as the impact is relatively minor, and the transition is gradual, the exact depth of alteration penetration is hard to assess. Variations in the Ca/Si-ratios mapped using EDS do not show clear differences with or



**Fig. 17.** SEM Micrographs of S4 samples exposed to water saturated with CO<sub>2</sub> containing 1.6 mol% H<sub>2</sub>S for 4 (a) and 16 (b) weeks. The graphs underneath each micrograph show the Si/Al and Ca/Al (blue and red, respectively, both on the 0–1.6 axis), and Ba/Al and S/Al (orange and purple, respectively, both on the 0–0.8 axis) elemental ratios (atom %/atom %) measured along the micrograph using EDS. The dashed lines are reference values (average values) measured at the centre of an unexposed sample. Scalebars shown with the micrographs and gridline spacing for the graphs are 100 μm.

without H<sub>2</sub>S.

In sealant S4, exposure to CO<sub>2</sub>-saturated water in the presence of H<sub>2</sub>S did not affect how CO<sub>2</sub>-exposure impacted the sealants in terms of chemical, microstructural, or mass changes. In sealant S5, the presence of H<sub>2</sub>S lead to an increase in the depth to which the sample was (somewhat) degraded, from ~200 to ~400 μm after 16 weeks. While exposure to water saturated with clean CO<sub>2</sub> and water saturated with CO<sub>2</sub> with H<sub>2</sub>S both lead to a depletion of the Ca/Si-ratio deep into the sample, this was not associated with any visible impacts on sealant microstructure or integrity.

Compared to exposure to water saturated with clean CO<sub>2</sub>, the most significant impact of H<sub>2</sub>S is to somewhat enhance the changes induced by CO<sub>2</sub>, and in particular the penetration depth of these effects in sealant samples based on PC. In sealants where the impact of exposure to CO<sub>2</sub>-saturated water was limited or negligible (S4 and S5), a 1.6 mol% H<sub>2</sub>S-content in the CO<sub>2</sub>-phase also has negligible to limited additional impact on sealant microstructure.

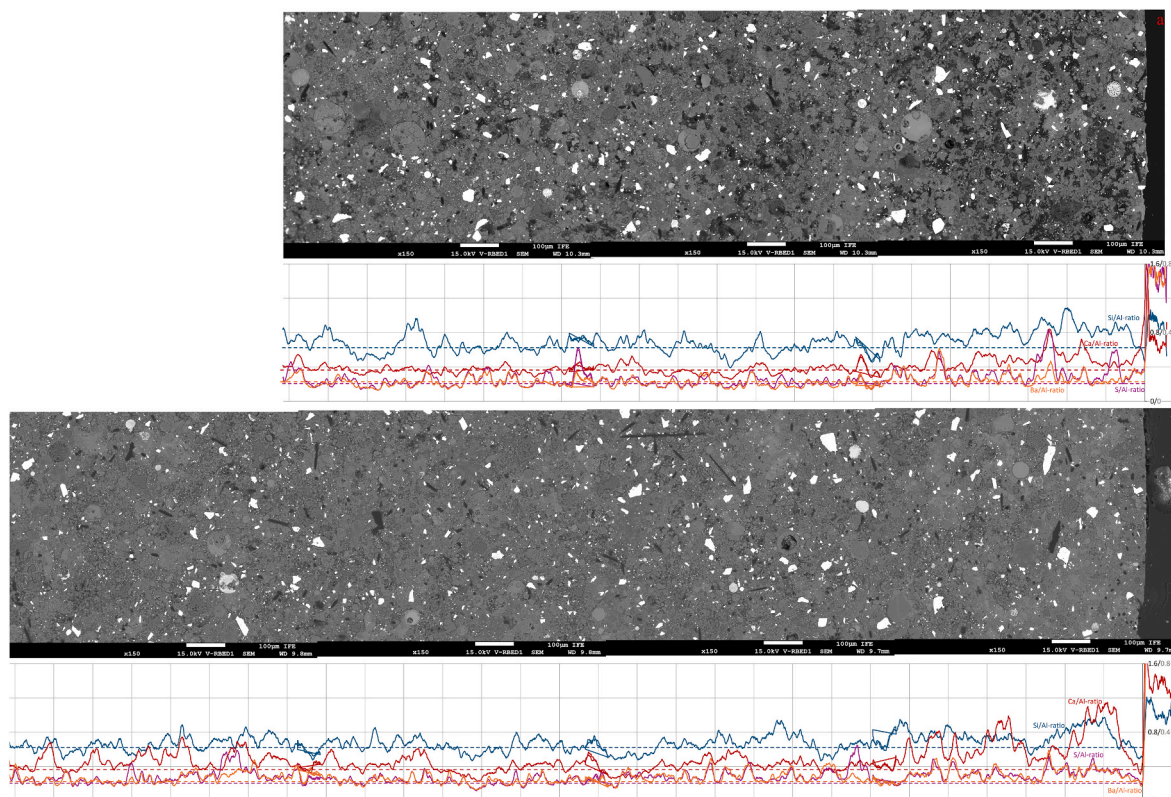
While chemical composition measurements of the hydrous exposure fluid were mostly consistent between exposures to clean CO<sub>2</sub> and exposures to CO<sub>2</sub> with H<sub>2</sub>S, some interesting differences were observed. Most notable are the significantly elevated concentrations of Mg for S1, S2 and S3, as well as elevated concentrations of Si and Ca for S1. For clean CO<sub>2</sub>, fluid concentrations of these elements were constant between 8 and 16 weeks, suggesting an equilibrium between precipitation and dissolution was attained. Thus, the significantly higher concentrations of these elements after 16 weeks exposure with H<sub>2</sub>S implies that the presence of H<sub>2</sub>S caused a shift in this equilibrium, by inhibiting precipitation of these elements as carbonates (and silica) or enhancing subsequent dissolution of precipitates. For S1, this is indeed confirmed through the lower Ca/Si-ratios in the samples exposed to CO<sub>2</sub> with H<sub>2</sub>S, as well as the much less prevalent carbonate precipitation seen in both CT-scans and SEM micrographs. As Mg-carbonates (or other Mg-bearing

precipitate phases) were not observed directly, an inhibition of Mg-bearing minerals cannot be confirmed directly. As the reaction between H<sub>2</sub>S and (dissolved) Fe<sup>2+</sup> to form pyrite can generate H<sup>+</sup> (cf. (Talman, 2015)), the resulting acidification is a potential mechanism by which H<sub>2</sub>S could lead to reduced carbonate precipitation.

In addition, ICP-OES analyses showed higher S-contents in the exposure fluids of S1, S2 and S3 after exposure to CO<sub>2</sub> with H<sub>2</sub>S compared to clean CO<sub>2</sub>. However, the S-concentrations in all exposure fluids were considerably lower than the calculated equilibrium concentration, suggesting that sulphur was removed from the fluid through interaction with the sealant samples. While in samples of S1, S2, and S3 exposed to CO<sub>2</sub> with H<sub>2</sub>S, Fe-sulphide particles were identified, no newly-formed S-binding minerals were identified in sealants S4 and S5 in this study.

In sealant samples exposed directly to wet supercritical CO<sub>2</sub>, for most compositions tested, the presence of H<sub>2</sub>S only had a limited impact on how the samples were affected, as assessed through mass changes, microstructural observations, and chemical mapping using EDS. CT-scans show that in sealant S1, the presence of H<sub>2</sub>S caused the densification near the outer surface of the samples, ascribed to carbonate precipitation, to be more pronounced, but restricted to a narrower zone. To the contrary, in sealant S2 the presence of H<sub>2</sub>S resulted in a more distributed density alteration, with less intense precipitates distributed deeper into the sample. In both these sealants, the presence of H<sub>2</sub>S resulted in less enhanced carbonate precipitation (i.e., densification) in the outer parts of the exposed sample than observed after exposure to clean CO<sub>2</sub>. While for S1, alteration depths were somewhat enhanced in the presence of H<sub>2</sub>S (620 μm compared to 500 μm with clean CO<sub>2</sub>, after 16 weeks), for sealant S2, alteration depths when exposed to wet supercritical CO<sub>2</sub> containing H<sub>2</sub>S were lower (700 μm compared to 1020 μm with clean CO<sub>2</sub>, after 16 weeks). In sealant S4, the presence of H<sub>2</sub>S had no impact on the exposed samples. In sealant S5, CT-scans show that





**Fig. 18.** SEM Micrographs of S4 samples exposed to wet supercritical CO<sub>2</sub> with 1.6 mol% H<sub>2</sub>S for 4 (a) and 16 (b) weeks. The graphs underneath each micrograph show the Si/Al and Ca/Al (blue and red, respectively, both on the 0–1.6 axis), and Ba/Al and S/Al (orange and purple, respectively, both on the 0–0.8 axis) elemental ratios (atom %/atom %) measured along the micrograph using EDS. The dashed lines are reference values (average values) measured at the centre of an unexposed sample. Scalebars shown with the micrographs and gridline spacing for the graphs are 100 μm.

carbonate precipitation near the surface of the sample, observed as a local increase in density, is more enhanced in the presence of H<sub>2</sub>S. Based on SEM images, after exposure to clean CO<sub>2</sub>, precipitation is concentrated between ~70 and 400 μm from the sample surface, while in the presence of H<sub>2</sub>S, this is limited to a considerably narrower band between 100 and 250 μm from the surface. Based on chemical compositions, in particular depletion of the Ca/Si-ratio, S5 was altered to a greater depth in the presence of H<sub>2</sub>S than with clean CO<sub>2</sub> (1400 vs 960 μm).

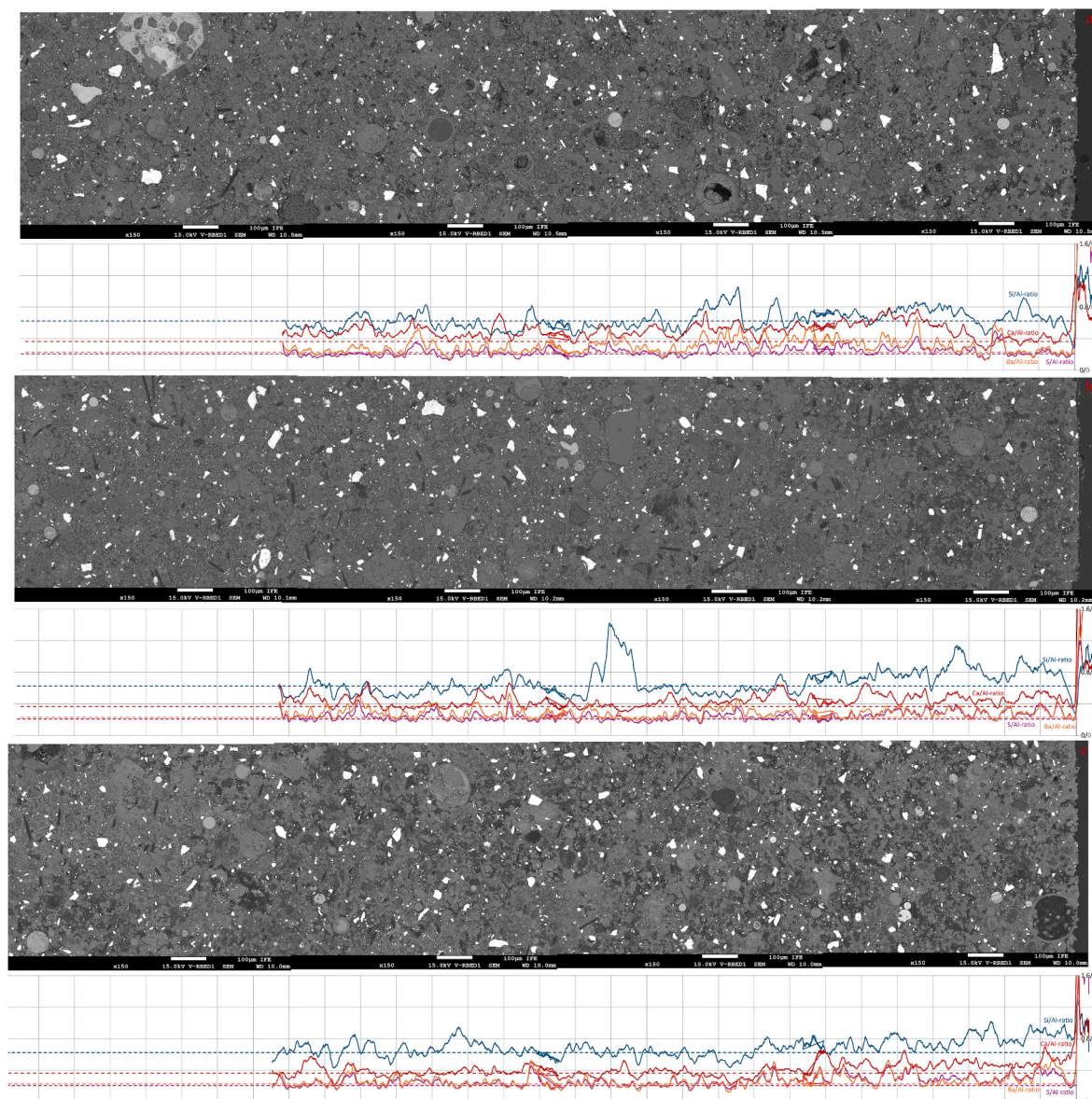
In sealant S3, the presence of H<sub>2</sub>S during exposure to wet supercritical CO<sub>2</sub> had a more complicated impact. In CT-scanning, the sample exposed to clean CO<sub>2</sub> showed a thin outer zone with enhanced carbonation, inwards of which a zone of reduced density was found giving the appearance of a carbonated outer shell detaching from the sample. Inwards from this, densities were enhanced again, and then dissipated towards the centre. In the sample exposed to CO<sub>2</sub> with H<sub>2</sub>S, the outer zone only shows increased density, which then dissipates inwards. While the SEM images of the sample exposed to clean CO<sub>2</sub> clearly show a decreased porosity due to precipitation between ~300 and 1200 μm from the surface, associated with an increasing Ca/Si-ratio, in the sample exposed to CO<sub>2</sub> with H<sub>2</sub>S, reduced porosities due to precipitation are only observed between ~50 and 200 μm. Ca/Si-ratios show similar depleted trends in both samples. Overall, the observed alteration depth in the presence of H<sub>2</sub>S (after 16 weeks) was lower than for clean CO<sub>2</sub> (700 vs. 1320 μm).

In all PC-based sealants (S1–S3), the S/Si-ratio was elevated throughout the sample, indicating full penetration of S-bearing fluids, for both exposure to CO<sub>2</sub>-saturated water and exposure to wet supercritical CO<sub>2</sub>. For the S2 and S3 samples, the elevated S/Si-ratios did not depend on exposure duration (4 vs. 16 weeks) or exposure conditions (i. e., whether they were exposed to wet supercritical CO<sub>2</sub> or CO<sub>2</sub>-saturated water). However, in the S1 samples exposed to wet supercritical CO<sub>2</sub>,

while the S/Si-ratios are elevated throughout (and to similar values for the 4- and 16-week exposures), the S/Si-ratios are even higher in the outer 100–150 μm (4-week) to 400 μm (16-week). In the S1-sample exposed to CO<sub>2</sub>-saturated water for 16 weeks, S/Si-ratios are likewise elevated throughout. However, they are less elevated in the depleted zone where Ca/Si-ratios are also depleted, and then rise further inwards of this zone (from ~2700 μm from the surface). In the sample exposed for 4 weeks, the S/Si-ratios are similarly less elevated in the depleted outer ~500 μm, and less elevated throughout than in the sample exposed for 16 weeks. Furthermore, in the S1 samples tested, the S/Si-ratios are most elevated in the sample exposed to CO<sub>2</sub>-saturated water, but the S/Si-ratios in the depleted zone of these samples are lower than the ratios measured in the samples exposed to wet supercritical CO<sub>2</sub>.

In sealant S5, exposure to wet supercritical CO<sub>2</sub> with H<sub>2</sub>S led to elevated S/Si-ratios throughout the samples. In the S5 sample exposed for 4 weeks, the S/Si-ratio is independent of distance from the contact surface, while in the sample exposed for 16 weeks, the S/Si-ratio is somewhat further elevated in the outer ~200 μm. After exposure to CO<sub>2</sub>-saturated water with H<sub>2</sub>S, S/Si-ratios were elevated in the outer ~80 μm (4-week exposure) to 200 μm (16-week exposure), decreasing inwards to the reference value (or just below that). Then, S/Si-ratios were elevated again from 600 to 700 μm (4-week exposure) or 900–1100 μm (16-week exposure) from the surface. Comparing exposure to CO<sub>2</sub>-saturated water to wet supercritical CO<sub>2</sub>, the S/Si-ratios after 16 weeks were somewhat higher in the outer ~1000 μm of the sample exposed to wet supercritical CO<sub>2</sub>, while further inwards the S/Si-ratios were similar. Minor increases in the S/Al-ratio were also observed for S4 sealants exposed to CO<sub>2</sub> with H<sub>2</sub>S, mostly in the outer 700–1000 μm of these samples.

These measurements show that sulphur penetrated quite deeply into most sealants. For the PC- based sealants (S1–S3), submicron high-



**Fig. 19.** SEM Micrographs of S4 samples exposed to wet supercritical  $\text{CO}_2$  equilibrated with concentrated  $\text{H}_2\text{SO}_4$  for 4 (a), 8 (b), and 16 (c) weeks. The graphs underneath each micrograph show the Si/Al and Ca/Al (blue and red, respectively, both on the 0–1.6 axis), and Ba/Al and S/Al (orange and purple, respectively, both on the 0–0.8 axis) elemental ratios (atom %/atom %) measured along the micrograph using EDS. The dashed lines are reference values (average values) measured at the centre of an unexposed sample. Scalebars shown with the micrographs and gridline spacing for the graphs are 100  $\mu\text{m}$ .

density particles were observed in the exposed samples using SEM. Based on EDS-analysis of such particles in the S1 sample exposed to  $\text{CO}_2$ -saturated water with  $\text{H}_2\text{S}$  for 16 weeks, at least part of the sulphur penetrating these samples precipitated as Fe-sulphides. More detailed SEM studies, combined with XRD analysis could be used to assert whether other sulphide minerals also formed.

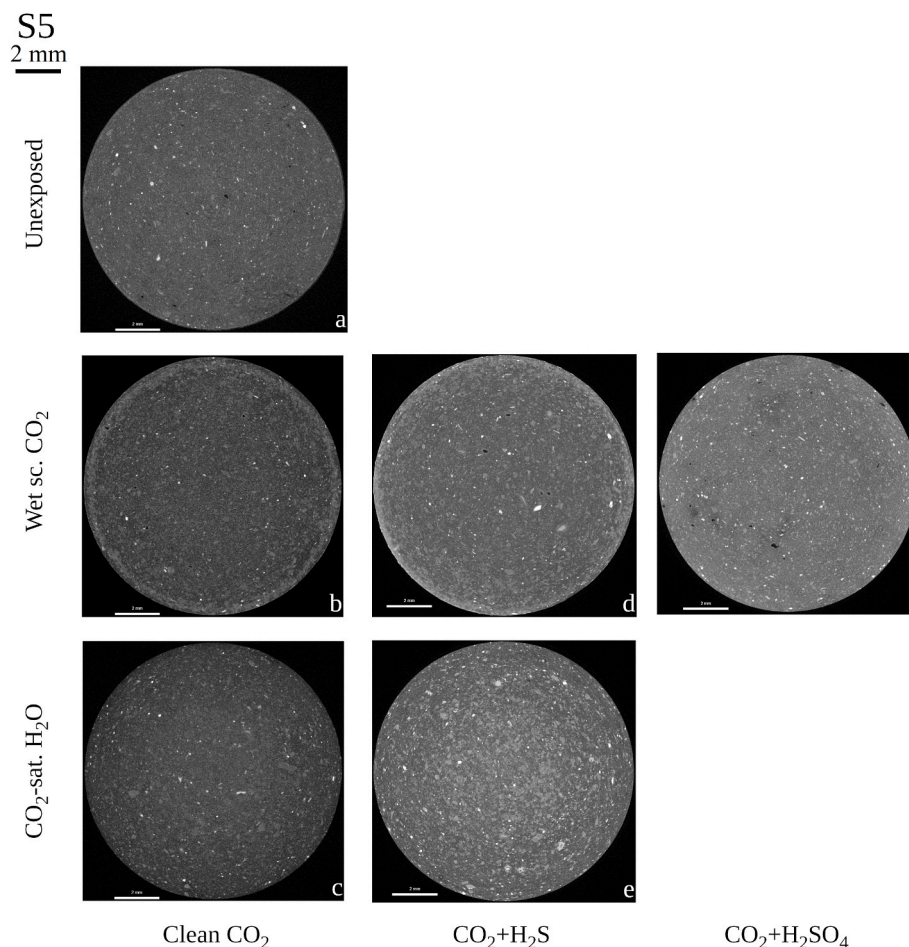
(van Noort et al., 2025) derived and reported extrapolations of the depths to which their samples were affected after exposure to clean  $\text{CO}_2$ . While the data obtained here for exposure to  $\text{CO}_2$  with 1.6 mol%  $\text{H}_2\text{S}$  is insufficient to attempt a similar extrapolation, comparison to the samples exposed by Van Noort et al. shows that in general the samples exposed to  $\text{CO}_2$  with  $\text{H}_2\text{S}$  are affected to similar depths (between about 0.5 and 2 times) as those of equivalent samples exposed to clean  $\text{CO}_2$ . Based on the available data, estimated extrapolations to 30 years fall within one order of magnitude from the given extrapolations for clean  $\text{CO}_2$ . However, it must be kept in mind that these extrapolations to 30 years exposure based on single exposure experiments with a total duration of 16 weeks carry very large uncertainties.

#### 4.3. Impact of $\text{H}_2\text{SO}_4$ as impurity in $\text{CO}_2$

$\text{SO}_x$  has been identified as a key impurity with potential high reactivity with reservoir minerals, reservoir fluids and wellbore cements when co-injected with  $\text{CO}_2$ .  $\text{SO}_x$  can react with water and other impurities to form  $\text{H}_2\text{SO}_4$  (Morland et al., 2019a,b), which is a strong acid. As  $\text{H}_2\text{SO}_4$  partitions into the hydrous phase, this can cause strong acidification of the hydrous fluids near the injection point, including in the pore fluids trapped in exposed sealants.

To simulate the presence of relatively large quantities of  $\text{H}_2\text{SO}_4$  at a low concentration in the  $\text{CO}_2$ -phase, wet sealant samples were exposed to supercritical  $\text{CO}_2$  in the presence of vials of concentrated sulphuric acid. Unfortunately, while this enabled simulation of exposure under realistic conditions, the saturated solutions of  $\text{H}_2\text{SO}_4$  also acted as drying agents, removing water from the initially water-saturated sealant samples. Based on drying tests, the sealants had water-contents of 21–25 wt. %. Comparing sample mass changes for the  $\text{H}_2\text{SO}_4$ -exposed samples to samples exposed to wet supercritical  $\text{CO}_2$  (without  $\text{H}_2\text{S}$ ), indicates





**Fig. 20.** CT-scans of sealant S5; a) unexposed, b) exposed to wet supercritical  $\text{CO}_2$ , c) exposed to  $\text{CO}_2$ -saturated, d) exposed to wet supercritical  $\text{CO}_2$  with 1.6 mol%  $\text{H}_2\text{S}$ , e) exposed to  $\text{CO}_2$ -saturated water with  $\text{H}_2\text{S}$ , and f) exposed to supercritical  $\text{CO}_2$  equilibrated with concentrated  $\text{H}_2\text{SO}_4$ . The scalebars shown with the scans are 2 mm. All exposure durations were 16 weeks. CT scans of the unexposed reference sample and samples exposed to clean  $\text{CO}_2$  taken from (van Noort et al., 2025).

exposed samples masses after 16 weeks that are 8–18 % lower (see Table 4). Under the assumption that the increase in mass due to carbonation for these samples is similar, this would indicate that during the  $\text{H}_2\text{SO}_4$ -exposure tests, the exposed samples did not dry out completely (though for S4 the remaining water content would be very low).

As sample mass change in these samples is a combination of the precipitation of carbonates (and sulphates) leading to an increase in mass, as well as the evaporation of pore water leading to a decrease in mass, a relatively small reduction in sample mass compared to the measured water content can also indicate a larger decrease due to dehydration compensated by a larger increase due to precipitation. However, considering the CT-scans and SEM images presented above, there are no indications that the presence of  $\text{H}_2\text{SO}_4$  led to such a significant enhancement in carbonation compared to clean  $\text{CO}_2$ . Note that for sealants S4 and S5, exposure to clean, wet supercritical  $\text{CO}_2$  did not lead to any significant changes in sample mass, meaning that the changes in sample mass observed in the samples exposed with  $\text{H}_2\text{SO}_4$  mostly represent dehydration. Furthermore, note that sample dehydration also explains the observed “bleaching” of the outer surfaces of these samples after exposure, while drying induced shrinkage could explain the brittle behaviour of S1 and S2 samples during cross-sectioning.

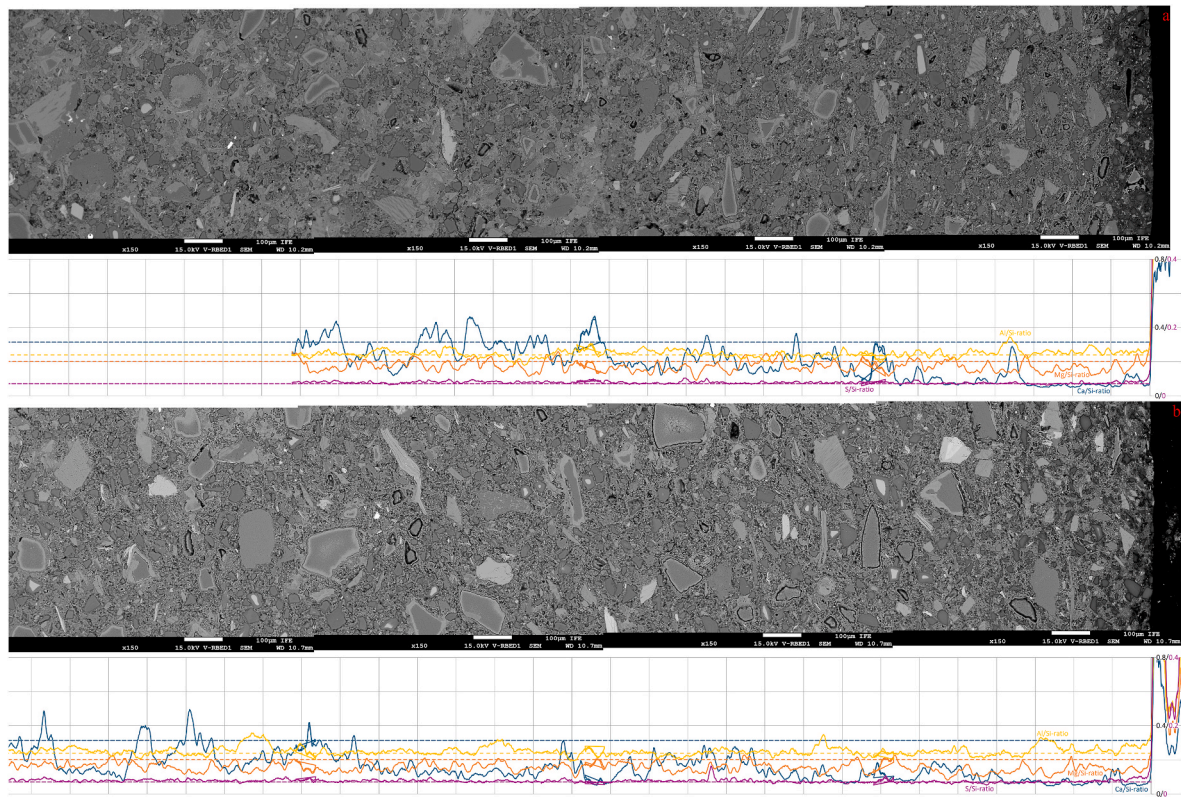
CT-scanning of the S1 sample exposed for 16 weeks shows a more diffuse, less intense densification of the outer part of this sample compared to S1 samples exposed to clean  $\text{CO}_2$  or  $\text{CO}_2$  with  $\text{H}_2\text{S}$ . Furthermore, the scan shows some inhomogeneity in density in the outer  $\sim 100 \mu\text{m}$ . SEM imaging of the S1 sample exposed to  $\text{CO}_2$  with  $\text{H}_2\text{SO}_4$

(for 16 weeks) shows minor degradation in the outer  $\sim 150 \mu\text{m}$  of this sample. Such degradation was not observed in the S1 samples exposed to clean wet supercritical  $\text{CO}_2$  or  $\text{CO}_2$  with  $\text{H}_2\text{S}$  for 16 weeks, though it was observed in S1 samples exposed to clean  $\text{CO}_2$  or  $\text{CO}_2$  with  $\text{H}_2\text{S}$  for 4 or 8 weeks. The degradation (increased porosity) is associated with a depleted Ca/Si-ratio in the outer 80–100  $\mu\text{m}$  of this sample. The same is observed for the S2 sample exposed to  $\text{CO}_2$  with  $\text{H}_2\text{SO}_4$ , where CT-scanning shows more diffuse densification, while SEM observations show minor degradation in the outer 100–150  $\mu\text{m}$ , associated with a minor decrease in the Ca/Si-ratio in the outer 50  $\mu\text{m}$ , and reduced porosity due to enhanced carbonation up to  $\sim 800 \mu\text{m}$  into the sample, deeper than observed in the samples exposed to clean  $\text{CO}_2$ , or  $\text{CO}_2$  with  $\text{H}_2\text{S}$ . In sealant S3, exposure to  $\text{CO}_2$  with  $\text{H}_2\text{SO}_4$  likewise resulted in more diffuse, deeper-reaching carbonation than exposure to clean  $\text{CO}_2$  or  $\text{CO}_2$  with  $\text{H}_2\text{S}$ .

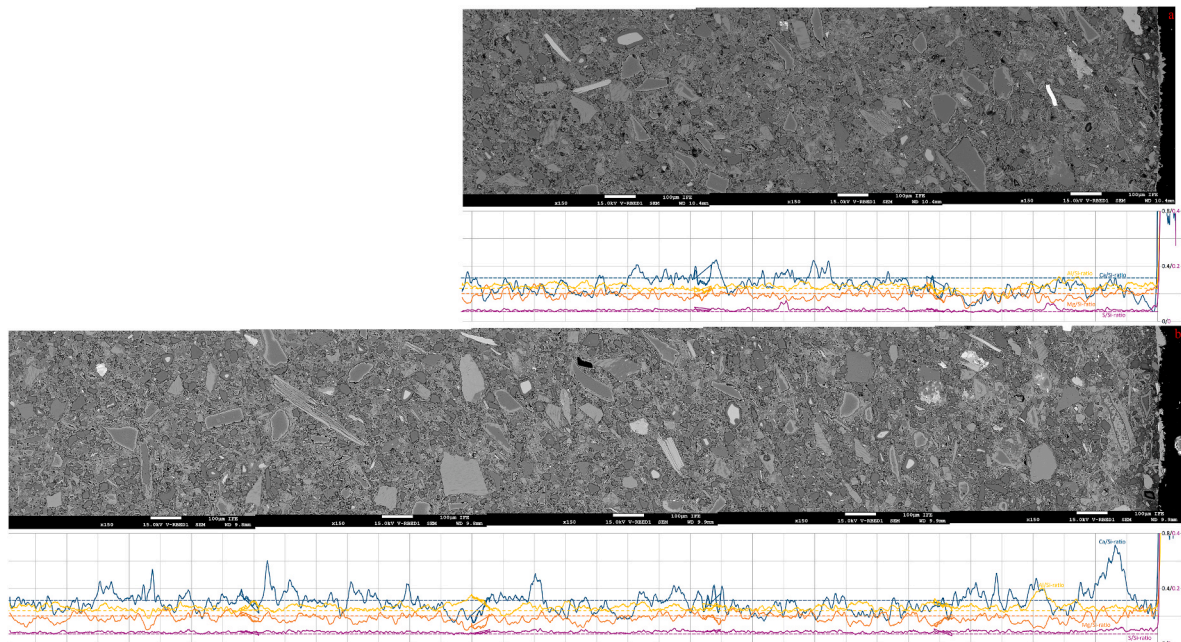
A potential explanation for the lack of carbonate precipitation in the outer part of the S1 and S2 samples exposed to  $\text{CO}_2$  with  $\text{H}_2\text{SO}_4$  is that in these samples, drying out prevented the dissolution-precipitation reactions necessary for carbonation to take place. This drying out would then lead to deeper penetration of  $\text{CO}_2$  through the dried pore network before  $\text{CO}_2$ -dissolution into pore fluids remaining deeper within the samples would lead to carbonate precipitation there, which would explain the deeper and more diffuse carbonation observed in these three samples. An alternative explanation for the reduction in carbonate precipitation observed in these samples is that this was inhibited as a result of acidification caused by the  $\text{H}_2\text{SO}_4$ .

In sealant S5, CT-scanning shows that the sample exposed to  $\text{CO}_2$



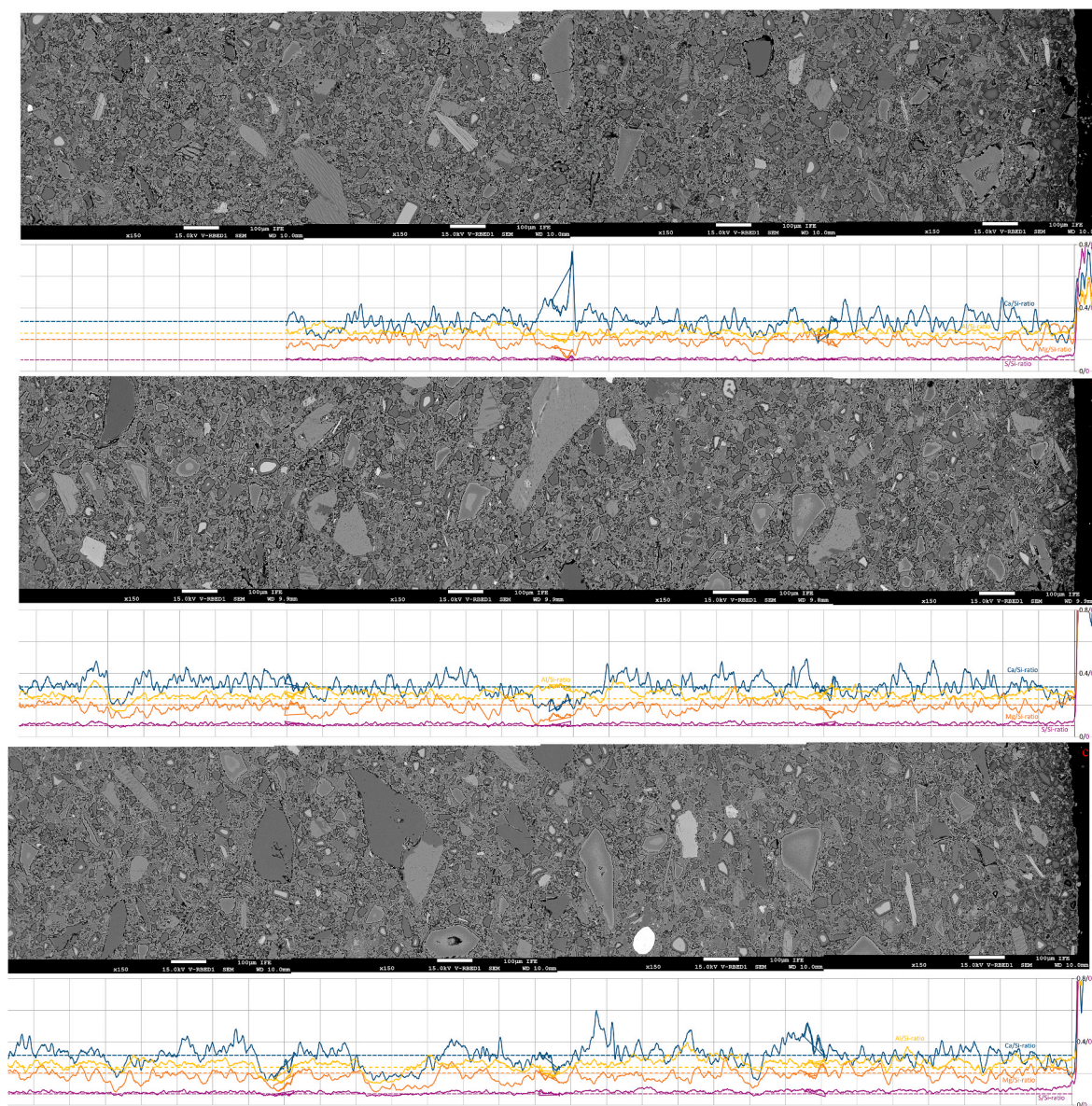


**Fig. 21.** SEM Micrographs of S5 samples exposed to water saturated with  $\text{CO}_2$  containing 1.6 mol%  $\text{H}_2\text{S}$  for 4 (a) and 16 (b) weeks. The graphs underneath each micrograph show the Ca/Si, Mg/Si and Al/Si (blue, orange and yellow, respectively, all on the 0–0.8 axis), and S/Si (purple, on the 0–0.4 axis) elemental ratios (atom %/atom %) measured along the micrograph using EDS. The dashed lines are reference values (average values) measured at the centre of an unexposed sample. Scalebars shown with the micrographs and gridline spacing for the graphs are 100  $\mu\text{m}$ .



**Fig. 22.** SEM Micrographs of S5 samples exposed to wet supercritical  $\text{CO}_2$  with 1.6 mol%  $\text{H}_2\text{S}$  for 4 (a) and 16 (b) weeks. The graphs underneath each micrograph show the Ca/Si, Mg/Si and Al/Si (blue, orange and yellow, respectively, all on the 0–0.8 axis), and S/Si (purple, on the 0–0.4 axis) elemental ratios (atom %/atom %) measured along the micrograph using EDS. The dashed lines are reference values (average values) measured at the centre of an unexposed sample. Scalebars shown with the micrographs and gridline spacing for the graphs are 100  $\mu\text{m}$ .





**Fig. 23.** SEM Micrographs of S5 samples exposed to wet supercritical  $\text{CO}_2$  equilibrated with concentrated  $\text{H}_2\text{SO}_4$  for 4 (a), 8 (b), and 16 (c) weeks. The graphs underneath each micrograph show the Ca/Si, Mg/Si and Al/Si (blue, orange and yellow, respectively, all on the 0–0.8 axis), and S/Si (purple, on the 0–0.4 axis) elemental ratios (atom %/atom %) measured along the micrograph using EDS. The dashed lines are reference values (average values) measured at the centre of an unexposed sample. Scalebars shown with the micrographs and gridline spacing for the graphs are 100  $\mu\text{m}$ .

with  $\text{H}_2\text{SO}_4$  was less altered near the sample surface. Whereas exposure to clean  $\text{CO}_2$  or  $\text{CO}_2$  with  $\text{H}_2\text{S}$  lead to densification due to enhanced carbonate precipitation in clearly delimited, relatively narrow outer zones, the sample exposed with  $\text{H}_2\text{SO}_4$  only shows a feint, diffuse densification, similar to the S1–S3 samples exposed to  $\text{CO}_2$  with  $\text{H}_2\text{SO}_4$ . SEM observations indicate some degradation at the sample surface, resulting in a reduction in matrix density and minor decrease in Ca/Si-ratio, but otherwise support the observed diffuse carbonation. While, based on sample mass changes, the S5 sample did not dry out during exposure, drying out of the outer shell can explain the relative lack of carbonation there, as well as more diffuse carbonation inwards. However, as for the PC-based sealants, acidification due to the presence of  $\text{H}_2\text{SO}_4$  provides an alternative explanation for the lack of carbonate precipitation in the outer parts of these samples.

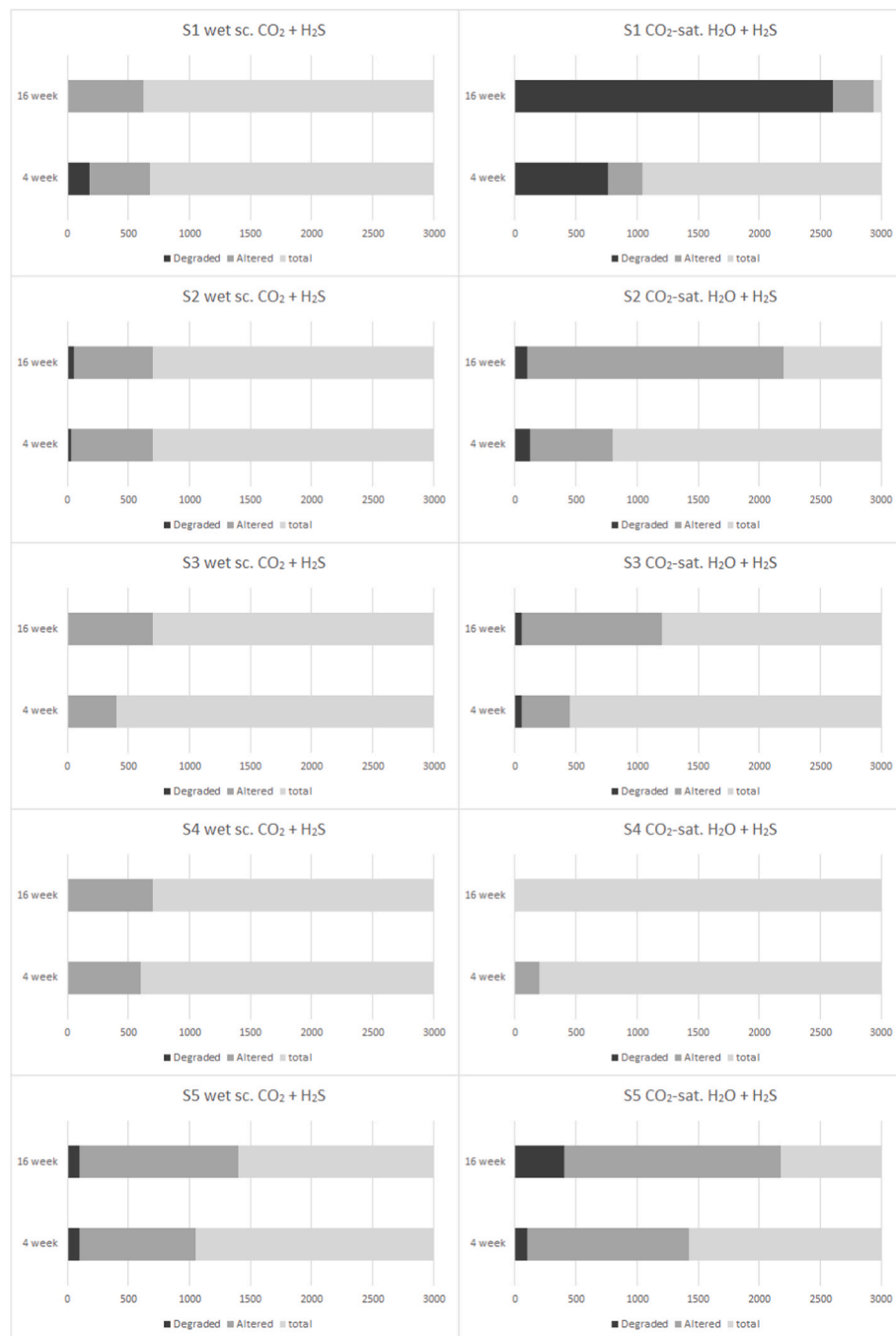
Finally, the negligible alterations induced by  $\text{CO}_2$ -exposure on S4 were not impacted by the presence of  $\text{H}_2\text{SO}_4$ . The sample mass decrease measured after 16 weeks exposure is close to the total water content as

measured by drying a sample.

Considering the penetration of sulphate into the samples exposed to  $\text{CO}_2$  with  $\text{H}_2\text{SO}_4$ , S/Si-ratios (or S/Al-ratios) are somewhat elevated in all samples. In the PC-based sealants (S1–S3), S/Si-ratios are consistently elevated throughout all exposed samples, though less elevated than in the samples exposed to wet supercritical  $\text{CO}_2$  with  $\text{H}_2\text{S}$ . Furthermore, while in S1 the S/Si-ratio is elevated independently of distance to the surface, in S2 and S3, after 16 weeks exposure, it is somewhat more elevated in the outer 1300 and 2200  $\mu\text{m}$ , respectively.

In S5, the S/Si-ratio is elevated throughout the sample, though most notably so in the outer  $\sim 300$   $\mu\text{m}$ . These elevated S/Si-ratios are comparably elevated to those observed in the S5 samples exposed to wet supercritical  $\text{CO}_2$  with  $\text{H}_2\text{S}$ . Finally, while the presence of  $\text{H}_2\text{SO}_4$  had negligible impact on the  $\text{CO}_2$ -exposure of S4, the S/Al-ratios are somewhat elevated in the outer 700–1000  $\mu\text{m}$  of the exposed S4 samples, to comparable values as observed in the S4 samples exposed to wet supercritical  $\text{CO}_2$  with  $\text{H}_2\text{S}$ .





**Fig. 24.** Bar diagrams indicating the depths of degradation and the depth to which sealants were altered by exposure to CO<sub>2</sub> with H<sub>2</sub>S based on SEM micrographs, elemental ratios, and CT scanning. “Degraded” indicates the depth to which the material is visibly degraded after exposure to CO<sub>2</sub> with H<sub>2</sub>S, with elevated porosity, lowered mechanical competence, and (commonly) strongly altered chemical composition (e.g., Ca/Si-ratio). “Altered” indicates the depth from which the material appears unaltered, based on microstructure and assessed elemental ratios, though it should be noted that free Ca(OH)<sub>2</sub> in all samples was fully reacted already within 4 weeks exposure (see also (van Noort et al., 2025)).

#### 4.4. Comparative analysis of the impact of impurities

In this study, five different sealants were exposed to CO<sub>2</sub> containing either H<sub>2</sub>S or H<sub>2</sub>SO<sub>4</sub>, in the presence of water, at 80 °C and 10 MPa. For the former, samples were exposed to a water-saturated CO<sub>2</sub>-phase containing 1.6 mol% H<sub>2</sub>S, and a CO<sub>2</sub>-saturated aqueous phase in equilibrium with that CO<sub>2</sub>-phase, containing 0.087 mol% H<sub>2</sub>S. While the H<sub>2</sub>S concentration is much higher than what would be expected during GCS (cf. (NorthernLights, 2024)), it is well within the range found in existing reservoirs. For the latter, samples were exposed to a CO<sub>2</sub>-phase in

equilibrium with concentrated sulphuric acid, which could be considered a worst-case scenario for GCS. The impact of exposure was interpreted in terms of carbonation, alteration and degradation, and compared to previous experiments exposing the same five sealants to clean CO<sub>2</sub>, at the same temperature and pressure. While exposure to CO<sub>2</sub>-saturated water is commonly used to assess the resistance of sealants (or similar materials) to CO<sub>2</sub>, during GCS in aquifers or depleted hydrocarbon reservoirs, the injected CO<sub>2</sub> will displace any water around the injection well, meaning exposure to (wet) supercritical CO<sub>2</sub> will be more relevant to the sealants in this well. In addition, as most reactive

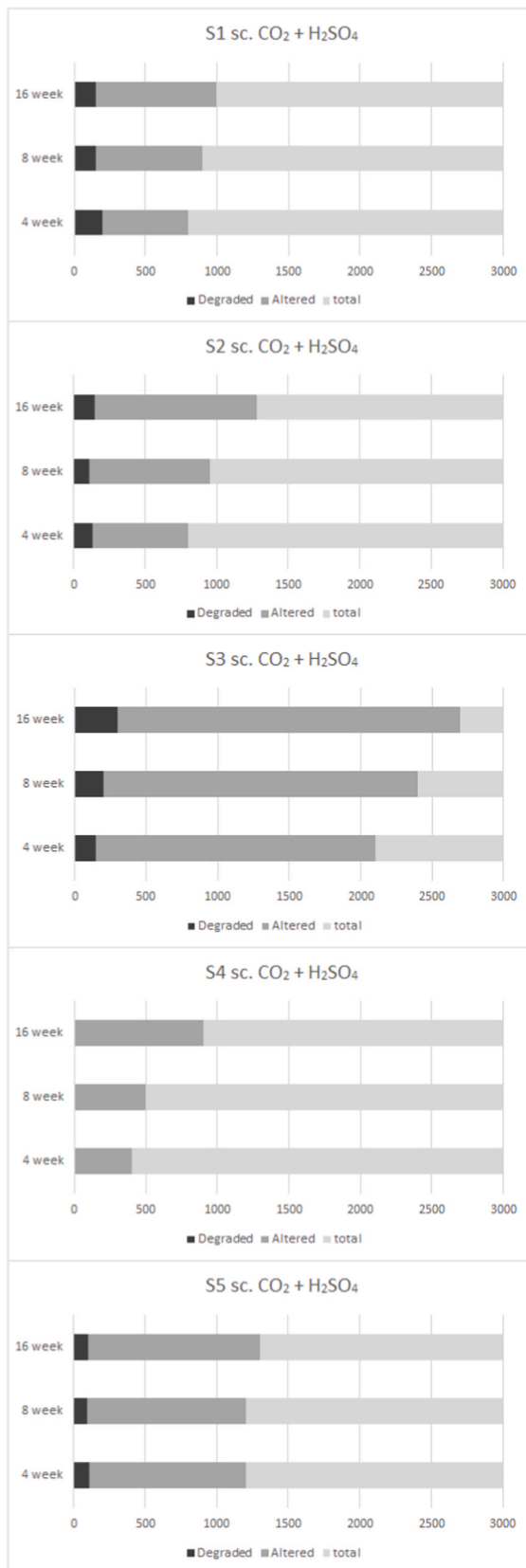


Fig. 25. Bar diagrams indicating the depths of degradation and the depth to which sealants were altered by exposure to  $\text{CO}_2$  with  $\text{H}_2\text{SO}_4$  based on SEM micrographs, elemental ratios, and CT scanning.

Table 4

Estimated sample water loss (as percentage of initial sample mass) after exposure to wet supercritical  $\text{CO}_2$  with  $\text{H}_2\text{SO}_4$ , compared to samples exposed to clean wet supercritical  $\text{CO}_2$ .

Sealant	Estimated water loss after 4 weeks (wt.%)	Estimated water loss after 8 weeks (wt.%)	Estimated water loss after 16 weeks (wt.%)
S1	8.8 %	10.2 %	8.4 %
S2	8.3 %	9.5 %	10.7 %
S3	13.6 %	13.6 %	15.2 %
S4	7.5 %	16.0 %	18.1 %
S5	10.2 %	10.5 %	13.7 %

impurities are expected to remain in the near-wellbore area due to their strong partitioning into the water phase (Bachu and Bennion, 2009; Talman, 2015; Wolf et al., 2017; Xu et al., 2007), wells further away from the injection point are unlikely to be exposed significantly to these impurities. Therefore, in the following comparison of the impact of impurities on sealant integrity, only direct exposure to a  $\text{CO}_2$ -phase will be considered. Furthermore, as in the analyses performed here, sealant S4 was not affected significantly by exposure to  $\text{CO}_2$ , with or without the tested impurities, this will also be left out of the following discussion.

Based on testing with phenolphthalein (van Noort et al., 2025), all PC-based samples (sealants S1-S3) were fully carbonated within 4 weeks. However, while this meant that all free  $\text{Ca}(\text{OH})_2$  had reacted to  $\text{CaCO}_3$ , the sealants were otherwise not strongly affected in terms of their overall chemical composition or microstructural integrity. These properties were affected by subsequent alteration and degradation reaction fronts penetrating more slowly into the exposed samples. In PC-based samples S1-S3, the full penetration of carbonation corresponded to S/Si-ratios that were elevated from edge to core for all exposure durations, and for both  $\text{H}_2\text{S}$  and  $\text{H}_2\text{SO}_4$ . While these S/Si-ratios were  $\sim 1.5$ – $2$  times higher after  $\text{H}_2\text{S}$ -exposure, the S-content in the  $\text{CO}_2$ -phase with  $\text{H}_2\text{S}$  was also several order of magnitude higher, which could easily account for this difference. Microstructurally, in S1, exposure to  $\text{H}_2\text{SO}_4$  led to a less dense microstructure in the outer zone compared to clean  $\text{CO}_2$  or  $\text{CO}_2$  with  $\text{H}_2\text{S}$ , due to a lower degree of carbonates precipitation. S2 shows similar trends, but in addition, from 100 to 150  $\mu\text{m}$  from the sample edge, the carbonates precipitated with  $\text{H}_2\text{SO}_4$  are much finer grained than for other exposure conditions, while in the outer 100–150  $\mu\text{m}$ , carbonates are more similar in grain size to those observed in samples exposed to clean  $\text{CO}_2$  or  $\text{CO}_2$  with  $\text{H}_2\text{S}$ . In sealant S3, the presence of  $\text{H}_2\text{SO}_4$  likewise resulted in the precipitation of finer-grained carbonates. Furthermore, as seen in the SEM images, in the PC-based sealants, exposure to  $\text{CO}_2$  with  $\text{H}_2\text{SO}_4$  led to degradation and reduced Ca/Si-ratios in an outer zone of up to 300  $\mu\text{m}$  wide (though typically in the range 100–200  $\mu\text{m}$ ), whereas during exposure to wet supercritical  $\text{CO}_2$  with  $\text{H}_2\text{S}$  degradation was only observed in some samples, and typically no deeper than  $\sim 50$   $\mu\text{m}$ . Likewise, for all three PC-based sealants, alteration depths were greater in the presence of  $\text{H}_2\text{SO}_4$  than with  $\text{H}_2\text{S}$  or clean  $\text{CO}_2$ .

The presence of  $\text{H}_2\text{S}$  or  $\text{H}_2\text{SO}_4$  during exposure to supercritical  $\text{CO}_2$  had similar impacts on S5 as on the PC-based samples. In the presence of  $\text{H}_2\text{S}$ , enhanced precipitation of carbonates was restricted to a narrow outer zone between  $\sim 100$  and  $\sim 250$   $\mu\text{m}$  from the sample surface. However, alteration (in particular a depletion of the Ca/Si-ratio) penetrated more deeply into the sample than with clean  $\text{CO}_2$  (1400 vs. 960  $\mu\text{m}$ ). On the other hand,  $\text{H}_2\text{SO}_4$  resulted in more disperse densification (due to enhanced carbonate precipitation), with densities being less elevated, but to greater depth – correlating with a more porous carbonate precipitate matrix observed in the SEM images. Alteration and degradation depths with  $\text{H}_2\text{S}$  and  $\text{H}_2\text{SO}_4$  were similar, and higher than with clean  $\text{CO}_2$ , though for most sealants tested the increases were limited.

Overall, the above comparison shows that, even though the  $\text{H}_2\text{SO}_4$  concentrations in the  $\text{CO}_2$ -phase were very low ( $0.091 \times 10^{-3}$  mol%), the presence of  $\text{H}_2\text{SO}_4$  had a clear impact on the microstructures of



exposed sealants, and was more deleterious overall than H<sub>2</sub>S (at much higher concentration). Most notably, the presence of H<sub>2</sub>SO<sub>4</sub> caused (minor) degradation at the surfaces of nearly all samples exposed (to a depth of ~100–200 µm), while such degradation was less common for exposure to wet supercritical CO<sub>2</sub> using either clean CO<sub>2</sub> or CO<sub>2</sub> with H<sub>2</sub>S.

Large differences in exposed sample colour were observed between samples exposed to CO<sub>2</sub> with H<sub>2</sub>S compared to samples exposed to clean CO<sub>2</sub> or CO<sub>2</sub> with H<sub>2</sub>SO<sub>4</sub>, where the former resulted in darker, blueish grey colours. This was ascribed to differences in oxidation state, and the formation of Fe-sulphides. XRD analysis should be included in a future study to confirm this interpretation, and to identify in what mineral species sulphur is bound within the sealants.

In this study, the impacts of only two impurities on sealant integrity were considered. The first impurity, H<sub>2</sub>S, was selected as this impurity is common in natural reservoirs, and expected to be common in captured CO<sub>2</sub> as well. The second impurity, SO<sub>x</sub>, added here in the form of H<sub>2</sub>SO<sub>4</sub>, was selected as this was identified as the impurity with the strongest potential impact on sealant integrity. Other key impurities that are expected to be reactive with typical sealant materials include NO<sub>x</sub> (when reacting to form HNO<sub>3</sub>), HCl and HF, which are all expected to cause acidification close to the injection point (cf. (Talman, 2015)), similar to SO<sub>x</sub>. As nitrate and chloride salts are typically highly soluble, no additional effects of these impurities are expected, though the presence of NO<sub>x</sub> could lead to oxidation, for example of ferrous iron to ferric iron. On the other hand, while HF is a weaker acid, the presence of F<sup>−</sup> can lead to enhanced dissolution of silica through the formation of silica-fluoride complexes, and to the precipitation of insoluble phases such as CaF<sub>2</sub>. As the enhanced dissolution of silica could lead to significant degradation, in projects where higher concentrations of HF may be expected, this potential impact should be studied experimentally.

#### 4.5. Implications for sealant integrity

For all sealants tested, exposure to a CO<sub>2</sub>-phase containing 1.6 mol% H<sub>2</sub>S or to CO<sub>2</sub> equilibrated with concentrated H<sub>2</sub>SO<sub>4</sub> did not change the main mechanisms by which CO<sub>2</sub>-exposure lead to carbonation, alteration and degradation. However, especially for sealants based on PC, these impurities did impact the degrees to which these samples were affected by the different reactions that take place when they are exposed to CO<sub>2</sub>, both in terms of depth and intensity.

Based on sample mass and fluid composition analyses, when sealants are exposed to CO<sub>2</sub>-saturated water, the presence of H<sub>2</sub>S can shift the balance between precipitation and dissolution of carbonates, leading to reduced overall carbonate precipitation. This was most apparent for the reference sealant, S1, which was also the most affected by clean CO<sub>2</sub>, and this was further supported by microstructural evidence showing less carbonate precipitation and increased leaching in the S1 samples exposed to CO<sub>2</sub>-saturated water with H<sub>2</sub>S. In addition, the presence of H<sub>2</sub>S, potentially as a consequence of the reduction in precipitated carbonates, increased the depth to which the sample was affected by about 1.5x. While in the other PC-based sealants, S2 and S3, higher concentrations of Mg were measured after 16 weeks of exposure to CO<sub>2</sub> with H<sub>2</sub>S, mass measurements indicate somewhat stronger increases in mass after exposure compared to clean CO<sub>2</sub> for both these samples, while microstructural observations indicate somewhat deeper (1.2x in the case of S2) alteration, or enhanced intensity of alteration but with reduced alteration depths (S3). While microstructural evidence suggests that exposure of sealant S5 to CO<sub>2</sub>-saturated water with H<sub>2</sub>S lead to somewhat enhanced degradation, this is not supported by differences in sample mass after exposure, or by fluid composition. Sealant S4, which was non-reactive with CO<sub>2</sub>, shows little impact of H<sub>2</sub>S as well. Based on chemical analyses (expressed as S/Si-ratios), H<sub>2</sub>S and CO<sub>2</sub> did fully penetrate the PC-based sealants (S1–S3), leading to the precipitation of submicron-sized particles of iron sulphide. In contrast, in sealant S4 elevated sulphur contents are mostly limited to the outer ~700 µm of

exposed samples. In S5, S/Si-ratios were elevated throughout the samples, but less so than in samples S1–S3. Specific sulphide precipitates were not identified in S4 or S5, and more detailed study to identify such phases, using, for example, higher resolution SEM imaging, or XRD analysis should be considered in future work. Overall, when the sealants tested here were exposed to CO<sub>2</sub>-saturated water at 80 °C and 10 MPa for up to 16 weeks, the presence of up to 1.6 mol% H<sub>2</sub>S resulted in a limited enhancement of the alteration and degradation of the exposed sealants.

Considering exposure to (wet) supercritical CO<sub>2</sub>, the impact of H<sub>2</sub>S is again dependent on the sealant composition, but overall minor. While exposure of S2 to supercritical CO<sub>2</sub> with H<sub>2</sub>S led to a somewhat smaller increase in mass, correlated with a more diffuse (deeper but less intense) densification zone in the CT-scans, other samples show no difference in mass change.

On the other hand, exposure to supercritical CO<sub>2</sub> with H<sub>2</sub>SO<sub>4</sub> did lead to large decreases in sample mass compared to samples exposed to clean supercritical CO<sub>2</sub>. However, this was ascribed to a drying out effect (experimental artefact), as water evaporated from the sealant samples to then be absorbed by the concentrated H<sub>2</sub>SO<sub>4</sub> solution. Considering microstructural changes, this effect is associated with a more diffuse but deeper penetration of the densification caused by carbonate precipitation, such that microstructures are affected to depths 1.3 to 2 times greater than with clean CO<sub>2</sub>. This deeper impact is interpreted as a result of the drying out of these samples rather than the presence of H<sub>2</sub>SO<sub>4</sub> itself, as CO<sub>2</sub> has a higher mobility through the dried-out pore network, and can also travel more deeply through this pore network before dissolving into a hydrous pore fluid (and then precipitating as carbonate). However, a potential inhibition of carbonate precipitation due to an acidification effect cannot be excluded. While elevated S/Si-ratios in these samples do indicate a deeper penetration of sulphur, specific sulphate minerals (or other sulphur-binding minerals) were not identified, and a more detailed analysis needs to be performed in future work. The observed degradation in the outer ~100–200 µm of all samples exposed to H<sub>2</sub>SO<sub>4</sub> (except S4) can be explained by the precipitation of droplets of highly acidic H<sub>2</sub>SO<sub>4</sub> solution on the outer surface of the exposed samples, where H<sub>2</sub>SO<sub>4</sub>-saturated CO<sub>2</sub> encountered either liquid water, or wet CO<sub>2</sub> from inside the pore network. As these droplets grew in size, they then rained down from the samples, removing dissolved components. A rain of acid containing solutes from the exposed cements would also explain the colour changes observed in some of the H<sub>2</sub>SO<sub>4</sub> vials placed underneath the samples. However, it cannot be fully excluded that sample degradation at the surface was caused by, for example, splashing with saturated H<sub>2</sub>SO<sub>4</sub> solution during experiment start-up.

The experiments reported here thus show that the presence of relatively low concentrations of H<sub>2</sub>S or H<sub>2</sub>SO<sub>4</sub> in CO<sub>2</sub> in general resulted in mostly minor enhancement of the alteration and degradation of these materials compared to clean CO<sub>2</sub>. One key impact of both impurities was a reduction in the quantity of precipitated carbonates in the outer parts of exposed samples. It should be noted that the H<sub>2</sub>S content used here was much higher than expected during normal GCS (NorthernLights, 2024), but well within the range expected for, for example, EOR/EGR in sour fields. However, the impacts observed were more pronounced on sealants that were also more affected by CO<sub>2</sub>. This suggests that these impacts are also more enhanced under exposure conditions where sealants are more strongly affected by CO<sub>2</sub>, such as under conditions where CO<sub>2</sub> leaks along a crack through a cement-based seal, or along an annular gap. Under such conditions, the presence of reactive impurities such as H<sub>2</sub>S or H<sub>2</sub>SO<sub>4</sub> may lead to a deeper and more intense alteration of the leakage pathway side-wall, which may exacerbate the leak. Inhibition of carbonate precipitation, such as was observed in the experiments reported here, may also limit self-sealing effects that would otherwise reduce the aperture and stop leakage.

While the impacts of impurities observed here were relatively limited, further research on the impact of impurities on wellbore sealant integrity when exposed to CO<sub>2</sub> is warranted. As the effect of impurities is correlated to sealant composition, studies on a wider range of sealant

compositions should map whether other sealants (for example with lower SiO<sub>2</sub>-content) are impacted more strongly. Likewise, the impact of other relatively reactive impurities, such as NO<sub>x</sub> or HF, as well as key combinations of impurities should be assessed in laboratory experiments. Temperature and pressure-dependencies should likewise be addressed. As impurities could have a more pronounced impact on the evolution of leakage pathways once a such a pathway has been established, this should also be assessed directly, for example through experiments simulating the flow of CO<sub>2</sub> with impurities along a leakage pathway under in-situ conditions.

Finally, as a drying out zone is expected to form around an injection wellbore used to inject CO<sub>2</sub> (Bachu, 2000; Miri et al., 2015; Peysson et al., 2014; Pruess and Müller, 2009), the interplay between drying out and carbonation (similar to that seen in the H<sub>2</sub>SO<sub>4</sub>-experiments reported here) also needs to be considered in more detail, through further experimental study.

## 5. Summary and conclusions

In the experimental research reported here, five different wellbore sealants (S1 – S5) were exposed to CO<sub>2</sub> with H<sub>2</sub>S or H<sub>2</sub>SO<sub>4</sub> at 80 °C and 10 MPa for up to 16 weeks. These experiments were carried out to assess how these key impurities impact wellbore seal integrity during CO<sub>2</sub>-injection and -storage in geological reservoirs. Microstructural and chemical analyses of the exposed sealant samples and exposure fluids showed that, in general, exposure to CO<sub>2</sub>-saturated water led to carbonate precipitation, as well as some material degradation through the leaching of soluble ions (such as Ca and Mg), while direct exposure to a (wet) supercritical CO<sub>2</sub>-phase mostly resulted in density enhancement through carbonate precipitation in the outer areas of the exposed samples. Based on the results obtained, it can be concluded that.

- During exposure to CO<sub>2</sub>-saturated water, in most sealants tested the presence of H<sub>2</sub>S enhanced the alterations observed. This resulted in deeper alteration depths (such as depletion of the Ca/Si-ratio) in sealants S1, S2 and S5. In sealants S1 and S5, the presence of H<sub>2</sub>S also inhibited carbonate precipitation, and enhanced material degradation. The impact of H<sub>2</sub>S was less pronounced on sealants that were less reactive with CO<sub>2</sub> (especially S4).
- During exposure to wet supercritical CO<sub>2</sub>, the presence of H<sub>2</sub>S had a limited impact on alteration and degradation, mainly leading to deeper microstructural alteration in sealants S1 and S5. The presence of H<sub>2</sub>S also resulted in less densification due to carbonate precipitation in the outer parts of exposed samples.
- During exposure to supercritical CO<sub>2</sub> with H<sub>2</sub>SO<sub>4</sub>, sample alterations were affected by both the presence of H<sub>2</sub>SO<sub>4</sub>, and the observed desiccation of the samples due to the absorption of water by the concentrated sulphuric acid (i.e., an experimental artefact). Mainly, microstructural densification due to carbonate precipitation in the presence of H<sub>2</sub>SO<sub>4</sub> was more diffuse, causing up to 2 times higher alteration depths in these samples. This may be partly ascribed to desiccation resulting in deeper CO<sub>2</sub>-penetration before mineralisation as the CO<sub>2</sub>-water interface receded, or alternatively to the acidifying effect of H<sub>2</sub>SO<sub>4</sub>. In addition, samples exposed to CO<sub>2</sub> with H<sub>2</sub>SO<sub>4</sub> also showed more degradation at the surfaces, though this was mostly limited to the outer 100–200 µm of these samples (and the degree of this degradation was quite minor). This degradation may be the result of the formation and subsequent run-off of highly acidic liquid droplets at the sample surfaces, where H<sub>2</sub>SO<sub>4</sub>-saturated CO<sub>2</sub> encountered water and precipitated.
- For geological CO<sub>2</sub>-storage applications, the impact of impurities co-injected with CO<sub>2</sub> on intact seals with compositions similar to those tested here, and under similar PT-conditions, will likely be relatively minor, at worst leading to an increase in alteration depths by (considerably) less than an order of magnitude.

- When CO<sub>2</sub> (or CO<sub>2</sub>-saturated water) flows along a leakage pathway through or along a wellbore seal, however, reactive impurities in the CO<sub>2</sub> may impact how this leakage pathway develops, potentially exacerbating the leakage, for example by inhibiting carbonate precipitation that could otherwise lead to self-sealing of the leakage pathway.
- More work is needed, to assess a wider range of sealant compositions, and to address the impact of other reactive impurities (and combinations of impurities) than those studied here (e.g., NO<sub>x</sub>, O<sub>2</sub> and HF). The impact of impurities on leakage pathway development also needs to be studied in more detail in targeted laboratory experiments, to constrain this potential storage integrity risk.

## Funding statement

The CEMENTTEGRITY project is funded through the ACT programme (Accelerating CCS Technologies, Horizon2020 Project No 691712). Financial contributions from the Research Council of Norway (RCN), the Netherlands Enterprise Agency (RVO), the Department for Energy Security & Net Zero (DESNZ, UK), and Harbour Energy are gratefully acknowledged.

## CRediT authorship contribution statement

**Reinier van Noort:** Writing – original draft, Visualization, Supervision, Project administration, Methodology, Investigation, Funding acquisition, Formal analysis, Conceptualization. **Gaute Svenningsen:** Writing – review & editing, Methodology, Investigation, Funding acquisition. **Kai Li:** Resources, Investigation.

## Declaration of competing interest

The authors declare the following financial interests/personal relationships which may be considered as potential competing interests: Reinier van Noort reports financial support was provided by Harbour Energy. Reinier van Noort reports samples were provided by Halliburton. If there are other authors, they declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

## Data availability

Data will be made available on request.

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