

Methoden der Validierung der FTIR-Spektrometrie in der Gasanalytik

Offen-Pfad- und passive Messungen

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VDI Guideline 4211, part 1

Burner and calibration gases

Calibration flame

Hot calibration gas cell

Instrumental Line Shape determination

Relevant information from advisory standards

VDI Guideline "Atmospheric measurements near ground with FTIR spectroscopy. Measurements of gaseous emissions and immissions. Fundamentals" (VDI 4211, part 1)

CEN working group TC 264/WG 18 "Open path optical methods for the measurement of ambient air quality"

Use of reference spectra

CEN

Primary Calibration

IR gas cell with calibration gas in the radiation path of the spectrometer

Five concentration levels minimum, run through in 10 cycles according to VDI Guideline 2449 Part 1 or ISO standard 9169

Test gases are produced and metered into the gas cell statically or dynamically according to VDI Guideline 3490

Determination of calibration function with its confidence ranges in accordance with VDI Guideline 2449 Part 1 or ISO standard 9169

CEN

Control calibration

Determination of N₂O (340 ppb) and CH₄ (1.7 ppm) concentration in ambient air

Determination of H₂O concentration

Comparison with independent water vapour concentration measurements

CEN

Calibration by using spectral lines from data bases and determination ILS

**Synthetic determination of calibration spectra with
molecular spectroscopic database and quantitative
ILS**

**Determination of actual ILS with measurement of
laser or CO of known concentration (spectral
resolution narrower than line width)**

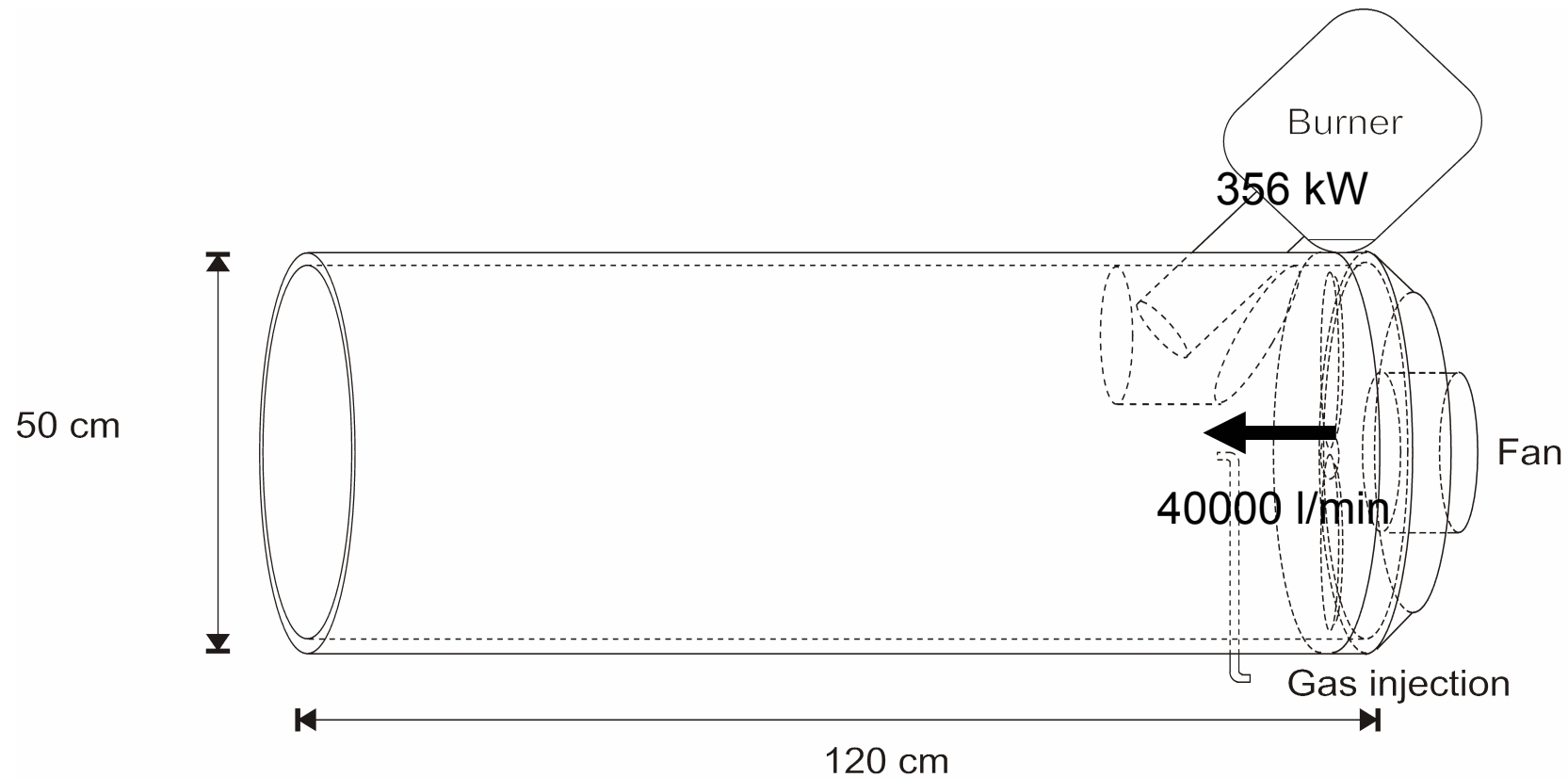
Evaluation of FTIR spectrometry applied for hot gas analyses

Evaluation of FTIR measurement results is necessary for routine application of the measurement method

Different methodologies and techniques for this task were considered:

- **calibration burner (high temperature gas producer),**
- **calibration flame,**
- **hot cell**

Calibration burner (high temperature gas producer)

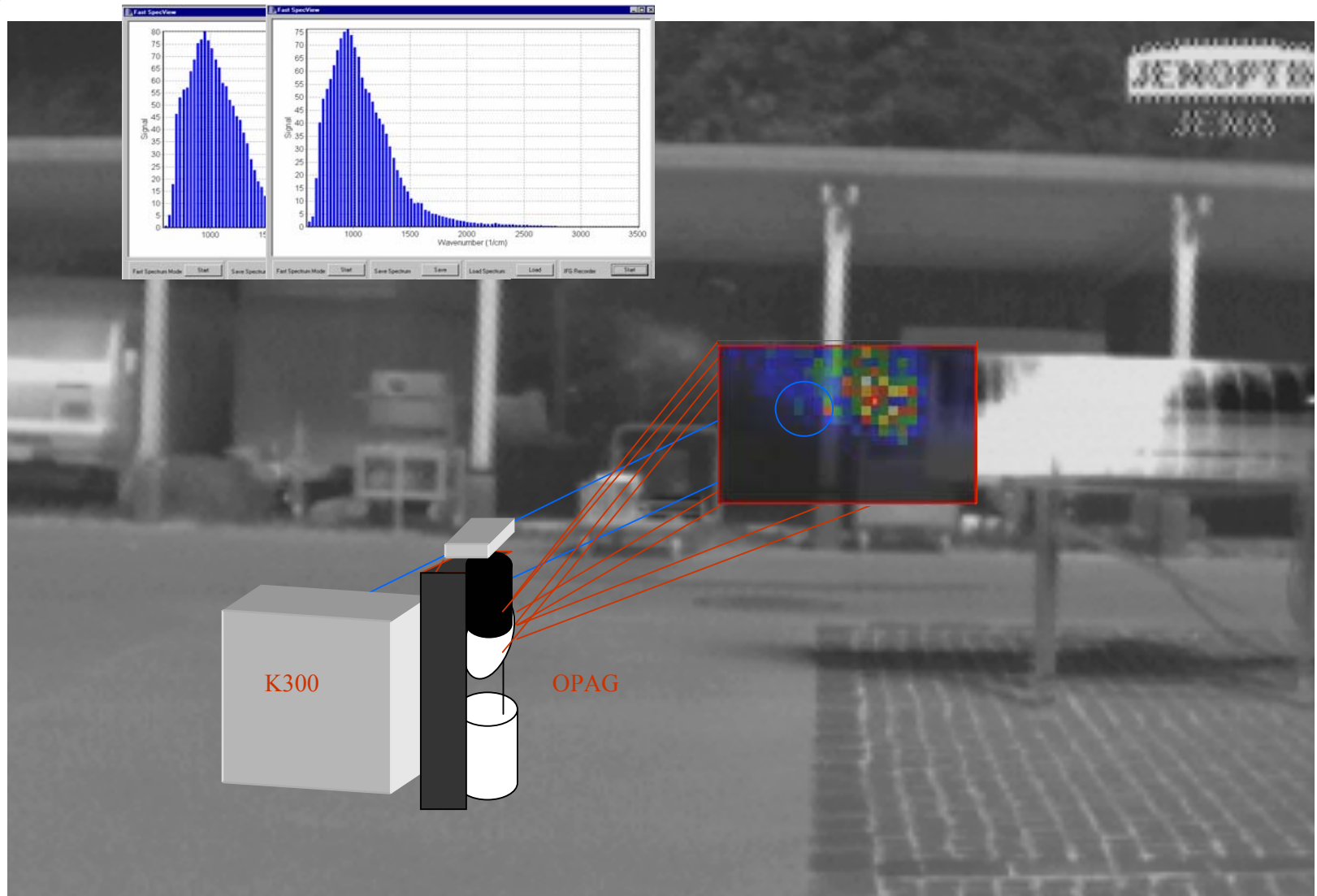


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Burner experiments

McKenna burner

Hot gas cell

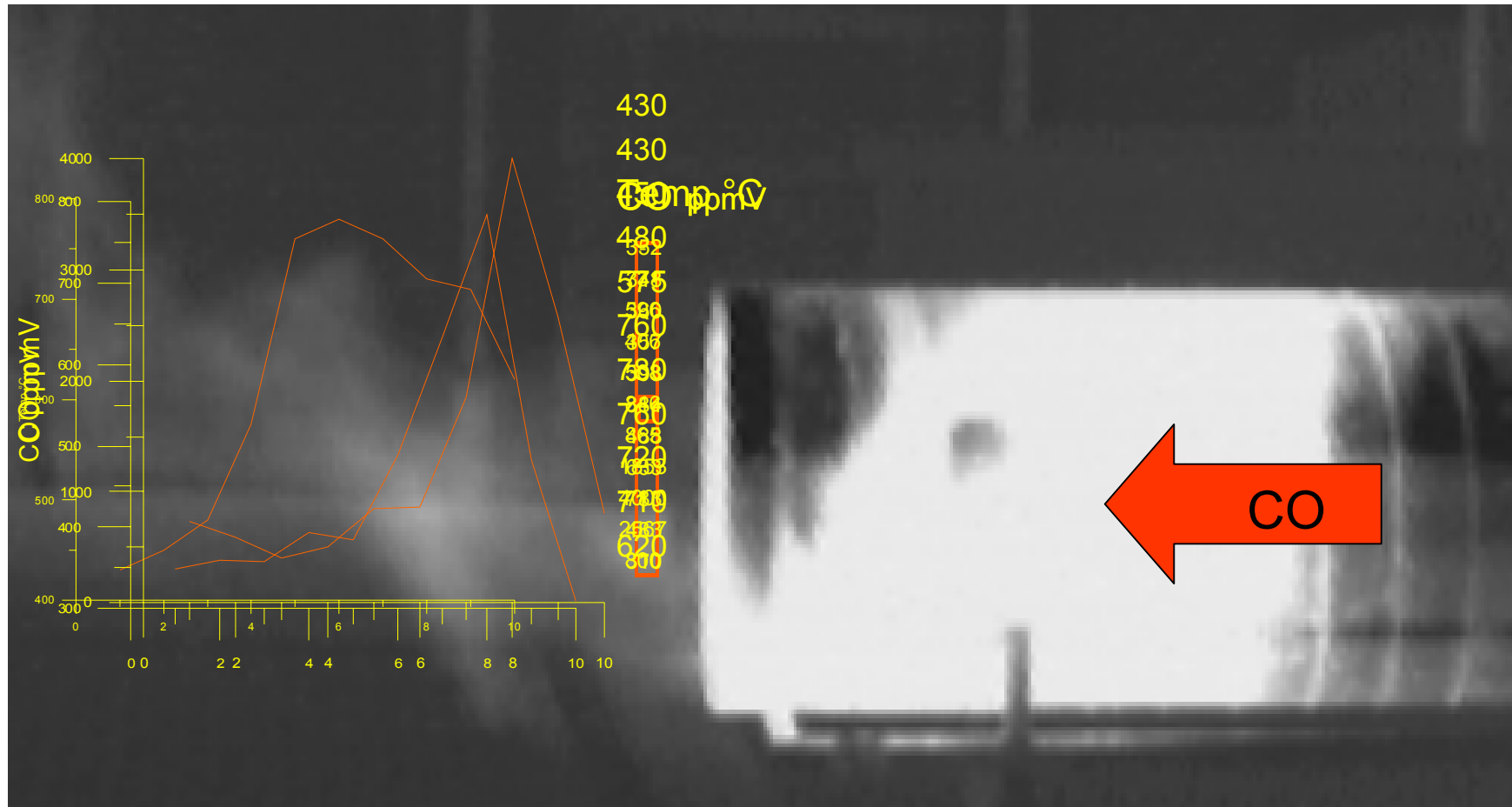


OPAG
CO injection

Burner experiments

McKenna burner

Hot gas cell

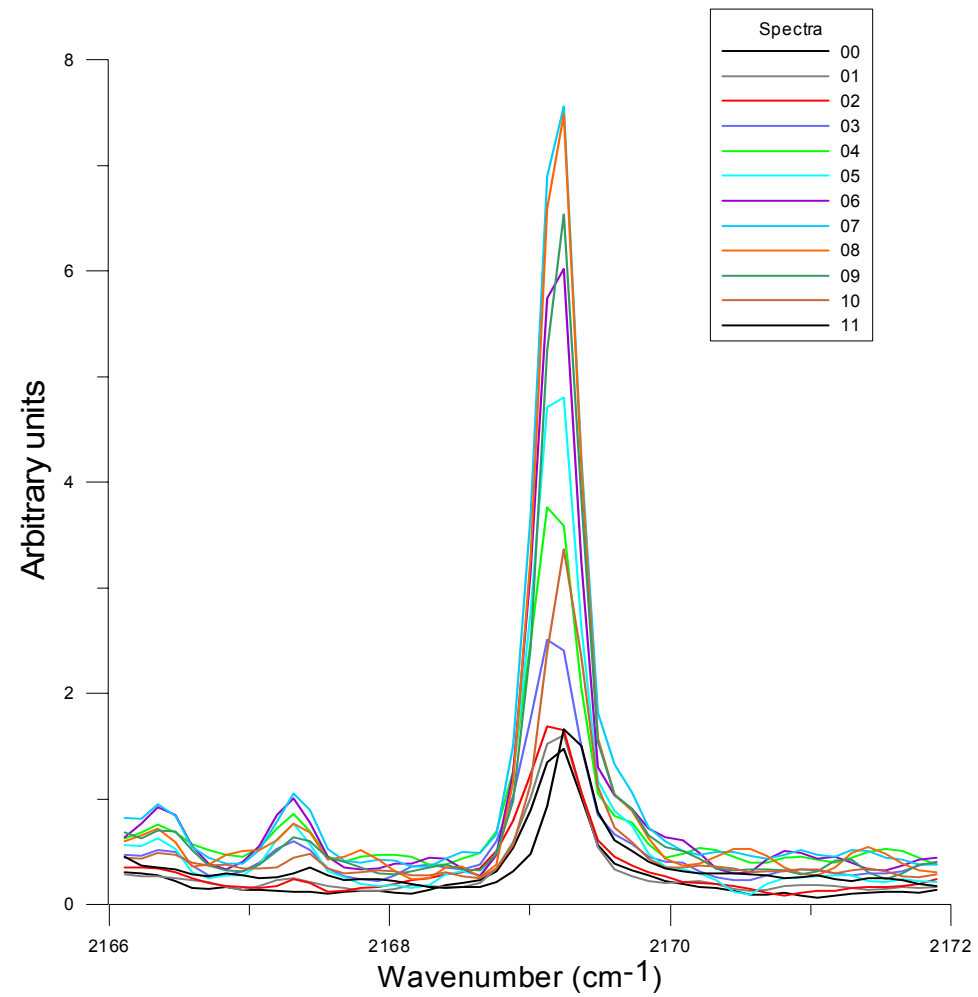
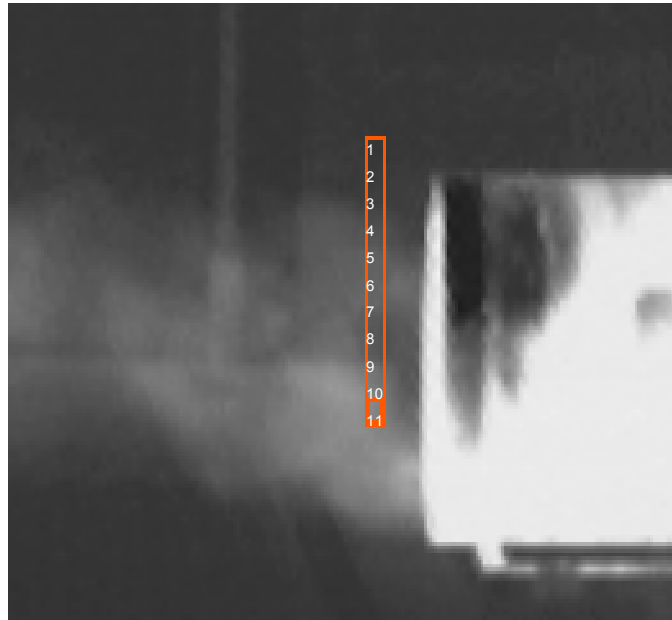


OPAG
CO injection

Burner experiments

McKenna burner

Hot gas cell

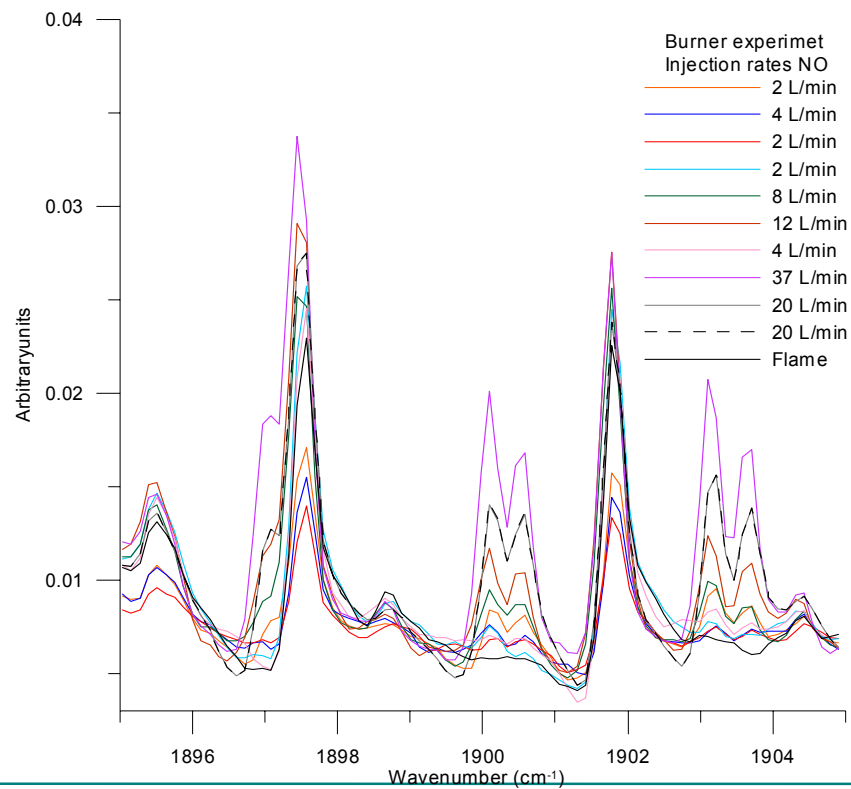
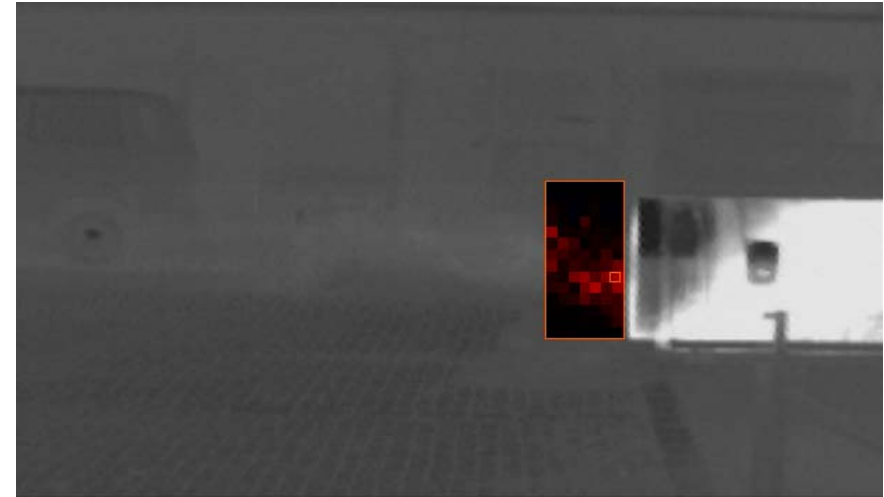


OPAG
NO injection

Burner experiments

McKenna burner

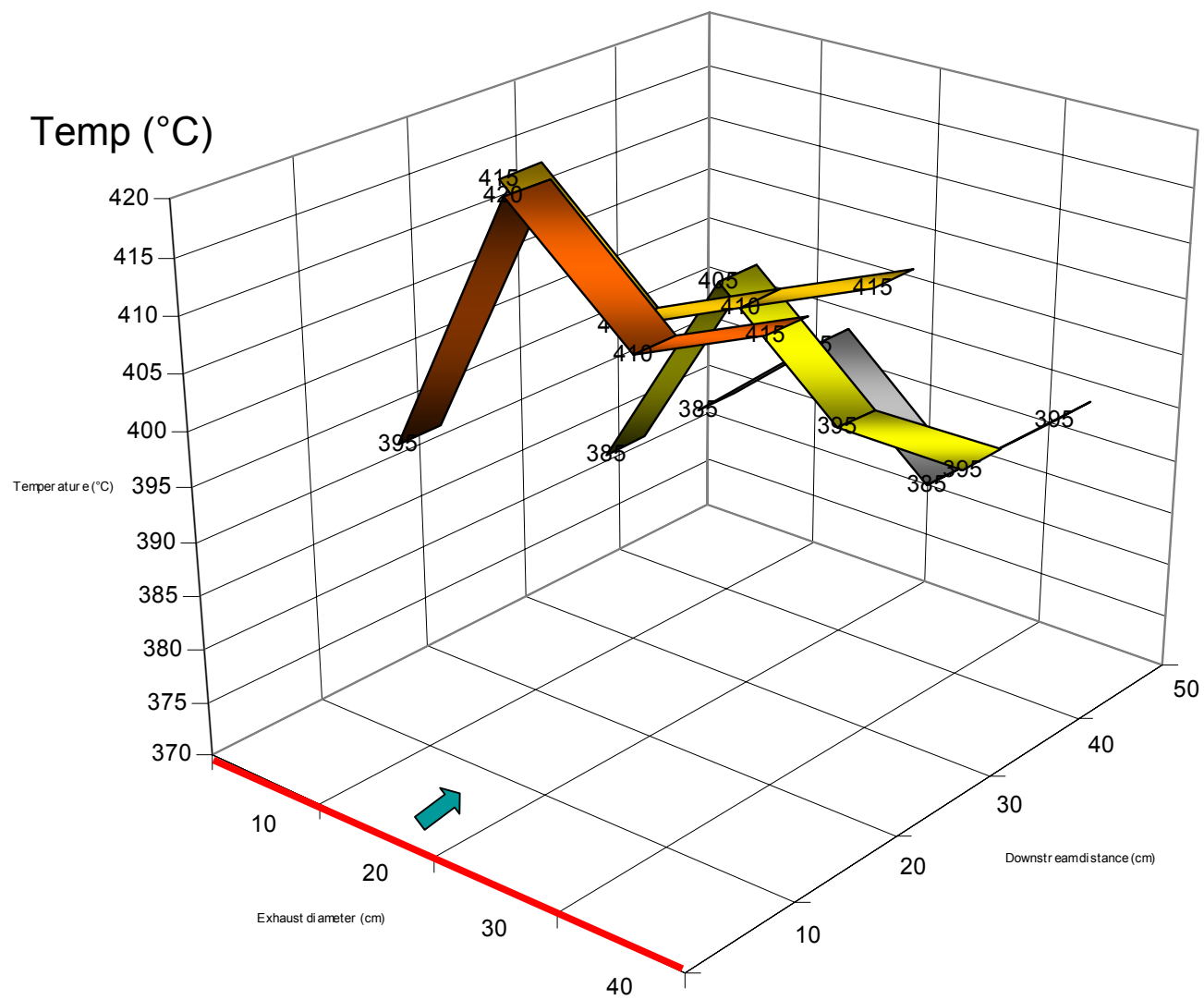
Hot gas cell



Burner experiments

McKenna burner

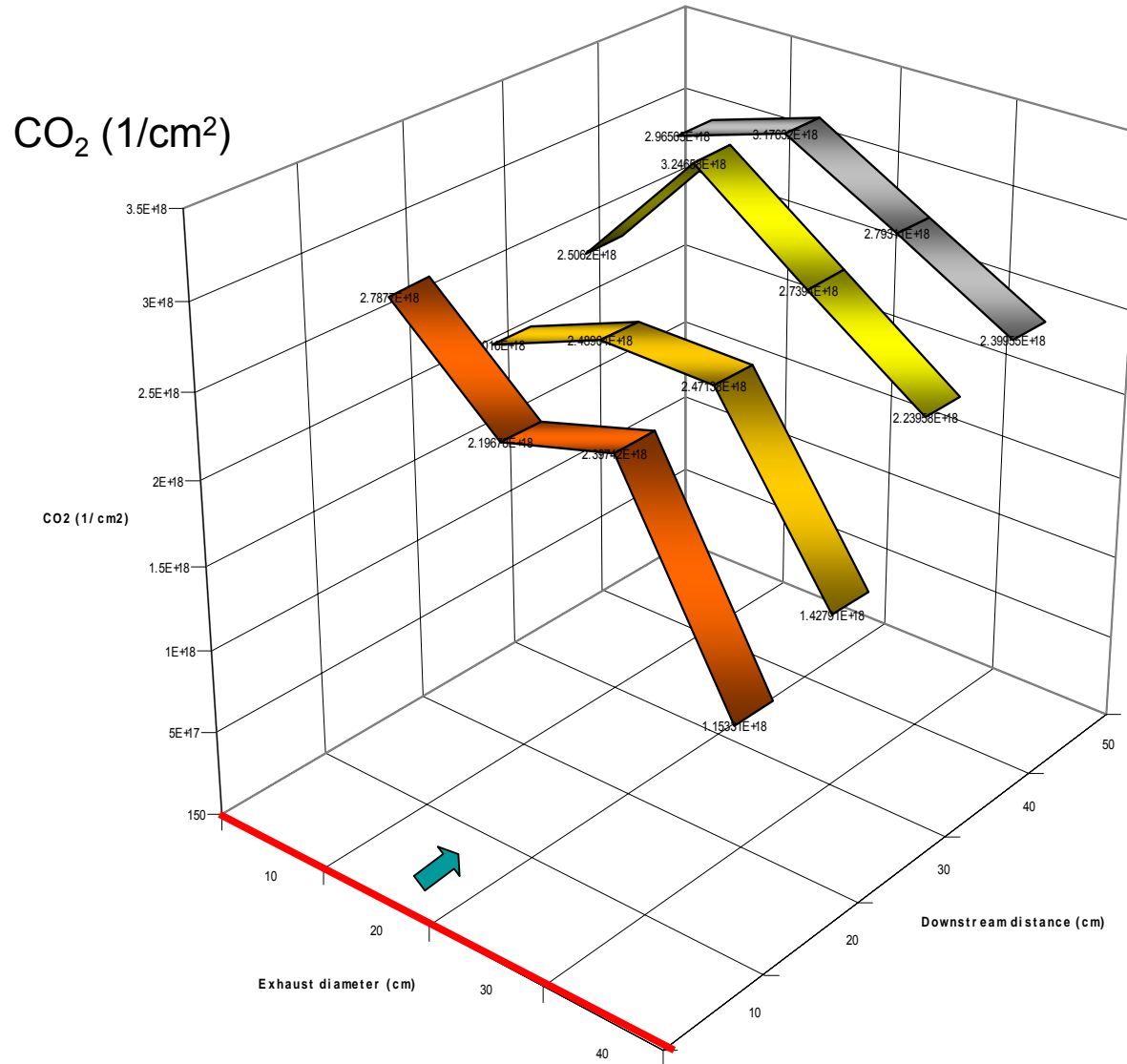
Hot gas cell



Burner experiments

McKenna burner

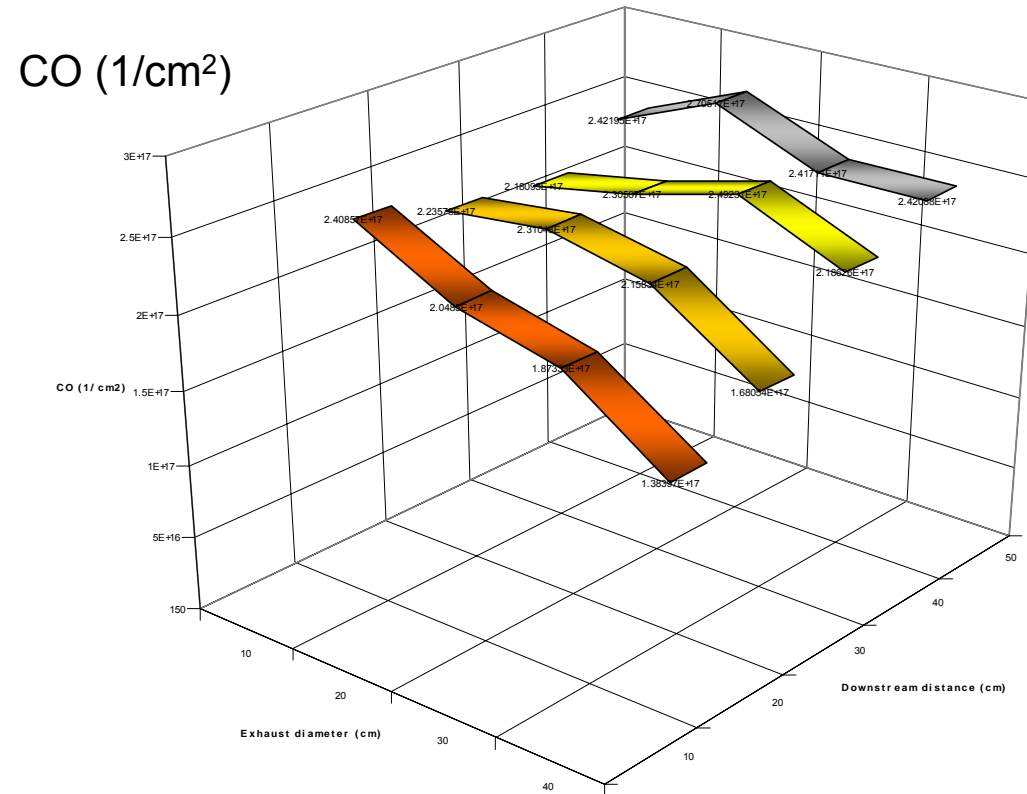
Hot gas cell



Burner experiments

McKenna burner

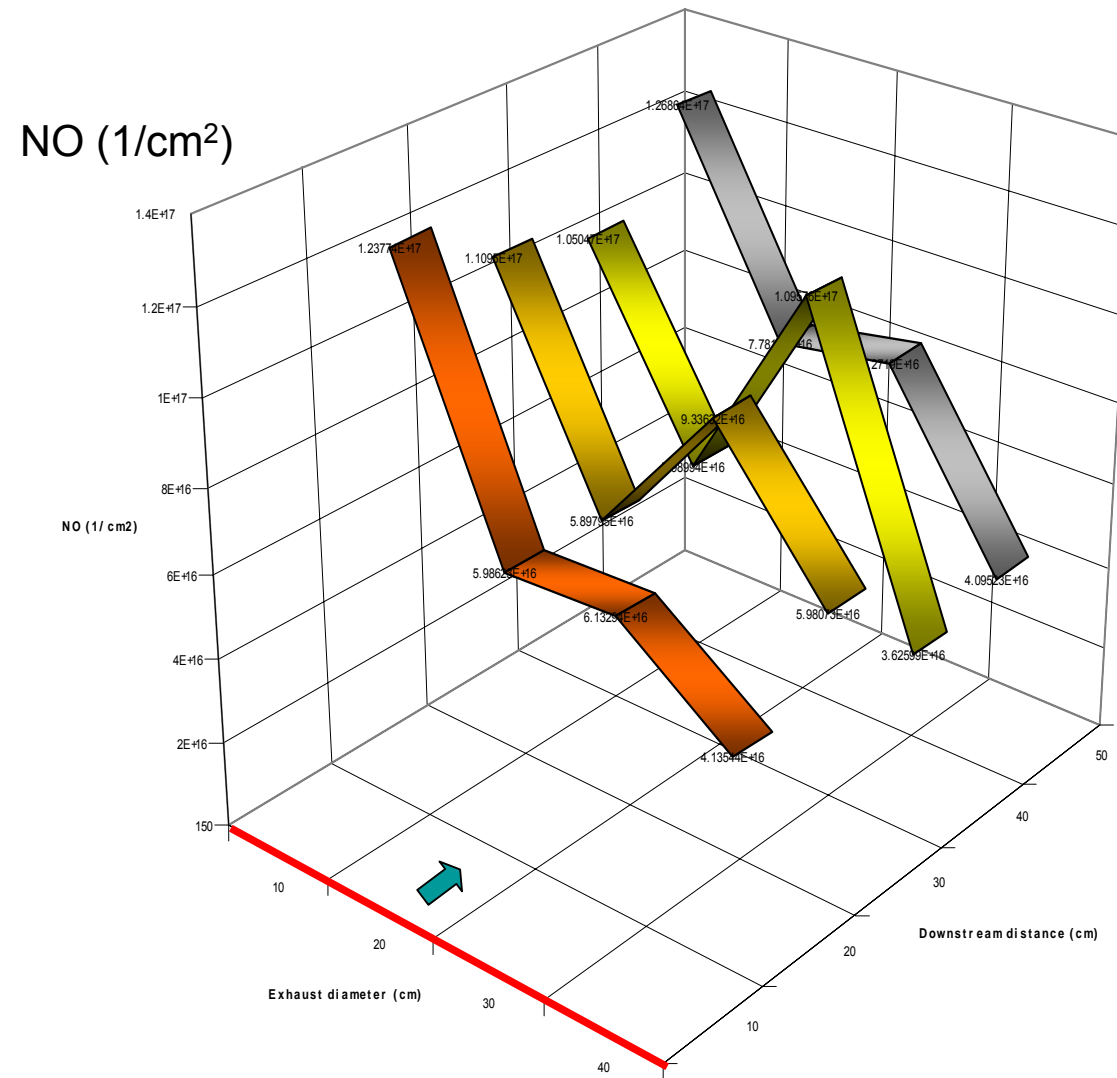
Hot gas cell



Burner experiments

McKenna burner

Hot gas cell



Experiments with burner

CO and NO (pure calibration gases) were injected in the exhausts with different amounts as calibration gases to vary the concentration of these gases

Relevant chemical transformation of the injected CO and NO in the exhaust plume

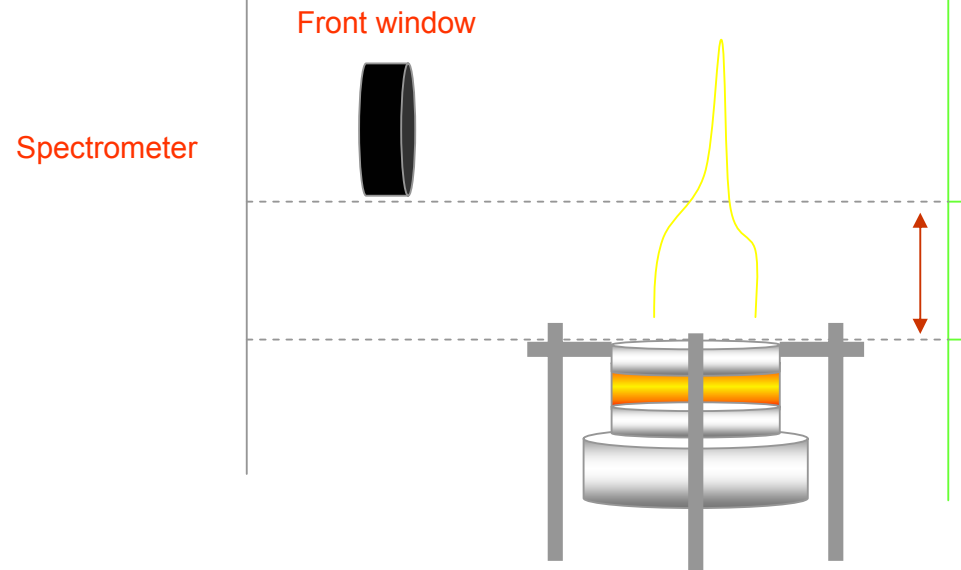
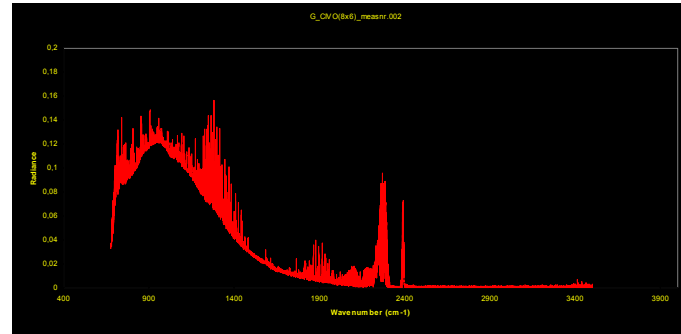
Problems with homogeneous mixing

Results show that this method is not accurate enough for operational use

Burner experiments

McKenna burner

Hot gas cell

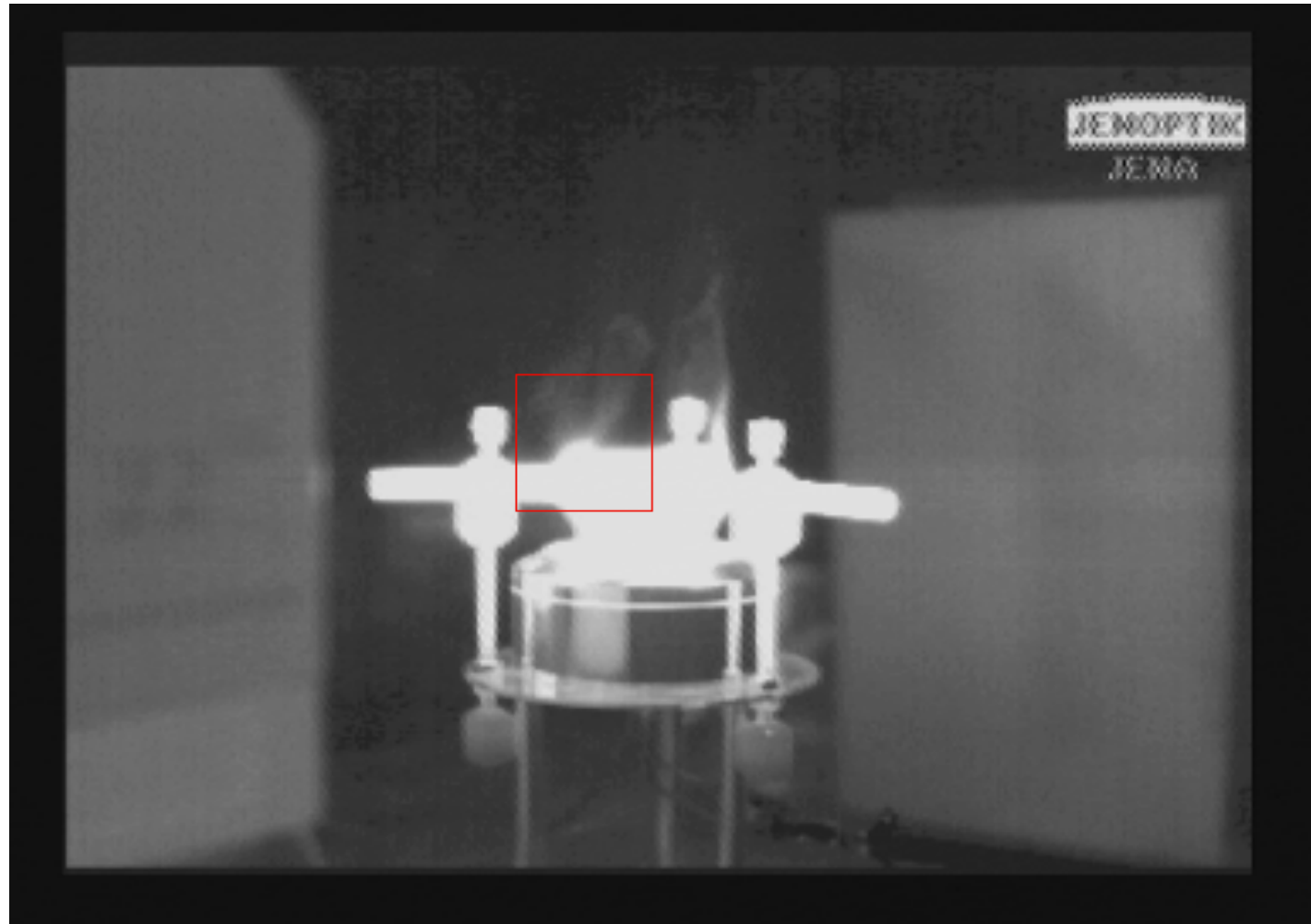


Distance and altitude of the flame were fixed
Time of measurements was about 5 minutes

Burner experiments

McKenna burner

Hot gas cell

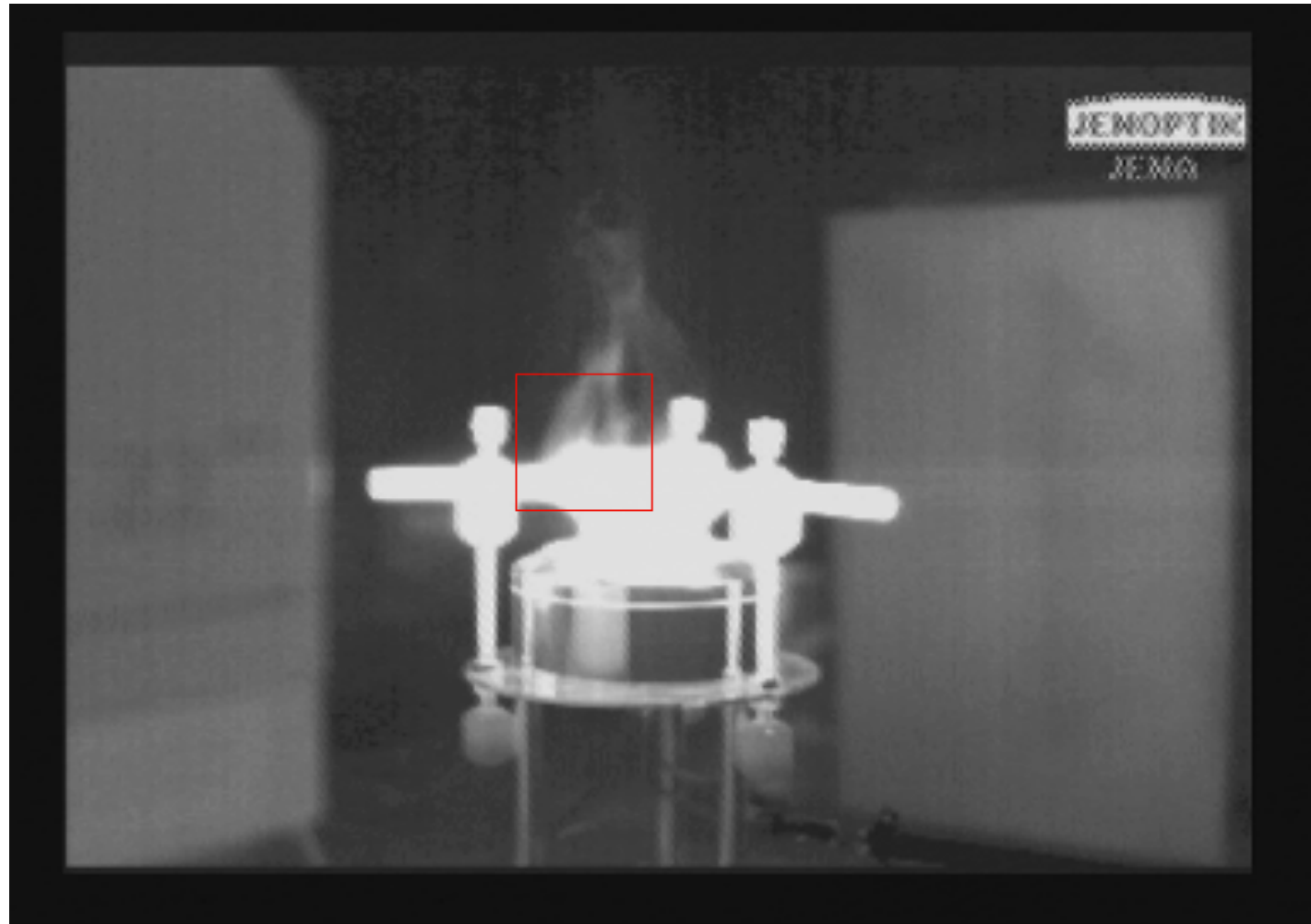


Thermo image from McKenna burner powered with 30 % of C_2H_4 and 30 % of air

Burner experiments

McKenna burner

Hot gas cell

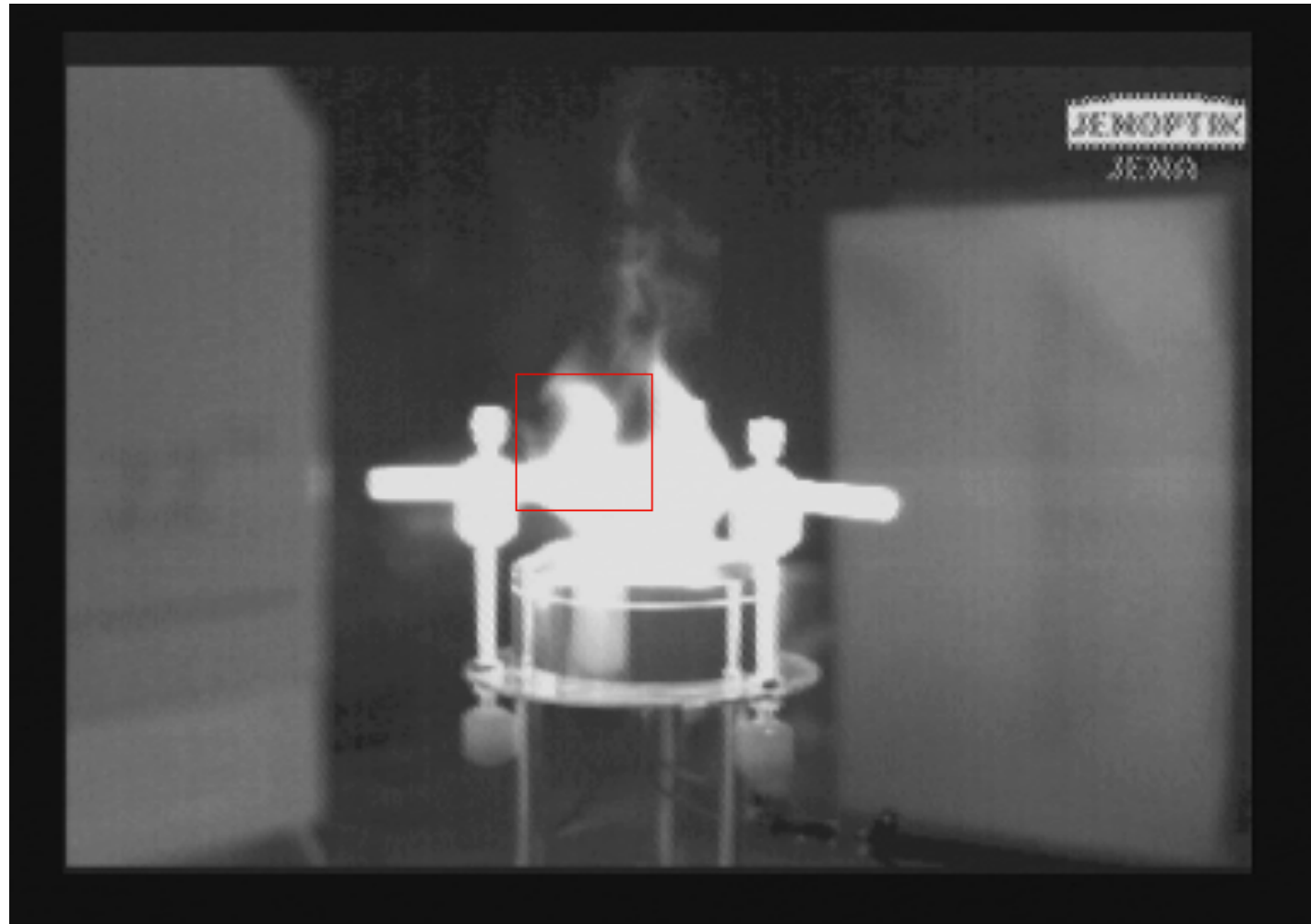


Thermo image from McKenna burner powered with 30 % of C_2H_4 and 30 % of air

Burner experiments

McKenna burner

Hot gas cell

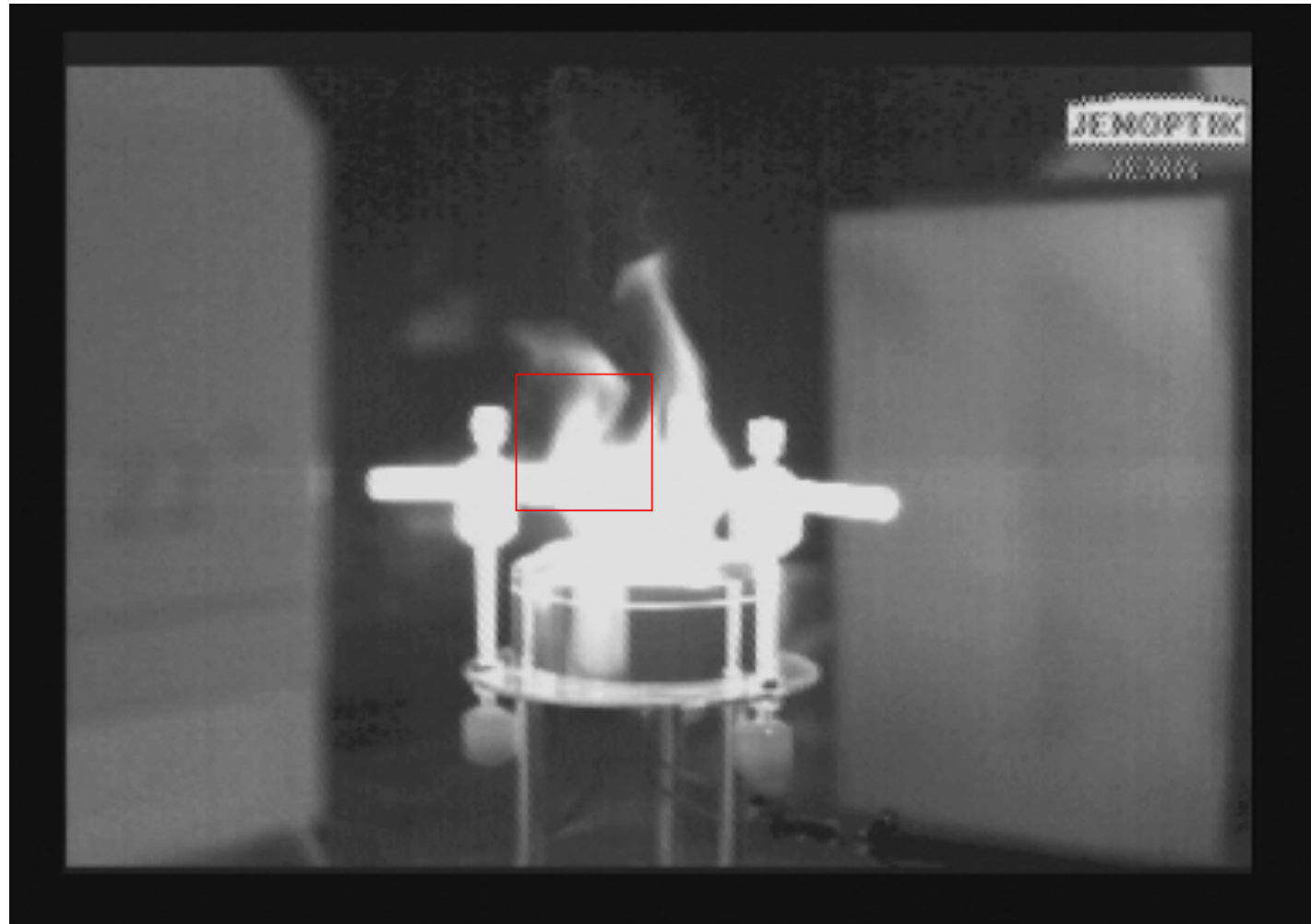


Thermo image from McKenna burner powered with 30 % of C_2H_4 and 30 % of air

Burner experiments

McKenna burner

Hot gas cell



Thermo image from McKenna burner powered with 30 % of C_2H_4 and 30 % of air

Experiments with calibration flame

Measurements with a McKenna burner to determine CO and NO concentrations as well as temperature

Influences by any air streaming

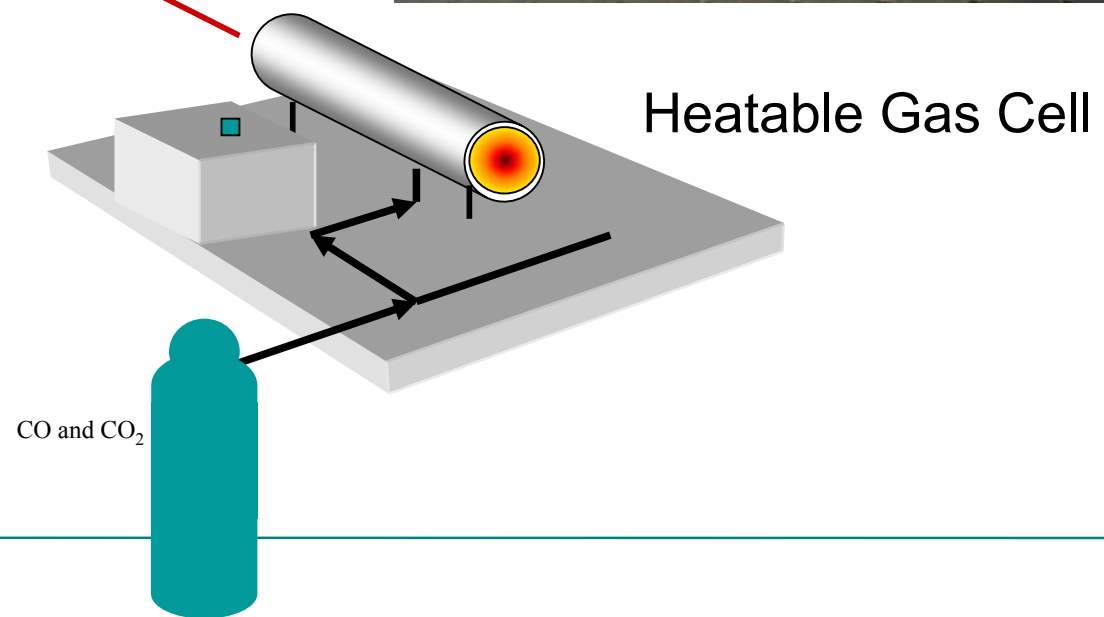
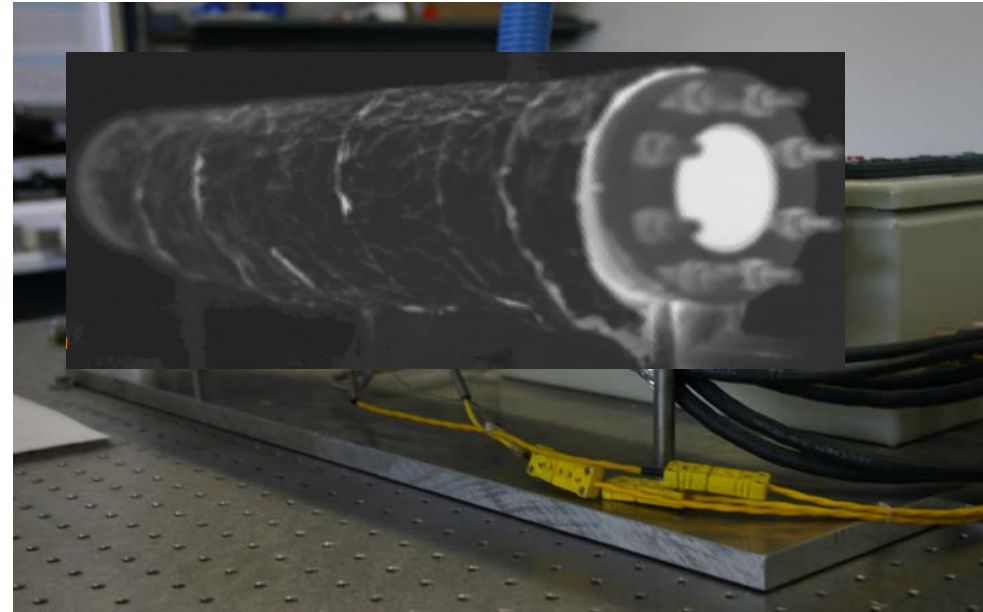
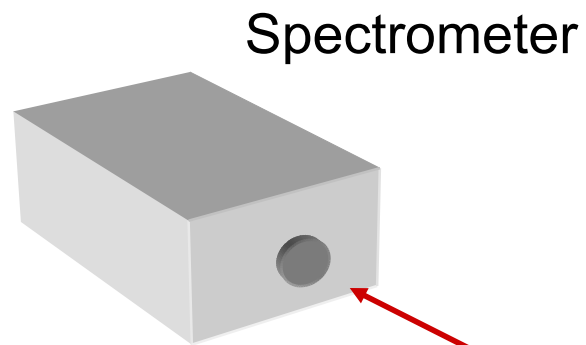
Repeatability of the experiment is not reliable

Calibration flames are much easier to handle than a burner but the same difficulties exist with added calibration gases

Burner experiments

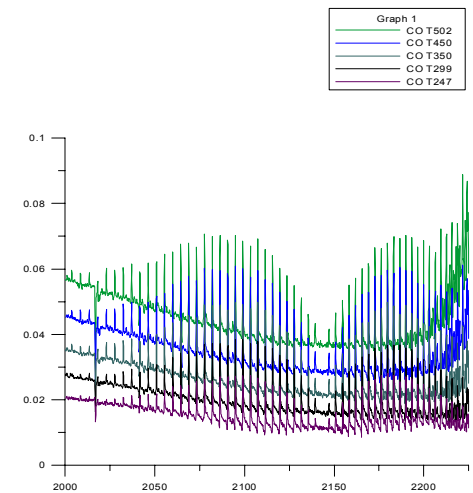
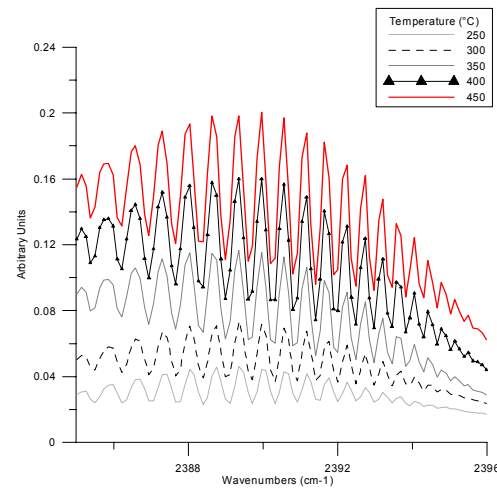
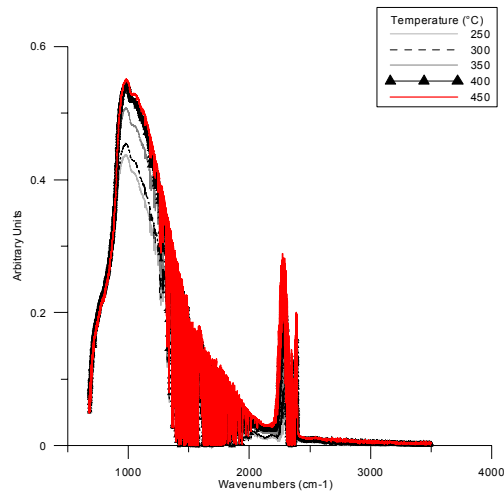
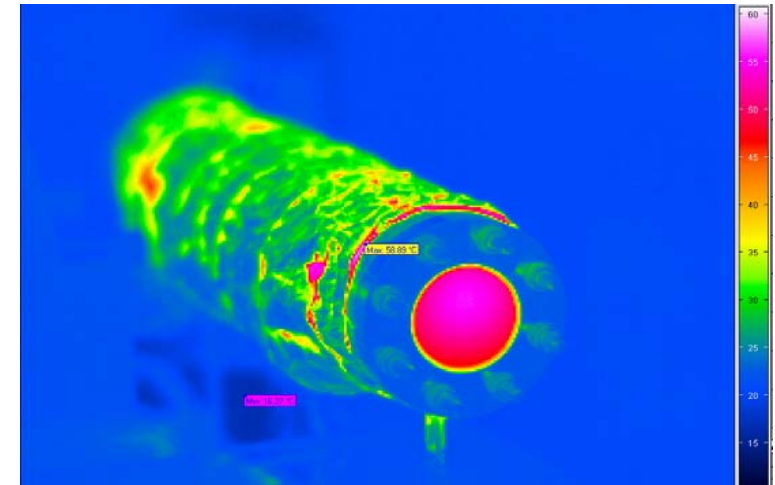
McKenna burner

Hot gas cell



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Absorption path length: 50 cm
Diameter: 5.5 cm
Window material: Calcium fluoride
Calibrated gas mixture:
CO₂ 3.5%, CO 500ppmV and air
Temperature range: 300 - 750 K.

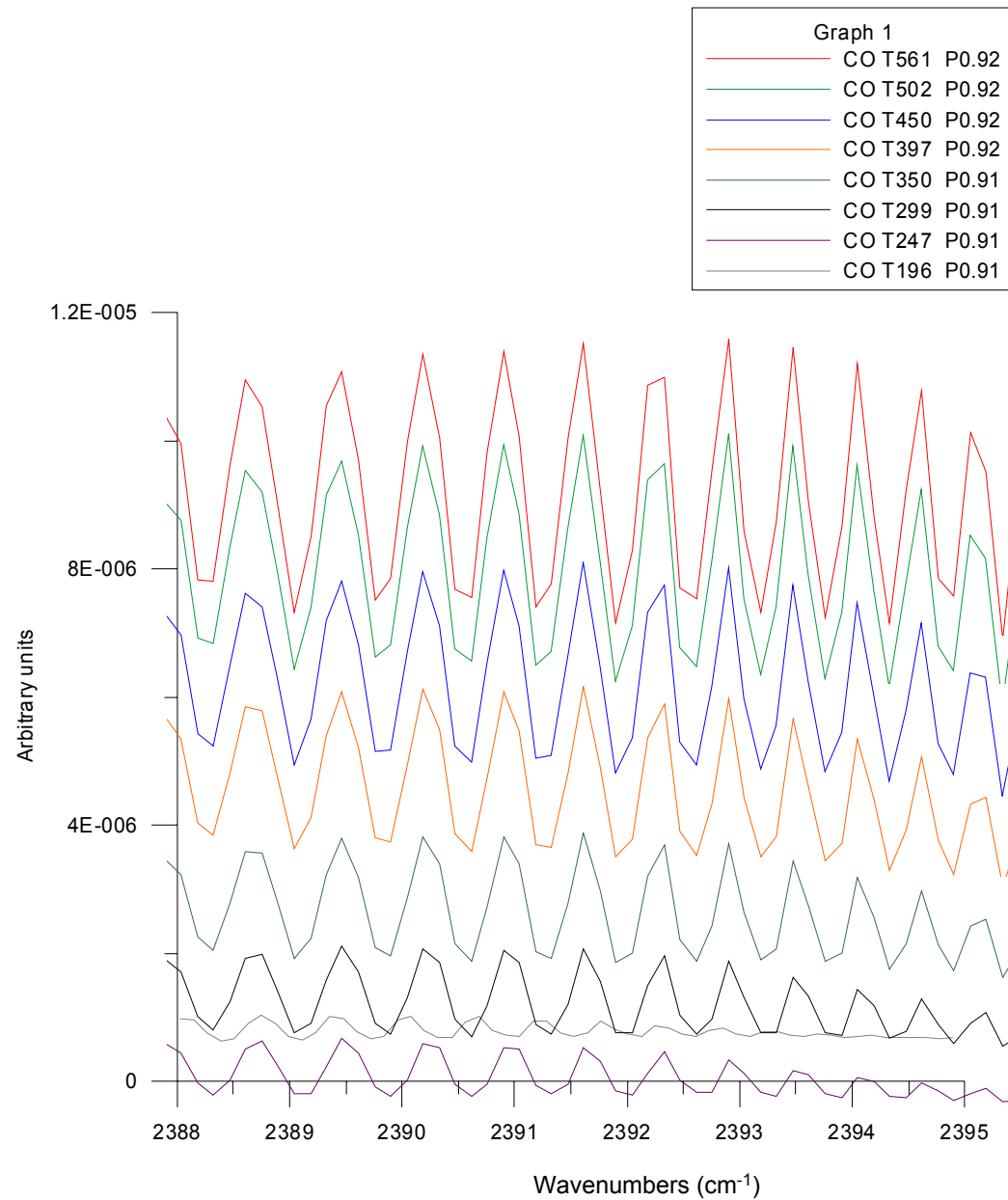


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Burner experiments

McKenna burner

Hot gas cell



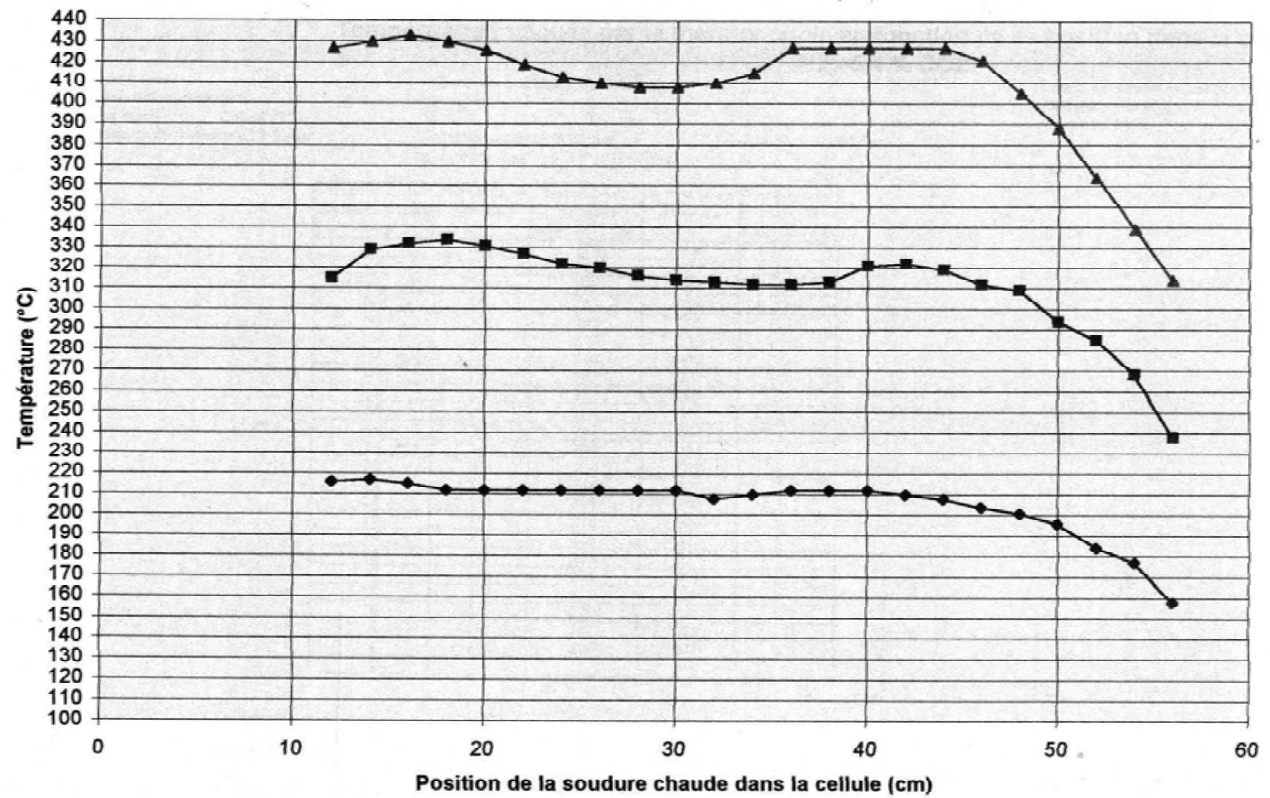
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Burner experiments

McKenna burner

Hot gas cell

Température indiquée par le thermocouple en fonction de sa position dans la cellule
(air ambiant)



Experiments with heatable gas cell

Experiments with the hot cell includes a heatable cell, thermo-couples for temperature control, manometer and a regulation device

Cell was operated with a constant gas mixture (CO₂ and CO in synthetic air) in the cell during the measurement (no gas flow)

Materials for temperatures higher than 500°C are necessary

In-homogeneities of temperature and mixed gases inside the cell and influences by windows and walls of the cell

Calibration with determination of real ILS

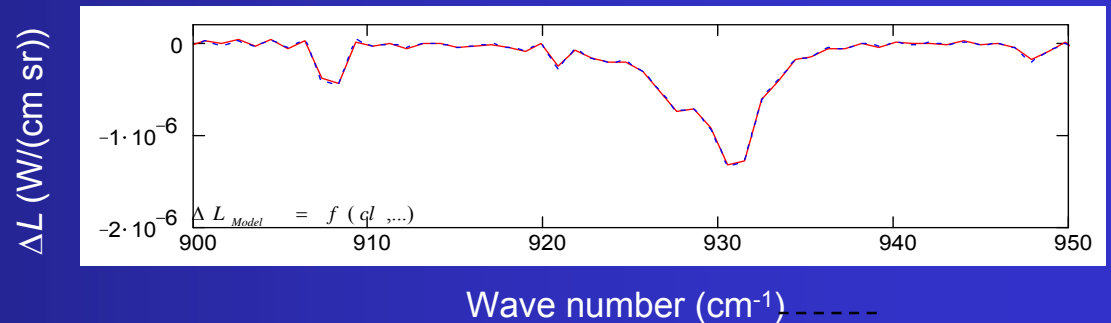
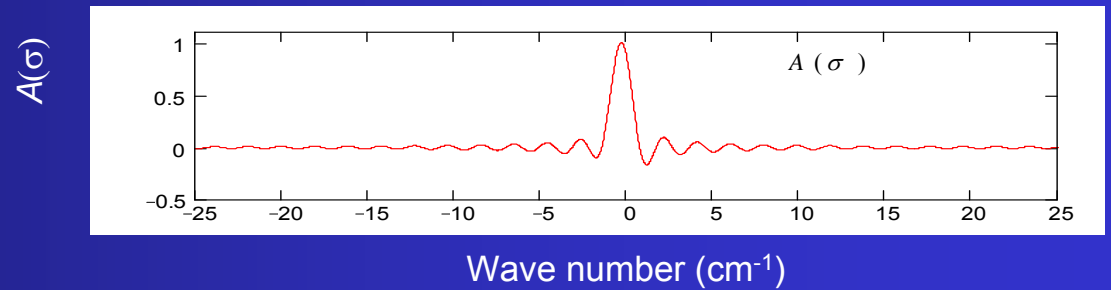
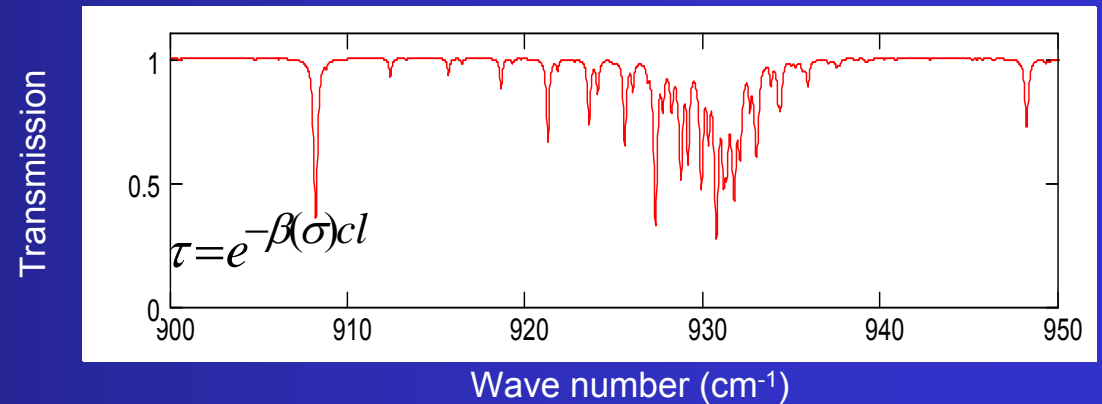
Example:

Radiative transfer model

Real ILS

Calculated and measured radiance

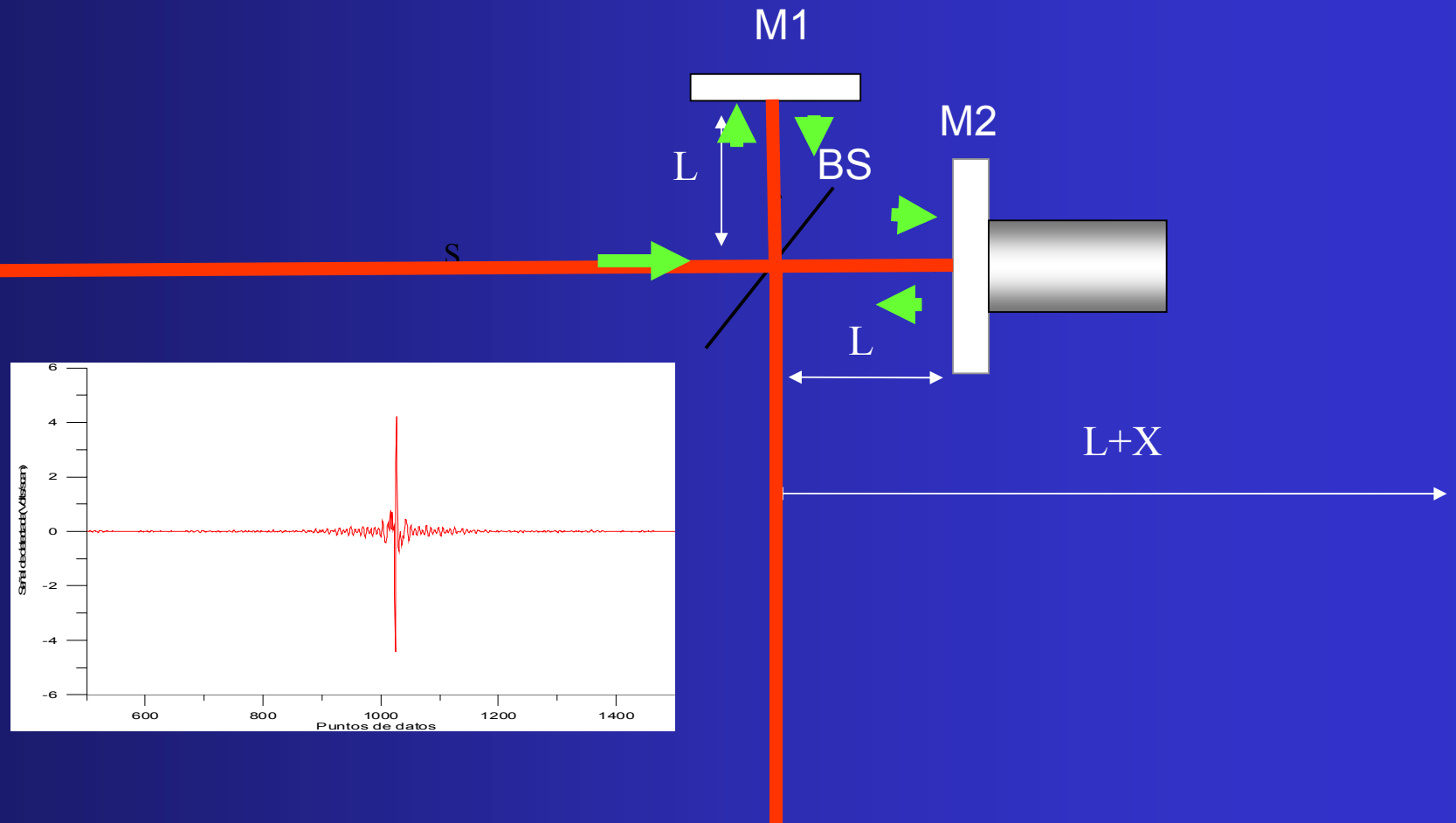
Non-linear Modelling Example: Spectrum of Ammonia



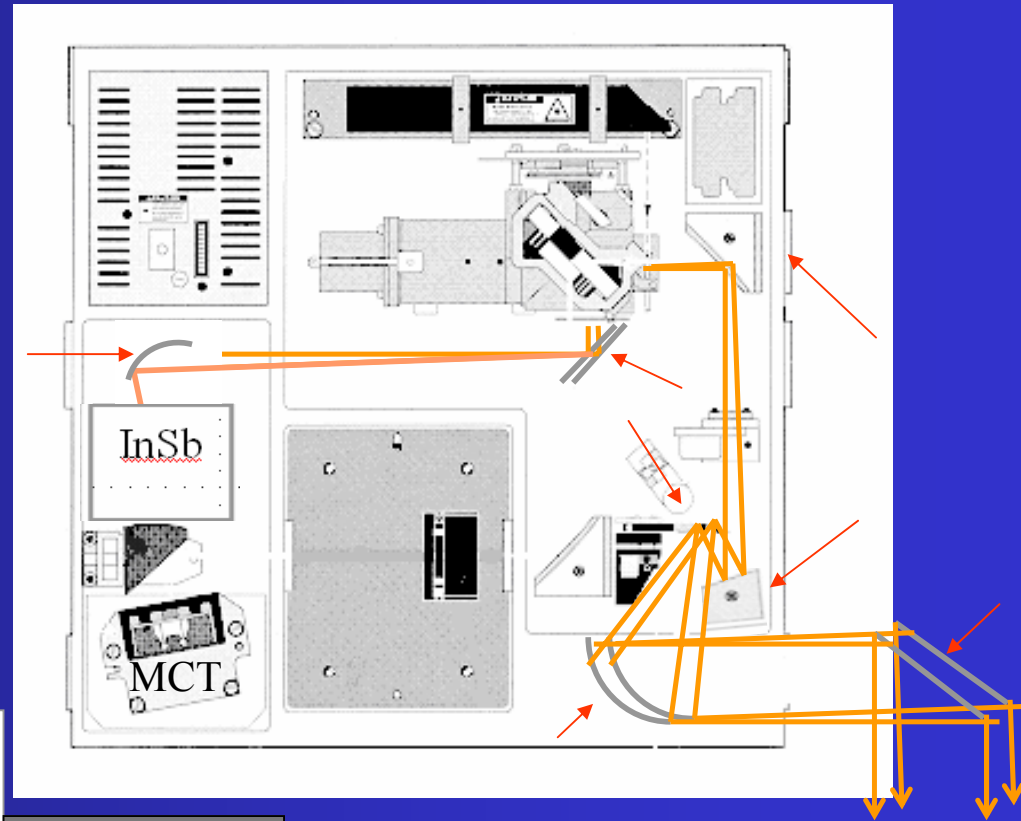
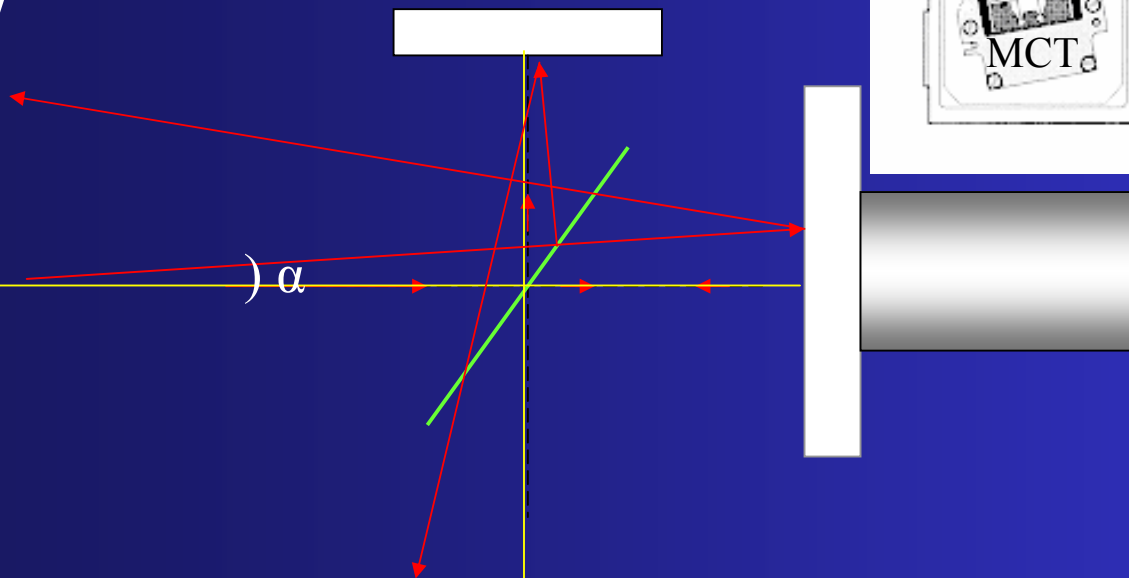
Meas. ΔL_{Meas}

Model ΔL_{Model}

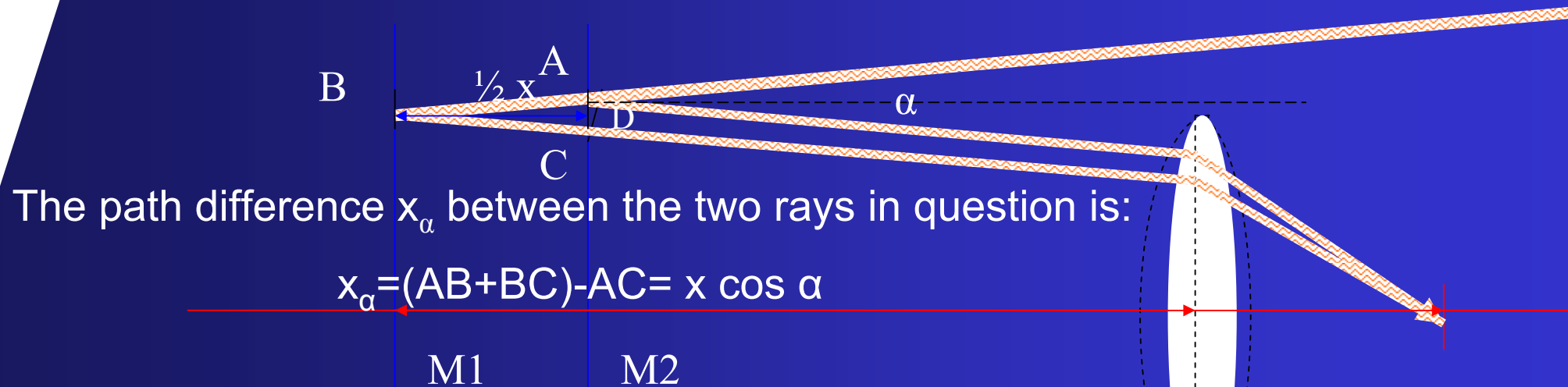
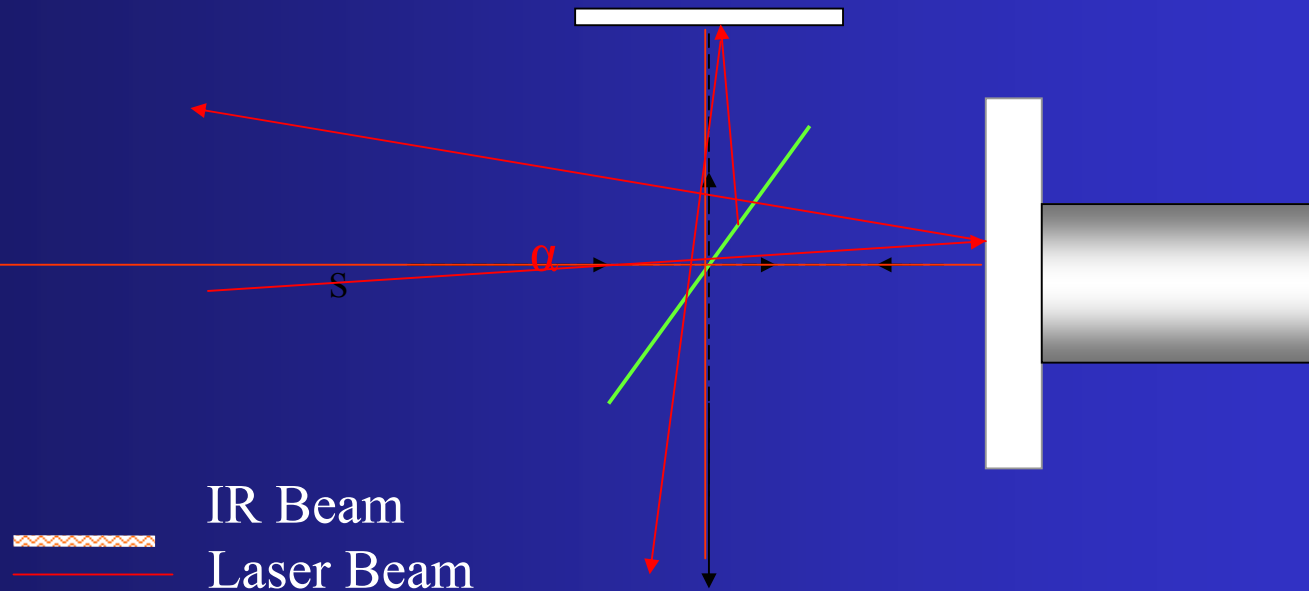
For an ideal interferometer operating with perfectly collimated radiation, the ideal instrumental line shape A_0 will be given by the Fourier transform of the function that will describe the finite movement of the mirror.



— Laser
— IR



Phase error- wrong sampling points



Determination of the real ILS

- Absorption experiment

Gas with well separated lines and narrower than the resolution of the spectrometer: NH_3 , CO

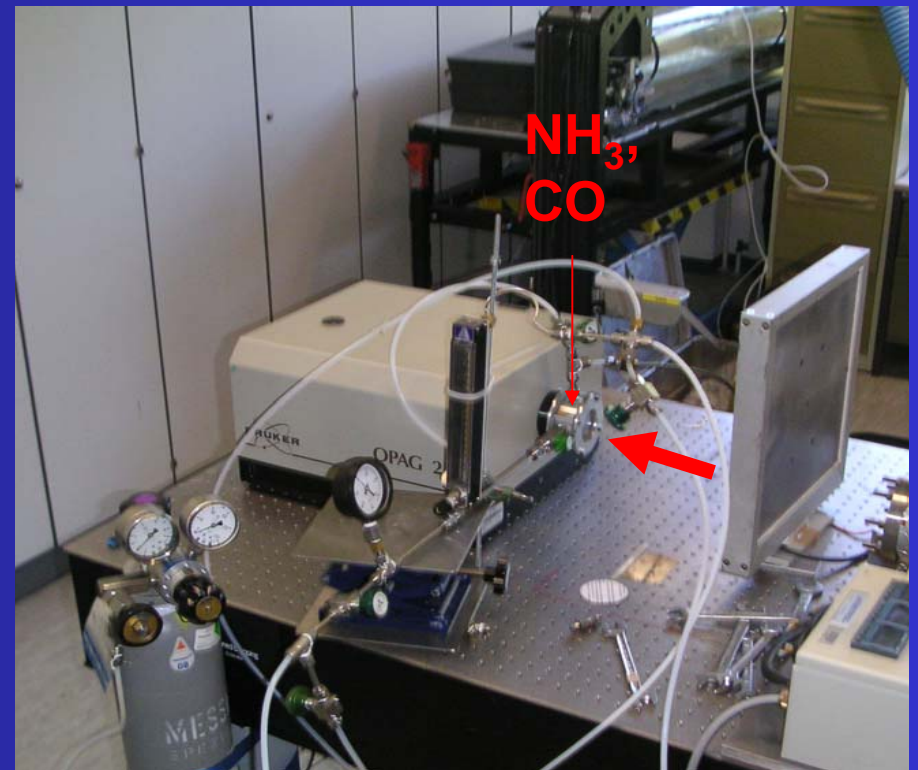
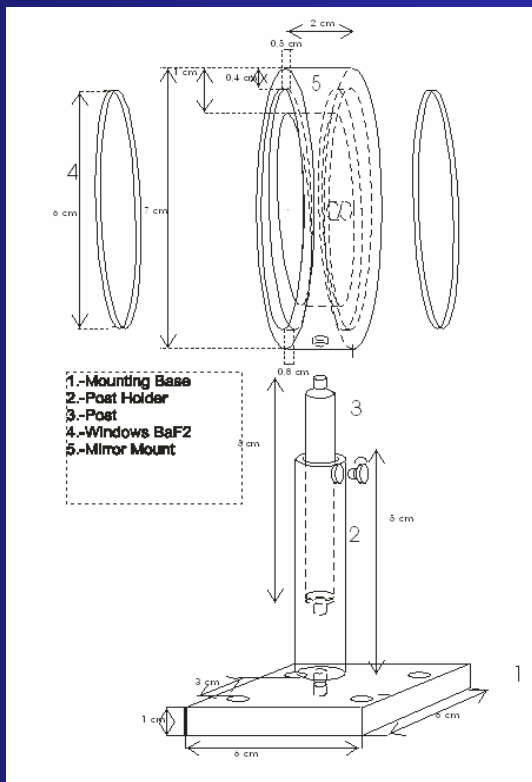
- Sub-models:

Radiative transfer model

Model of the ILS

Transmittance of a gas

Material: Stainless-steel
Optical depth: 1 cm
Field of view: 5 cm
Window material: BaF₂

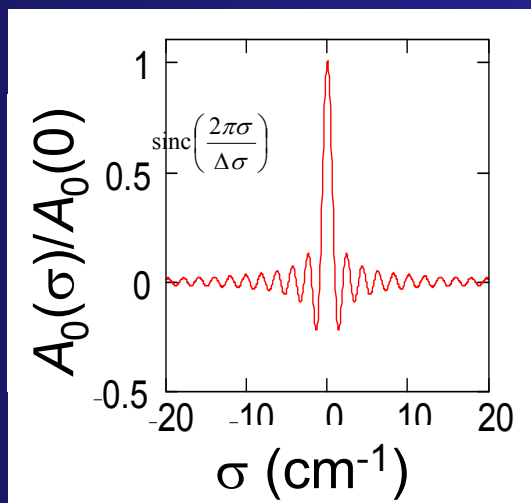


Real ILS calculation

Calculation of the Instrument Line Shape (ILS):
Model for Real Instrument

Ideal
ILS:

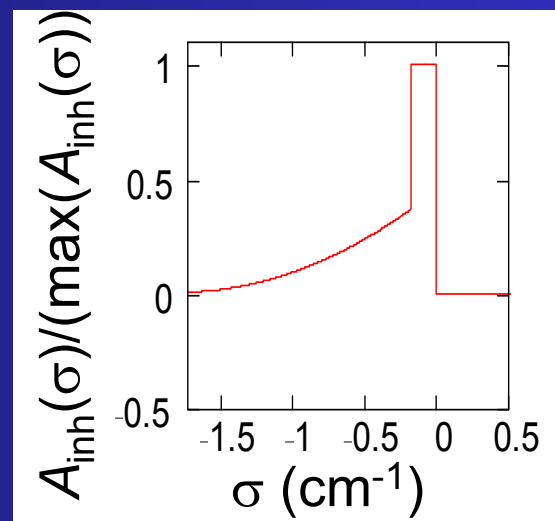
$$A_0(\sigma, \Delta\sigma)$$



*

Model for the
inherent ILS:

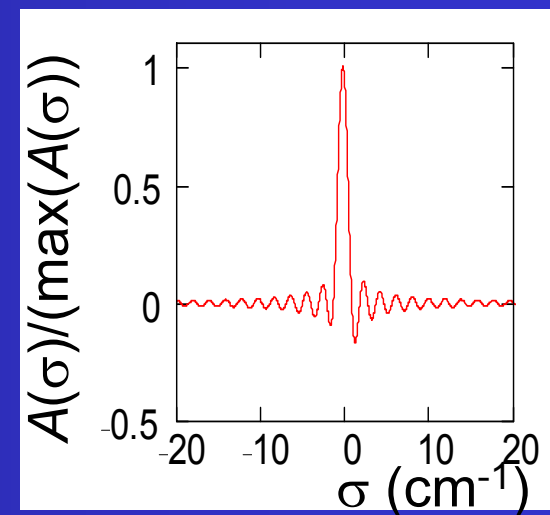
$$A_{inh}(\sigma, p_1 \cdot p_Q)$$



=

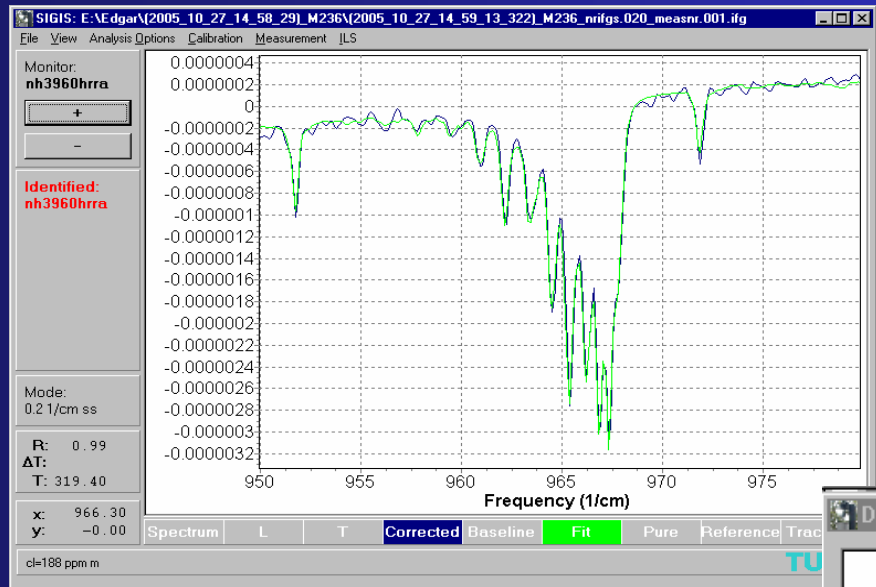
Real
ILS:

$$A(\sigma)$$

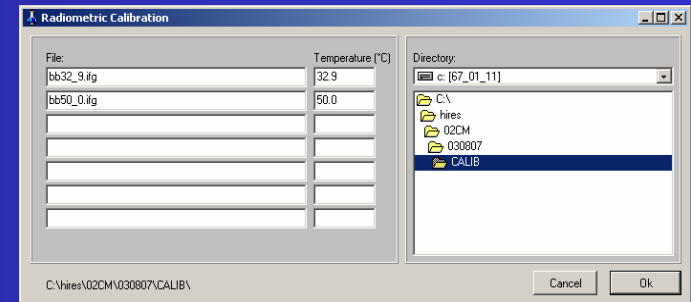


ILS determination

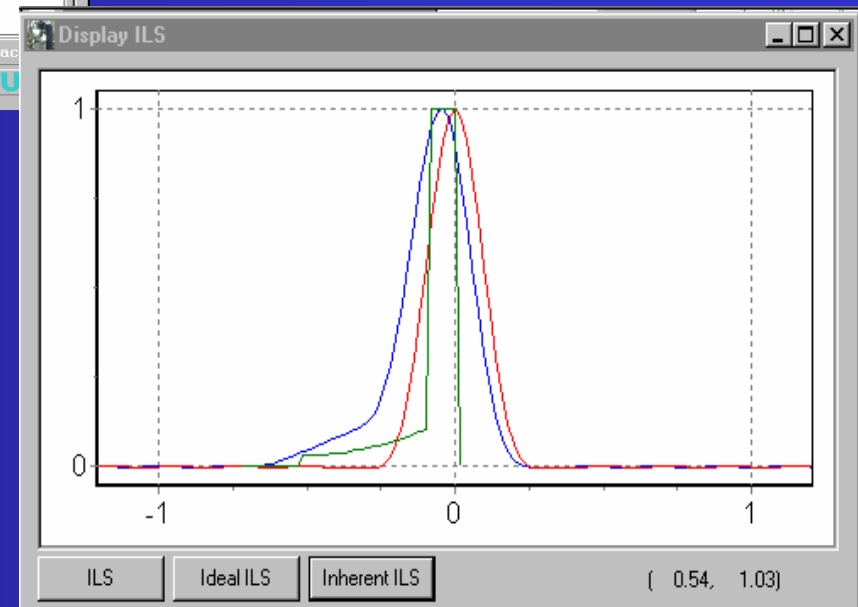
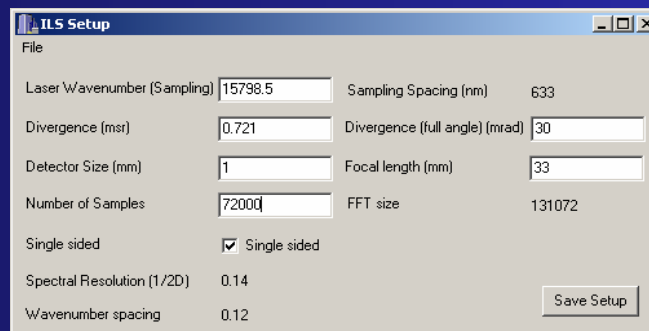
User Interface



Calibration

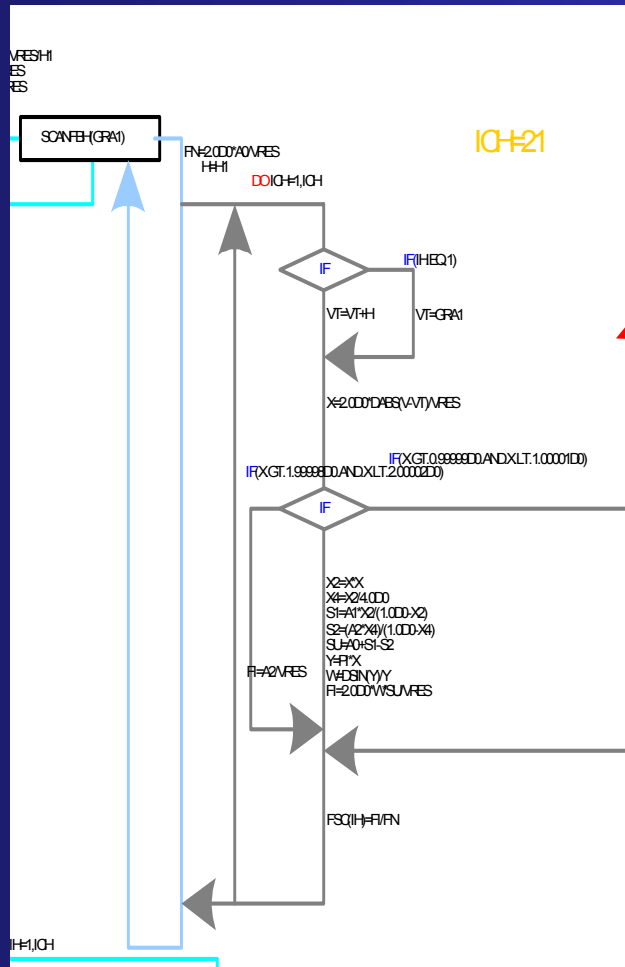


ILS Visualization

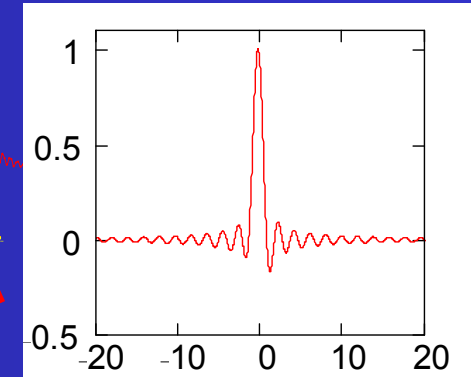


MAPS

INPUT



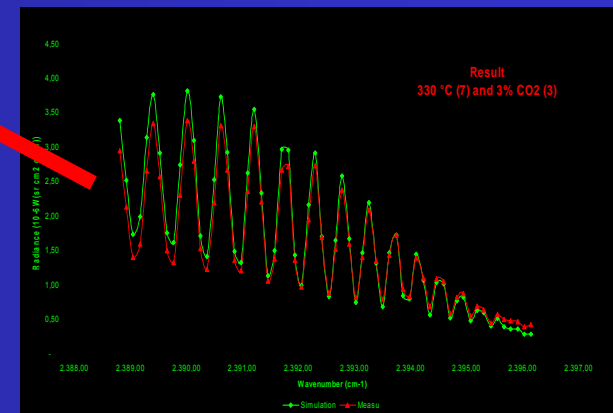
ILS MODULE



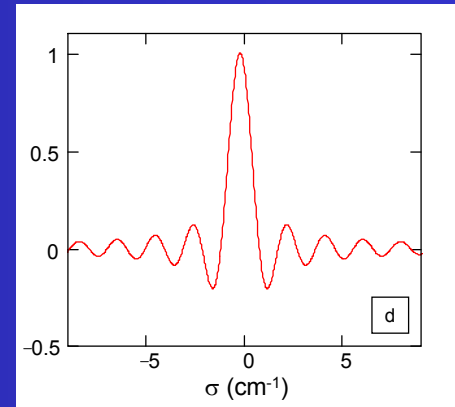
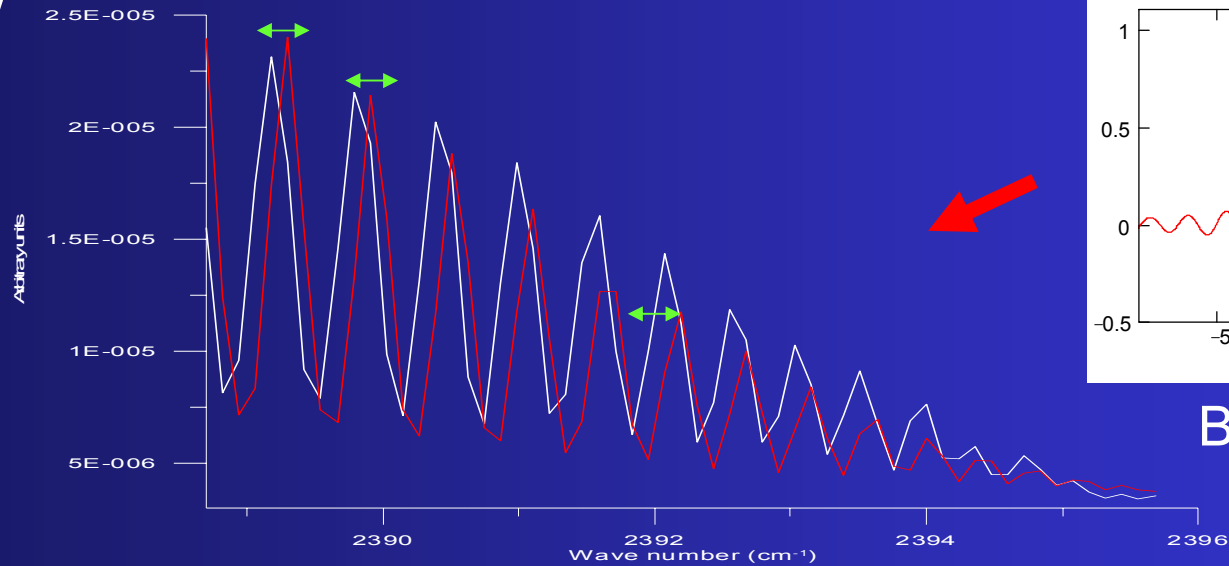
$f_j^0(T, p)$

LBL

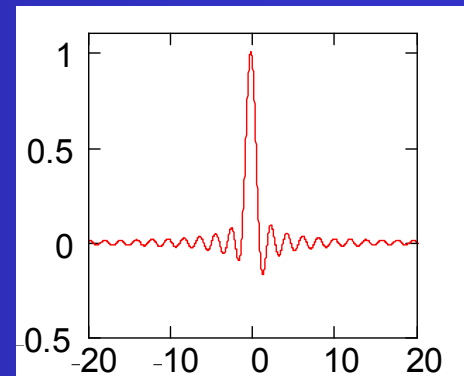
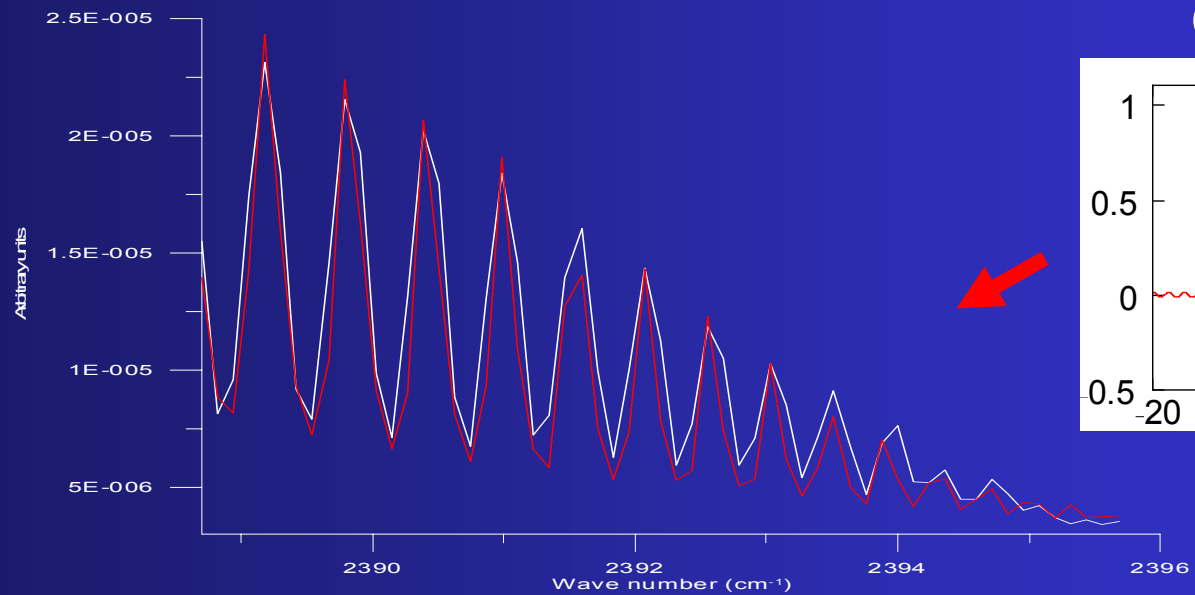
$$k_i(\sigma, T, P) = \sum_j S_{ij}(T) f_{ij}(\sigma - \sigma_j^0, \sigma_j^0, T, p)$$



Implementation



BH ILS



OPAG ILS

Acknowledgements

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Burner measurements were supported financially by ENI (Italy) also.
