

# THERMO-MECHANICAL SCREENING TESTS TO QUALIFY BERYLLIUM PEBBLE BEDS WITH NON-SPHERICAL PEBBLES

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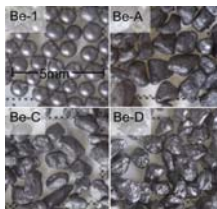
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## Objectives

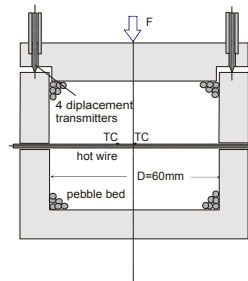
- In present ceramic breeder blankets, pebble-shaped beryllium is used as a multiplier. As candidate material, spherical pebbles with diameters of  $d \approx 1$  mm are considered.
- Non-spherical particles are of significant economical interest. Except of packing factors<sup>1</sup>, no thermo-mechanical pebble bed data exist for non-spherical beryllium grades.
- Qualification tests were performed in helium atmosphere at ambient temperature: Uniaxial Compression Tests (UCTs) combined with the Hot Wire Technique (HWT) to measure the thermal conductivity  $k$ .

## Experimental



**Investigated beryllium grades:**  
 Be-1: spherical 1mm pebbles, NGK, Japan  
 Be-A, Be-C: 2.5mm pebbles, different grain sizes, Bochvar, Russia,  
 Be-D: 2mm pebbles, Materion, USA

**UCT and HWT experimental set-up:** Only  $\approx 120\text{cm}^3$  of non-spherical beryllium grades were available. This resulted in a small set-up with a somewhat reduced measurement accuracy, "screening tests". Therefore, the comparison with the spherical beryllium pebbles was important.

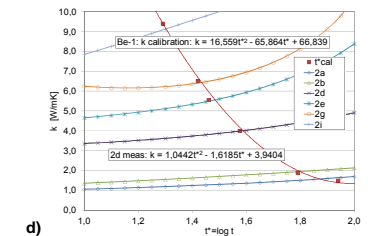
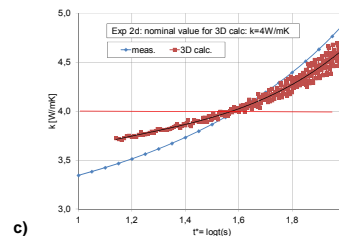
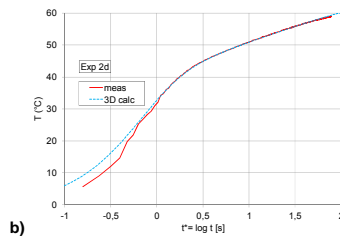
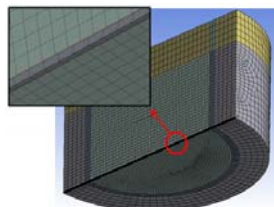


Batch	Exp N°	$\gamma$ (%)	$\sigma_{max}$ (MPa)
Be-1	1	61.6	7.0
Be-1	2	62.4	4.8
Be-A	3	61.8	4.3
Be-A	4	63.2	4.7
Be-C	5	59.7	3.9
Be-D	6	60.9	4.7
Be-D	7	62.1	4.4

↑ **Experimental parameters:** packing factors  $\gamma$  and maximum uniaxial stresses  $\sigma$

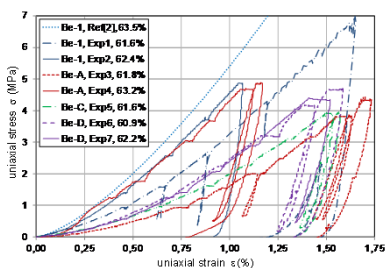
## Hot Wire Modelling

The HW Technique is a standard technique for thermal conductivity  $k$  measurements of materials with *low*  $k$  values in *large* containers. Both requirements are not fulfilled in the present case. Therefore, a detailed modelling of the HWT is required for the interpretation of the HW signal.

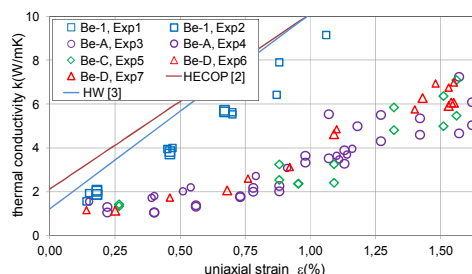


- 3-D transient analyses with the FE ANSYS code were performed modelling in detail the HW (with inner structure) and the container.
- A nominal value for the pebble bed thermal conductivity has been assumed, and then, the measured curve is approached by varying the HTC's at the HW and the container walls. After a first period of time, the slope of an ideal HW temperature curve becomes constant (half-log plot). This is not the case for both the measured and calculated signal.
- Because of the varying slope, the measured and calculated values of  $k$  are not constant. As correct value  $t^*$  that value is taken where measured and calculated values agree (iteration process)
- This procedure is carried out for different values of  $k$  and a calibration curve is obtained. Different curves are determined for spherical and non-spherical pebble beds.

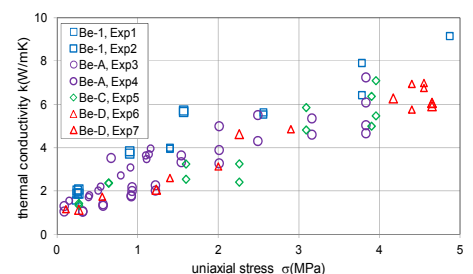
## Experimental Results



↑ **UCT results:** uniaxial stress  $\sigma = f(\text{pebble bed strain } \epsilon)$ . With decreasing packing factor  $\gamma$ , the pebble beds become "softer", (larger strain  $\epsilon$  for a given stress  $\sigma$ ). Be-1 and Exp 4 with Be-A show the stiffest behaviour, the values are, however, below the correlation obtained with a larger experimental set-up<sup>2</sup>.



↑ **HWT results:**  $k = f(\epsilon)$ . For non-spherical pebbles,  $k$  is distinctly smaller than for spherical ones, mainly caused by the softer  $\sigma$ - $\epsilon$  relation. No differences exist between the different non-spherical grades. Again,  $k$  is fairly linear dependent on  $\epsilon$  as found previously<sup>2,3</sup>.



↑ **HWT results:**  $k = f(\sigma)$ .  $k$  for spherical pebbles is at the upper bound of the data which might be caused by different sizes of generated contact surfaces during compression.

## Conclusions

- Compared to spherical pebble beds, the thermal conductivity for non-spherical pebble beds is lower caused by i) the softer bed behaviour (smaller stress  $\sigma$  for a given strain  $\epsilon$  value), and, ii) the generation of smaller contact surfaces because of the non-regular shape.
- For blanket operation, the pebble bed strain is the primary parameter; for softer pebble beds the anticipated increase of the thermal conductivity during heating-up is smaller because of the reduced build-up of thermal stresses.

<sup>1</sup>Reimann, J.; Abou-Sena, A.; Nippen, R.; Tafforeau, P., Fus. Eng. and Des. 88 (2013) 2343-2347 <sup>2</sup>Reimann, J.; Piazza, G.; Harsch, H., Fus. Eng. and Des. 81(2006) 449-454 <sup>3</sup>Reimann, J.; Hermsmeyer, S.; Piazza, G.; Wörner, G., CBBI-9, Toki, Japan, (2000) 199-214