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Microstructure and Mechanical Properties of Zircaloy-4 Cladding Hydrogenated at **Temperatures Typical for Loss-of-Coolant Accident (LOCA) Conditions** A. Pshenichnikov, J. Stuckert, M. Walter anton.pshenichnikov@kit.edu, juri.stuckert@kit.edu, mario.walter@kit.edu Tensile test at room temperature Introduction small amounts of hydrogen as a solid solution can tead to hydrides precipitation, which in turn teads to sufficient degradation of any wome when shall adapting indegrads LOCs contains when after tablooting and burst the invert calding surface aboots any structure of the solid so n that re MPa attempts to describe the influence of hydro are close to phase transformation point and hydro 1100 K 120 s 1375 wpp 1100 K 240 s 2173 wpp 1100 K 480 s 3332 wpp 1200 K 60 s 543 wppm 1 ē Metallography investigations As-received Zircaloy-4 tube showed approximately 13% of true strain and 750 MPa of util led to the reduction of maximal true stress down to 600 MPa. True strain at rupture has risen up as soon as hydrogen was absorbed, it has had an immediate imgact on mechanical pr plasticity drastically. The rupture was in all cases brittle. In extreme cases at the maximum maximal strain was only 1%. In the case of 1100 K and 1200 K the plasticity of alloy still remair (according to Silverth's Iaw for Z). aling in Ar and fast cooling Microstructure of Zircaloy-4 cladding after and in air (5 K/s) results in recrystallization of as-Equilibrium phase diagram of Zr-H system at 1000 K gen of 485 Microhardness test Microhardness tests of annealed and hydrogenated samples were carried The heat treatment led to immediate decrease in microhardness in arison to as-received state. It is usual phenomenon after recrystallization. In the presence of hydrogen microhardness started to increase from the very beginning aiready hydrogenation at 900 K where beat transition was detected only in small local regions near to grain boundaries. The one of the first possible reasons for microhardness increase is β-quenching and martensitic transformation in presence of hydrogen which occur after cooling with 5 K/s. The temperature and hydrogen together will boot § formation process. So at 1100 and 1200 K more β-phase after short time period will be formed, and a fast increase of microhardness increase in level occur. But there is a saturation limit approximately at 320 HV as most of materials will be converted to 6-hydrodes. ek et al., Bull. Alloy Phase Diagr. (1990), 385 le at 1300 K Scanning Electron Microscopy X-Ray diffraction analysis Fractured surface after tensile tests Grinded a Degree of embrittlement vs hydrogen conter Hydrogenation at 1000 K α-Zr #05-0665 ZrH γ-hydride #34-069 ZrH1.66 δ-hydride #34n Ar <u>at 1100 K</u> 'g 240 s -nydride #34 d 0 wppm H 000 K 1330 wppm H -{100}a-Z -{002}α-Zr +-{101}α-Zr ¹¹², -222 200)8 Inten Arbitrary 100)a z 02}a-Z (201)a-z 40 £..... Angle 20.° wppm H ted specimens. All hydride peaks and in Zr matrix. The question of str Hexagonal lattice parameter analysis urized. During the heat treatment in absence of hydrogen the usual process of recrystallization and then phase reases (5 to 10 μm) and after phase transition relative large regions (30-50 μm) of same oriented sub-grains are ample was highly tex ce. The grain size inc Parameter "c" Parameter "a' dinally. Instead typical grain structure a guite complicate mixture e appearance of microsructural pattern caronally, instead uprice gene source a gene compresse moute of exact of the developed. During the cooling phase of hydrogenatids specimens a new acicular prior (or or chase) of martensitic-type was as in all cases brittle even at the lowest obtained hydrogenation degree of 720 wppm H. But there is a fact that at 900 and 1000 K very brittle while at 1100 and 1200 K at the similar hydrogenation degree there are a tot of big needles with plasticity indications we shown a better plasticity (5%) in comparison to 900 and 1000 K (<1%). The phenomenon of such type of plasticity can be 000000000000 w). A scheme of plasticity after hydrogenation above 1100 K 0000000 000000000000 211 nalysis of -0.2° hoxagonal close packed tallice parameters "a" and "c" by means of two independent methods has twoed complicated behaviour troomum latics after hydrogenation. The parameter "was about 3.200" to 0.0006 A at all obtained hydrogen content levels (eith-haod drah). This levels qual to as-received material. The parameter "c" increases continuously from 5.146 (0 wppm H as-received) to 5.160 A (4000 wppm H and furth ydrogenation degrees) (righ-hand d-ahr). Due to this increase the c/a-ratio and elementary outime also increased. The explanation of lattice embrittlement The lattice of Zr consists of atomic layers. And it is common knowledge that the ato layers. Every Zr atom has 4 fee electrons to maintain lattice integrity. In the presence of and H to build a zironium hydride. In this case resist of free electrons must be regrou-interesting feature that hydrogen can build only one bond with subsequent electro embrittement is applicable in the case of Zirconium and his alloys. ce of hydrogen free el Though fracture surfaces at 1100 and 1200 K were brittle a signs of ductility still can be observed. The white stripe in the middle of every needle shows that the needles deformed plastically in comparison to flake-like regions between them. This results are in accordance with tension tests (see on the right-not side of this poster). It was not clear why at the same hydrogenation degree the specimens hydrogenated at 1100 and 1200K still had 5% of plastic strain hile specimens hydrogenated at lower temperatures had <1%. The SEM investigations allow to suggest this kind of ductility as the main reason of this hild exployed accular structure will be more ductile at noom temperature than the specimers hydrogenated at lower temperatures. At 900 and 1000K they lib efully britts. Joss of plasticity because of lack of free electrons. Joss of plasticity because of lack of free electrons. Joecrase the strength of atomic bonds (decohesion) between Zr atomic layers -- lower energy Johanna stresses because of charge redistribution (hydrogen starts acting as a proton after giv connection with his Zr atom in current layer). tron to Zr and repulses another lay Conclusions A lot of optical microscopy data showed, it is impossible to distinguish hydrides from another elements of structure, especially at low hydrogen content level. High magnification SEM observations reveal hydrides at high hydrogen content level. Fracture surface analysis showed that even at lowest obtained hydrogen content the fracture was of mixed type with signs of plasticity. With increasing hydrogen content there was a transition to a brittle flake-like structure with the rests of the α-Zr needles. Tensile tests showed that hydrogen content has a significant impact on mechanical properties, especially on the strain to rupture. The XRD-analysis showed a relationship between hydrogen hardening, annealing softening and hardening due to $\beta \rightarrow \alpha$ transformation during the cooling phase. The XRD-analysis showed the presence of γ , δ -phases of zirconium hydride in all of performed experiments. With the increase of hydrogen content the hydride peak intensity was also increased. Simultaneously the hydrogen should be partially dissolved in the lattice which is indicated by increase of the lattice parameter "c". Because carried out observations have proved only the presence of hydrides and gave not enough information on the hydride structure and distribution, further detailed EBSD and TEM investigations should be performed in order to determine the location, morphology and orientation of hydrides and to separate them from other structural features. The performed experiments can explain the absence of macroscopic hydrides in QUENCH-LOCA experiments. The increased brittleness of some zirconium claddings after QUENCH-LOCA tests could be caused by submicro-scaled hydrides which are distributed in the bulk of material. The proposed scheme of the decohesion mechanism helps to understand the embrittlement of zirconium and other hydride forming alloys. The fact of the increase of the lattice parameter "c" allows to suggest that the decohesion mechanism attributed to increased internal stresses due to hydrogen atoms inside the lattice could be responsible for cladding destruction.

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