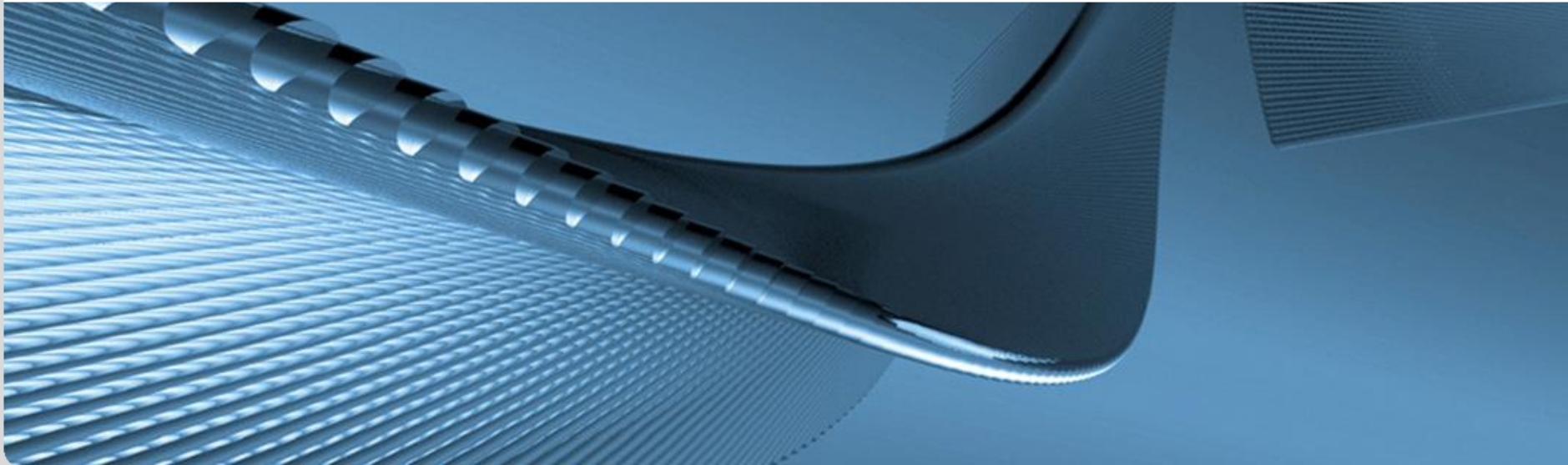


TUNGSTEN

Properties, possible and impossible applications

Michael Rieth

KARLSRUHE INSTITUTE OF TECHNOLOGY – Campus Nord, INSTITUTE FOR APPLIED MATERIALS – Applied Material Physics (KIT, IAM-AWP)



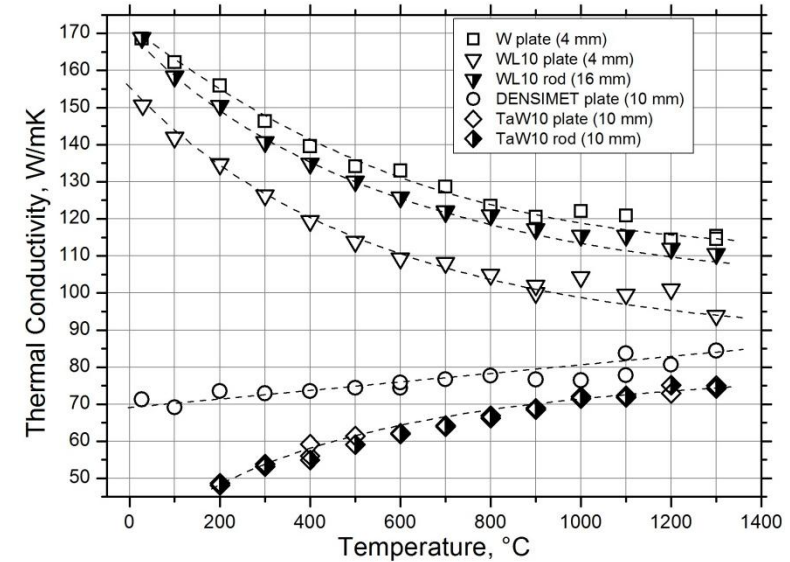
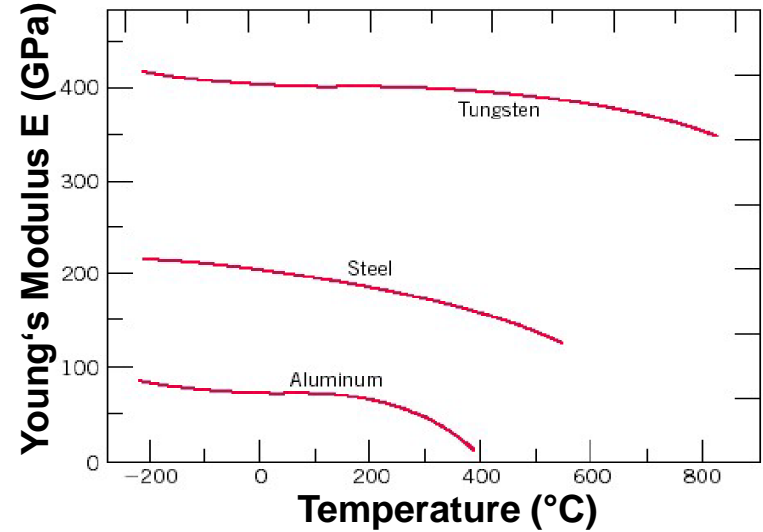
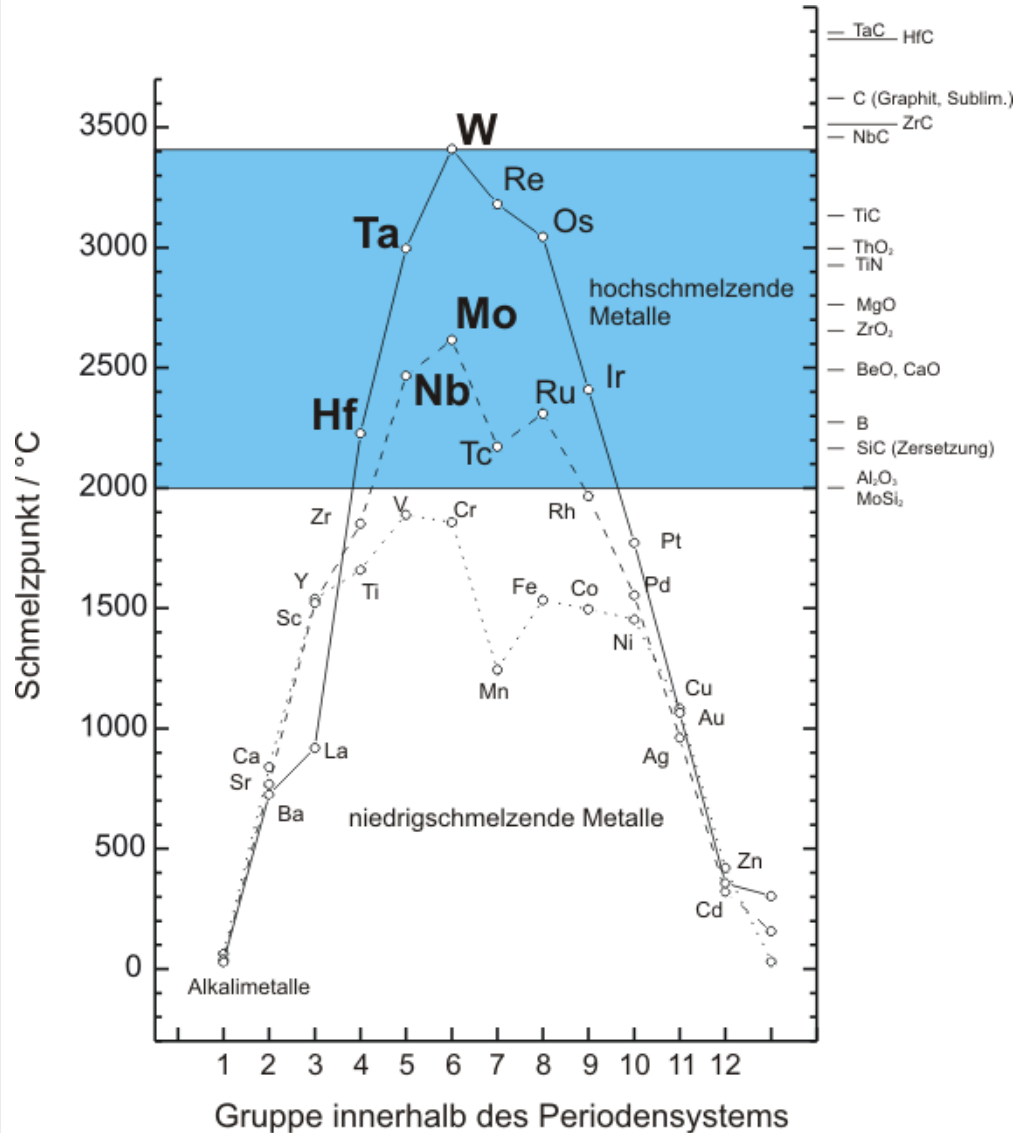
CONTENTS

- Tungsten basics
- Production, resources, applications
- Mechanical properties
- Helium cooled divertor designs
- Design analysis
- Design assessment
- Summary and path forward



TUNGSTEN BASICS

BASIC PROPERTIES



BASIC PROPERTIES

W^{183.85}
74

Stable isotopes W182, 183, **184**, 186, (180)
 Density 19.3 g/cm³
 Crystal structure body centered cubic (bcc)
 Super conductor T_j = 15 mK

Reactions with Non-metals

| | | |
|-----|---------|---|
| C | >800 °C | W ₂ C, WC |
| P | >700 °C | WP ₂ |
| As | >600 °C | WAs ₂ |
| O | >400 °C | WO ₃ (sublim. at 800 °C) |
| S | >400 °C | WS ₂ |
| Se | >480 °C | WSe ₂ (exothermic) |
| F | >RT | WF ₆ (volatile) |
| F+O | >RT | WOF ₄ |
| Cl | >250 °C | WCl ₆ (WOC _l ₄ , WO ₂ Cl ₂) |
| Br | >450 °C | WBr _{6,5,4} |
| I | >550 °C | W ₆ I ₁₂ |

Reactions with Acids/Alkalis

| Reagent | 20 °C | 100 °C |
|-----------------------------------|---------------|---------------|
| HF | none | none |
| HNO ₃ | slight attack | oxidation |
| H ₂ SO ₄ | none | slight attack |
| HCl | none | slight attack |
| H ₃ PO ₄ | none | slight attack |
| H ₂ O ₂ | none | dissolution |
| NH ₄ OH | none | none |
| KOH | none | none |
| NaOH | none | none |
| HCl+HNO ₃ | oxidation | dissolution |
| HF+HNO ₃ | dissolution | dissolution |
| KOH+H ₂ O ₂ | slight attack | dissolution |

BASIC PROPERTIES

Reactions with Compounds

| | | |
|--------------------------------|---------------|--|
| H ₂ O | >RT | WO ₂ (OH) ₂ (volatile) |
| NH ₃ | >600 °C | >3.5wt.% N → fcc W ₂ N, γ-W ₃ N ₄ |
| HF | <600 °C | only little corrosion |
| | >600 °C | volatile WF ₆ |
| HCl | <700 °C | stable |
| H ₂ S | >350 °C | WS ₂ + 2H ₂ |
| SO ₂ | 300 °C | WO ₃ + S ₂ |
| CO | 80-200 °C | tungsten hexacarbonyl |
| | >1000 °C | W ₂ C + CO ₂ (bulk tungsten) |
| SiO ₂ | >2000 °C | slight oxidation |
| SiC | >1100-1900 °C | WC and WSi |
| Al ₂ O ₃ | <1900 °C | compatible in vacuum |
| BeO | <2000 °C | compatible in vacuum |
| MgO | <1500 °C | compatible in vacuum |
| ZrO ₂ | <1600 °C | compatible in vacuum |
| Glass | <1400 °C | stable |

“REASONABLE” ALLOYING ELEMENTS FOR W

| | | | | | | | | |
|----------------------------|-----------|---------------------|----------------------------------|---------------------------|------------------------|---------------------|-----------|-----------|
| M_2W Be | Mg | MW B | MW_2 C $M_{1-x}W$ | M_4W Al | | Y | La | |
| Ti >3wt.% >300°C | V | MW_3 Cr | Mn | MW, M_7W_6 Fe | M_7W_6 Co | MW Ni | Cu | |
| MW_2 Zr | Nb | Mo | | Ru < 3 wt. % | Rh < 2 wt. % | M_3W Pd | Ag | Cd |
| MW_2 Hf | Ta | | MW Re < 26 % | Os < 5 % | MW Ir | MW Pt | Au | |

Insoluble

Intermetallic Phases

Line Compounds

Solid Solution

Pure Tungsten

Grain Stabilized Tungsten „ODS Tungsten“

Potassium Doping

WVM, WVMW,
AKS, etc.
→ Bulb Wire

Oxides & Carbides

- La_2O_3 (e.g. WL10, WL15, WL20)
- CeO_2 (e.g. WC20)
- ThO_2 (e.g. WT20)
- Weld Electrodes
- Y_2O_3 , ZrO_2 , TiC, HfC, etc.

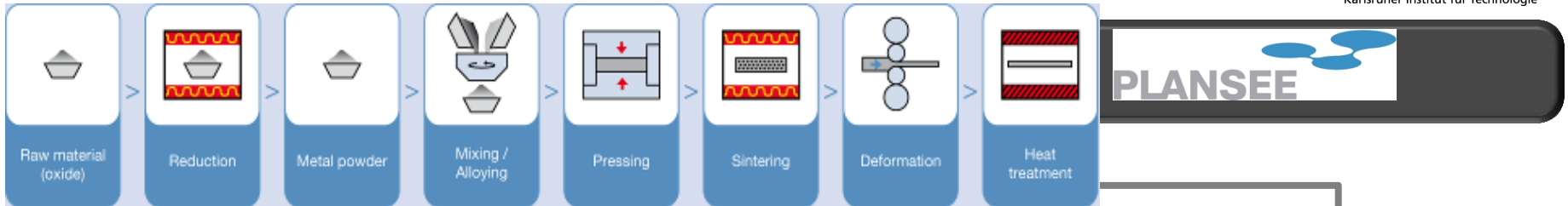
„Heavy Metals“ (Two Phases)

- W-Ni-Fe (e.g. Densimet, Inermet)
- W-Cu
- Functional Applications

Alloys (Solid Solution)

- W-Re (<26%)
→ only commercial alloy
- W-V
- W-Ta
- W-Mo
- W-Ti
- W-Nb
- Even more brittle as pure tungsten !!!

PRODUCTION ROUTES



- Blending
- Pressing
- Sintering
- Hot Forming

- Blending with Binder
- Injection Molding
- Debinding/Sintering
- HIP

- Ball Milling
- Encapsulation
- HIP/Hot Forming

This is so far the only large-scale production route which could handle 500 tons of W (or more) needed for power plant applications.

- + Mass Production
- + Nearly Finished Products
- + Homogenous Microstructure

- S. Antusch, KIT
- J. Opschoor, ECN

- + Near Net Shape
- + Fine Microstructure
- + Full Scale Production Route

- H. Kirushita, IMR
- N. Baluc, PSI
- A. Muñoz, CIEMAT

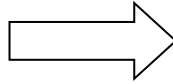
only in very small amounts

COMMERCIAL PRODUCTION ROUTE

WO₃ powder



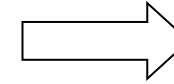
powder reduction



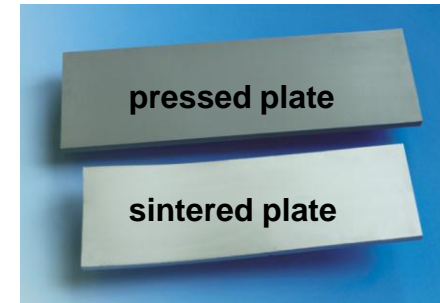
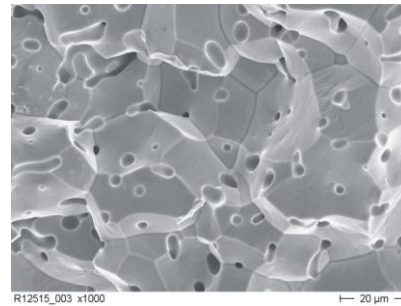
W powder



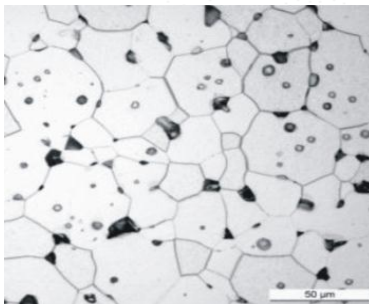
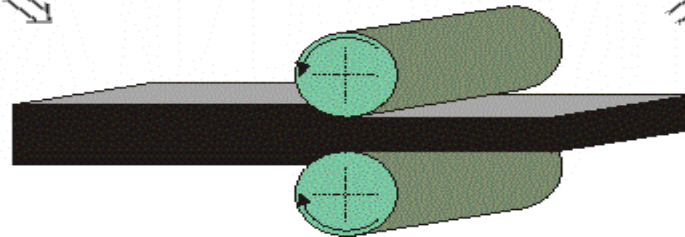
**pressing
sintering**



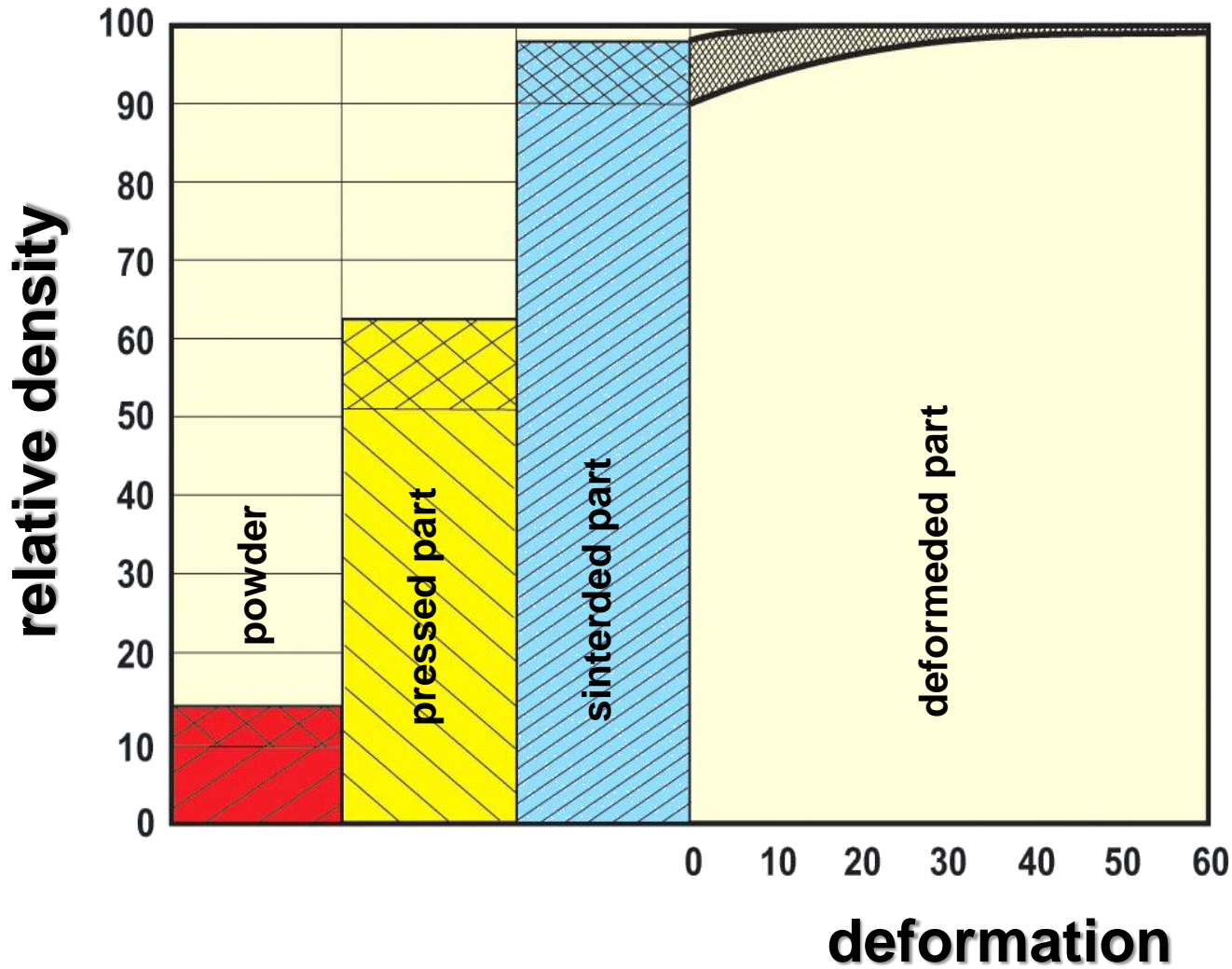
**sintered W part
(fracture surface)**



**thermomechanical treatment
(deformation & annealing to adjust properties)**

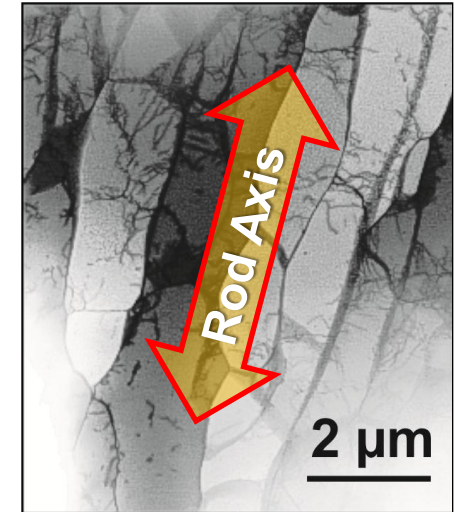
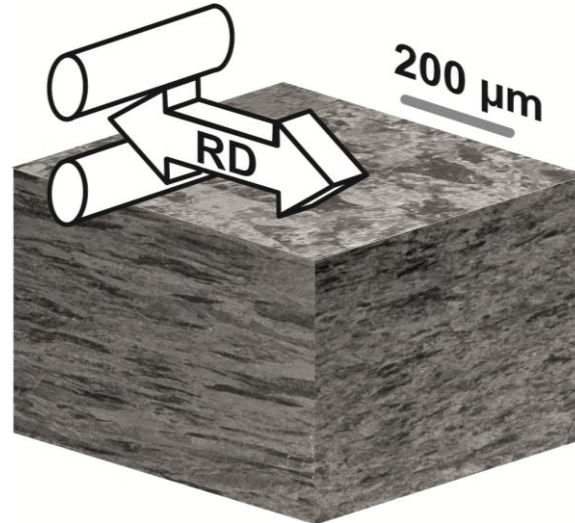
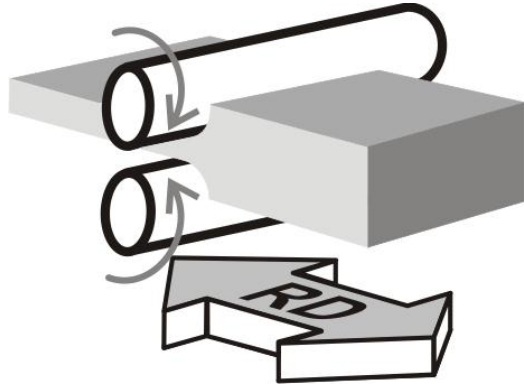


COMMERCIAL PRODUCTION ROUTE

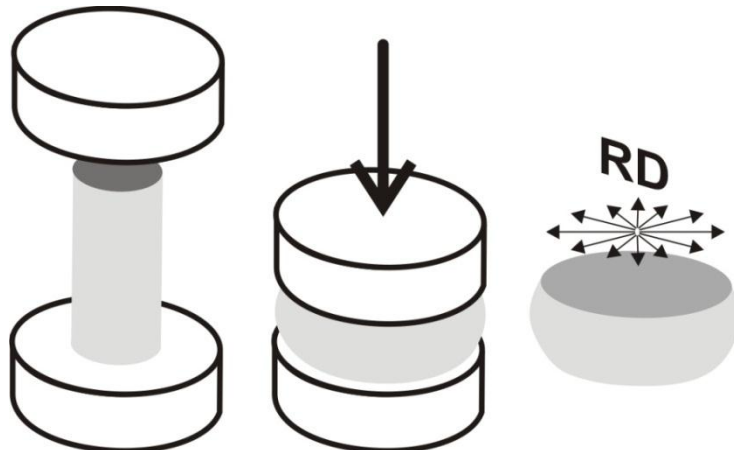


COMMERCIAL SEMI-FINISHED W PRODUCTS

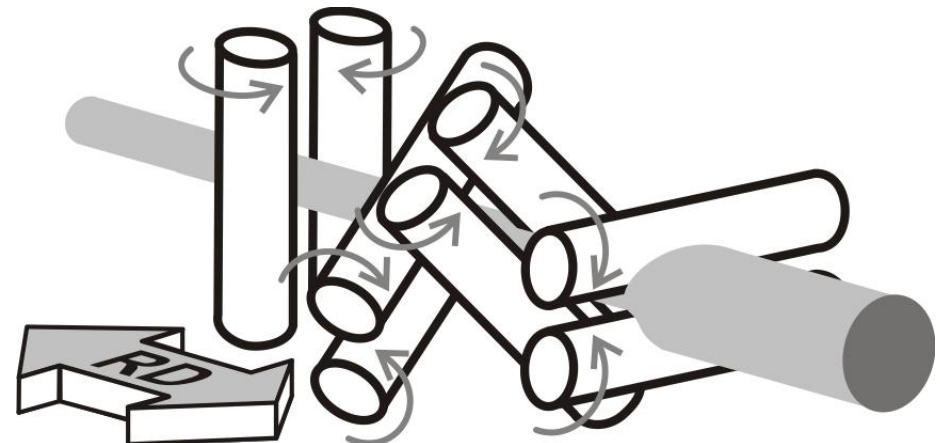
Rolling Plates



Forging Round Blanks

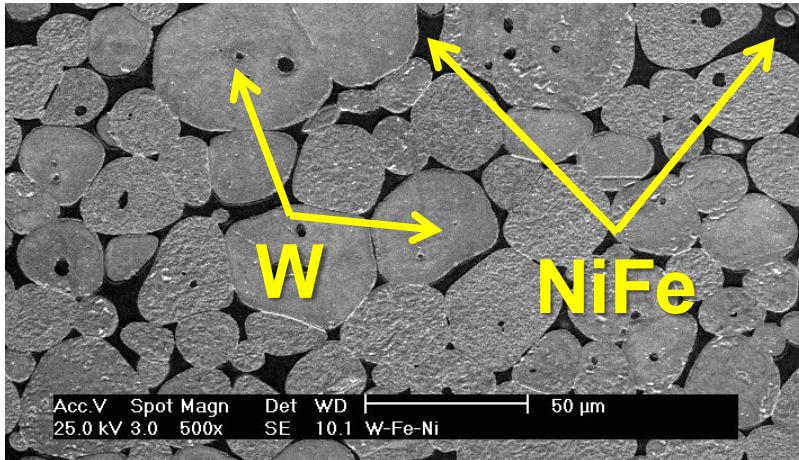


Rolling/Swaging Rods

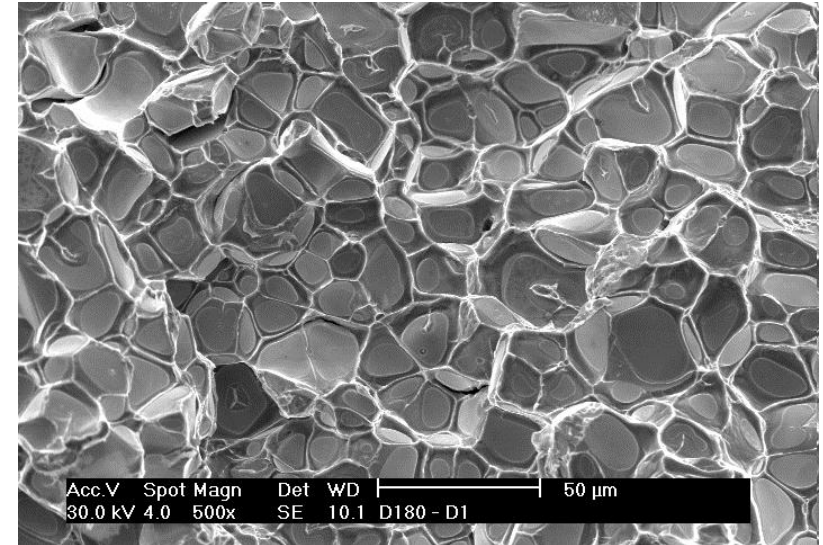


MICROSTRUCTURE OF “HEAVY METALS”

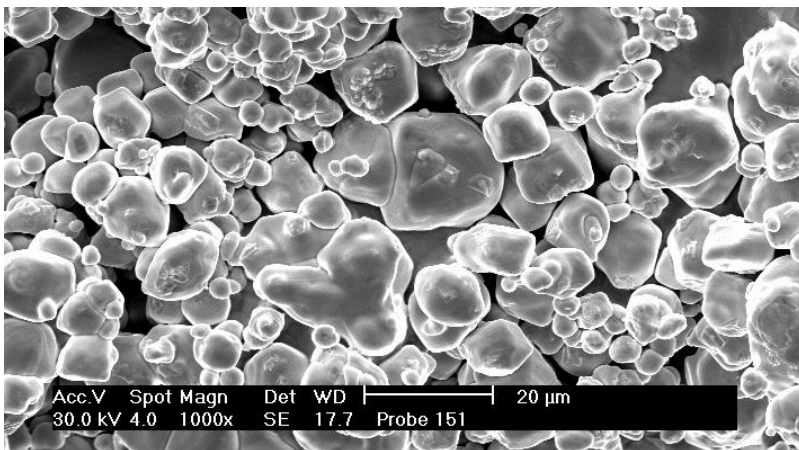
DENSIMET D180, W-3.5Ni-1.5Fe



Cold fracture surface



W-Cu, hot fracture surface



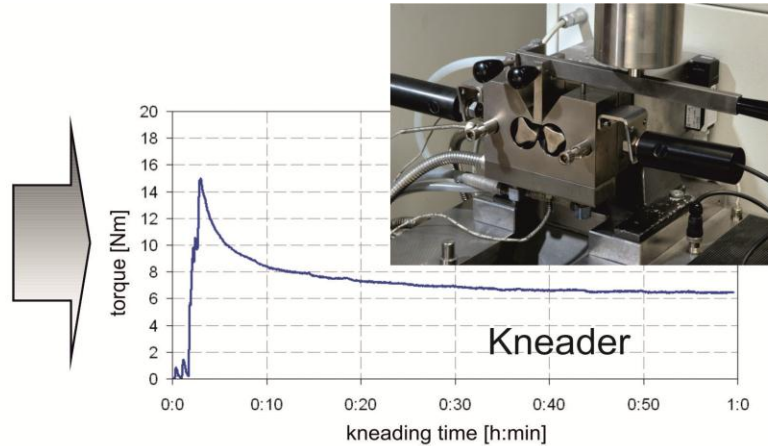
DENSIMET D180

| | |
|---------------|-------------------------|
| Density | 18 g/cm ³ |
| Young's mod. | 380 GPa |
| Therm. Cond. | 83 W/mK |
| Therm. Exp. | 5.5x10 ⁻⁶ /K |
| ferromagnetic | |

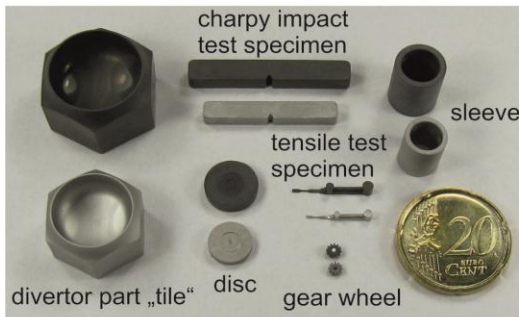
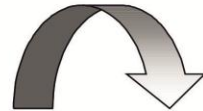
POWDER INJECTION MOLDING



Powder + Binder



Feedstock



Green parts (dark)
Finished parts (bright)



debinding; pre-sintering + HIP



Injection molding
of green parts

→ S. Antusch, IAM-WPT, 2011

POWDER INJECTION MOLDING

Materialherstellung:

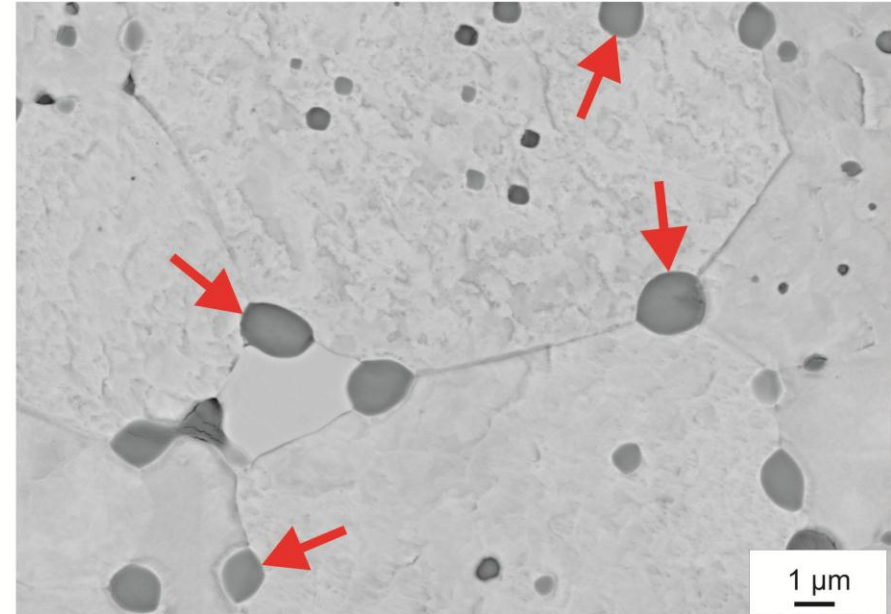
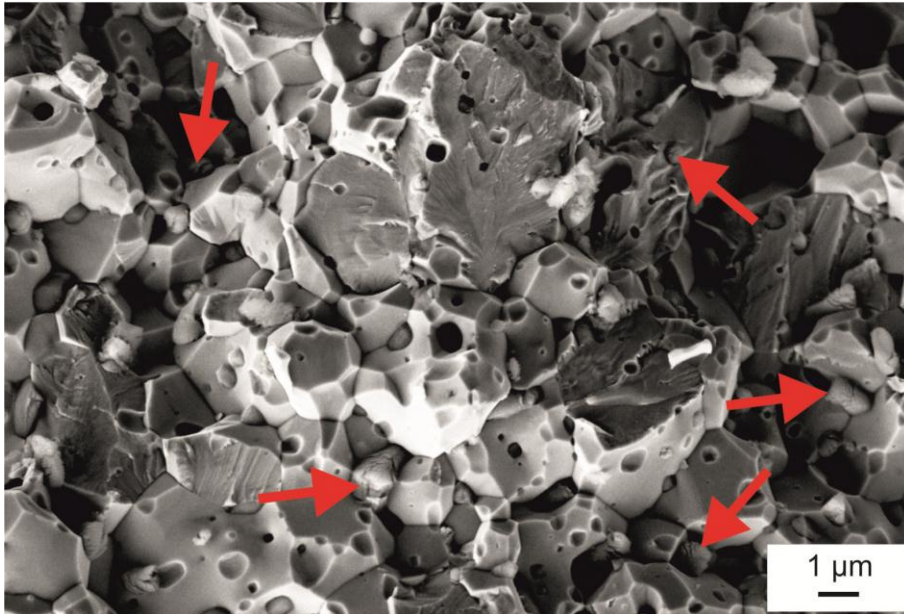
Mechanisches Legieren (Dotieren)

- 2 h / n-Hexan / ZrO_2 Kugeln/Becher

$W-2La_2O_3$ / $W-2Y_2O_3$ / $W-1TiC$...

Thermische Prozessführung:

- Vor-Sintern (1800 °C, 2 h, H_2) +
- HIP Prozess (2100 °C, 2500 bar, 3 h, Ar)



SEM Mikrostruktur (Bruchfläche) und Schliffbild für $W-2La_2O_3$, die Pfeile zeigen La_2O_3 -Partikel

Material-Eigenschaften:

Vickers-Härte: 586HV0.1

Dichte: 96.5 – 97.2 % TD

→ S. Antusch, IAM-WPT, 2011

POWDER INJECTION MOLDING

Materialherstellung:

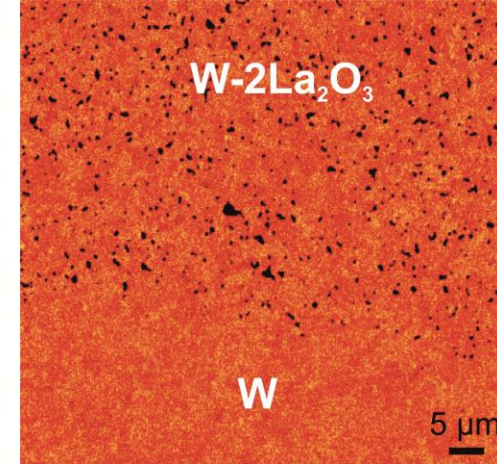
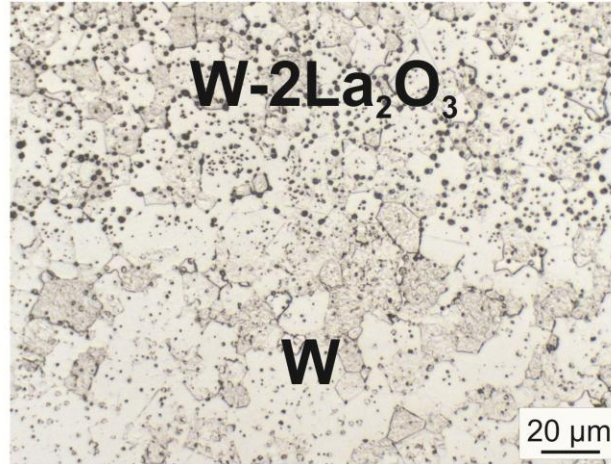
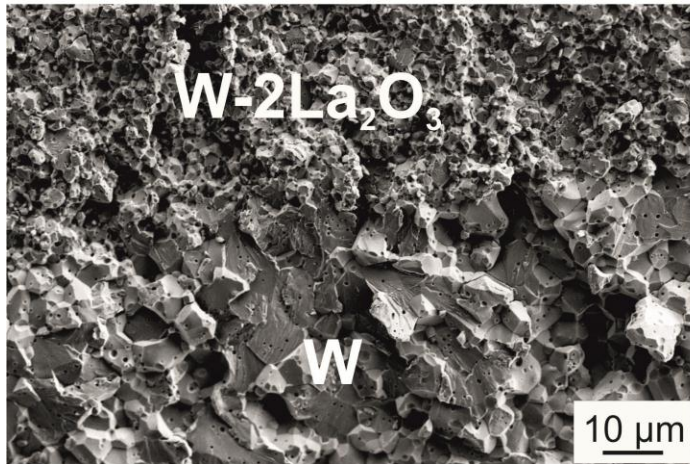
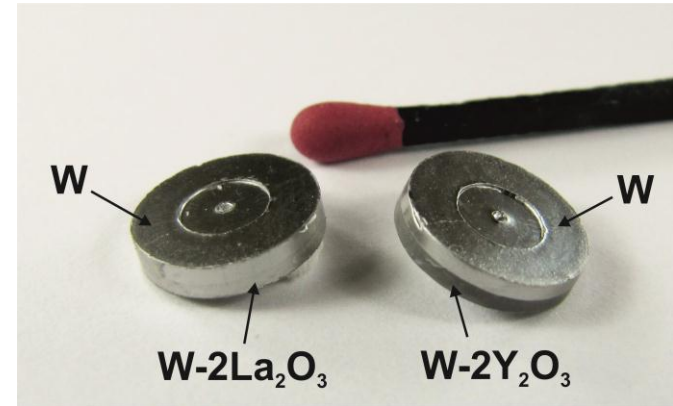
Mechanisches Legieren (Dotieren)

- 2 h / n-Hexan / ZrO_2 Kugeln/Becher

$W+W-2La_2O_3$ / $W+W-2Y_2O_3$ / $W+W-1TiC...$

Thermische Prozessführung:

- Vor-Sintern ($1800\text{ }^\circ\text{C}$, 2 h, H_2) +
- HIP Prozess ($2100\text{ }^\circ\text{C}$, 2500 bar, 3h, Ar)



SEM Mikrostruktur (Bruchfläche)

$W+W-2La_2O_3$

⇒ Fügezone: frei von Rissen und Spalten ✓

⇒ Materialverbund erfolgreich ✓

SEM Mikrostruktur (Schliff) und AES-Map $W+W-2La_2O_3$

Rot: W
Schwarz: La_2O_3

→ S. Antusch, IAM-WPT, 2011

2

PRODUCTION,
RESOURCES,
APPLICATIONS

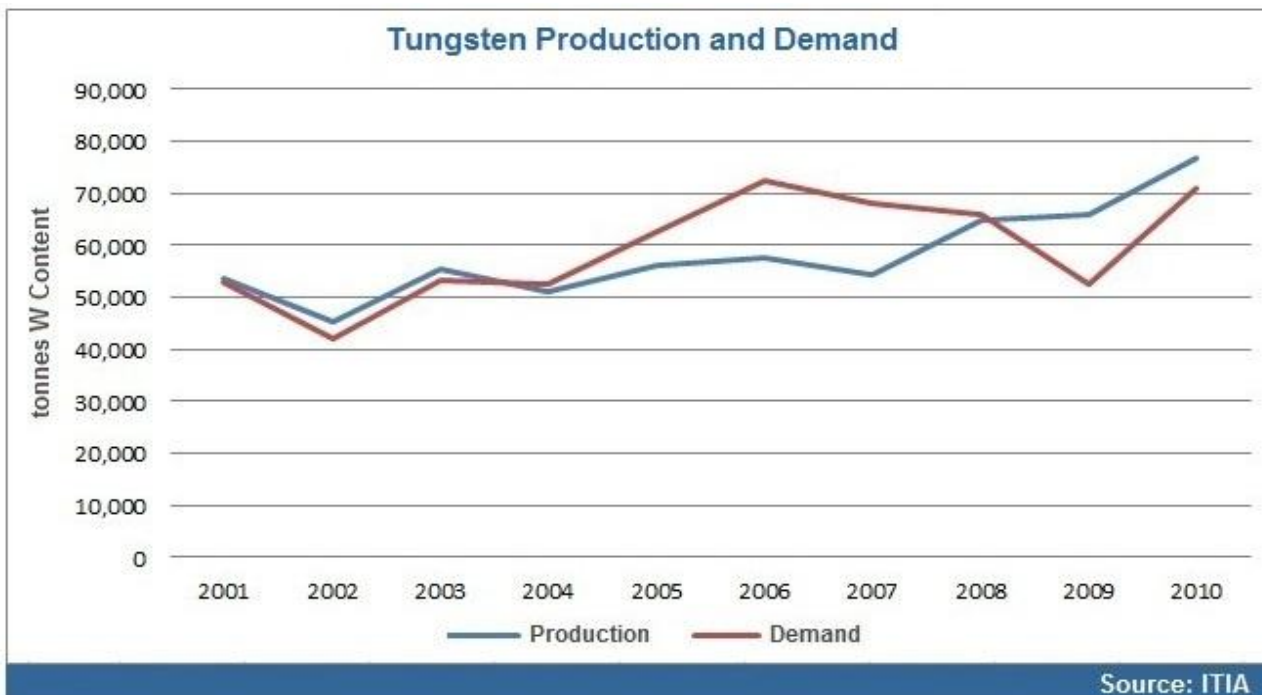
PRODUCTION

| Country/Continent | Production (tonne W) | Country/Continent | Production (tonne W) |
|-------------------|----------------------|-------------------|----------------------|
| China | 67,000 | Peru | 550 |
| Russia | 2,800 | Canada | 400 |
| Bolivia | 1,200 | Thailand | 250 |
| Vietnam | 1,150 | Brazil | 250 |
| Austria | 1,000 | Spain | 250 |
| Portugal | 800 | Mongolia | 200 |
| Africa | 800 | Other | 200 |

Source: ITIA



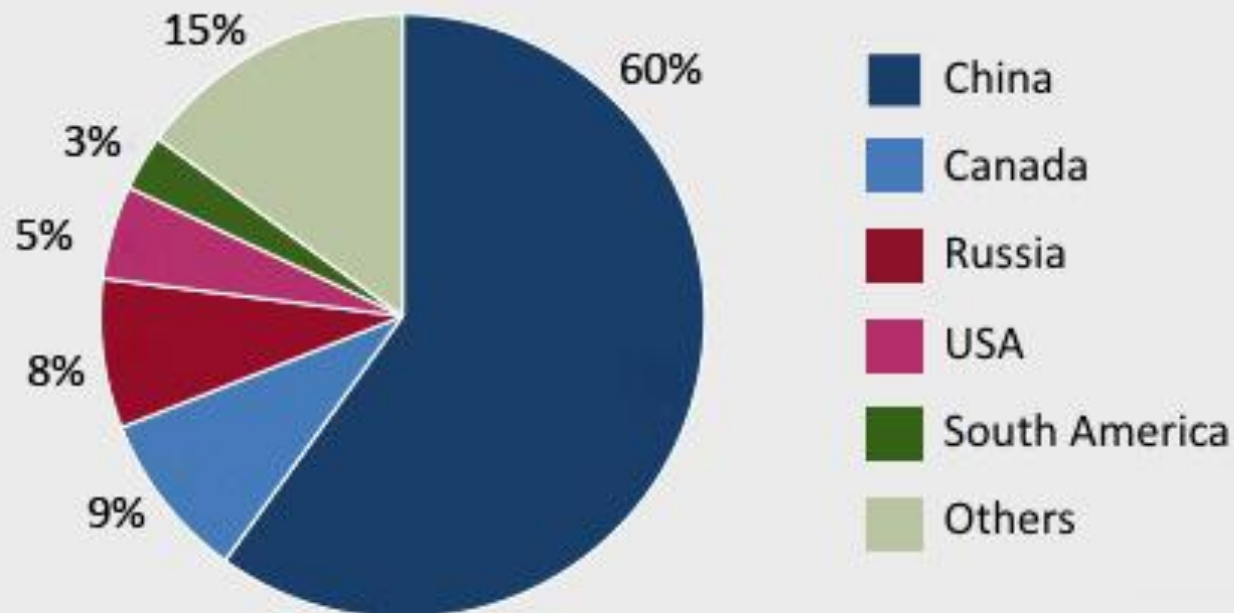
Chinese character
for tungsten



INTERNATIONAL
TUNGSTEN INDUSTRY
ASSOCIATION

RESERVES

Tungsten Reserves
(3 million tonnes, W content)

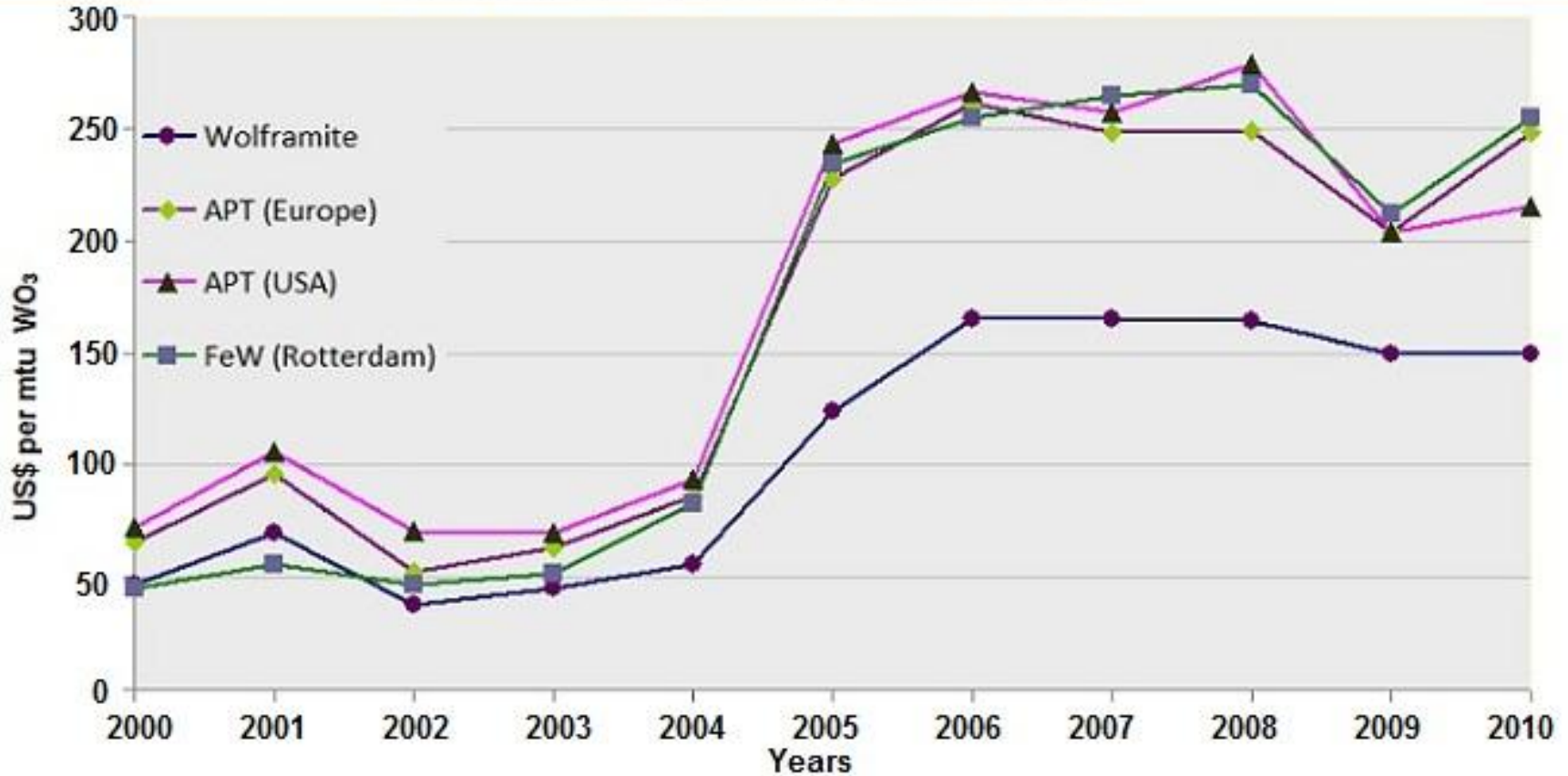


Source: USGS



U.S. Geological
Survey

Metal Bulletin Quotations (Annual Average)*



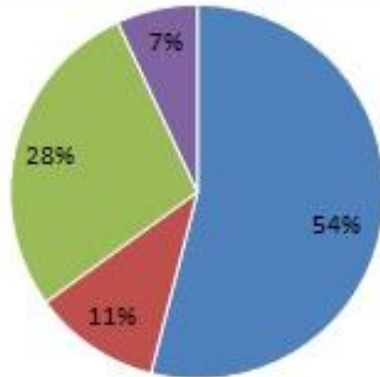
- *A metric ton unit (mtu) is 10 kg*
- *A metric ton unit of tungsten trioxide (WO₃) contains 7.93 kg of tungsten*

INTERNATIONAL
TUNGSTEN INDUSTRY
ASSOCIATION

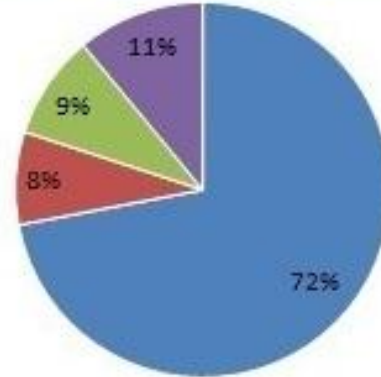


APPLICATIONS

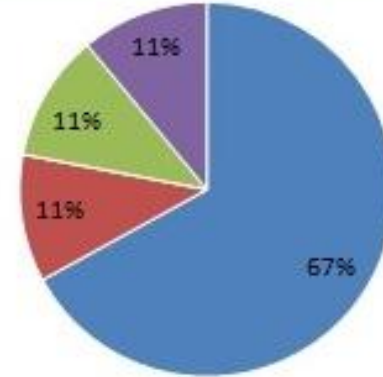
Primary Uses



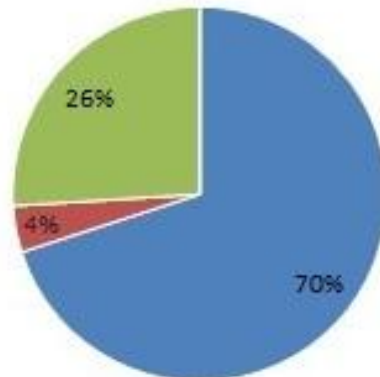
China



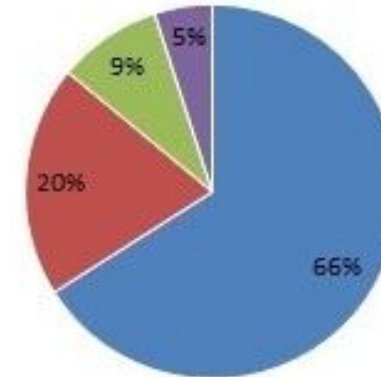
Europe



Japan



Russia



USA

- Cemented Carbide
- Mill Products
- Steels/Alloys
- Others

Estimated global consumption 2010: Total 71,000t W (virgin demand), 95,000t W consumption (including scrap)

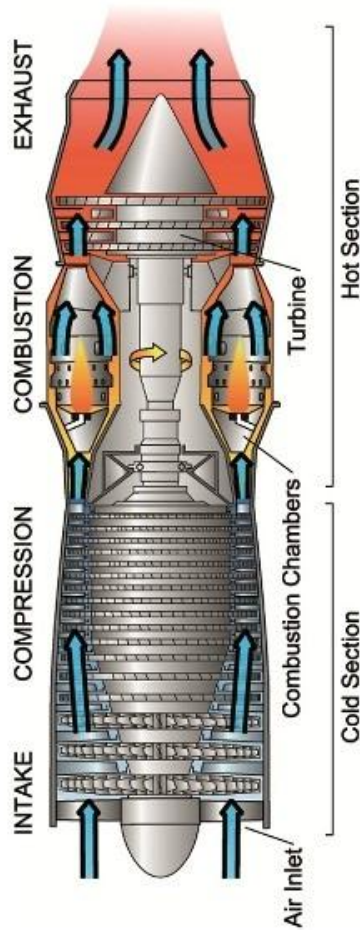
APPLICATIONS

Cemented Carbides



Coated inserts indicating the manifold geometries which exist to different cutting operations

Steel & Superalloys



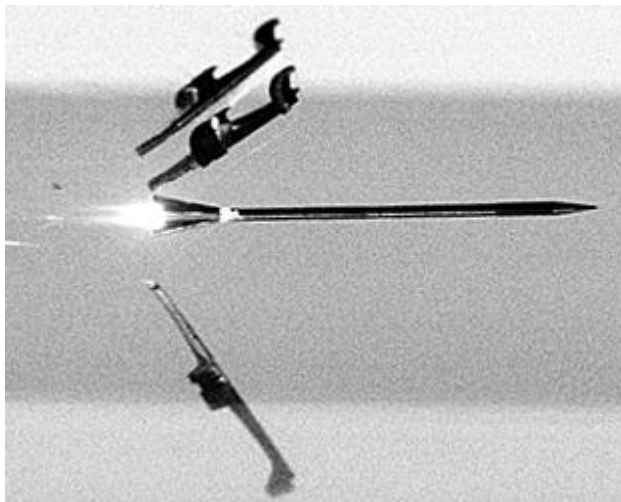
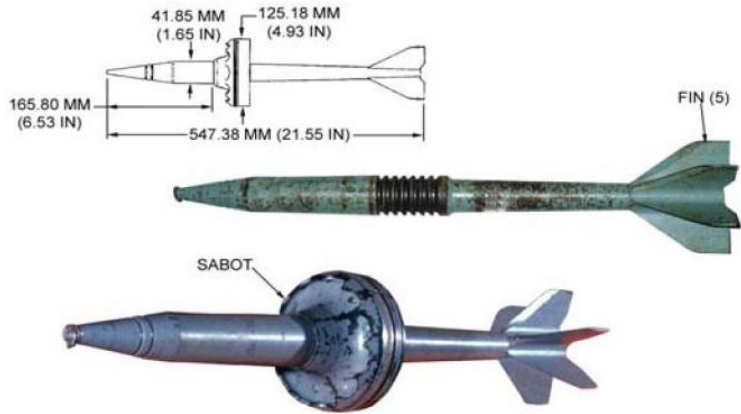
Design of a typical gas turbine jet engine. Turbine blades are made of tungsten-containing superalloys

| Typical Compositions of Selected High Speed Steels (%) | | | | | | |
|--|------|-----|-----|------|-----|-----|
| Grade | C | Cr | Mo | W | V | Co |
| T-1 | 0.75 | - | - | 18.0 | 1.1 | - |
| M-2 | 0.95 | 4.2 | 5.0 | 6.0 | 2.0 | - |
| M-7 | 1.00 | 3.8 | 8.7 | 1.6 | 2.0 | - |
| M-42 | 1.10 | 3.8 | 9.5 | 1.5 | 1.2 | 8.0 |



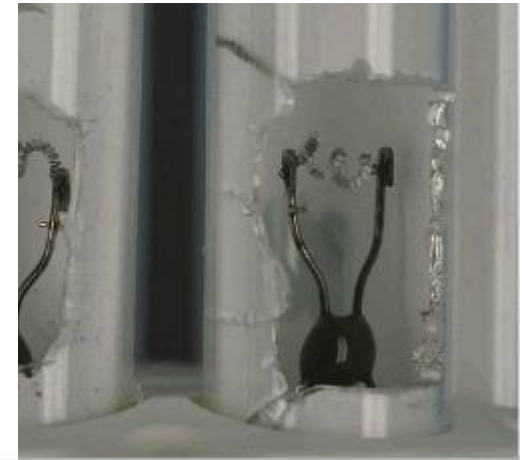
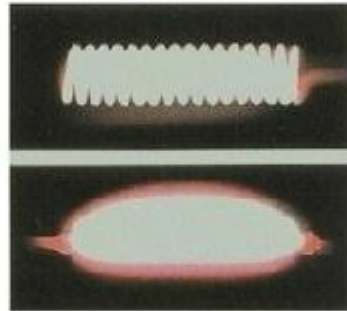
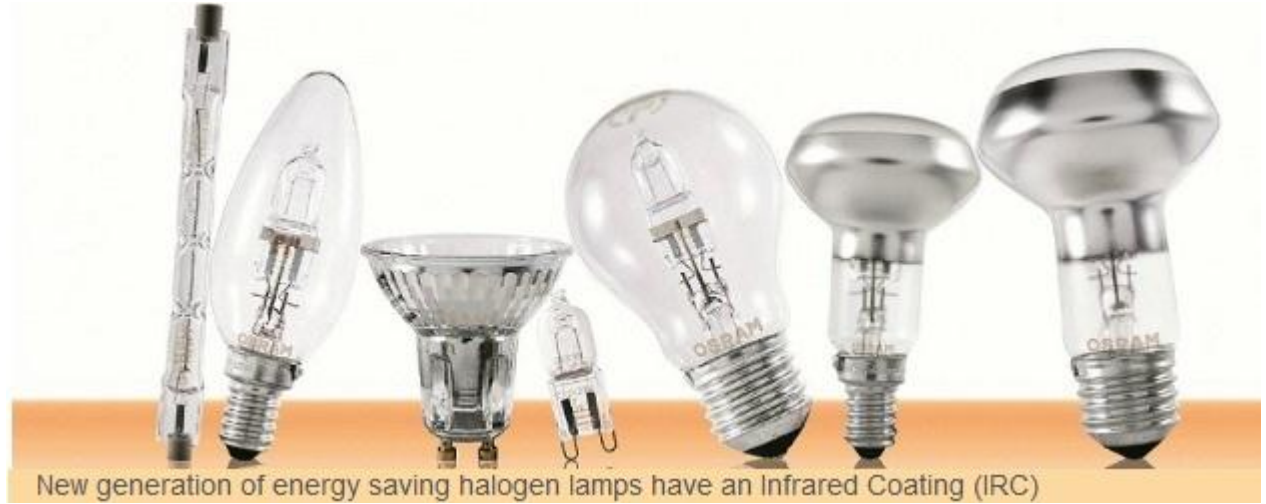
APPLICATIONS

Heavy Metal



APPLICATIONS

Lamp Industry

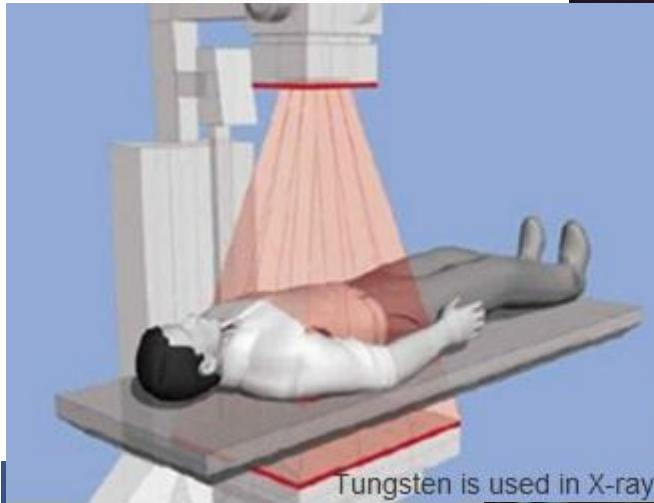


Modern automotive lighting - comparison of halogen lamp (left) and discharge lamp (right)

lectrodes

APPLICATIONS

Electronic & Electric



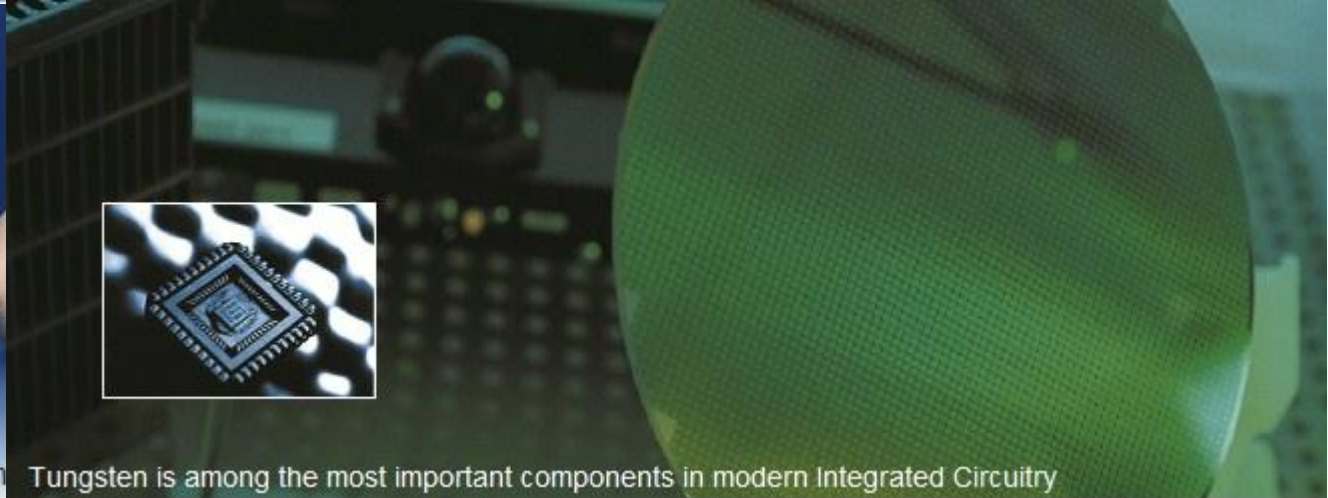
Tungsten is used in X-ray tubes for medical investigations



Tungsten rod electrodes are used for inert gas welding



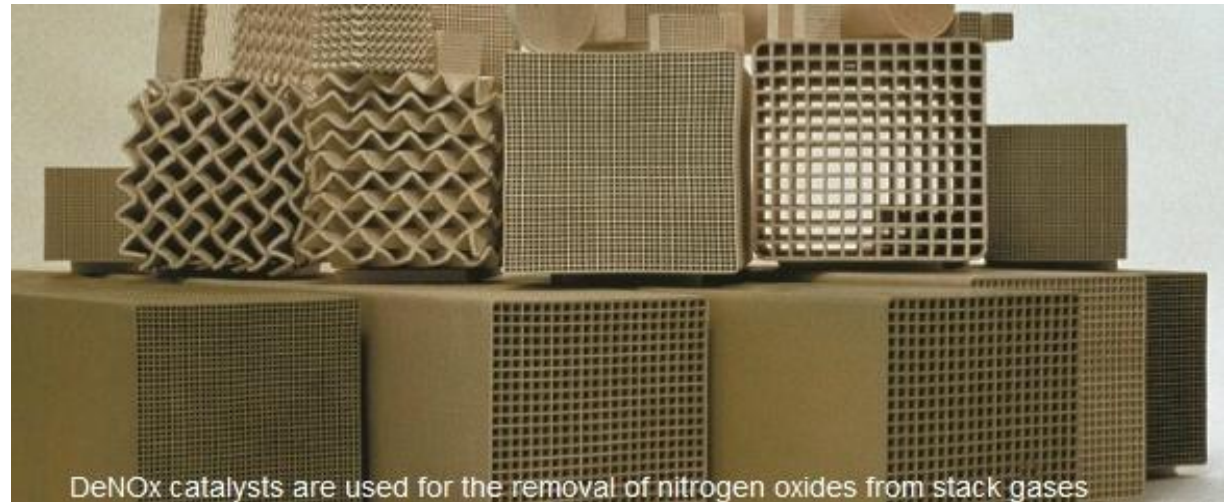
Tungsten parts are used for high



Tungsten is among the most important components in modern Integrated Circuitry

APPLICATIONS

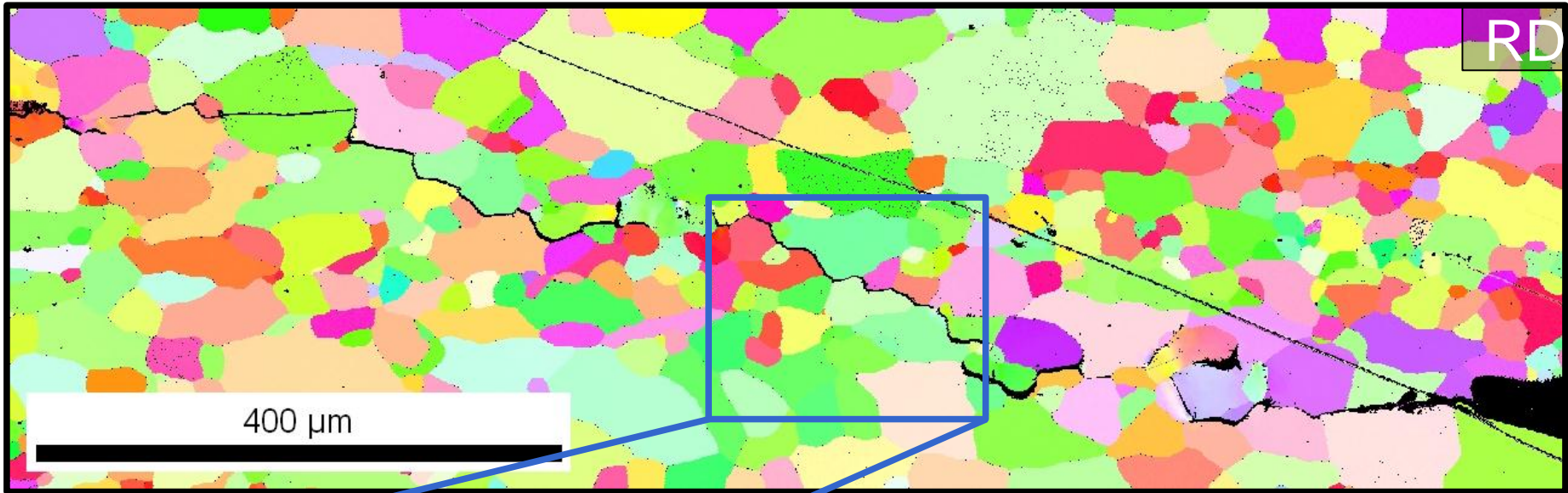
Chemistry



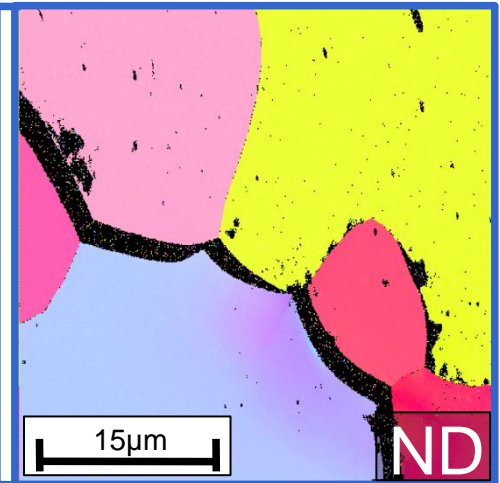
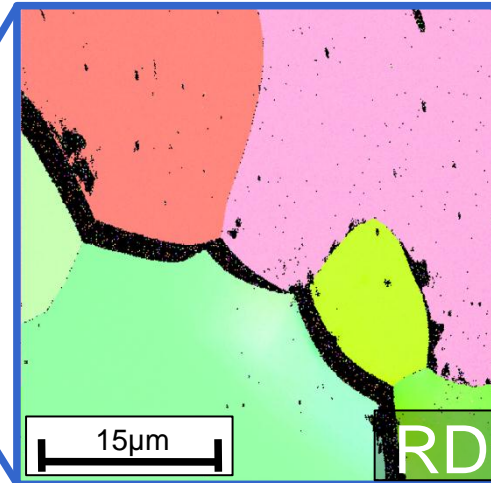
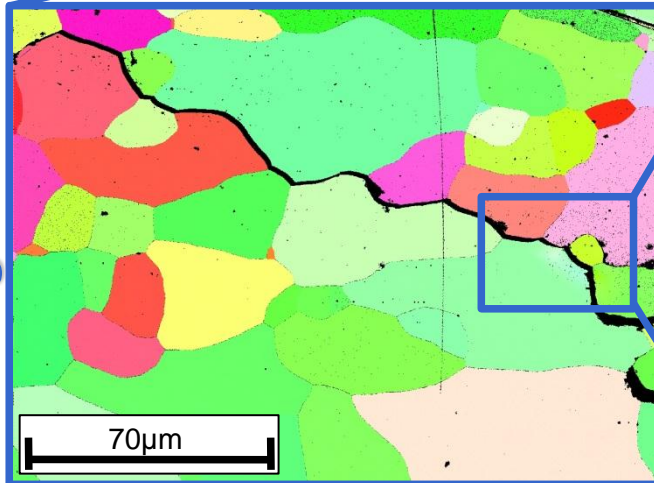
B

MECHANICAL PROPERTIES

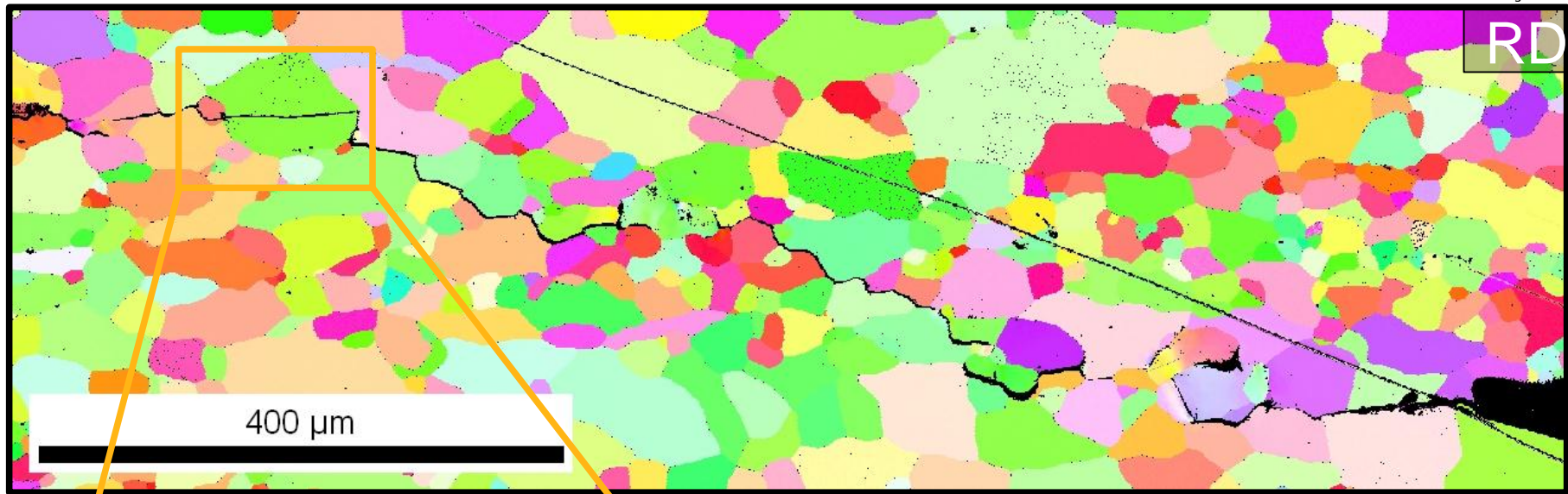
FRACTURE BEHAVIOUR/DUCTILITY/BRITTLINESS



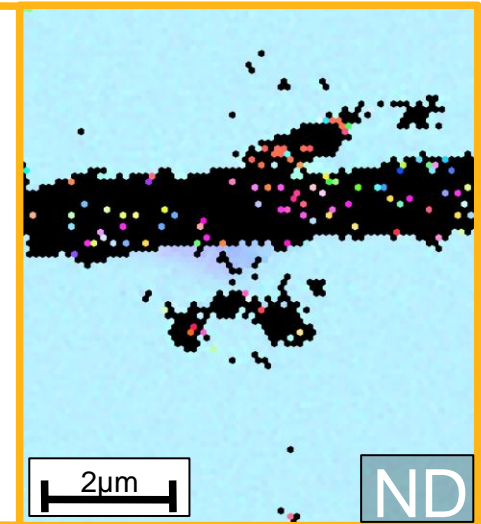
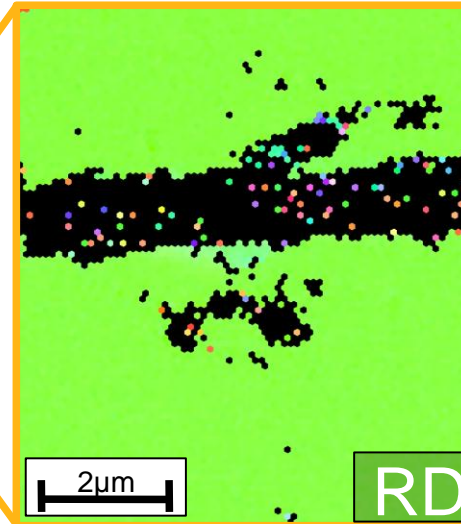
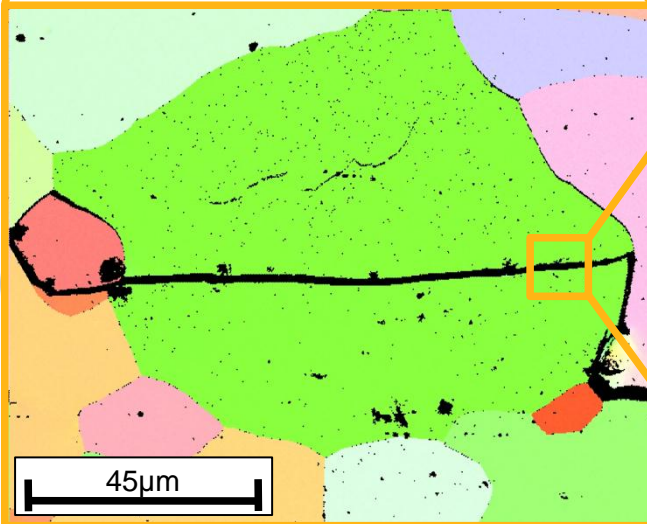
inter-granular



FRACTURE BEHAVIOUR/DUCTILITY/BRITTLINESS



trans-granular

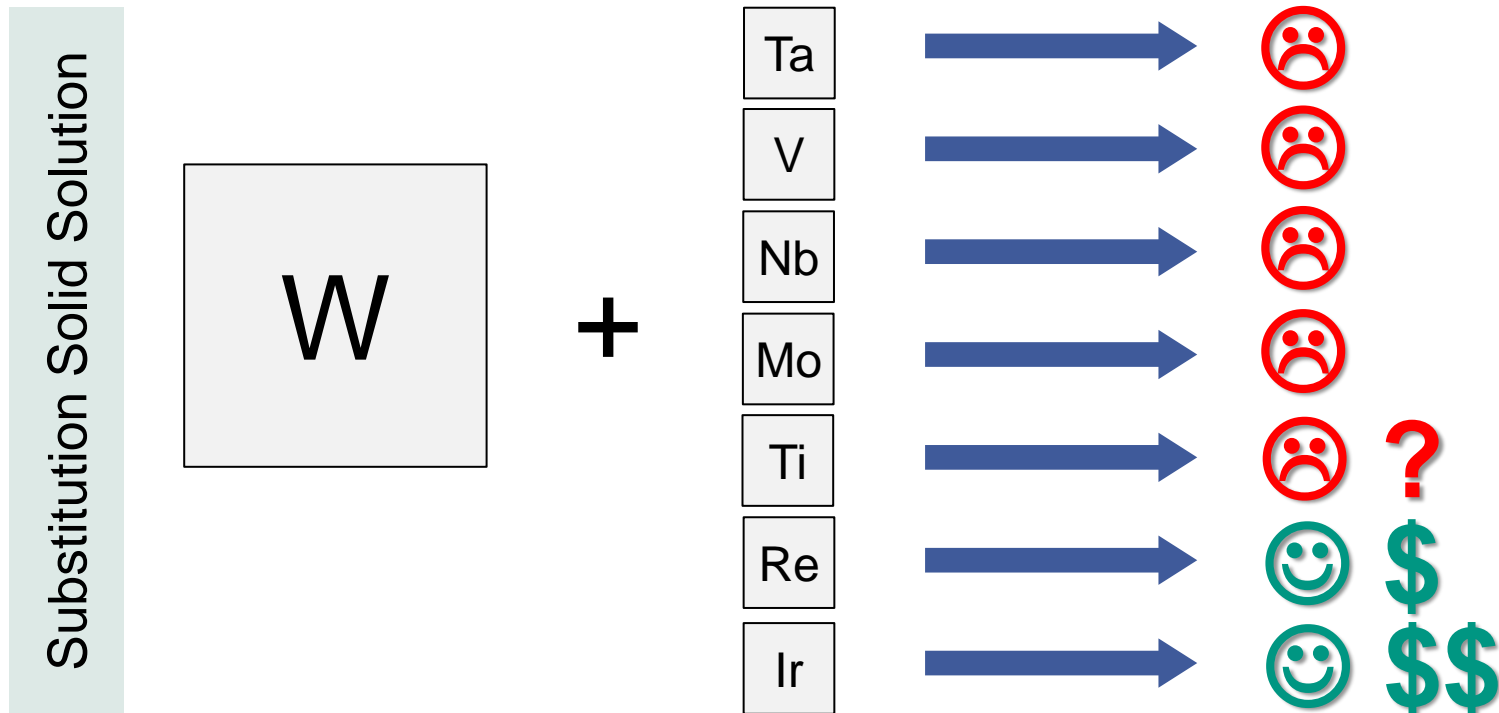


DUCTILISATION

Known Strategies

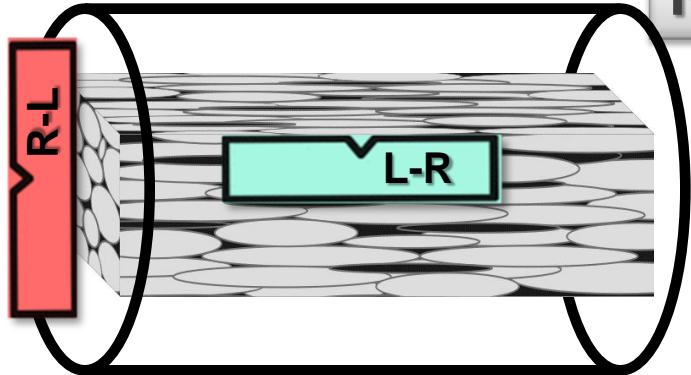
1. Nanostructuring
2. Composites
3. Alloying

→ **Small quantities only!**
→ **Not yet available!**



Conclusion: For large-scale applications we have to live with the intrinsic brittleness of tungsten materials!

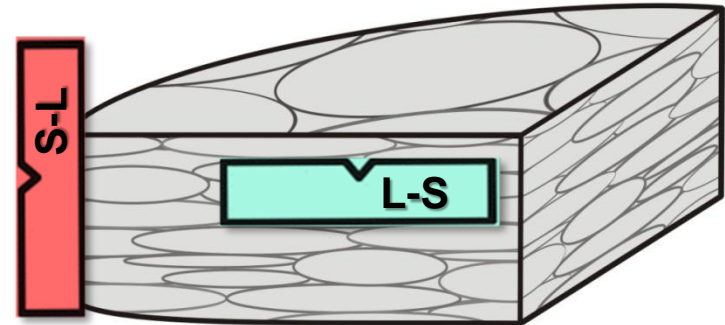
Rods



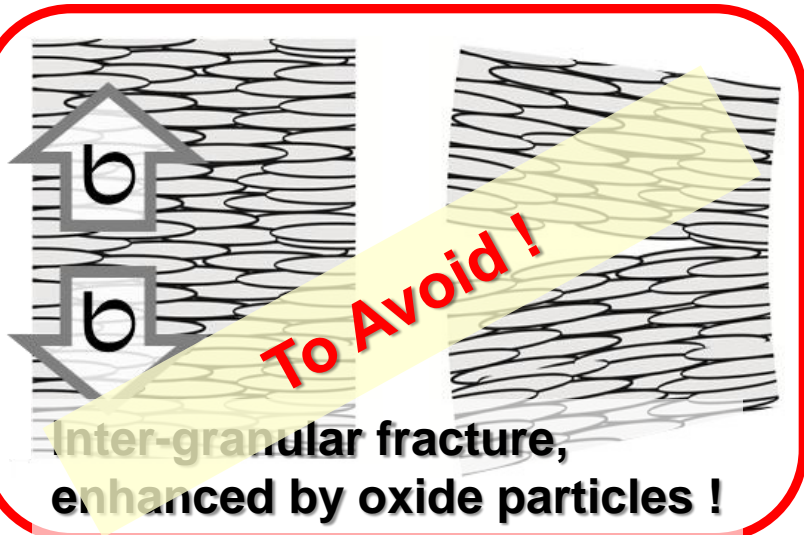
Bundle of „Fibres“

Plates

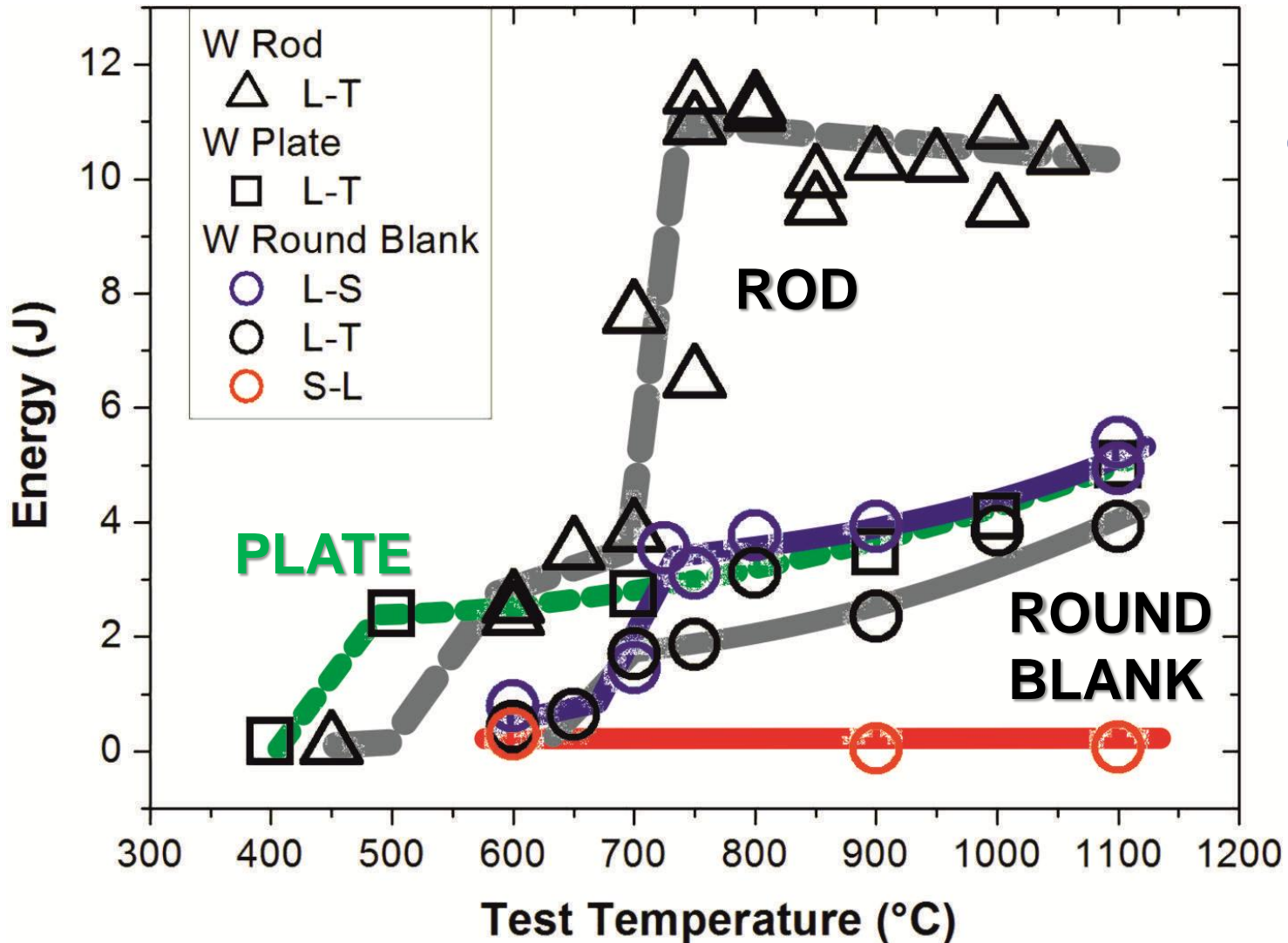
Round Blanks



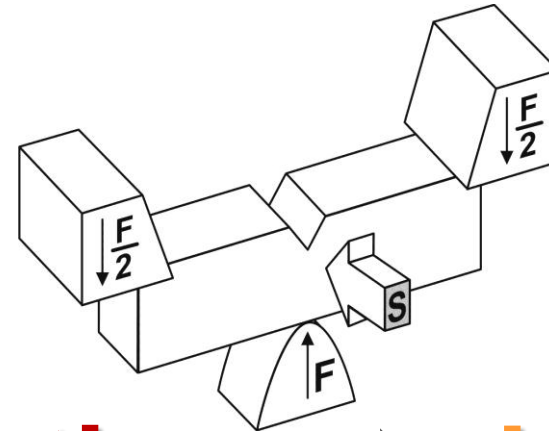
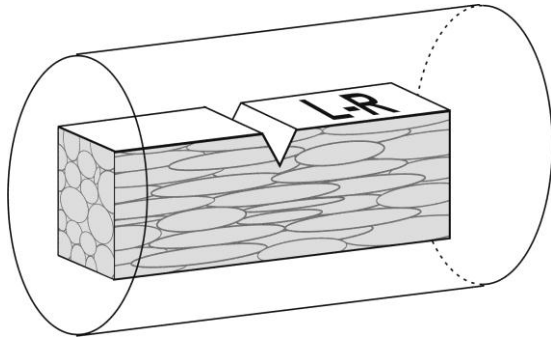
Stack of „Pancakes“



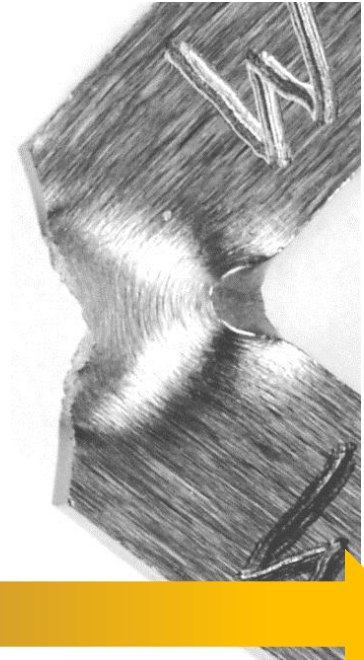
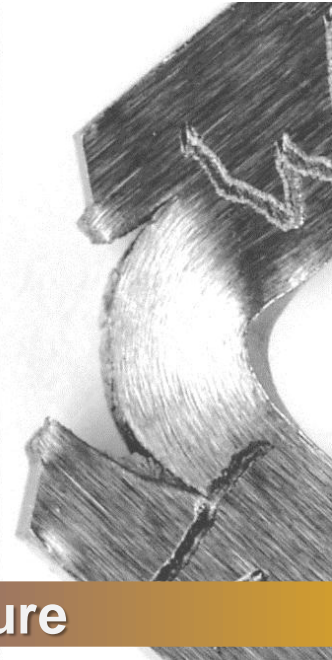
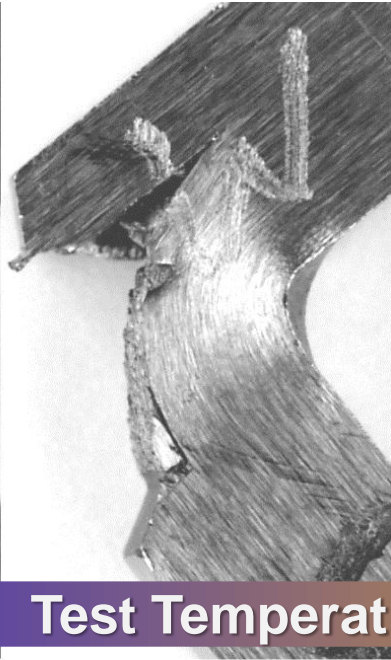
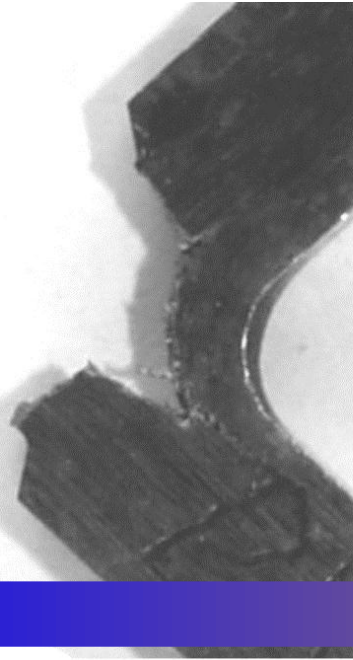
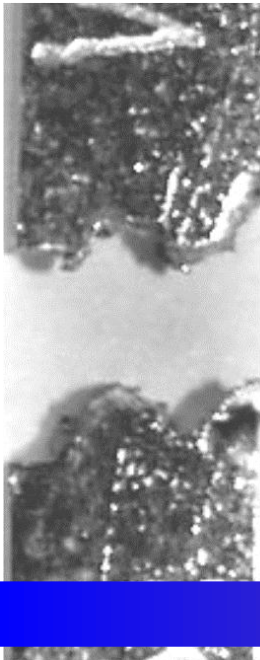
Impact on Toughness



Delamination Fracture



brittle → **delamination** → **ductile**



Test Temperature

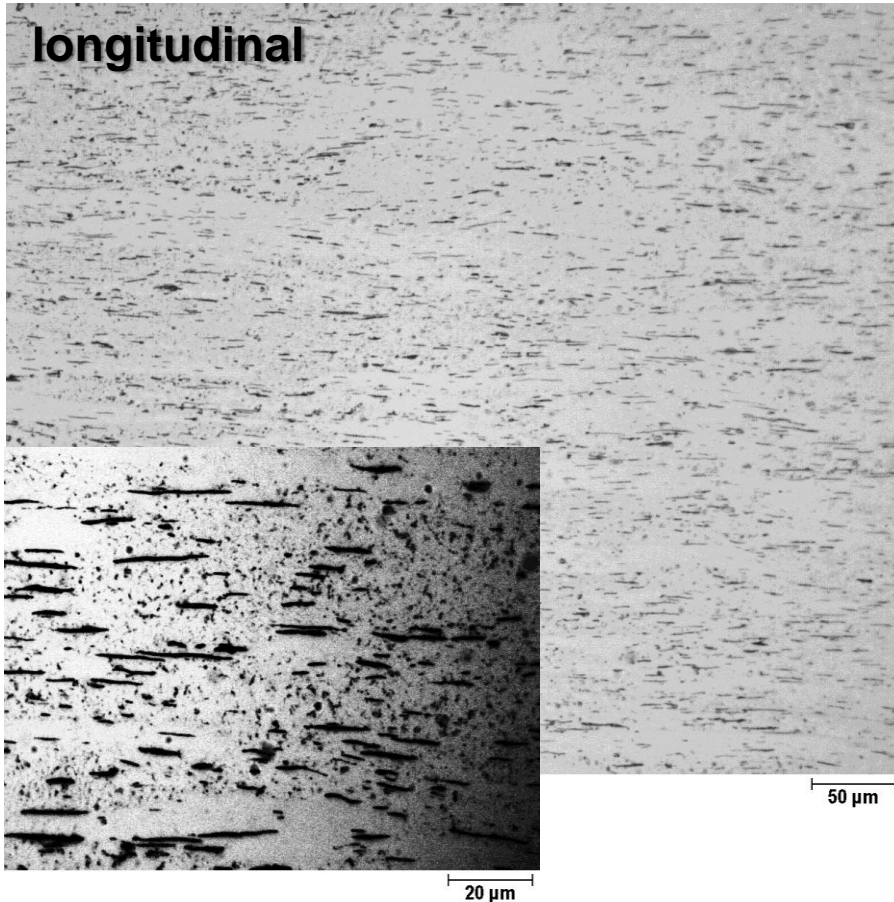
Effect of ODS particles in W

WL10 Rod, Ø7 mm

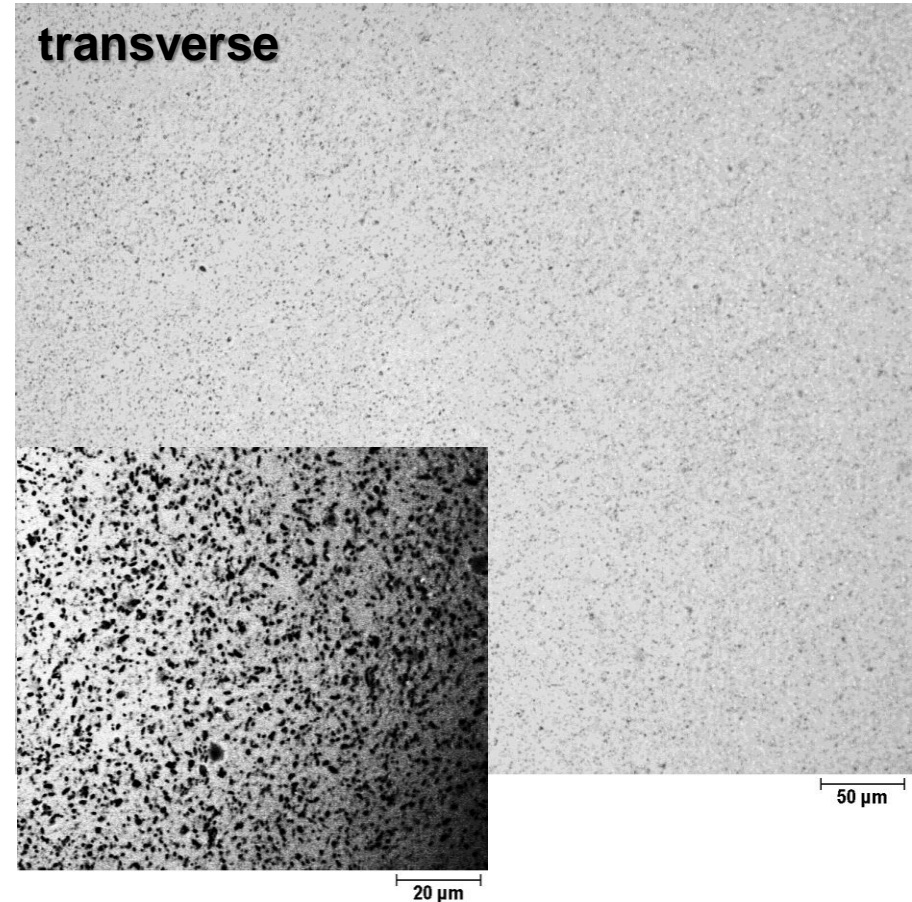


Rods: Metallography

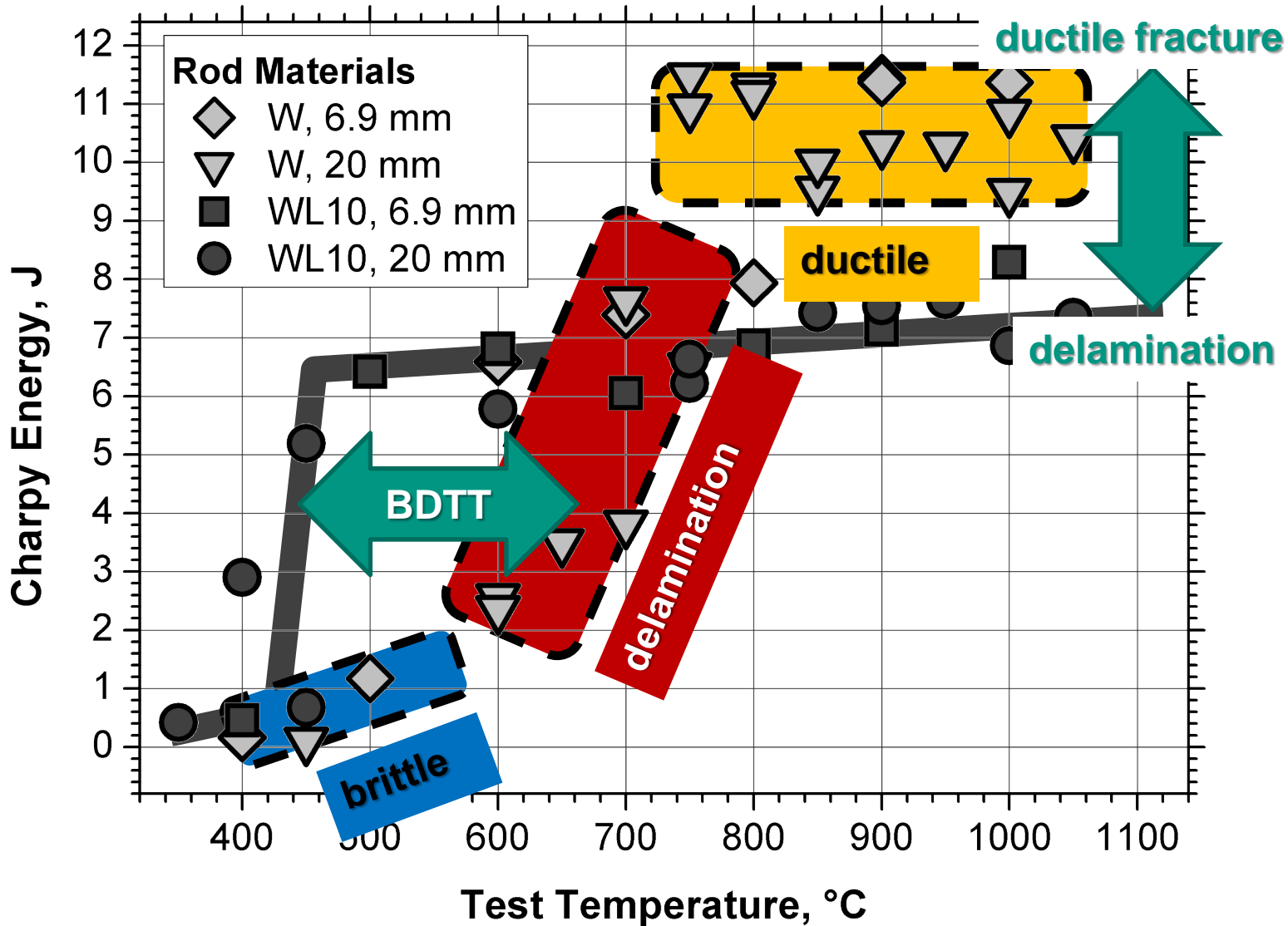
longitudinal



transverse



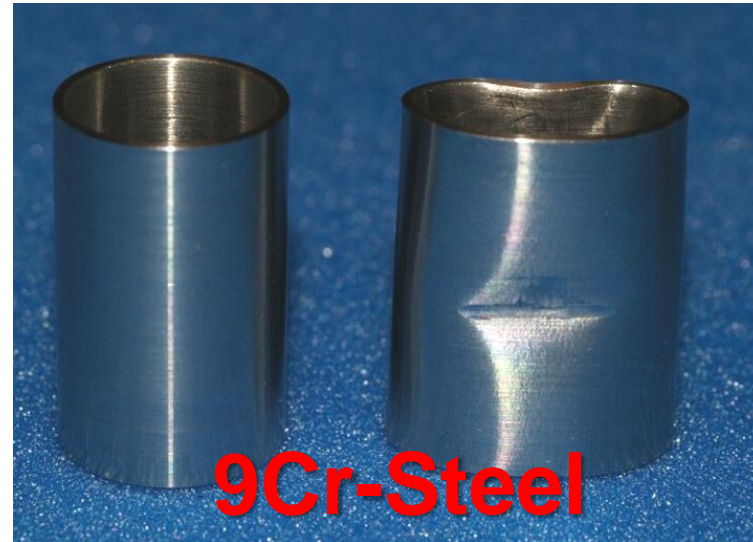
Effect of ODS particles in W



Problem of Microstructure Orientation



Pipe Impact Test



9Cr-Steel



So far, the best suitable tungsten materials for structural applications (divertor or other large scale components) are

Thin Plates, Thickness < 4 mm

Produced by Sintering (Hydrogen Atmosphere) and Cross-Rolling

Pure Tungsten (maybe small amounts of grain stabilizers, like La_2O_3)

4

HELIUM COOLED DIVERTOR DESIGNS

The life time of a power plant divertor is **TWO** years – hopefully!

High heat flux

- High operating temperatures (peaks > 1800°C)
- Microstructural stability, aging, ...
- Thermo-shocks, cyclic loading, fatigue, ...

Heavy ion bombardment

- Sputtering, cracking/fracturing
- Surface interactions and modifications
- Microstructural changes

Neutron load
15 dpa/year (in W)

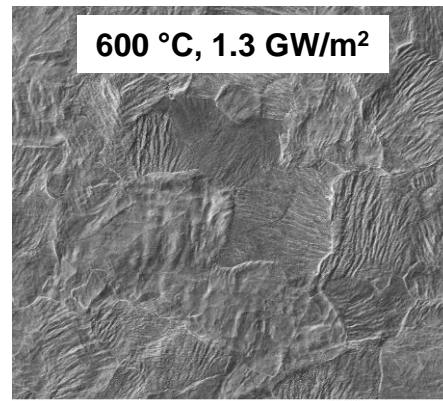
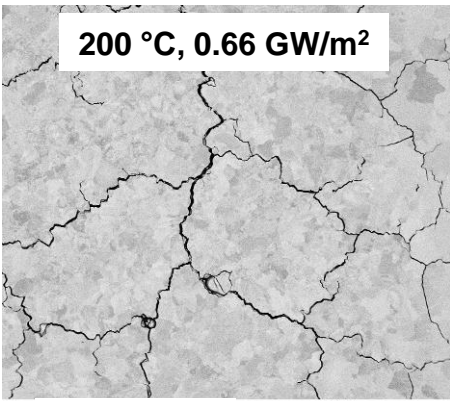
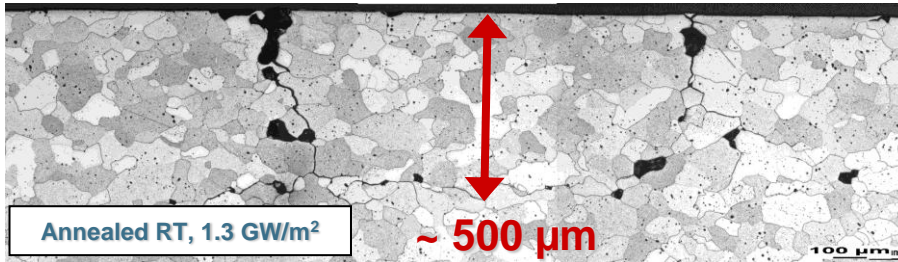
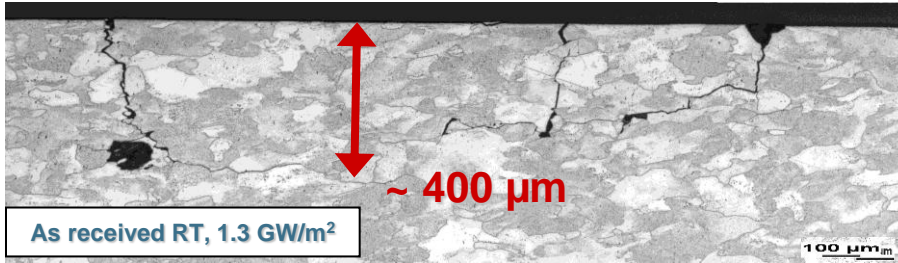
- 30 dpa (in W) until end of service
- Transmutation effects (Re, Os)
- Swelling (order of magnitude: 3% for pure W)

QUESTION: What can we do about this? How can we improve **ARMOR** materials?

ANSWER: There is not much we can do now! We have to live with most properties and effects. A final assessment would require real in-service conditions.

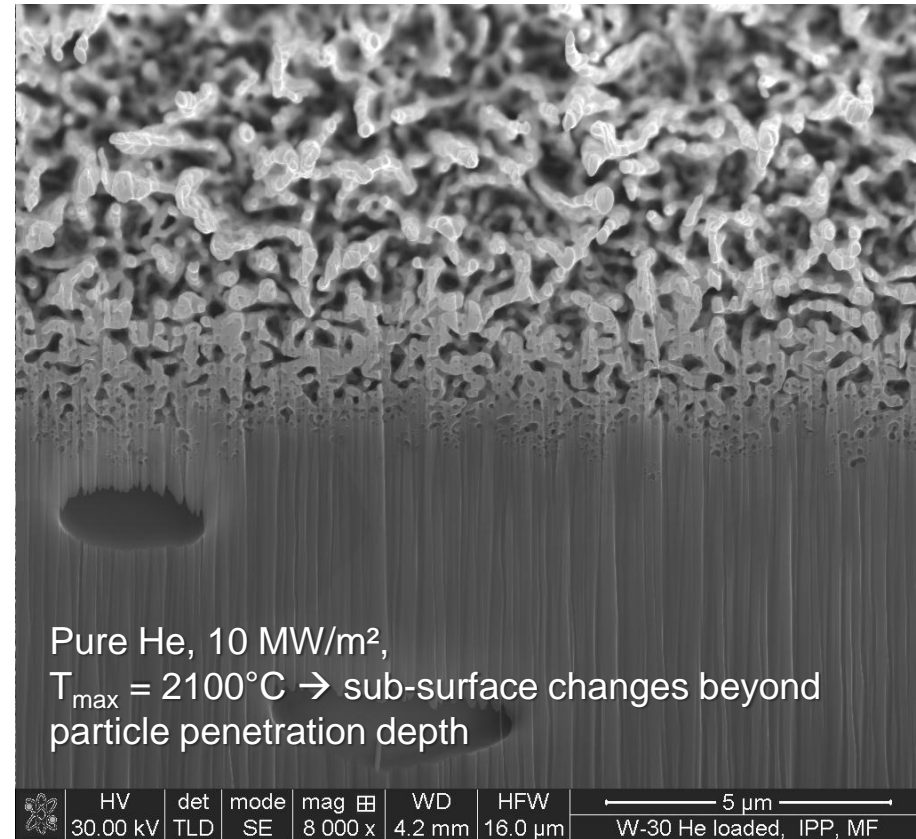
HIGH HEAT FLUX EFFECTS

Electron Beam



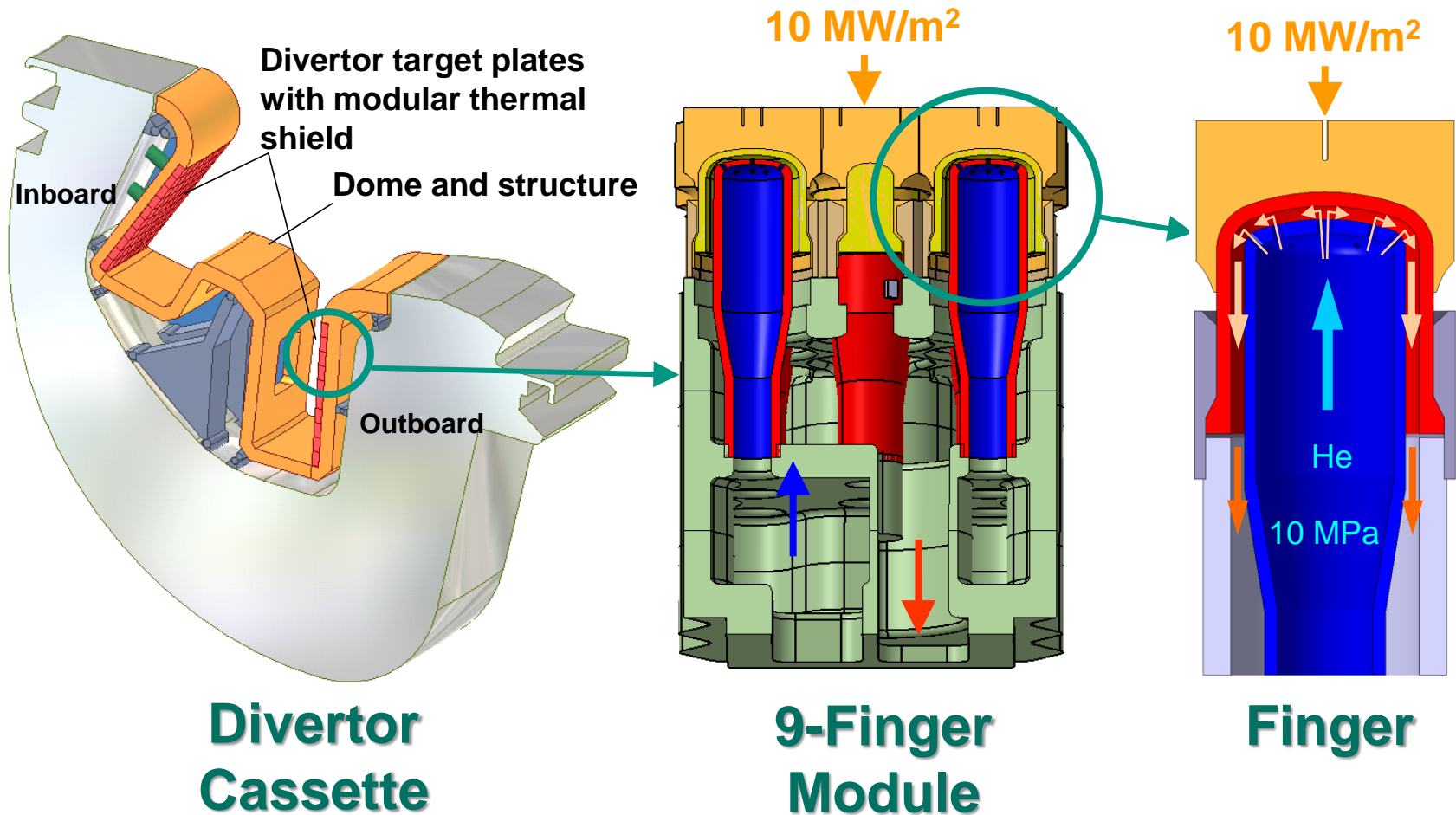
→ G. Pintsuk, J. Linke, et al., FZJ

Hydrogen/Helium Ion Beam



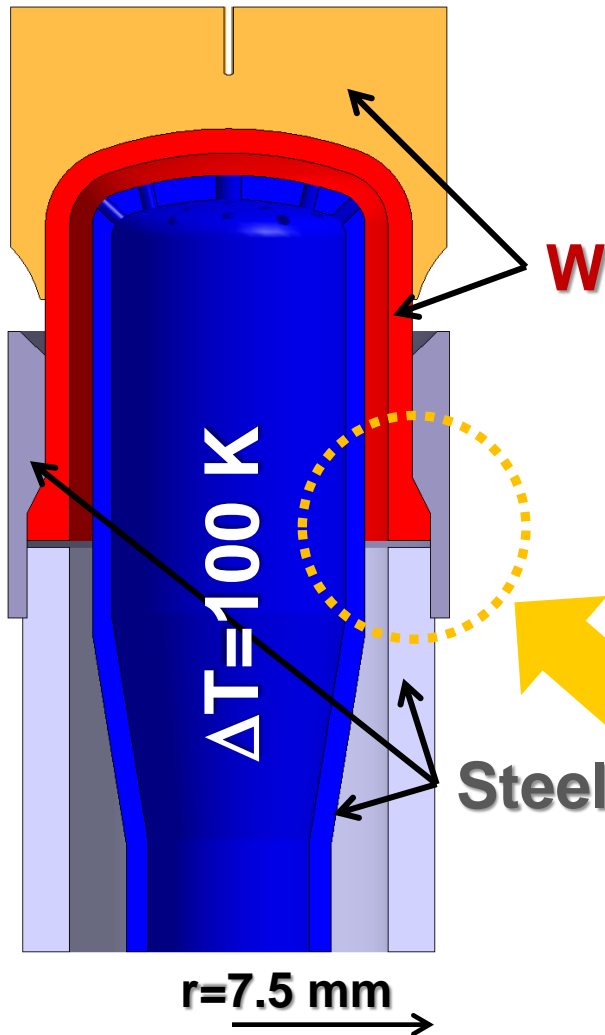
→ H. Maier, H. Greuner, M. Rasinski,
Ch. Linsmeier, IPP

FINGER DESIGN, JET COOLING



→ P. Norajitra, T. Ihli *et al.*, 2003-2009

FINGER DESIGN, JET COOLING



+ High heat flux: $>10 \text{ MW/m}^2$

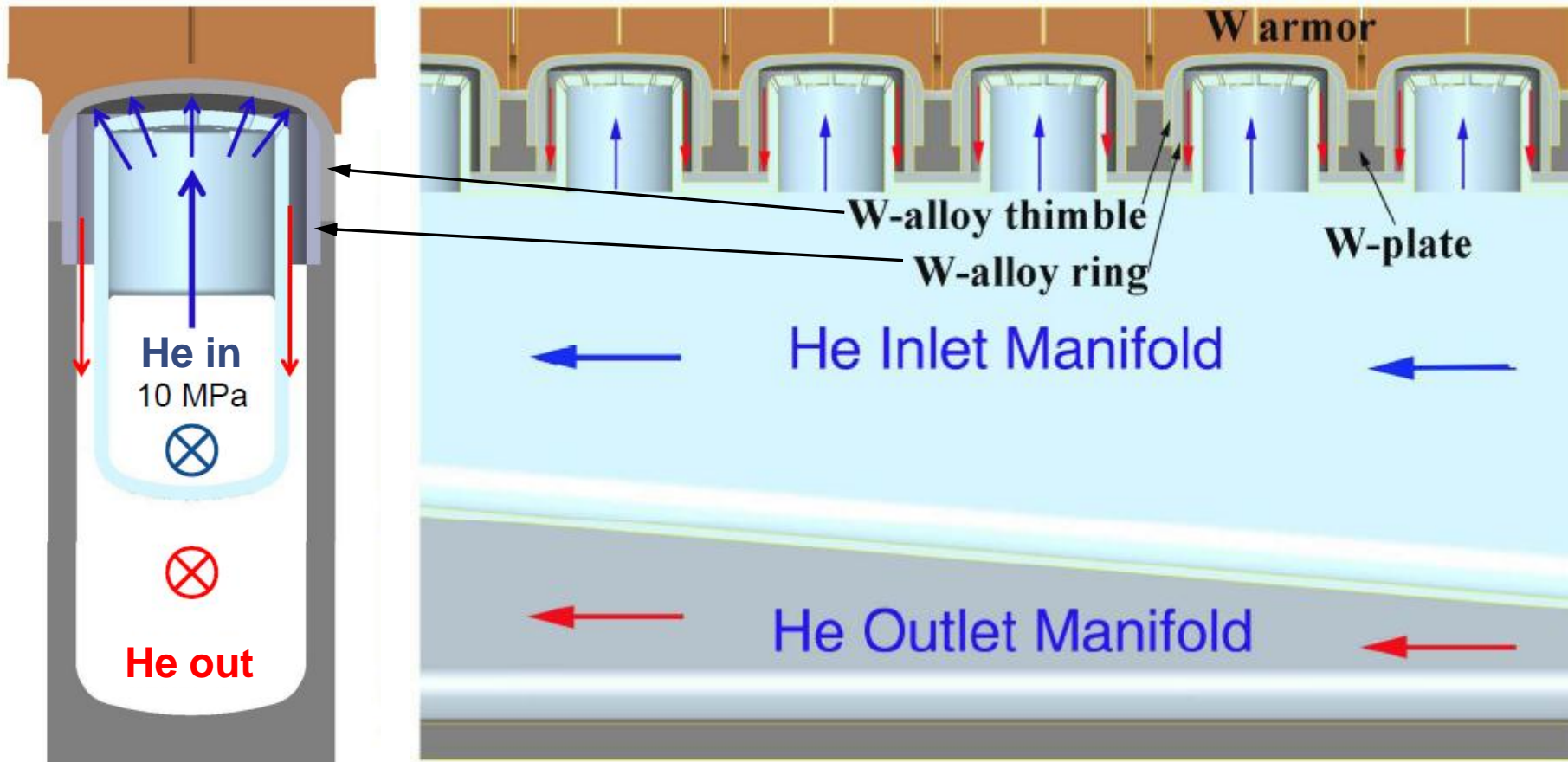
+ Small Size, Thin Walls

- Large Numbers: $\sim 500\,000$

- Joints between W and Steel

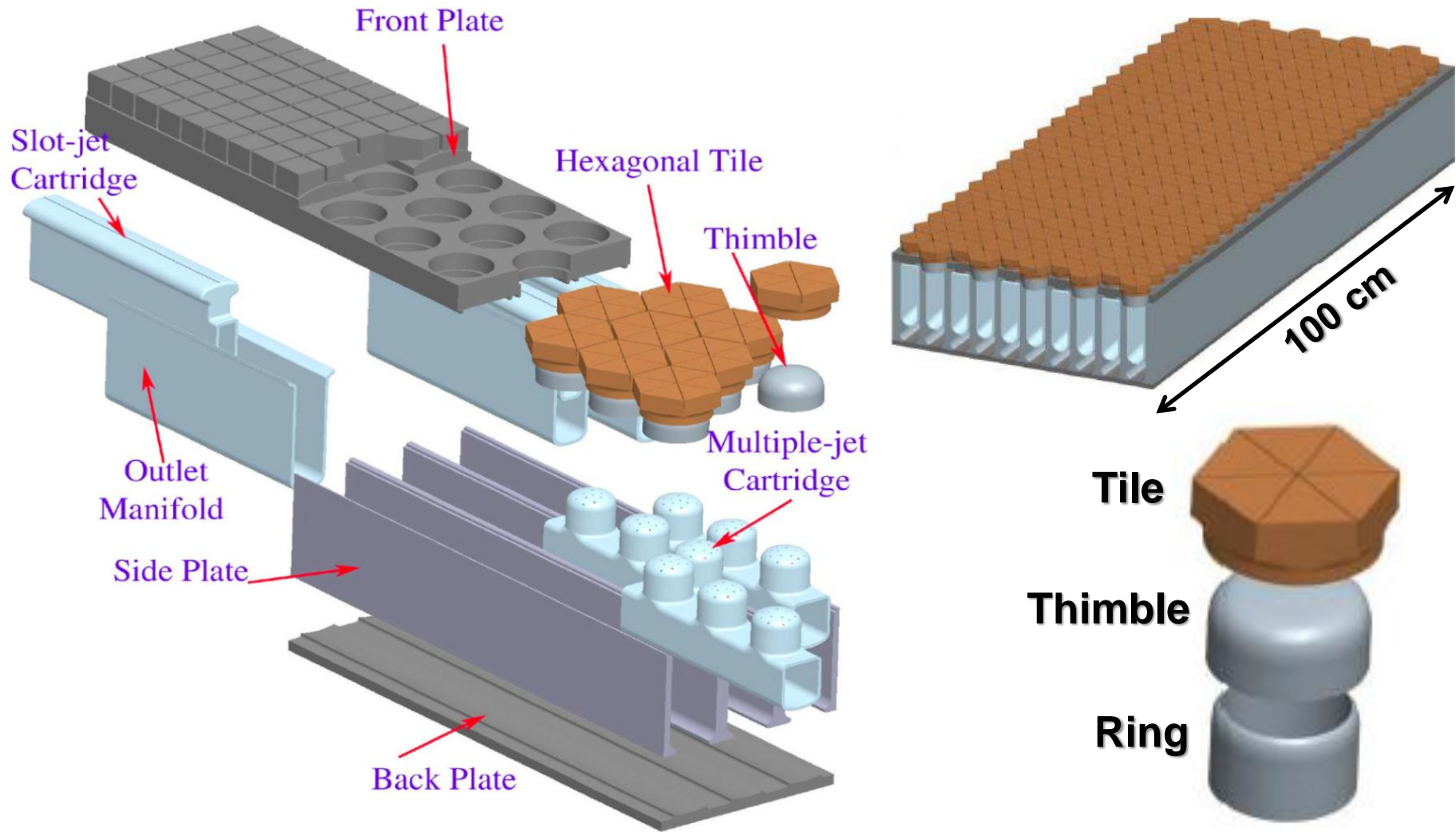
He and W temperature limited by steel
Ferritic ODS $\rightarrow 750^\circ\text{C}$???
Eurofer ODS, 9Cr ODS $\rightarrow 650^\circ\text{C}$
Eurofer 97, F82H $\rightarrow 550^\circ\text{C}$

PLATE DESIGN (ARIES), JET COOLING



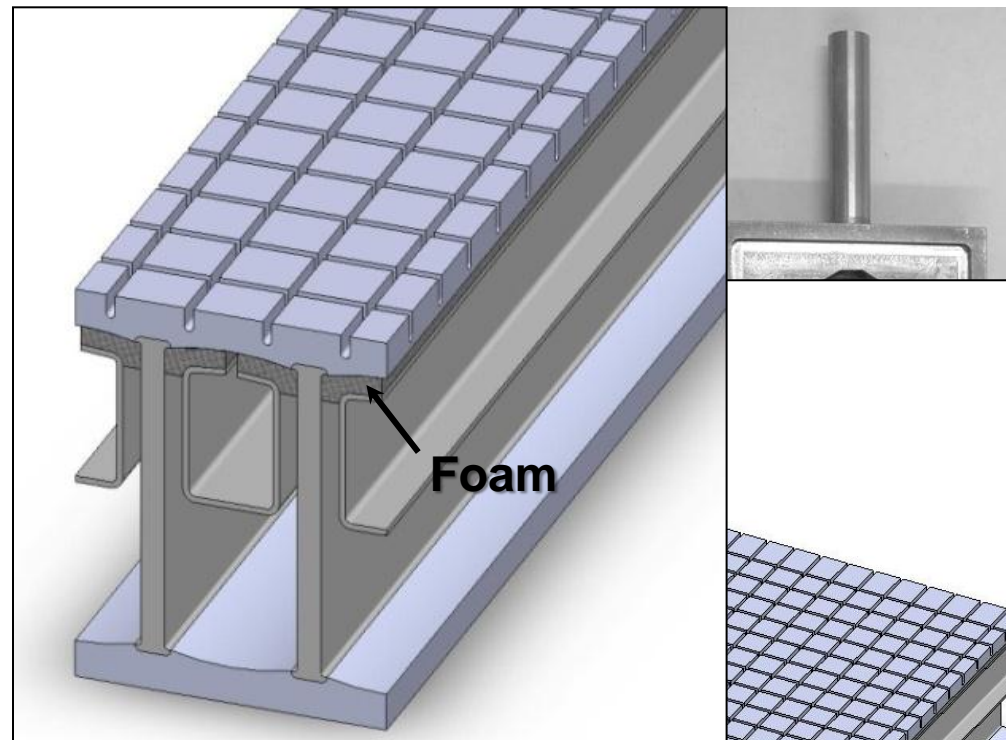
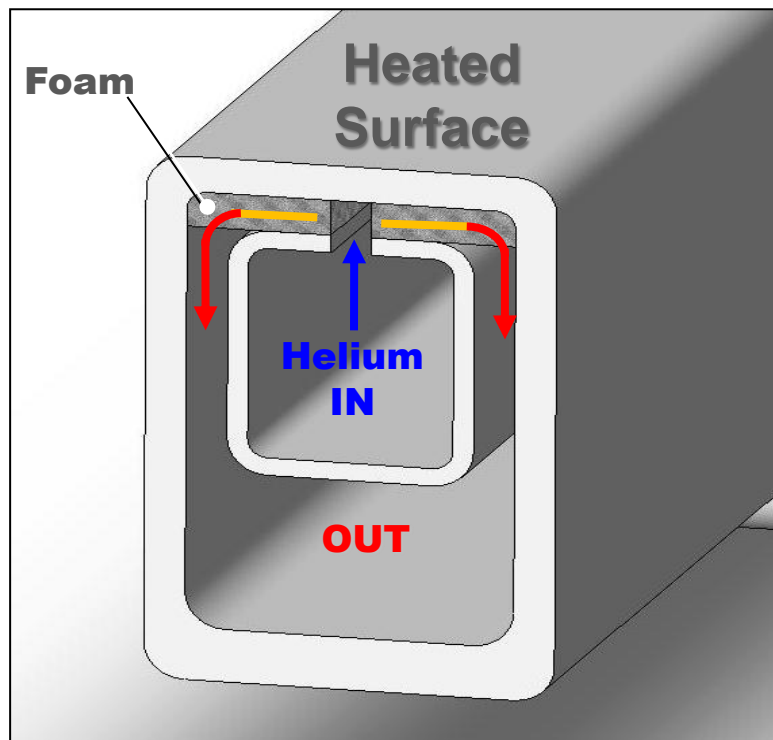
X.R. Wang, S. Malang, M.S. Tillack & ARIES Team, 2008-2011

PLATE DESIGN (ARIES), JET COOLING



X.R. Wang, S. Malang, M.S. Tillack & ARIES Team, 2008-2011

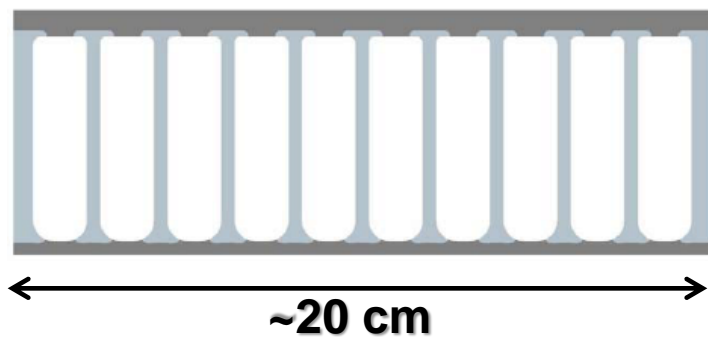
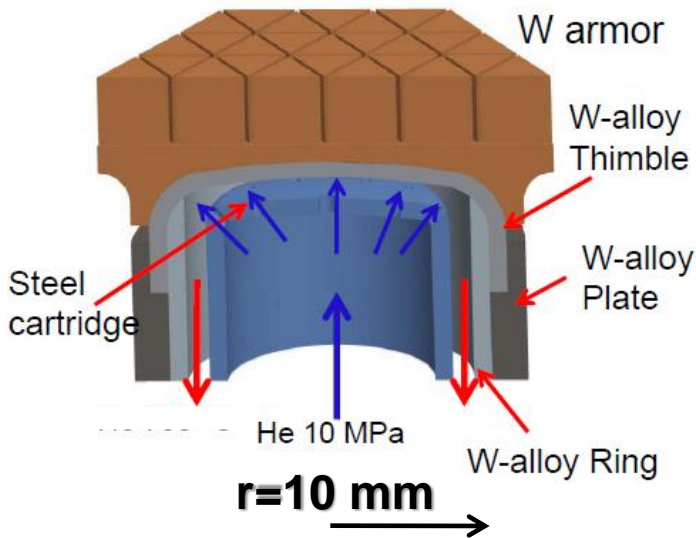
PLATE DESIGN, FOAM PROMOTER



→ S. Sharafat *et al.*, UCLA, 2005-2009

→ Mo, Nb, SiC Foam:
D. Youchison *et al.*, SNL, 2011

PLATE DESIGN (ARIES), JET COOLING



+ High heat flux: $\sim 15 \text{ MW/m}^2$

+ Small Size, Thin Walls

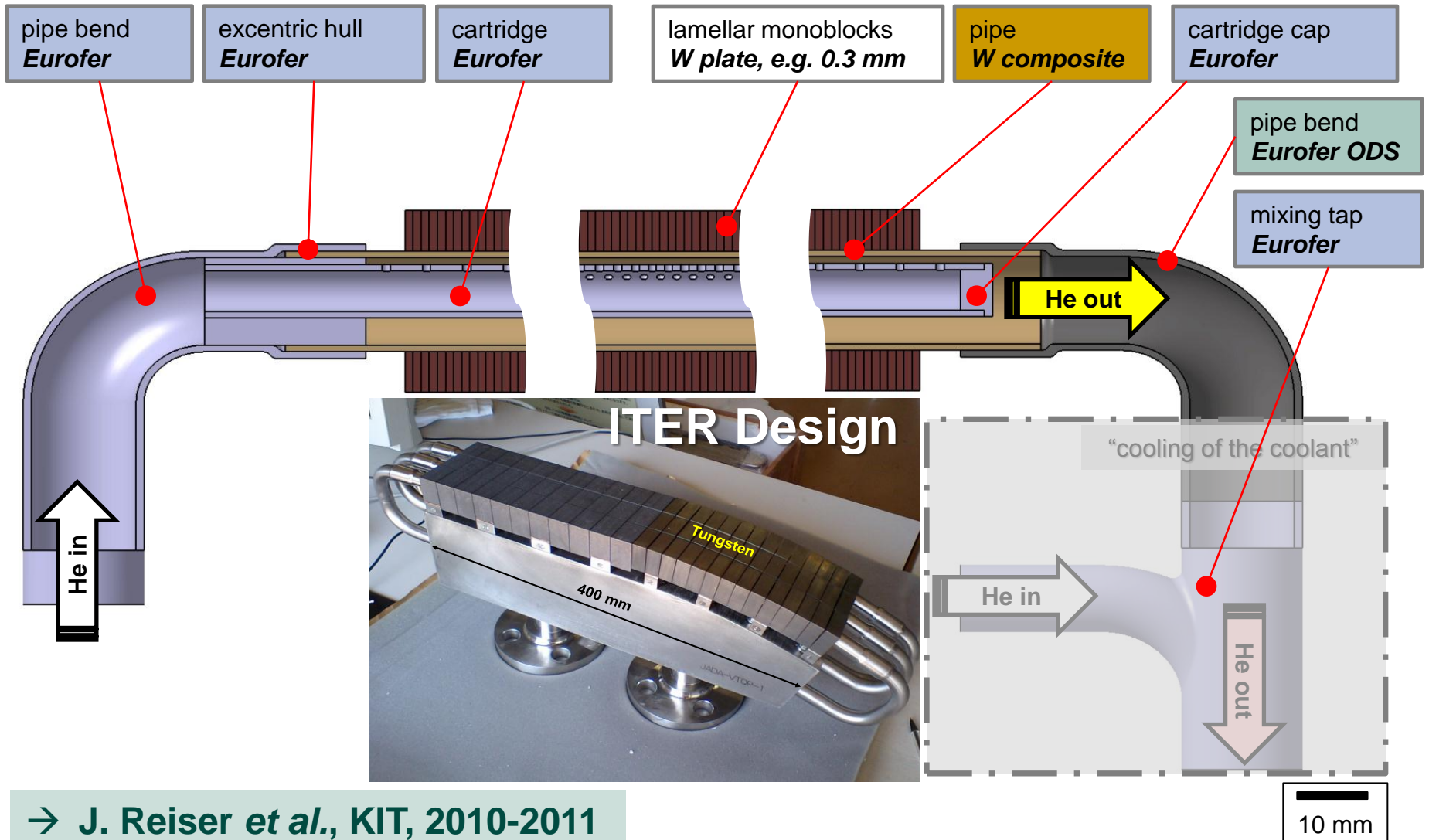
+ “Double Containment”

- Large Numbers: $\sim 300\,000$

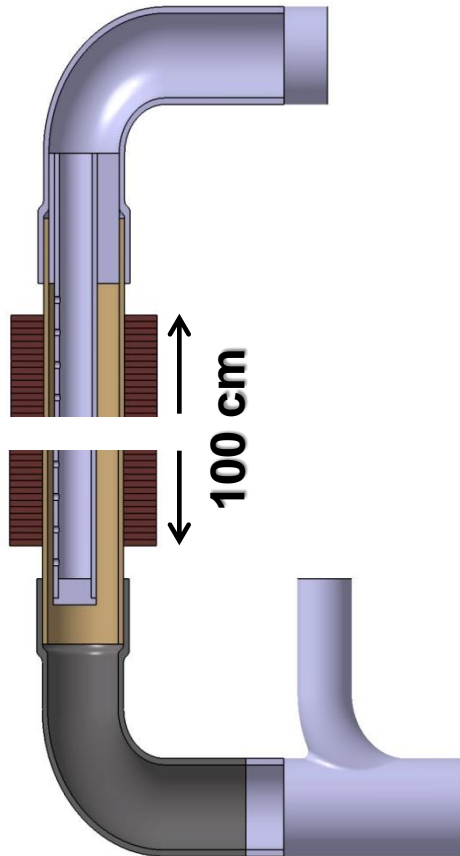
- Many/Long Struct. W-W Joints

He temperature limited by steel
(multiple jet cartridges)
Ferritic ODS $\rightarrow 750^\circ\text{C}$???
Eurofer ODS, 9Cr ODS $\rightarrow 650^\circ\text{C}$
Eurofer 97, F82H $\rightarrow 550^\circ\text{C}$

PIPE/MONOBLOCK DESIGN, JET COOLING



PIPE/MONOBLOCK DESIGN, JET COOLING



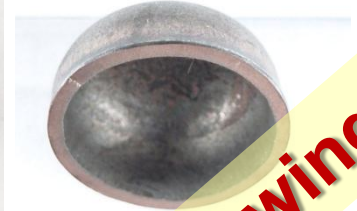
- + Simple Design
- + “Easy Joints”
- + “Small Number of Parts”
- + Inexpensive
- Low Temperatures for W
- Low Performance
- Speculative Pipe Material

He temperature limited by steel
Eurofer ODS → 650°C (upper)
Eurofer 97 → 350°C (lower)

5

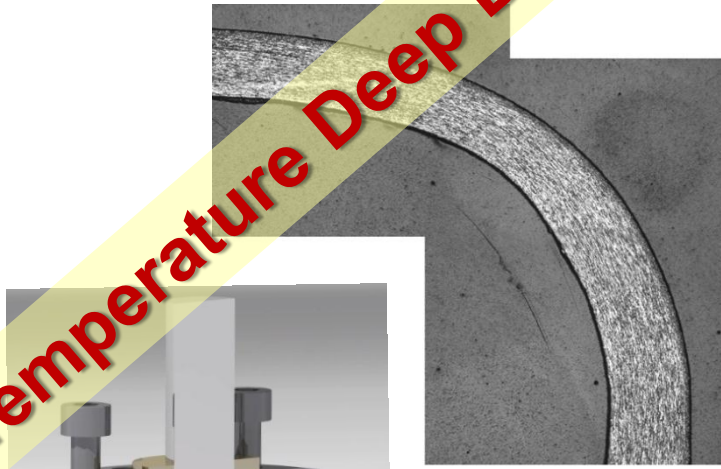
DESIGN
ANALYSIS

FABRICATION

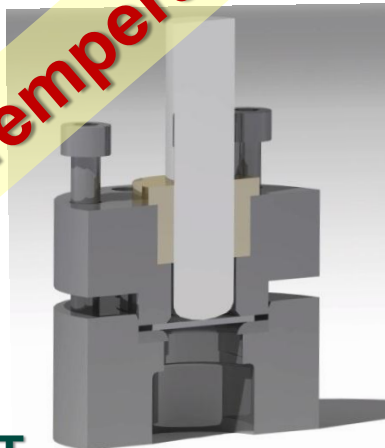


Machining: Turning, Milling, Grinding, ...

High Temperature Deep Drawing

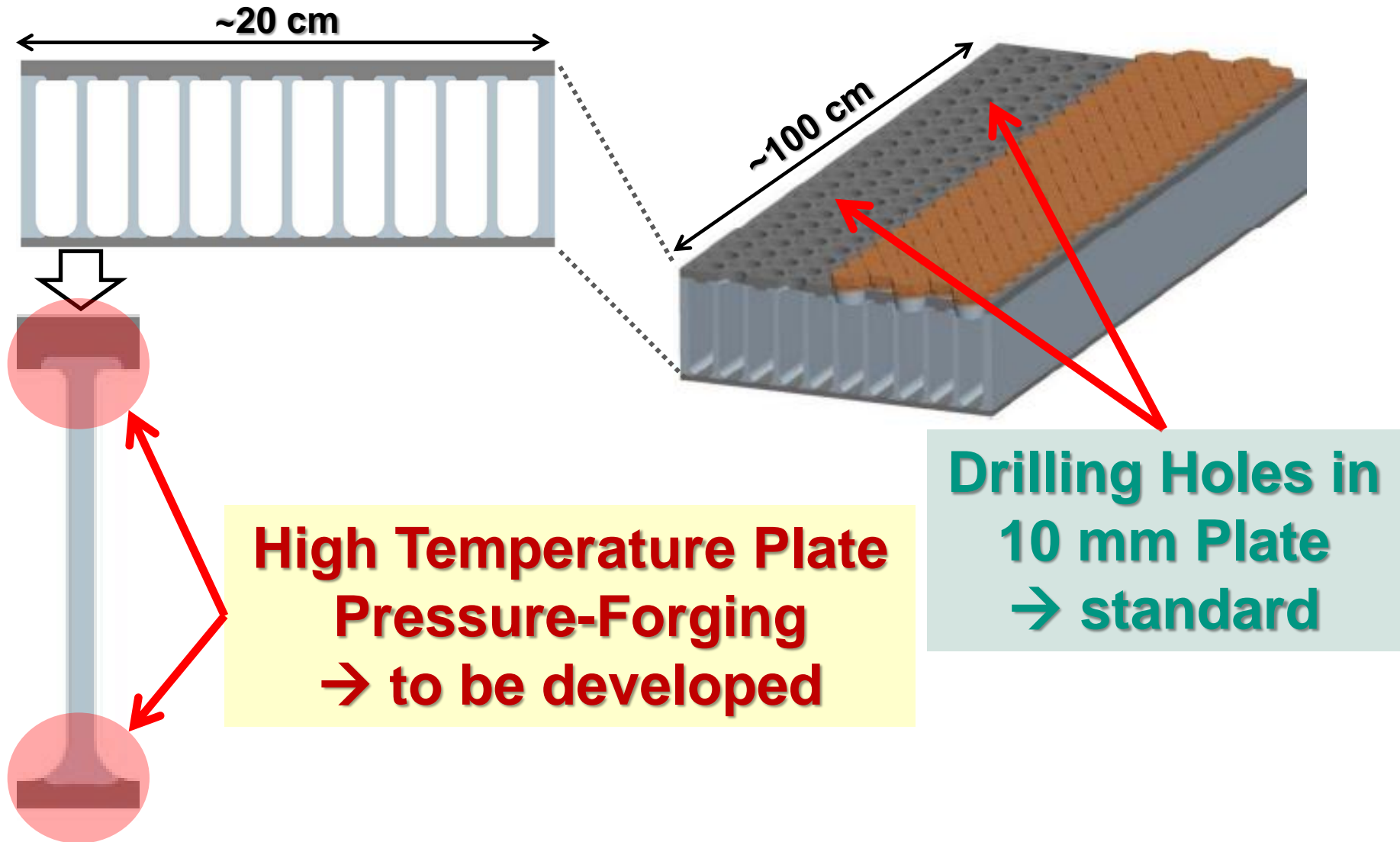


1mm



P. Norajitra, J. Reiser, S. Baumgärtner *et al.*, KIT

FABRICATION



**IMPORTANT: We have to consider joints for STRUCTURAL applications!!!
Joining W tiles to W timbers is NOT considered as structural application!**

Brazing Material for W-W Joints

Brazing temperature must be $\gg 900-1200$ °C (operating temp.)

Brazing temperature must be < 1800 °C → Grain growth

Formation of brittle compounds cannot be tolerated

Brazing Material for W-Steel Joints

Brazing temperature < 1100 °C → Grain growth (in steel)

Brazing temperature must be $\gg 550-750$ °C (operating temp.)

Formation of brittle compounds cannot be tolerated

BRAZING W→W

| | | | | | | | | |
|--------------|----|--------------|---------------------------|--------------|----------|----------|----|----|
| M_2W Be | Mg | MW B | MW_2 C $M_{1-x}W$ | M_4W Al | | Y | La | |
| Ti | V | MW_3 Cr | Mn | MW, M_7W_6 | M_7W_6 | MW Ni | Cu | |
| MW_2 Zr | Nb | Mo | Ru | Rh | M_3W | Pd | Ag | Cd |
| MW_2 Hf | Ta | Re | Cs | MW | MW | MW Pt | Au | |

W Insoluble

Intermetallic Phases

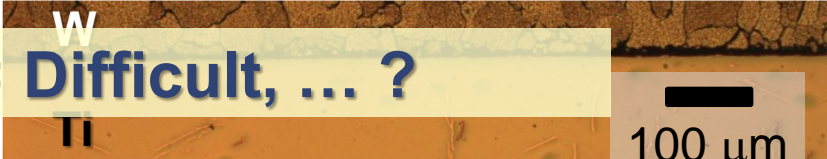
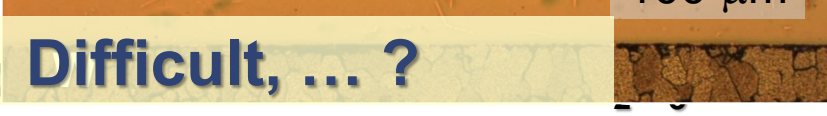

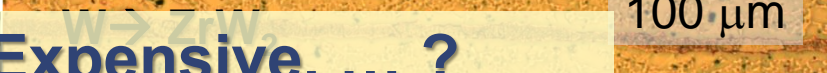




W Rich Line Compounds

Solid Solution

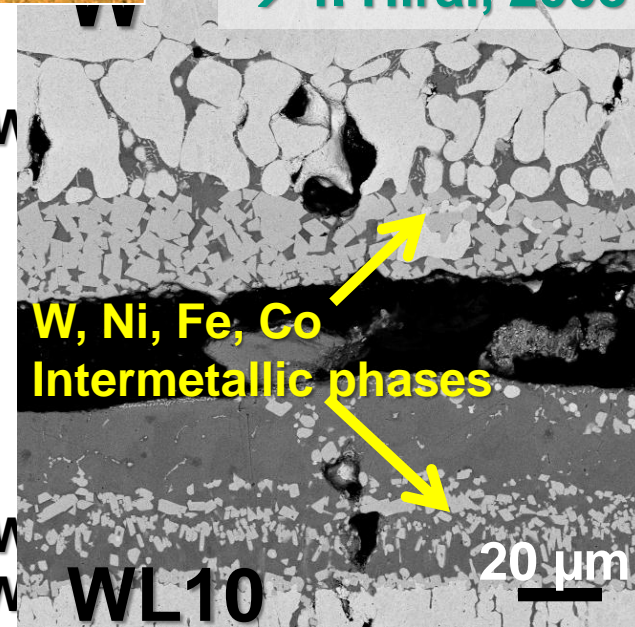
$T_m > 1800^\circ$

$T_m < 1400^\circ$

BRAZING MATERIALS, W→W

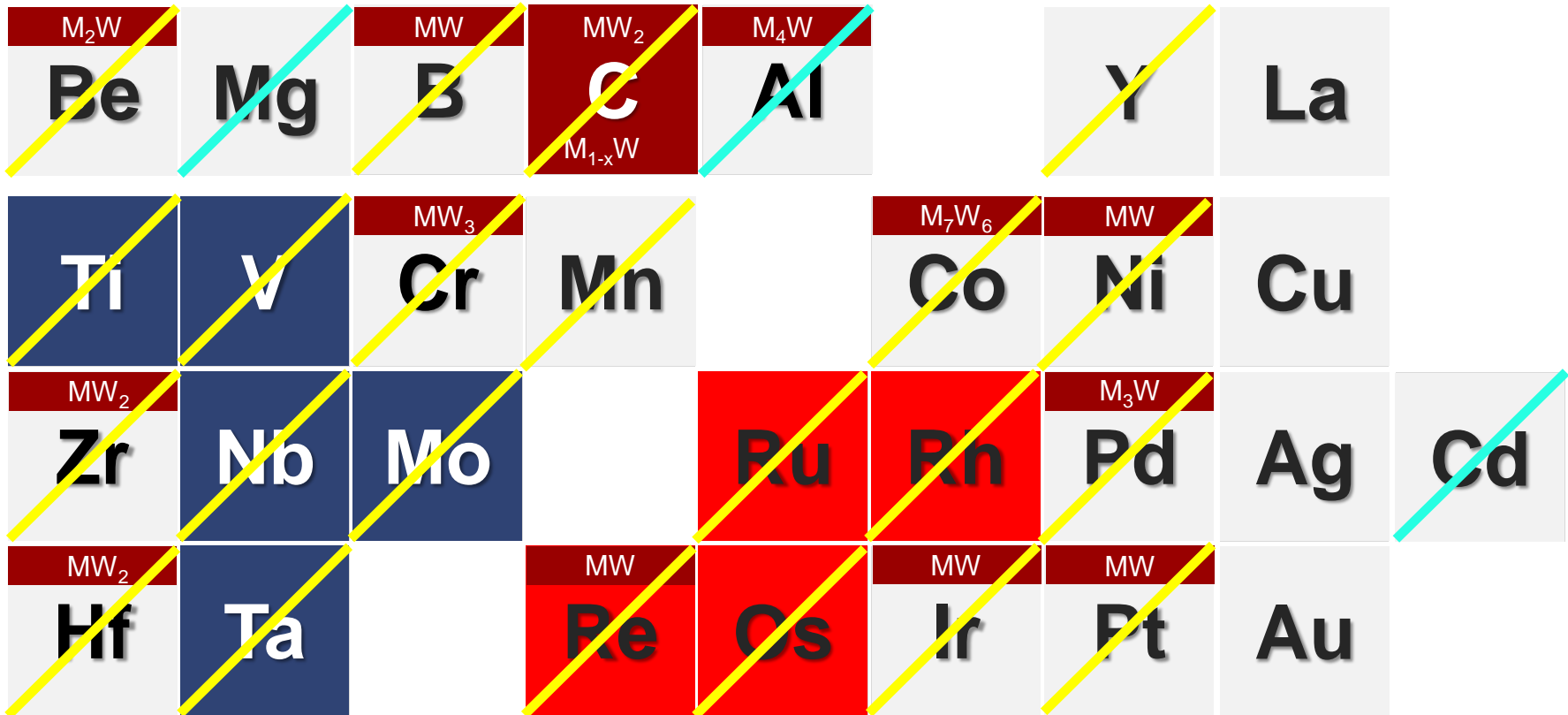
| | | | | |
|--------|-----------|---|--|--------|
| 1670°C | Ti | <740°C: Difficult, ... ? |  | 100 μm |
| 1520°C | Y | Strong <1570°C: Difficult, ... ? |  | 100 μm |
| 1850°C | Zr | <2160°C: W → ZrW <1700°C: Brittle Joint <860°C: Zr → ZrW ₂ |  | 100 μm |
| 1550°C | Pd | <1800°C: W → ZrW <900°C: intermetallic Pd ₃ W ??? |  | 100 μm |
| 1770°C | Pt | <2400°C: Very expensive, ... ? Pt ₃ W phase |  | 100 μm |
| 1540°C | Fe | <1700°C: μ phase Fe ₇ W ₆ (Fe,W) ₄ <1000°C: Laves phase Fe ₂ W |  | 100 μm |
| 1500°C | Co | <1700°C: μ phase Co ₇ W ₆ (Co,W) ₄ <1000°C: Laves phase Co ₃ W |  | 100 μm |
| 1450°C | Ni | <1000°C: peritectoid intermetallics NiW <950°C: peritectoid intermetallic Ni ₄ W |  | 100 μm |

→ T. Hirai, 2008



Brittle Joints

BRAZING W → STEEL



W Insoluble

Intermetallic Phases

W Rich Line Compounds

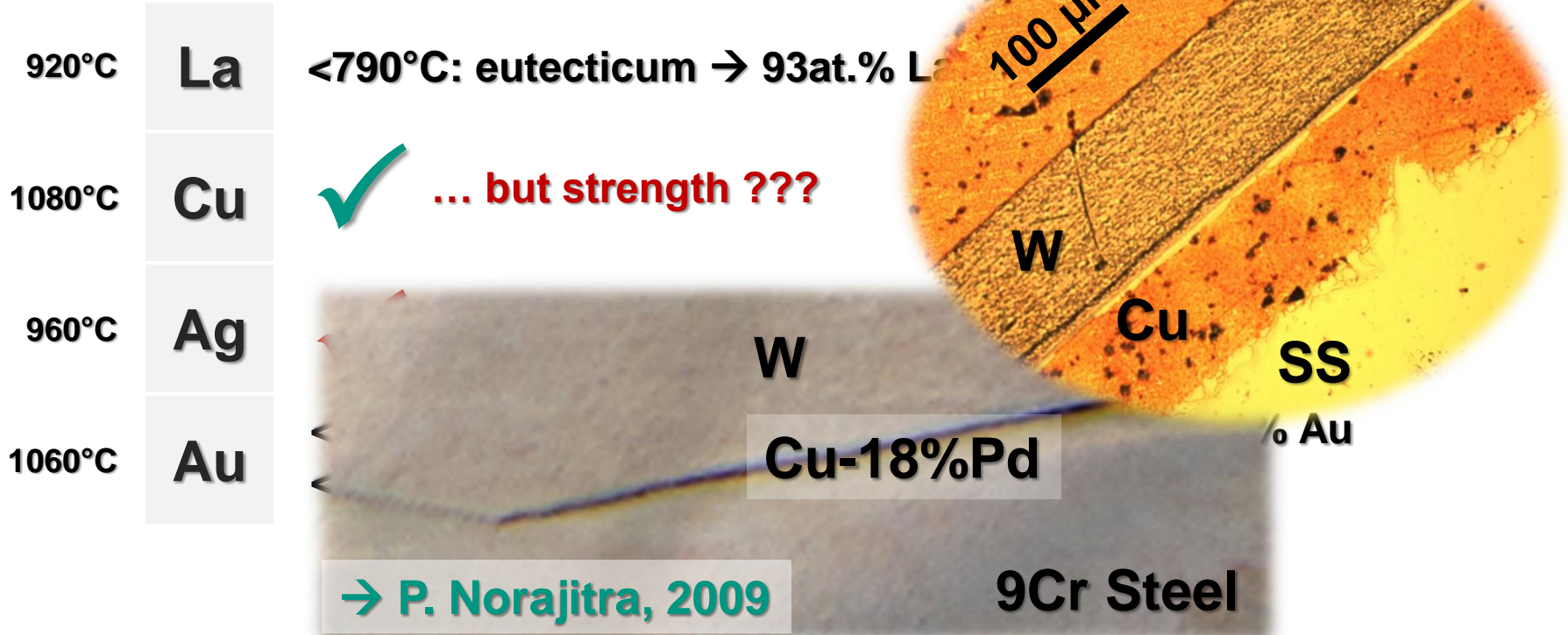
Solid Solution

$T_m > 1200^\circ$

$T_m < 900^\circ$

BRAZING MATERIALS, W → STEEL

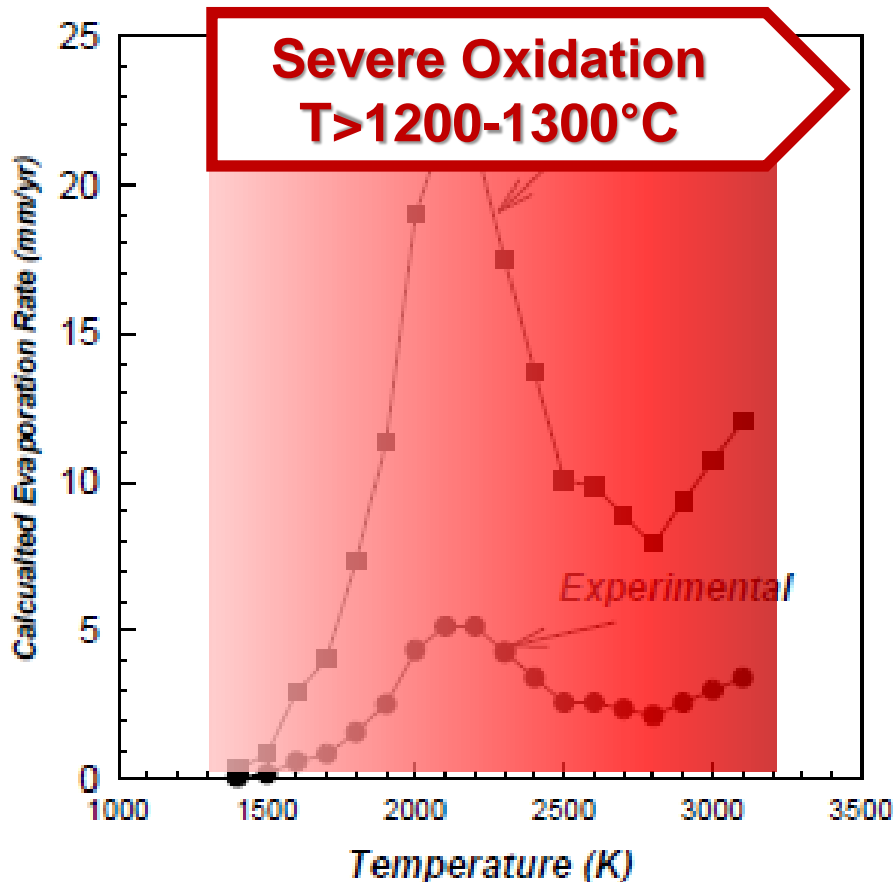
→ J. Reiser, 2011



CONCLUSION: Copper has to be used as sealing rather than as a braze material !!!

ENVIRONMENT → OXIDATION

WO_3 yellow, $T_m=1470^\circ\text{C}$, 7200 kg/m^3 , volatile in vacuum



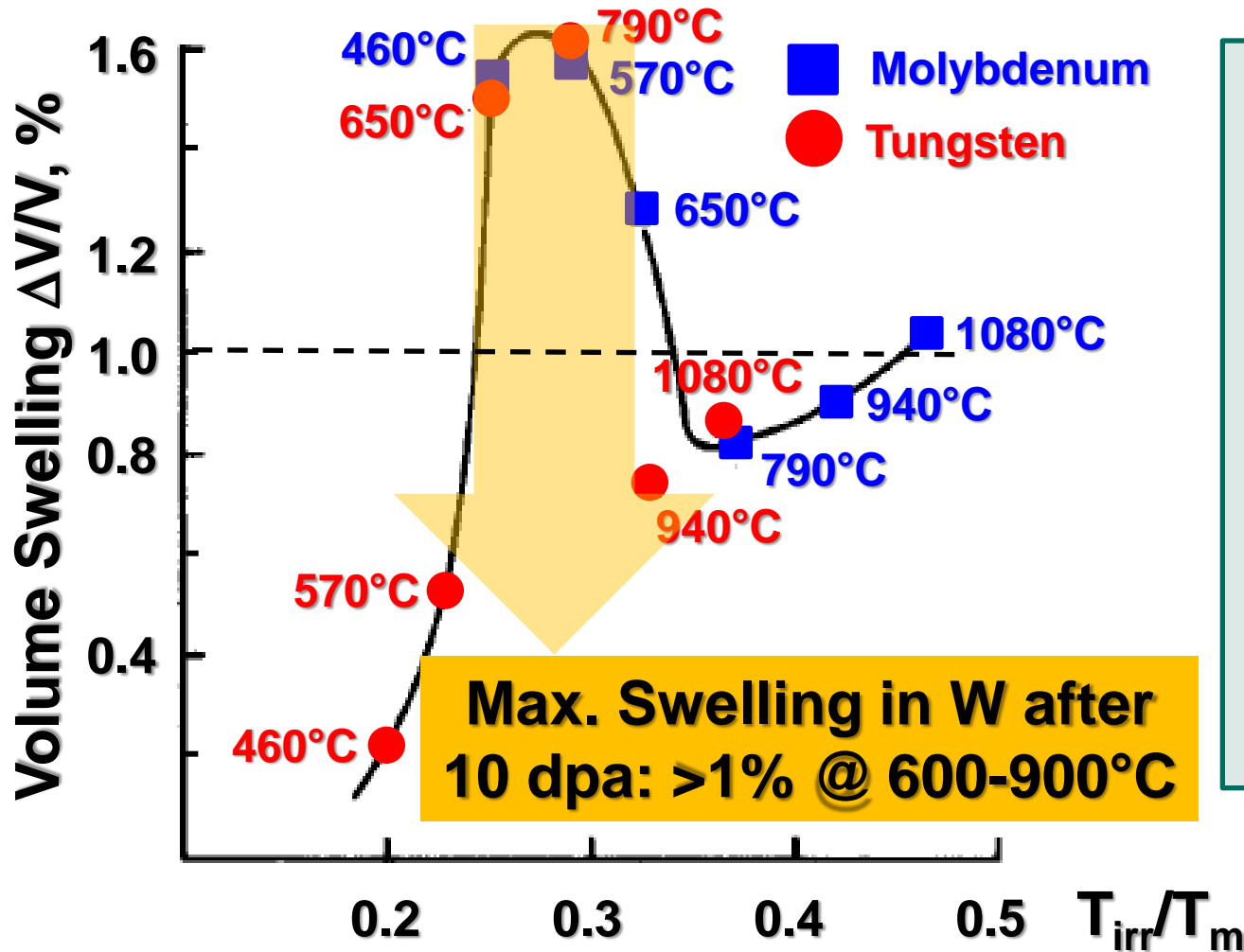
→ N.M. Ghoniem, 1998



CONCLUSION

For tungsten operating at 50 atm. He coolant, at 0.1 ppm oxygen, the upper temperature is estimated at 1200-1300°C.

IRRADIATION EFFECTS → SWELLING



EBR-II

$E_n > 1 \text{ MeV}$
 $1 \times 10^{22} \text{ n/cm}^2$

$E_n > 0.1 \text{ MeV}$
 $1.6 \times 10^{22} \text{ n/cm}^2$

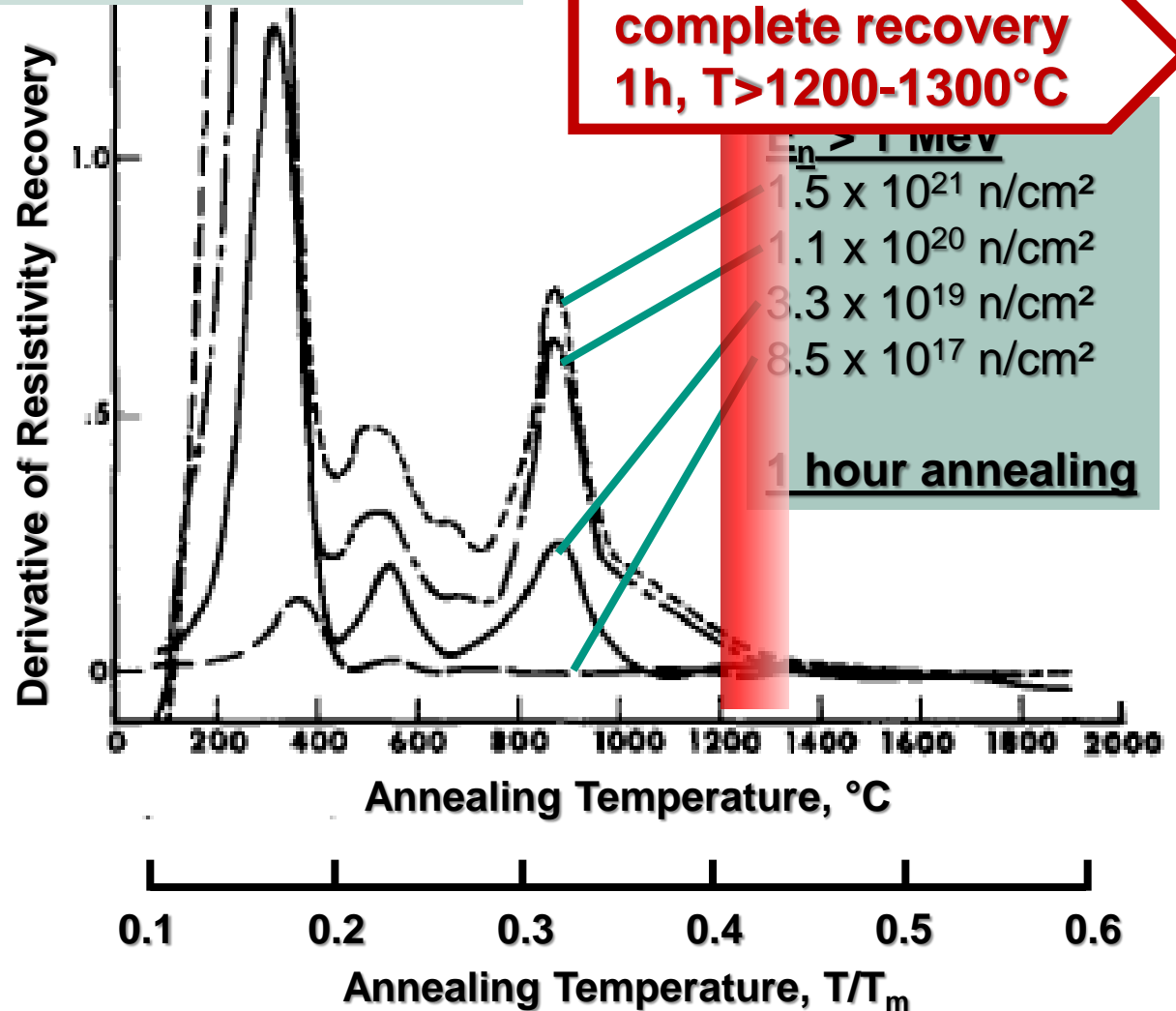
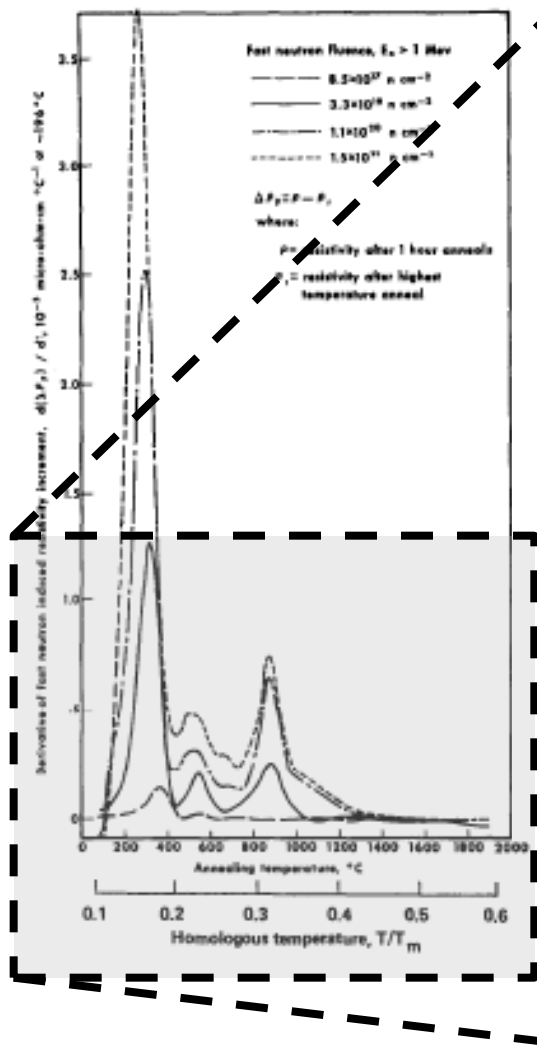
→ 29 dpa in Mo

→ 9.6 dpa in W

→ F. Lee, J. Matolich, J. Moteff, JNM 62 (1976) 115-117

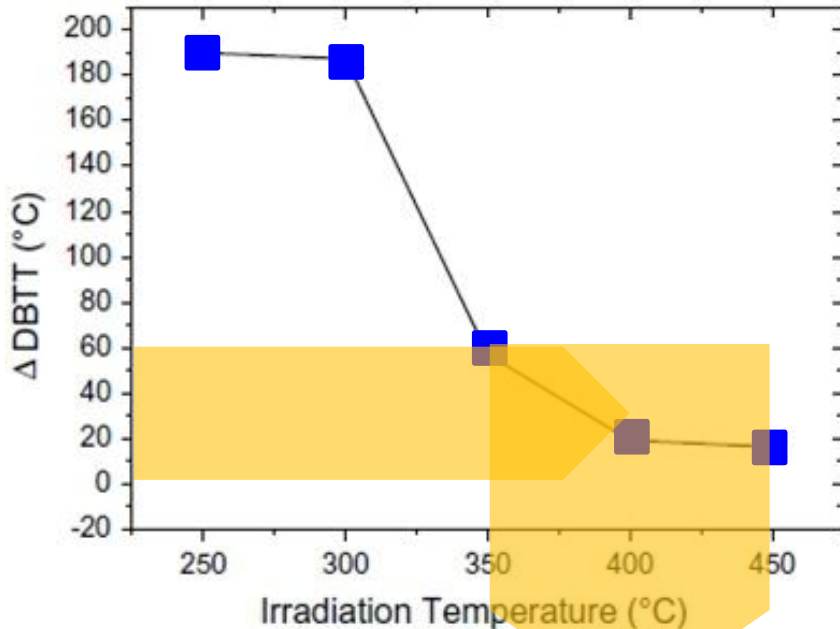
IRRADIATION EFFECTS → RECOVERY

→ L.K. Keys, J. Moteff, JNM 34 (1970) 260-280



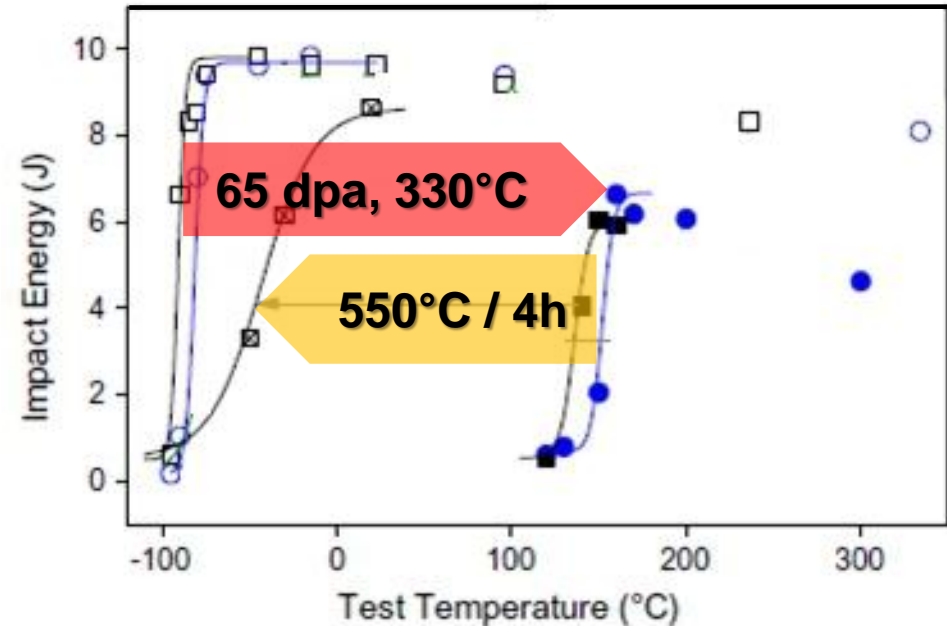
IRRADIATION EFFECTS → EMBRITTLEMENT

EUROFER: In-service irradiation embrittlement after ~10 dpa



Possible Operating Temperature $T_{op} > 350^{\circ}\text{C}$

EUROFER: Recovery of 65 dpa irradiation embrittlement

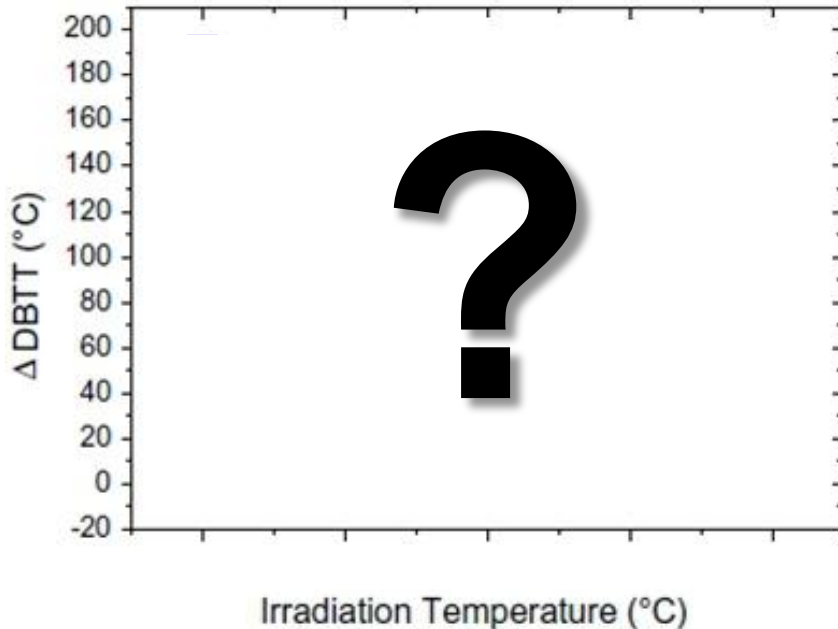


Possible Recovery Temp.
 $T_{rec} > 550^{\circ}\text{C}$

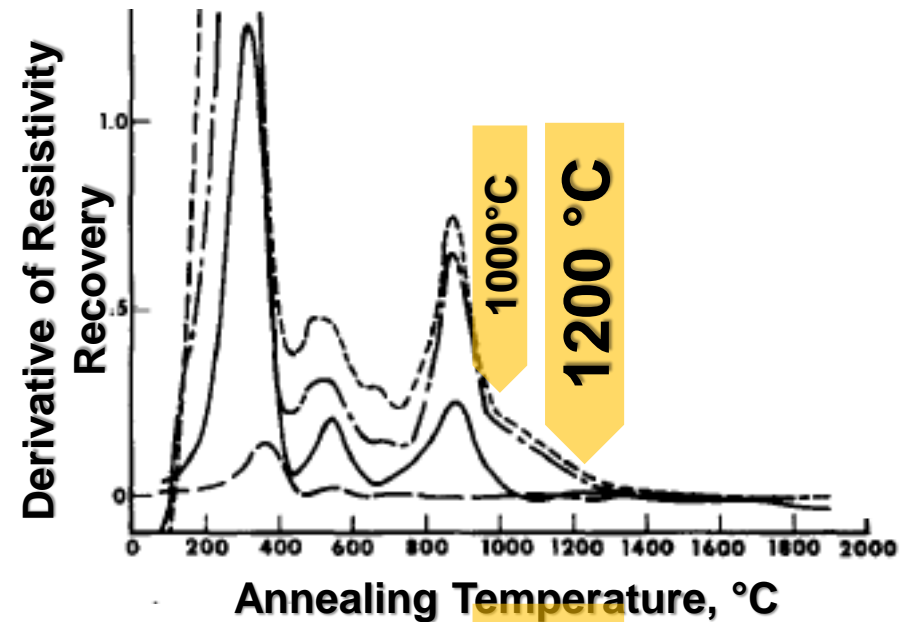
→ E. Gaganidze *et al.*, KIT

IRRADIATION EFFECTS → EMBRITTLEMENT

TUNGSTEN: In-service irradiation embrittlement after 10-20 dpa



Tungsten: Recovery of ~2 dpa stage IV irradiation hardening

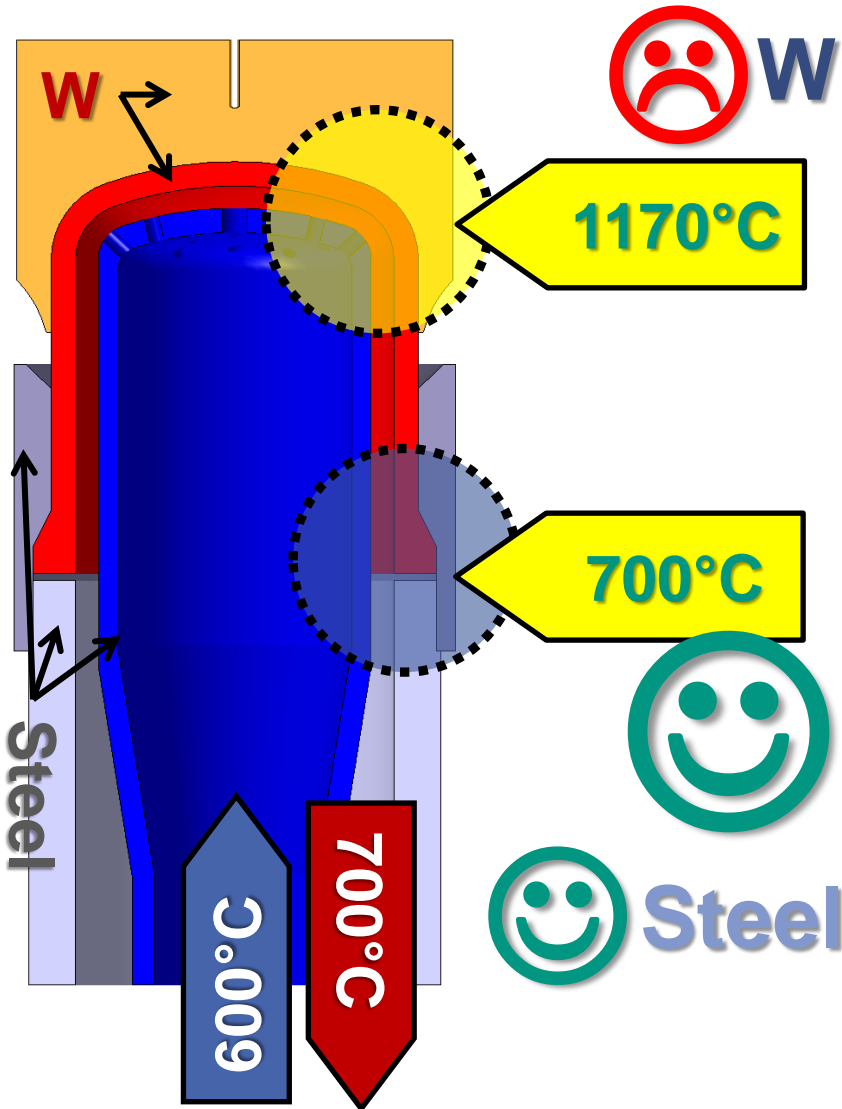


Possible Operating Temp.
 $T_{op} > 800^{\circ}\text{C} \dots 1000^{\circ}\text{C}$



DESIGN ASSESSMENT

MATERIALS / DESIGN WINDOW → FINGER



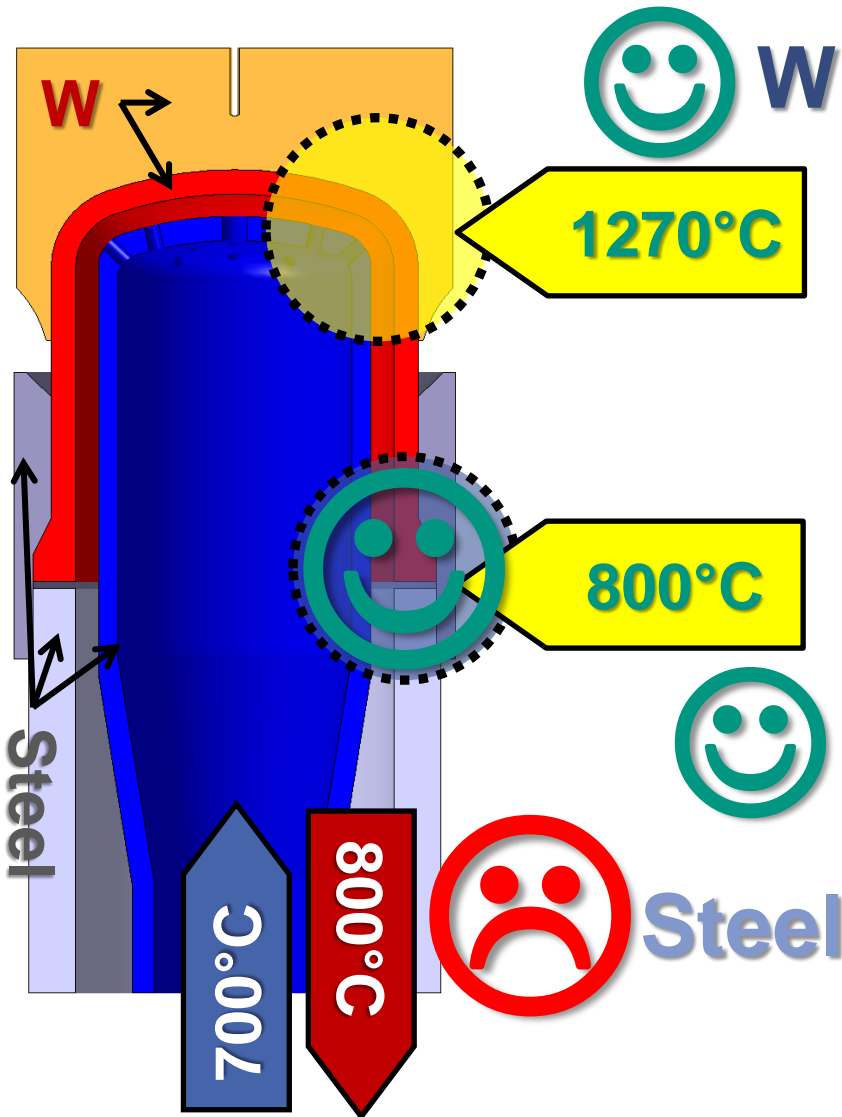
| | | |
|---------------|---|---------|
| Oxidation | → | OK |
| Swelling ~3% | → | ? |
| Embrittlement | → | OK |
| Grain Growth | → | ? (ODS) |

| | | |
|---------------|---|------------------|
| Swelling ~5% | → | ? |
| Embrittlement | → | NO GO (?) |

| | | |
|--------------|---|----------|
| Brazing (Cu) | → | OK (...) |
|--------------|---|----------|

| | | |
|---------------|---|------------------|
| Embrittlement | → | OK |
| Strength, ... | → | ? (ODS) |

MATERIALS / DESIGN WINDOW → FINGER



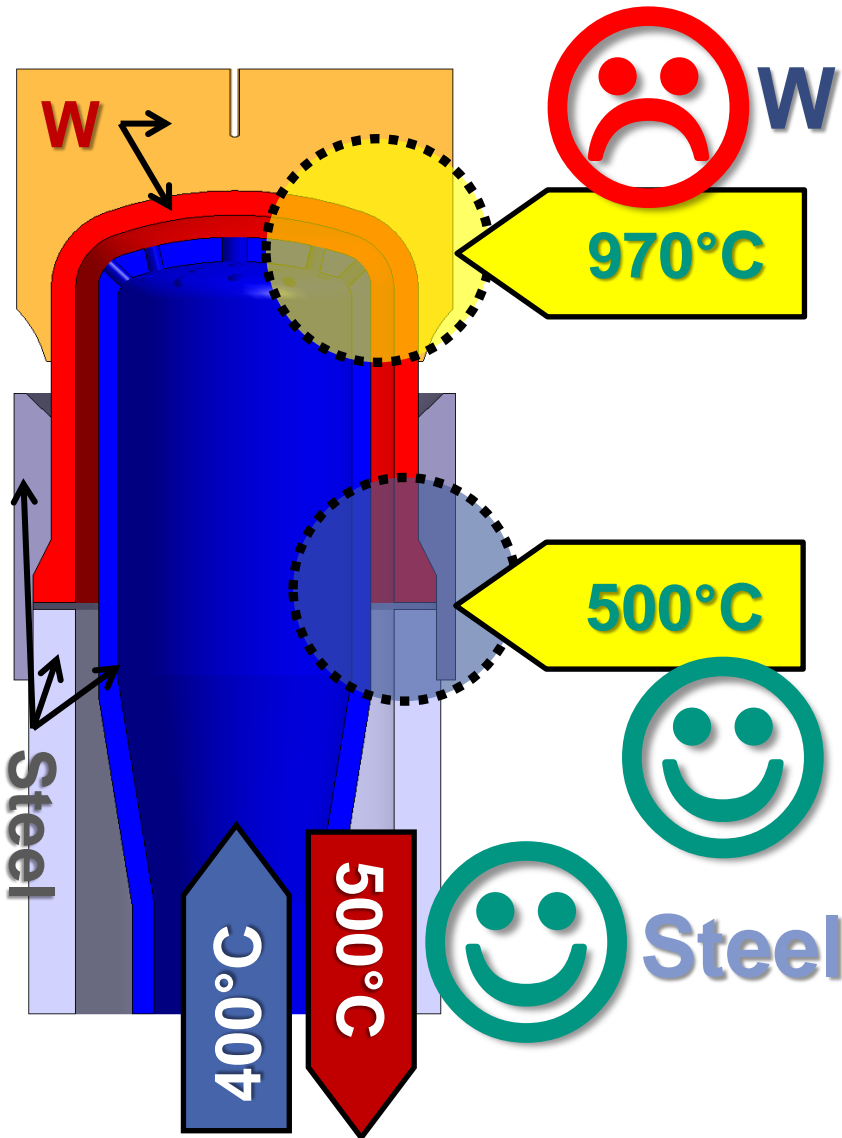
| | | |
|---------------|---|-----|
| Oxidation | → | OK |
| Swelling ~3% | → | ? |
| Embrittlement | → | OK |
| Grain Growth | → | ODS |

| | | |
|---------------|---|----------|
| Swelling ~5% | → | ? |
| Embrittlement | → | OK (tbc) |

| | | |
|--------------|---|----------|
| Brazing (Cu) | → | OK (...) |
|--------------|---|----------|

| | | |
|---------------|---|---------|
| Embrittlement | → | OK |
| Strength, ... | → | ODS ??? |

MATERIALS / DESIGN WINDOW → FINGER



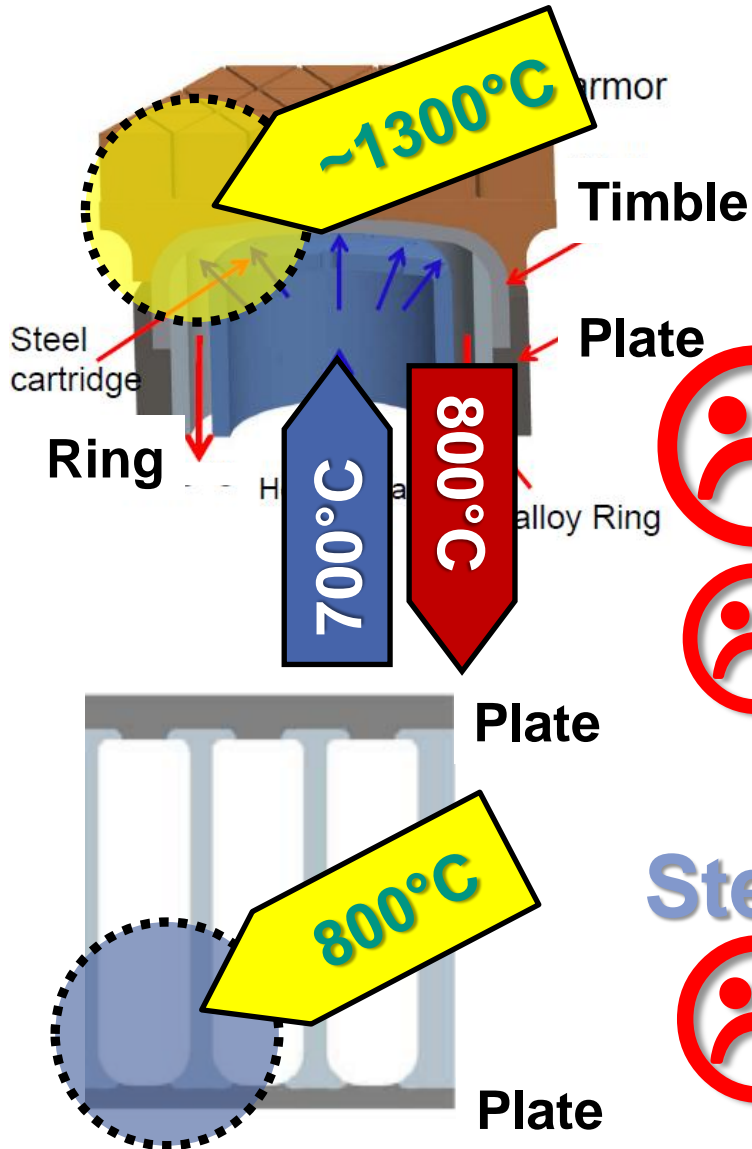
| | | |
|---------------|---|--------|
| Oxidation | → | OK |
| Swelling <3% | → | OK (?) |
| Embrittlement | → | OK |
| Grain Growth | → | OK |

| | | |
|---------------|---|--------------|
| Swelling <2% | → | OK (?) |
| Embrittlement | → | NO GO |

| | | |
|--------------|---|----------|
| Brazing (Cu) | → | OK (...) |
|--------------|---|----------|

| | | |
|---------------|---|----|
| Embrittlement | → | OK |
| Strength, ... | → | OK |

MATERIALS / DESIGN WINDOW → PLATE



W

| | | |
|---------------|---|-----|
| Oxidation | → | OK |
| Swelling ~3% | → | ??? |
| Embrittlement | → | OK |
| Grain Growth | → | ODS |



| | | |
|-------------|---|------------|
| Brazing W→W | → | Pd, Pt ??? |
|-------------|---|------------|



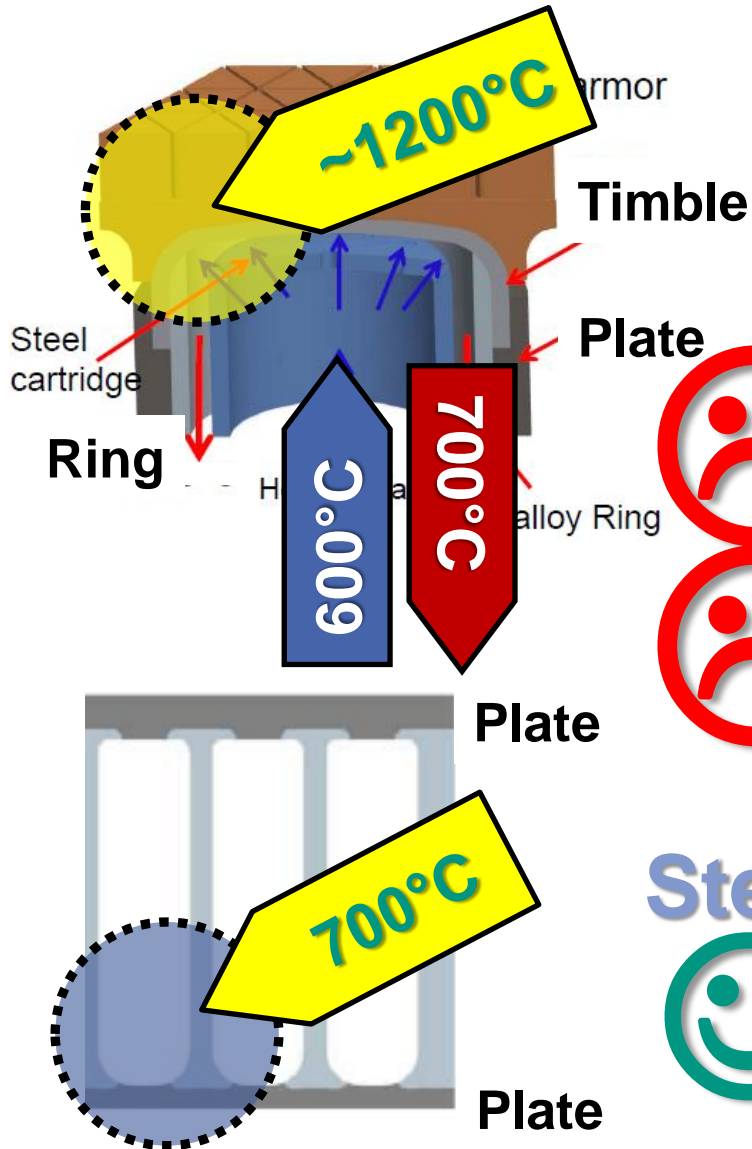
| | | |
|---------------|---|----------|
| Swelling ~5% | → | ????? |
| Embrittlement | → | OK (tbc) |

Steel



| | | |
|---------------|---|---------|
| Embrittlement | → | OK |
| Strength, ... | → | ODS ??? |

MATERIALS / DESIGN WINDOW → PLATE



W

| | | |
|---------------|---|---------|
| Oxidation | → | OK |
| Swelling ~3% | → | ??? |
| Embrittlement | → | OK |
| Grain Growth | → | ? (ODS) |

| | | |
|-------------|---|------------|
| Brazing W→W | → | Pd, Pt ??? |
|-------------|---|------------|

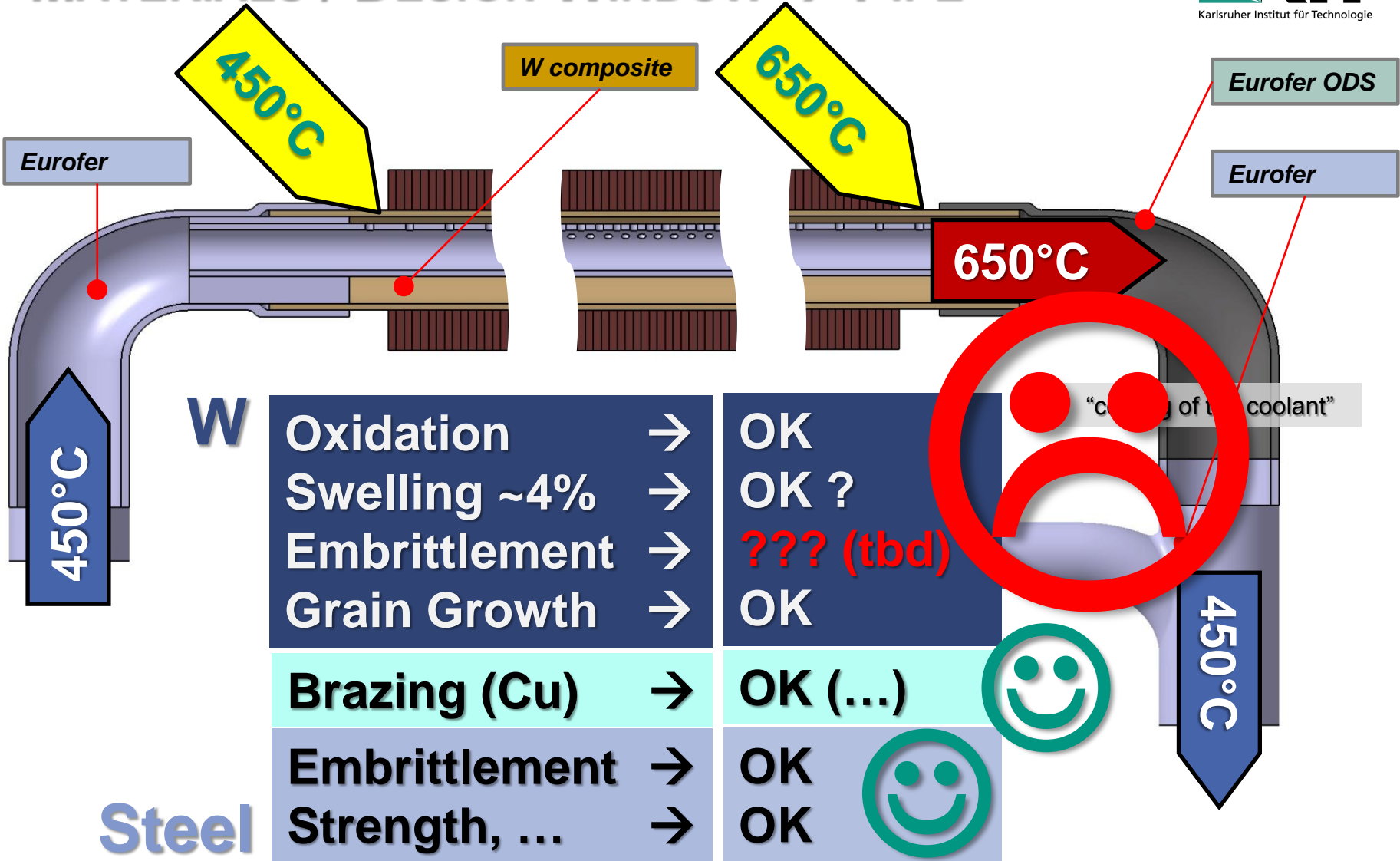
| | | |
|---------------|---|-----------|
| Swelling ~5% | → | ????? |
| Embrittlement | → | NO GO (?) |



Steel


| | | |
|---------------|---|---------|
| Embrittlement | → | OK |
| Strength, ... | → | ? (ODS) |

MATERIALS / DESIGN WINDOW → PIPE





SUMMARY AND PATH FORWARD

SUMMARY

→ Thin plates (<4 mm) of pure W (including small amounts of grain stabilizers, if necessary) are the most suitable semi-finished products for structural applications !

→ The microstructure has to be adapted to the contour of the component (some fabrication processes have to be developed) !

Specific Design Rules for Structural Tungsten Components

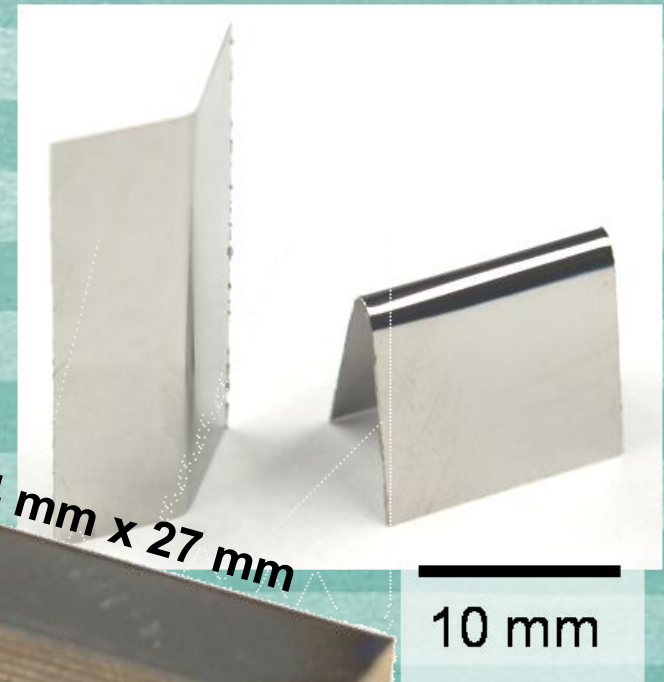
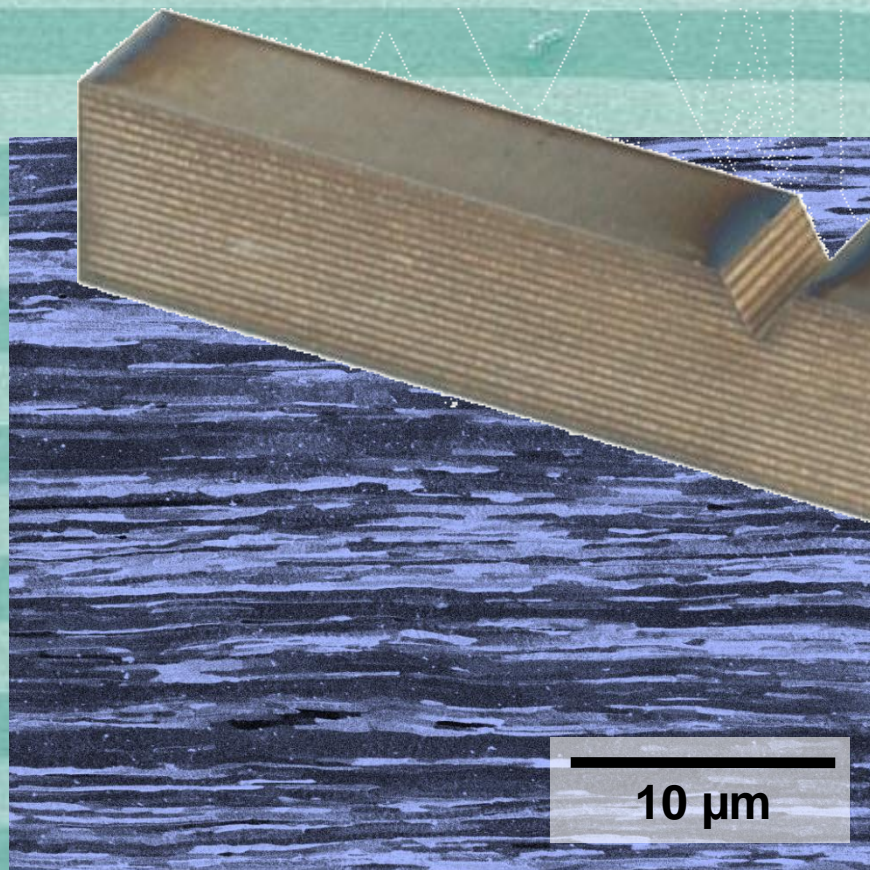
→ Coatings can be used as brazing material for W-steel joints, but needs additional strengthening by desing !

→ Suitable structural W-W joints are not yet demonstrated and characterized ! → Pt, Pd, ...?

→ W irradiation data needed for design (determination of lowest possible operating temperature) !!!

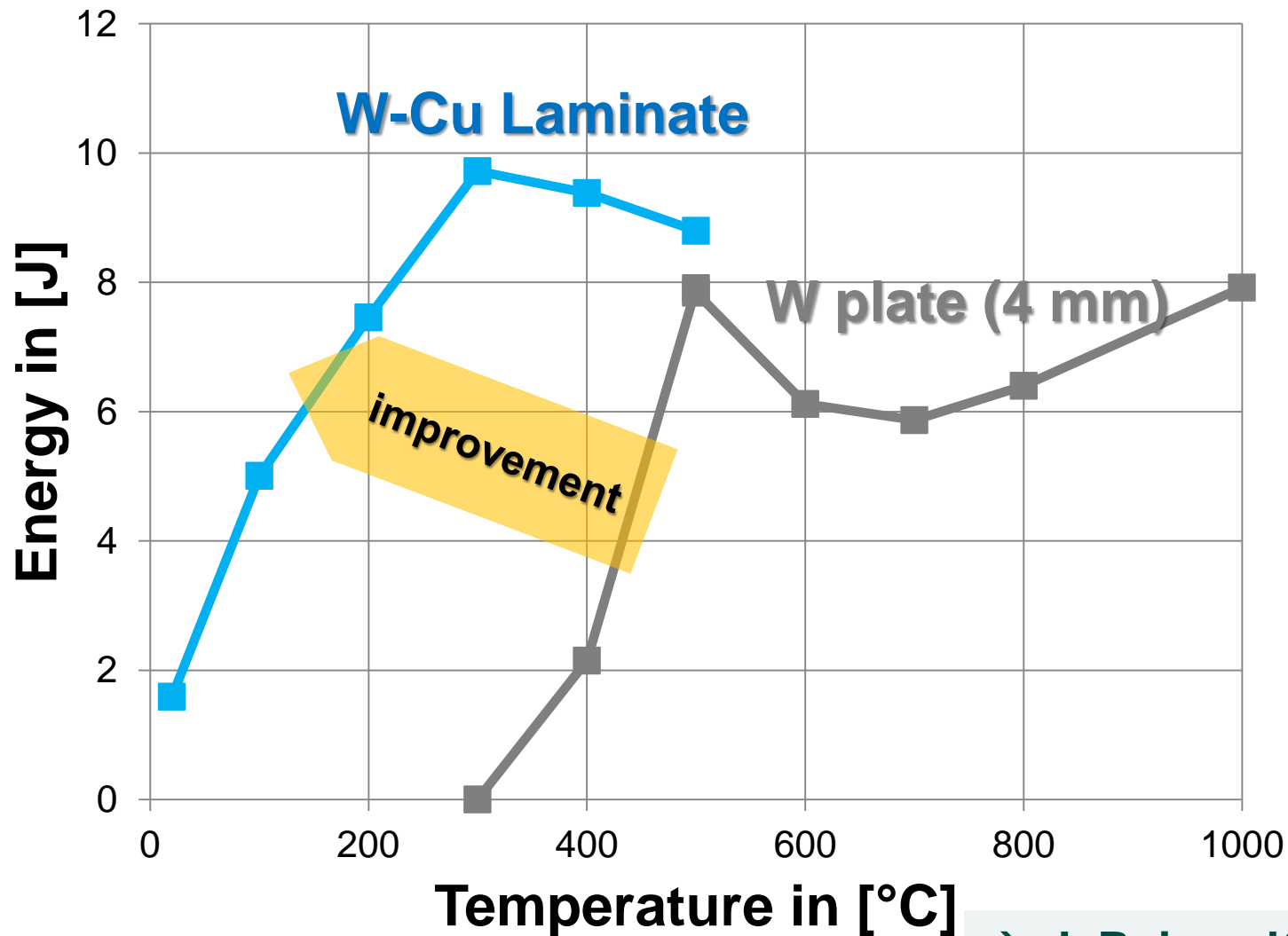


W Laminate Material



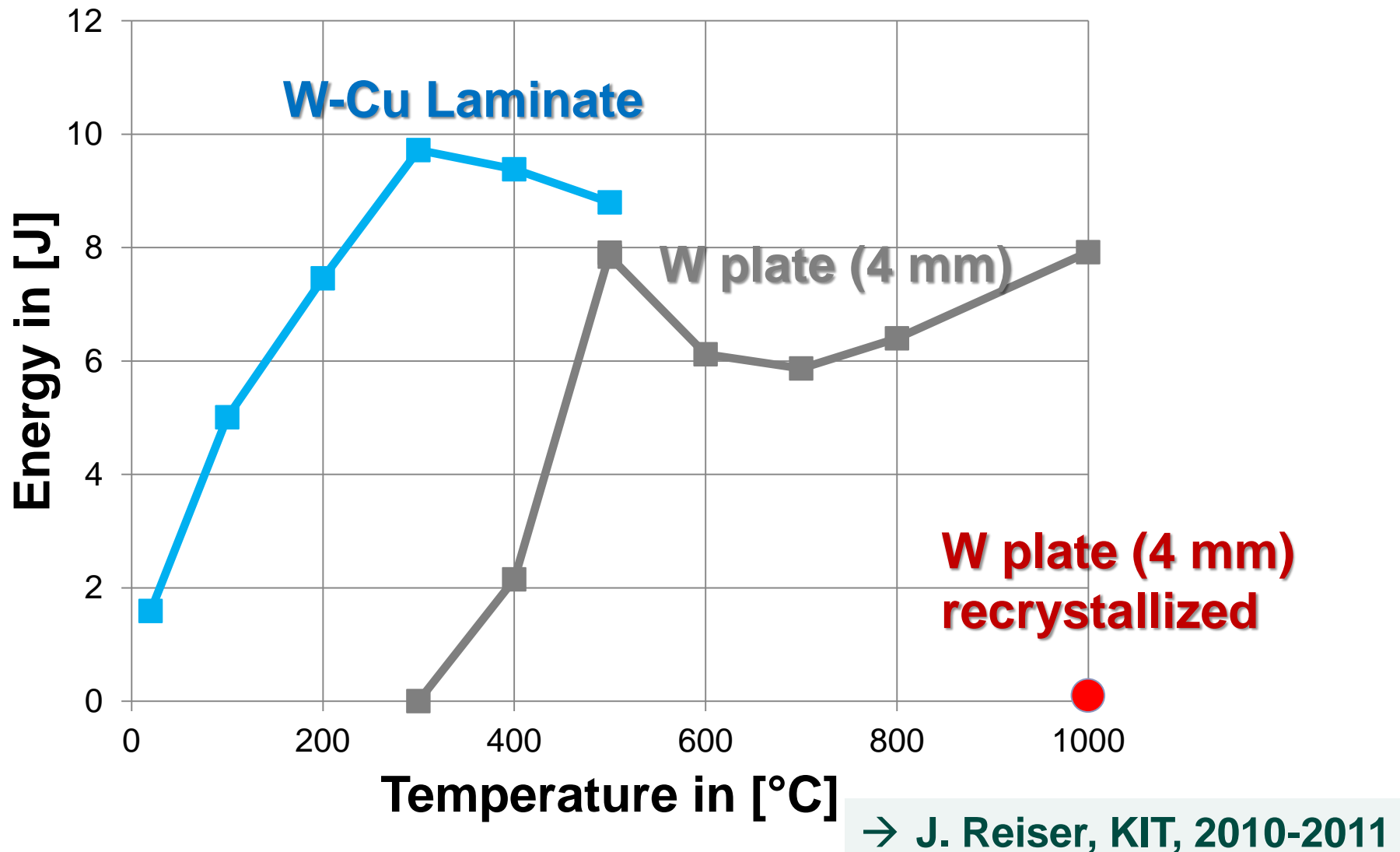
→ J. Reiser, KIT, 2010-2011

PATH FORWARD → TUNGSTEN ALTERNATIVES

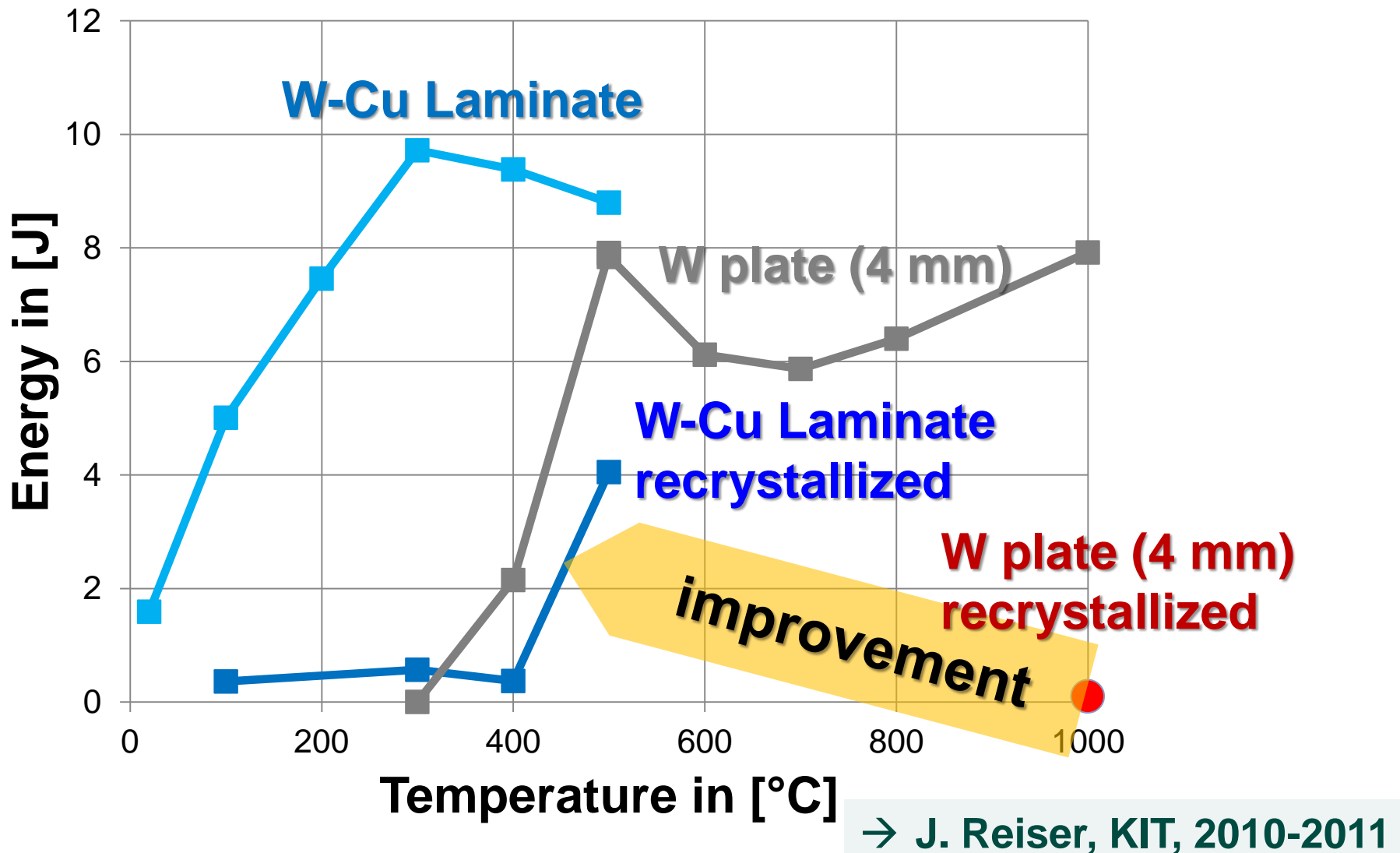


→ J. Reiser, KIT, 2010-2011

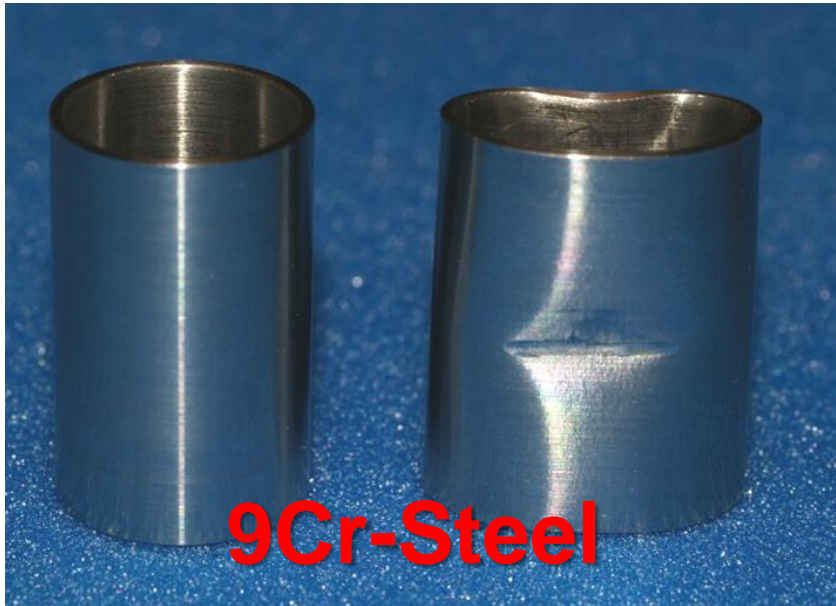
PATH FORWARD → TUNGSTEN ALTERNATIVES



PATH FORWARD → TUNGSTEN ALTERNATIVES



PATH FORWARD → TUNGSTEN ALTERNATIVES



THE ULTIMATE DIVERTOR → GENERIC DESIGN

