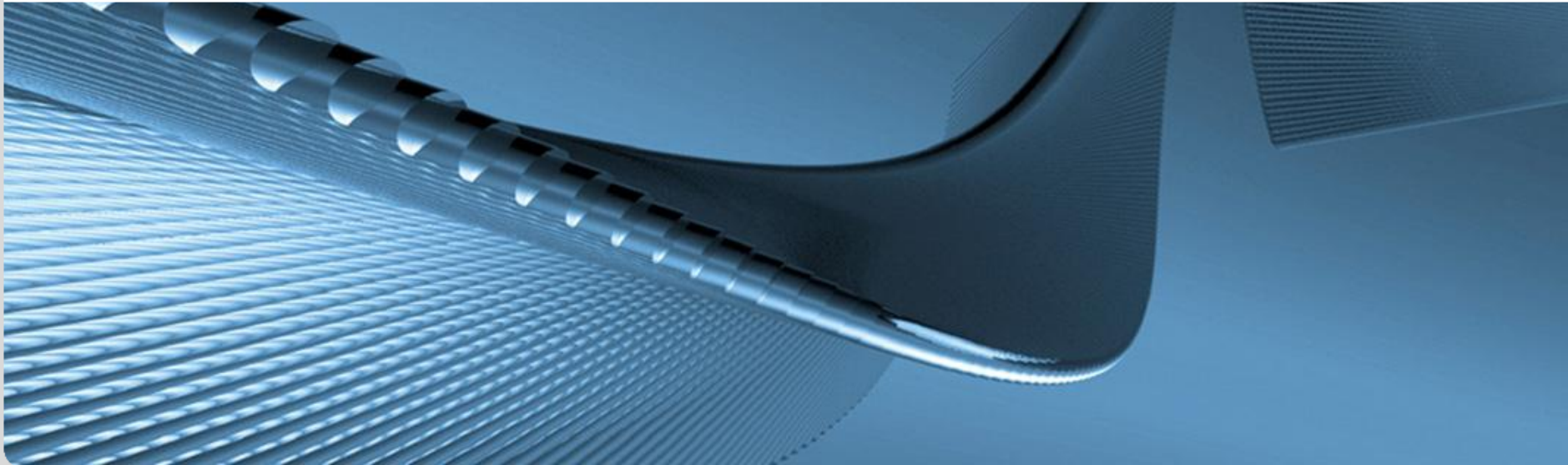


# International tungsten development efforts and the ~~German~~ gas cooled divertor design

**Michael Rieth**

KARLSRUHE INSTITUTE OF TECHNOLOGY – Campus Nord, INSTITUTE FOR APPLIED MATERIALS – Applied Material Physics (KIT, IAM-AWP)



# CONTENTS (→ PRE-DEFINED BY LANCE)

- **Introduction (or focusing on the not quite hopeless problems)**
- **Gas cooled divertor designs**
- **Identification of issues**  
(fabrication, properties, environment, irradiation effects)
- **Material system mapped to design window**  
(Where do we look good, where are still gaps?)
- **Summary and path forward**

# INTRODUCTION



The life time of a power plant divertor is **TWO** years – hopefully!

High heat flux

- High operating temperatures (peaks > 1800°C)
- Microstructural stability, aging, ...
- Thermo-shocks, cyclic loading, fatigue, ...

Heavy ion bombardment

- Sputtering, cracking/fracturing
- Surface interactions and modifications
- Microstructural changes

Neutron load  
15 dpa/year (in W)

- 30 dpa (in W) until end of service
- Transmutation effects (Re, Os)
- Swelling (order of magnitude: 3% for pure W)

**QUESTION:** What can we do about this? How can we improve **ARMOR** materials?

**ANSWER:** There is not much we can do now! We have to live with most properties and effects. A final assessment would require real in-service conditions.

# “REASONABLE” ALLOYING ELEMENTS FOR W

$M_2W$ <b>Be</b>	<b>Mg</b>	$MW$ <b>B</b>	$MW_2$ <b>C</b> $M_{1-x}W$	$M_4W$ <b>Al</b>		<b>Y</b>	<b>La</b>	
<b>Ti</b> >3wt.% >300°C	<b>V</b>	$MW_3$ <b>Cr</b>	<b>Mn</b>	$MW, M_7W_6$ <b>Fe</b>	$M_7W_6$ <b>Co</b>	$MW$ <b>Ni</b>	<b>Cu</b>	
$MW_2$ <b>Zr</b>	<b>Nb</b>	<b>Mo</b>		<b>Ru</b> < 3 wt. %	<b>Rh</b> < 2 wt. %	$M_3W$ <b>Pd</b>	<b>Ag</b>	<b>Cd</b>
$MW_2$ <b>Hf</b>	<b>Ta</b>		$MW$ <b>Re</b> < 26 %	<b>Os</b> < 5 %	$MW$ <b>Ir</b>	$MW$ <b>Pt</b>	<b>Au</b>	

Insoluble

Intermetallic Phases

Line Compounds

Solid Solution

## Pure Tungsten

Grain Stabilized Tungsten  
„ODS Tungsten“

Potassium  
Doping

e.g. WVM, WVMW  
→ Bulb Wire

Oxides &  
Carbides

- $\text{La}_2\text{O}_3$  (e.g. WL10, WL15, WLF0)
- $\text{CeO}_2$  (e.g. WC20)
- $\text{ThO}_2$  (e.g. WT20)
- Weld Electrodes
- $\text{Y}_2\text{O}_3$ ,  $\text{ZrO}_2$ ,  $\text{TiC}$ ,  $\text{HfC}$ , etc.

„Heavy Metals“  
(Two Phases)

- W-Ni-Fe (e.g. Densimet, Inermet)
- W-Cu
- Functional Applications

Alloys  
(Solid Solution)

- W-Re (<26%)  
→ only commercial alloy
- W-V
- W-Ta
- W-Mo
- W-Ti
- (W-Nb)
- Even more brittle as pure tungsten !!!

**Not suitable for structural divertor applications**

## Powder Metallurgy

- Blending
- Pressing
- Sintering
- Hot Forming

**This is so far the only large-scale production route which could handle the 500 tons of W needed for one divertor !**

- Blending with Bin
- Injection Molding
- Debinding/Sintering
- HIP

+ Mass Production  
 + Near finished products  
 + Intrinsic homogeneous microstructure

- S. Antusch, KIT
- J. Opschoor, ECN

- Ball Milling
- Encapsulation
- HIP/Hot Forming

+ Near finished structure  
 + Full scale production route

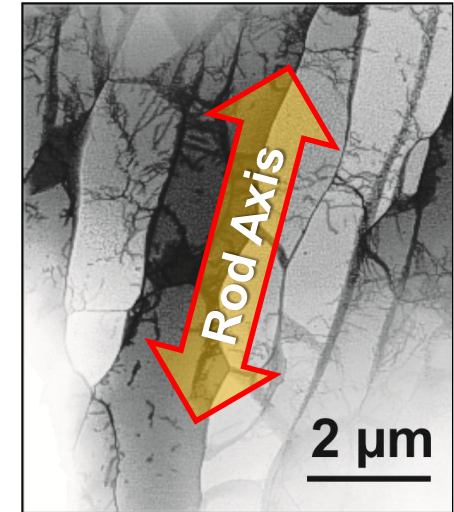
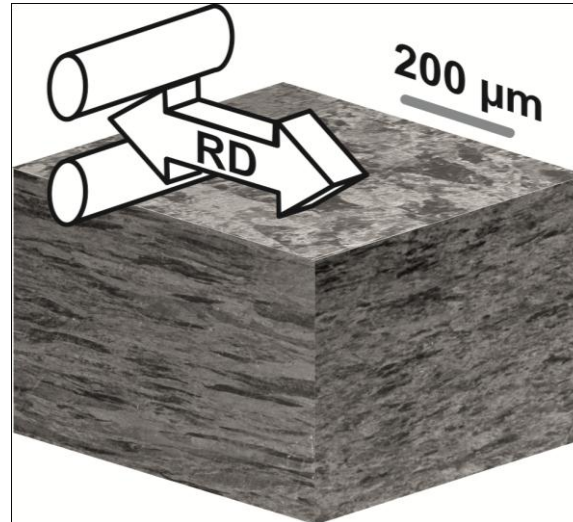
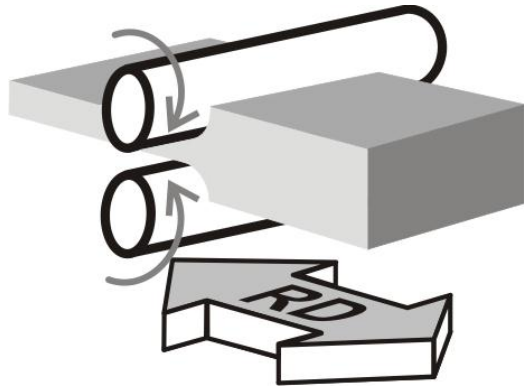
- H. Kirushita, IMR
- N. Baluc, PSI
- A. Muñoz, CIEMAT

**Functional Applications**

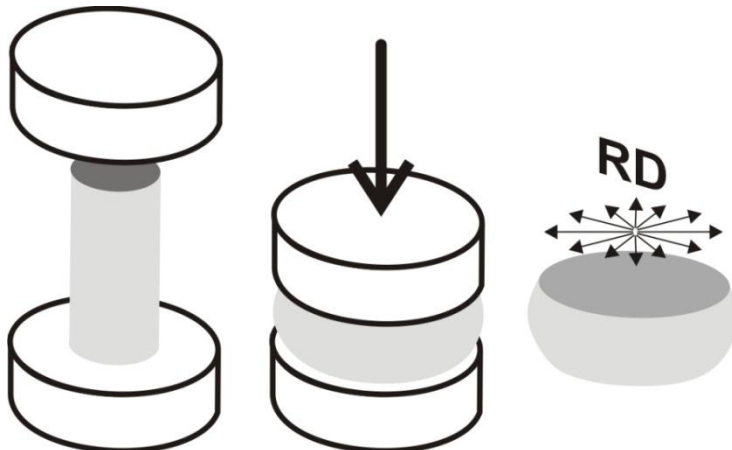
**Still Under Investigation**

# COMMERCIAL SEMI-FINISHED W PRODUCTS

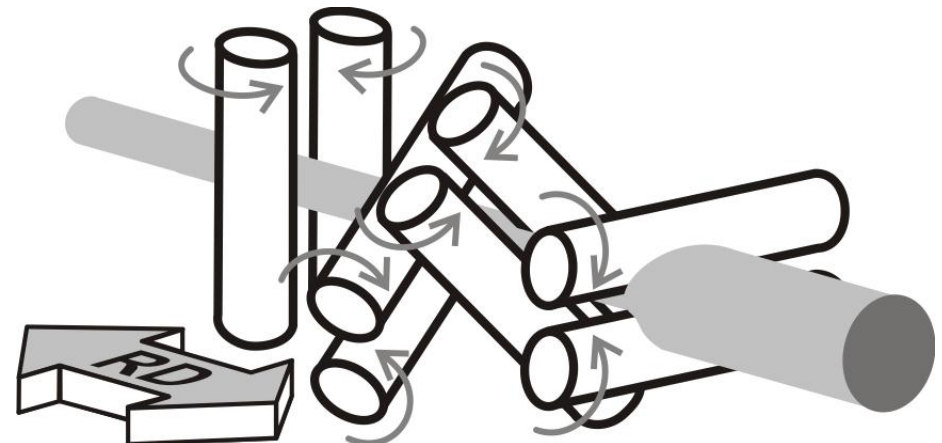
## Rolling Plates



## Forging Round Blanks



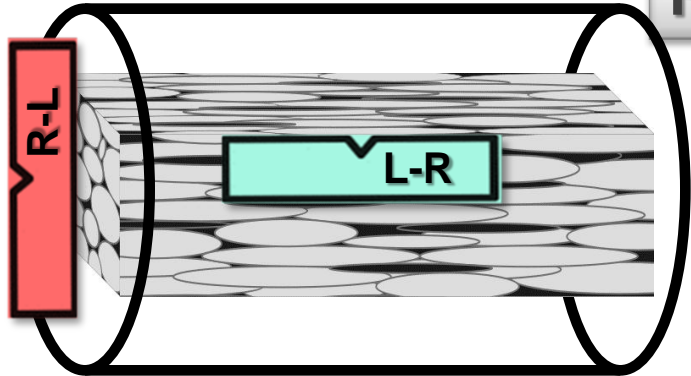
## Rolling/Swaging Rods





# MICROSTRUCTURE AND RELATED PROPERTIES

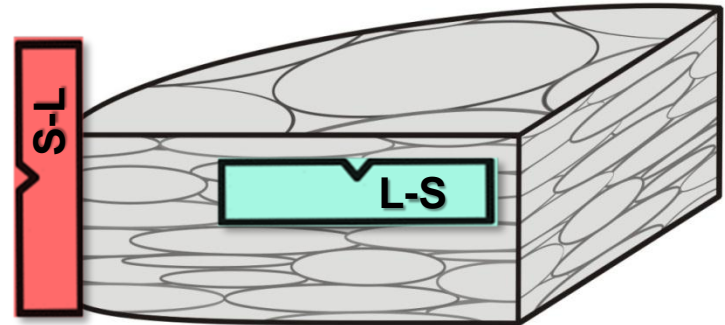
Rods



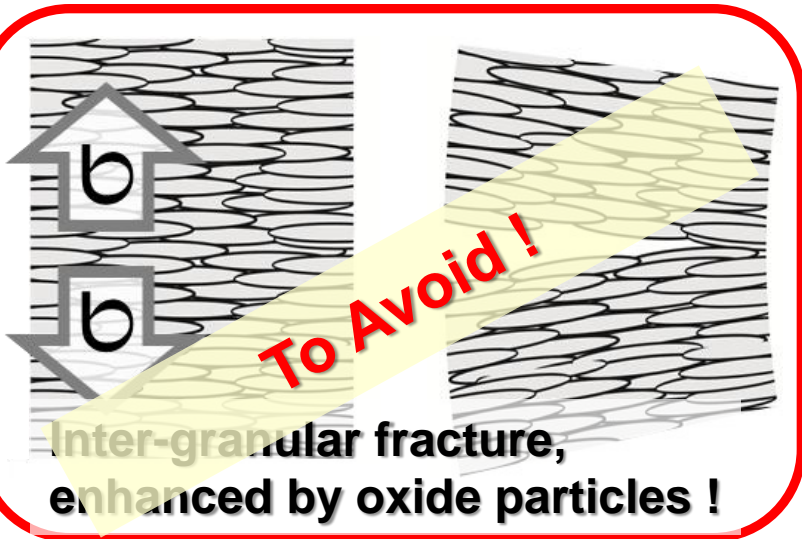
Bundle of „Fibres“

Plates

Round Blanks



Stack of „Pancakes“



So far, the best suitable tungsten materials for structural applications (divertor or other large scale components) are

Thin Plates, Thickness  $< 4$  mm

Produced by Sintering (Hydrogen Atmosphere) and Cross-Rolling

Pure Tungsten (maybe small amounts of grain stabilizers, like  $\text{La}_2\text{O}_3$ )

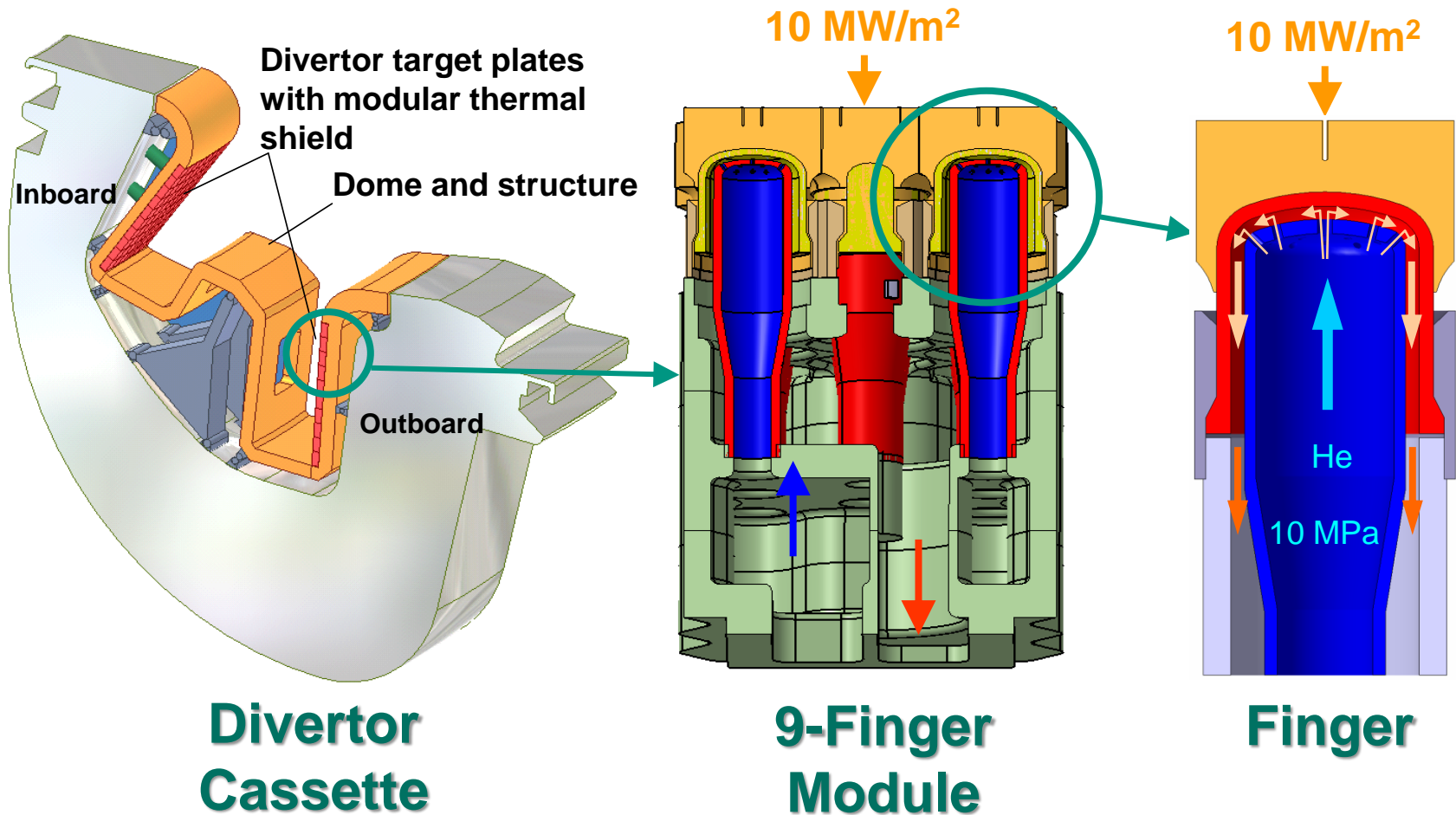
Costs for 500 t → **over 100 Mio. US \$**

based on PLANSEE online catalogue, September 2011, including discount

# 2

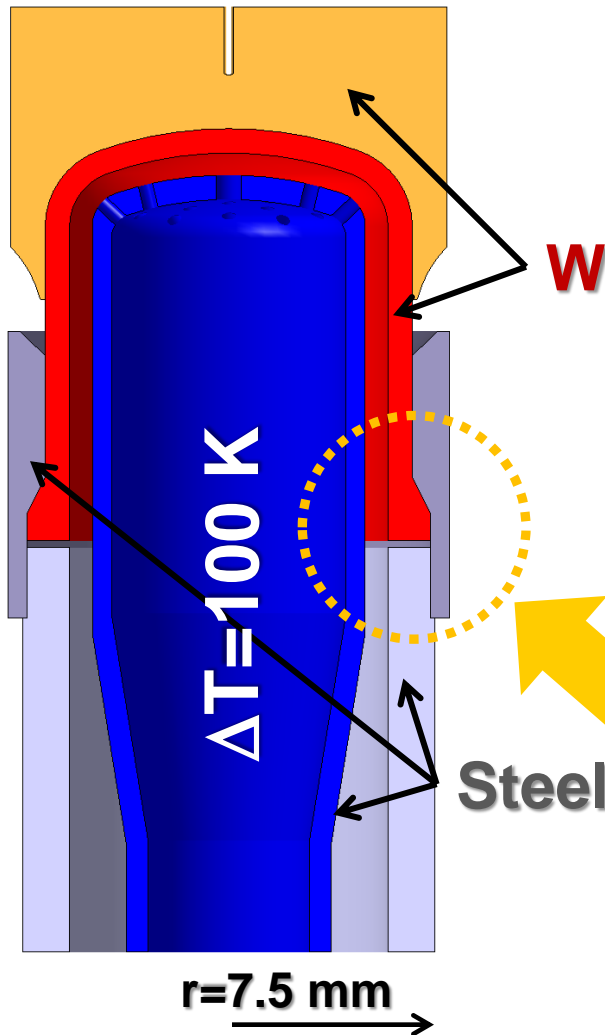
# HELIUM COOLED DIVERTOR DESIGNS

# FINGER DESIGN, JET COOLING



→ P. Norajitra, T. Ihli *et al.*, 2003-2009

# FINGER DESIGN, JET COOLING



+ High heat flux:  $>10 \text{ MW/m}^2$

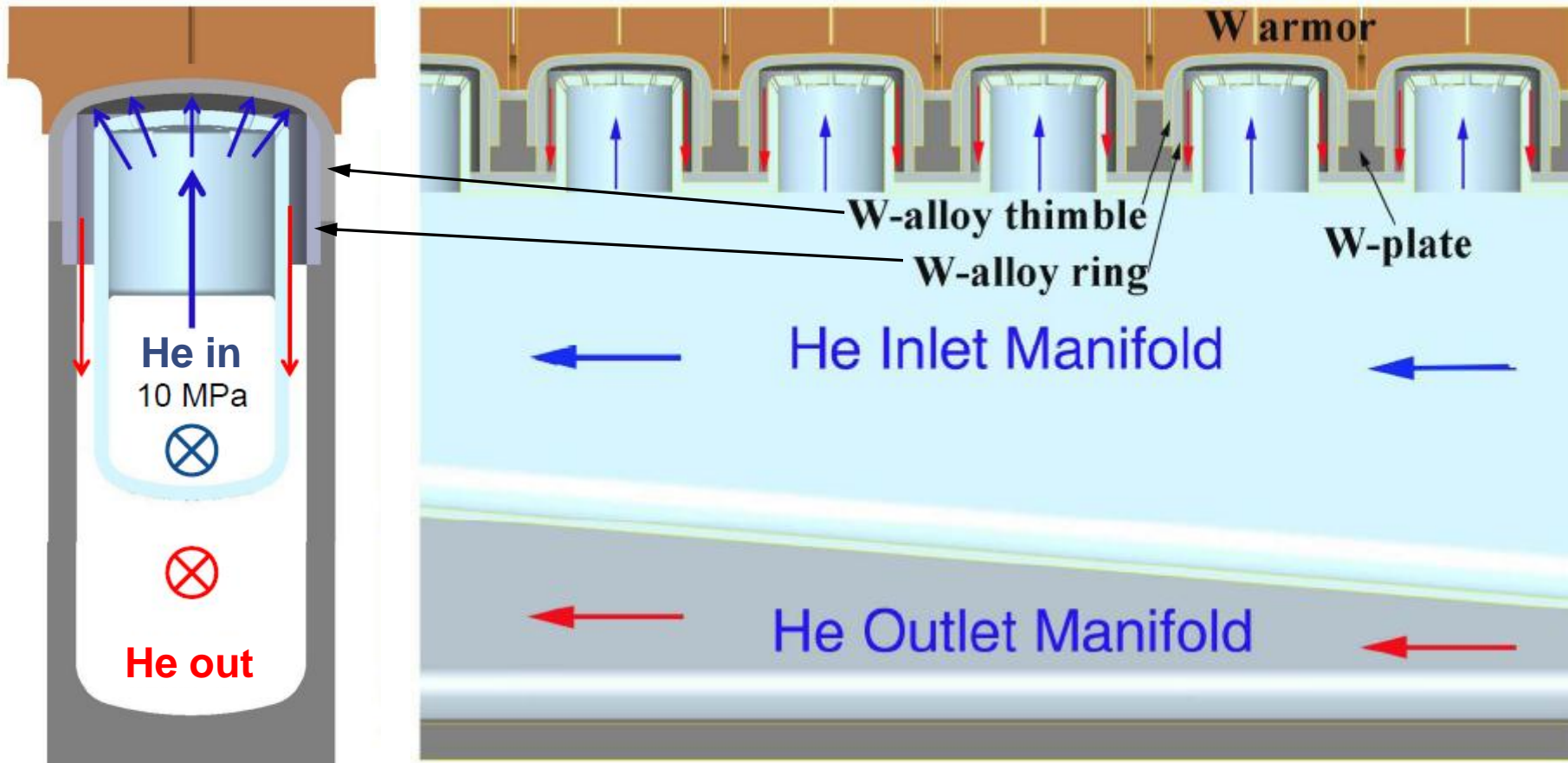
+ Small Size, Thin Walls

- Large Numbers:  $\sim 500\,000$

- Joints between  $W$  and Steel

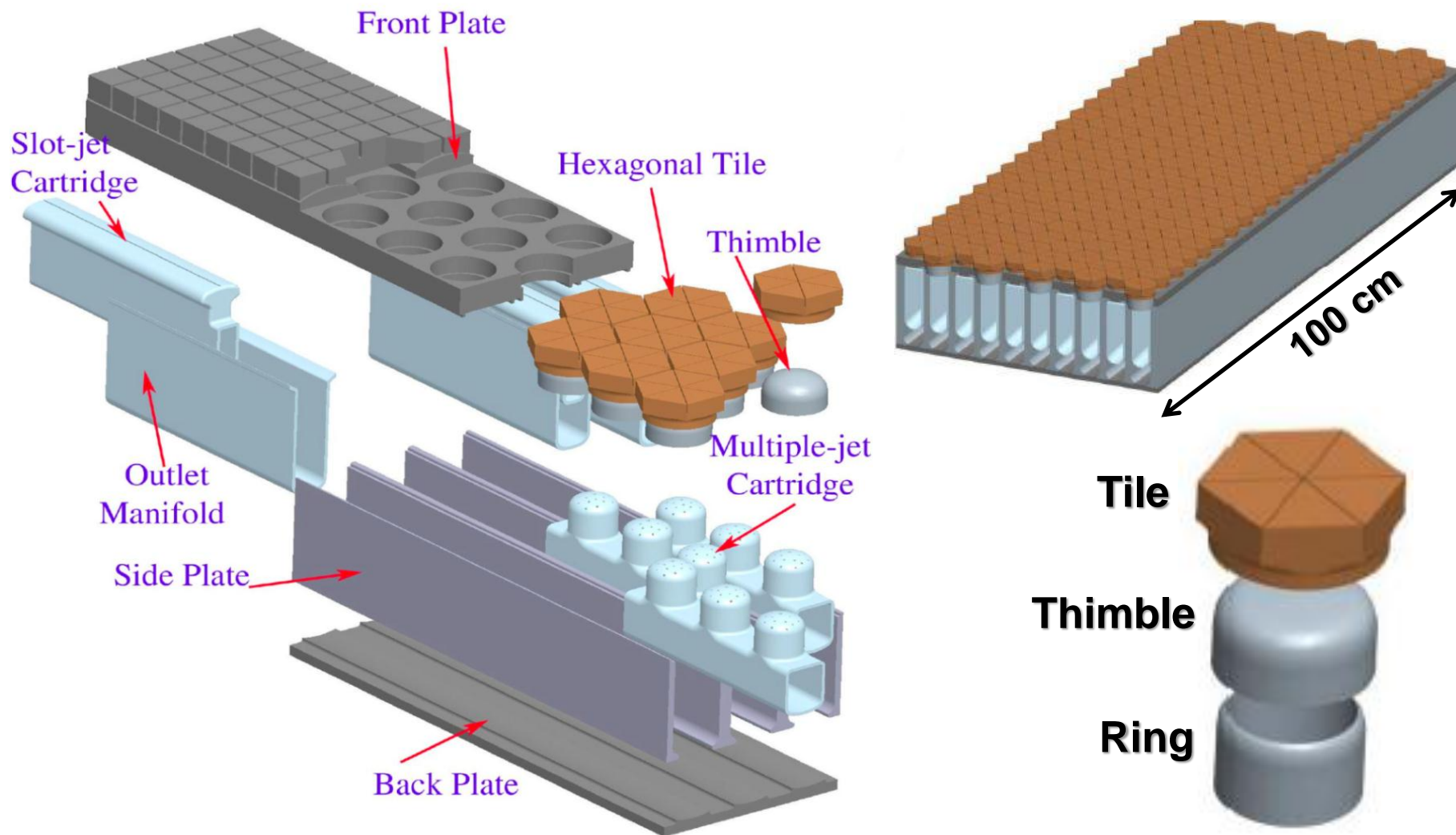
He and W temperature limited by steel  
Ferritic ODS  $\rightarrow 750^\circ\text{C} ???$   
Eurofer ODS, 9Cr ODS  $\rightarrow 650^\circ\text{C}$   
Eurofer 97, F82H  $\rightarrow 550^\circ\text{C}$

# PLATE DESIGN (ARIES), JET COOLING



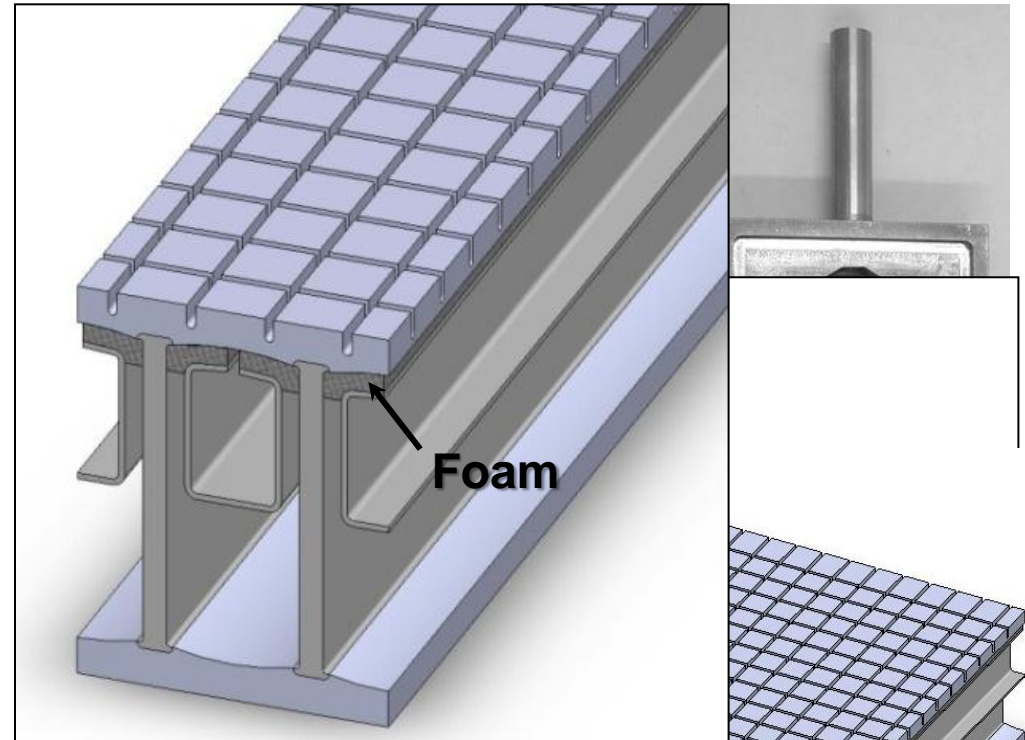
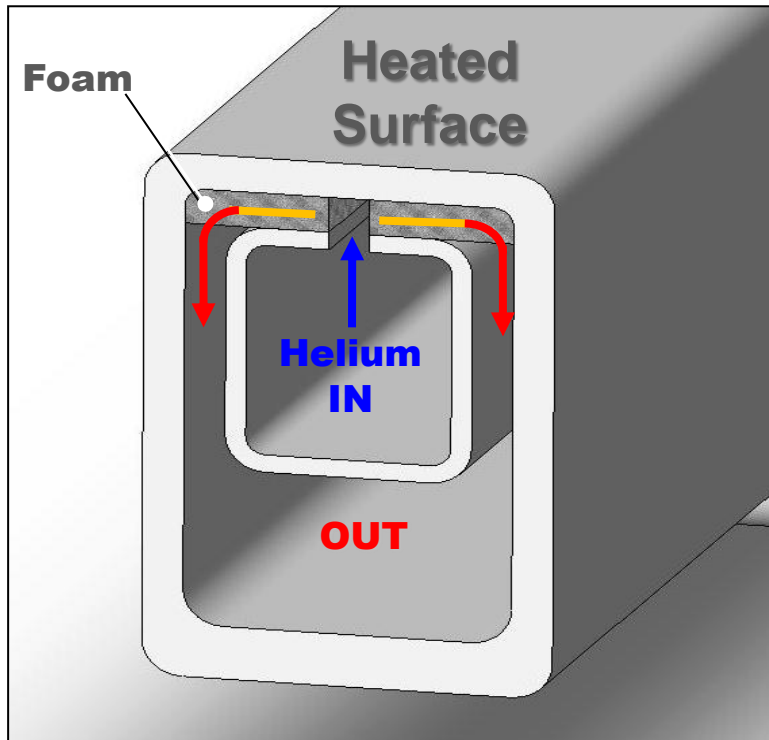
X.R. Wang, S. Malang, M.S. Tillack & ARIES Team, 2008-2011

# PLATE DESIGN (ARIES), JET COOLING



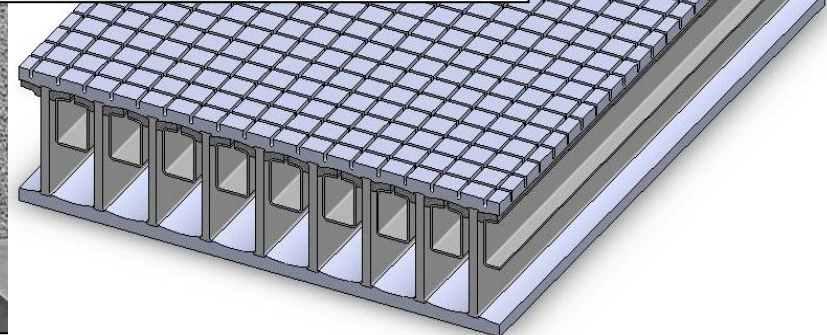
X.R. Wang, S. Malang, M.S. Tillack & ARIES Team, 2008-2011

# PLATE DESIGN, FOAM PROMOTER



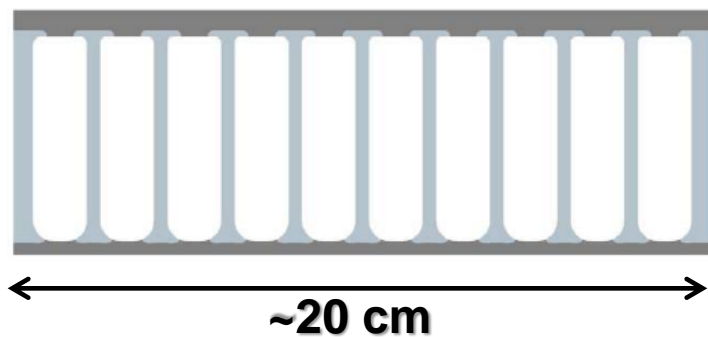
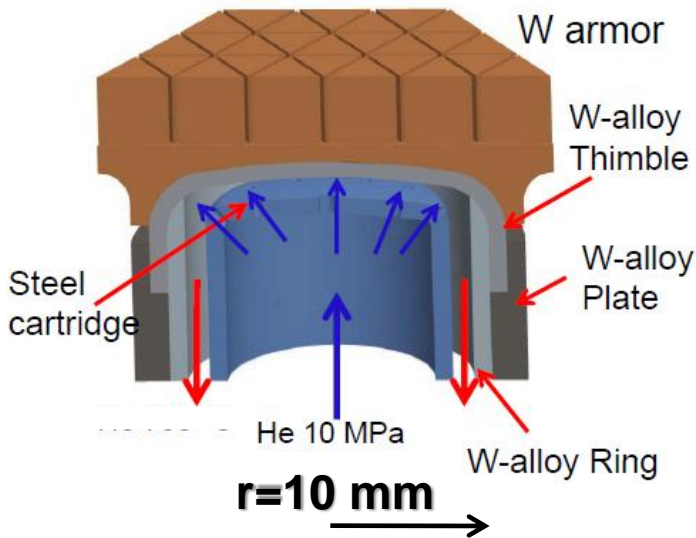
→ S. Sharafat *et al.*, UCLA, 2005-2009

→ Mo, Nb, SiC Foam:  
D. Youchison *et al.*, SNL, 2011





# PLATE DESIGN (ARIES), JET COOLING



+ High heat flux:  $\sim 15\text{ MW/m}^2$

+ Small Size, Thin Walls

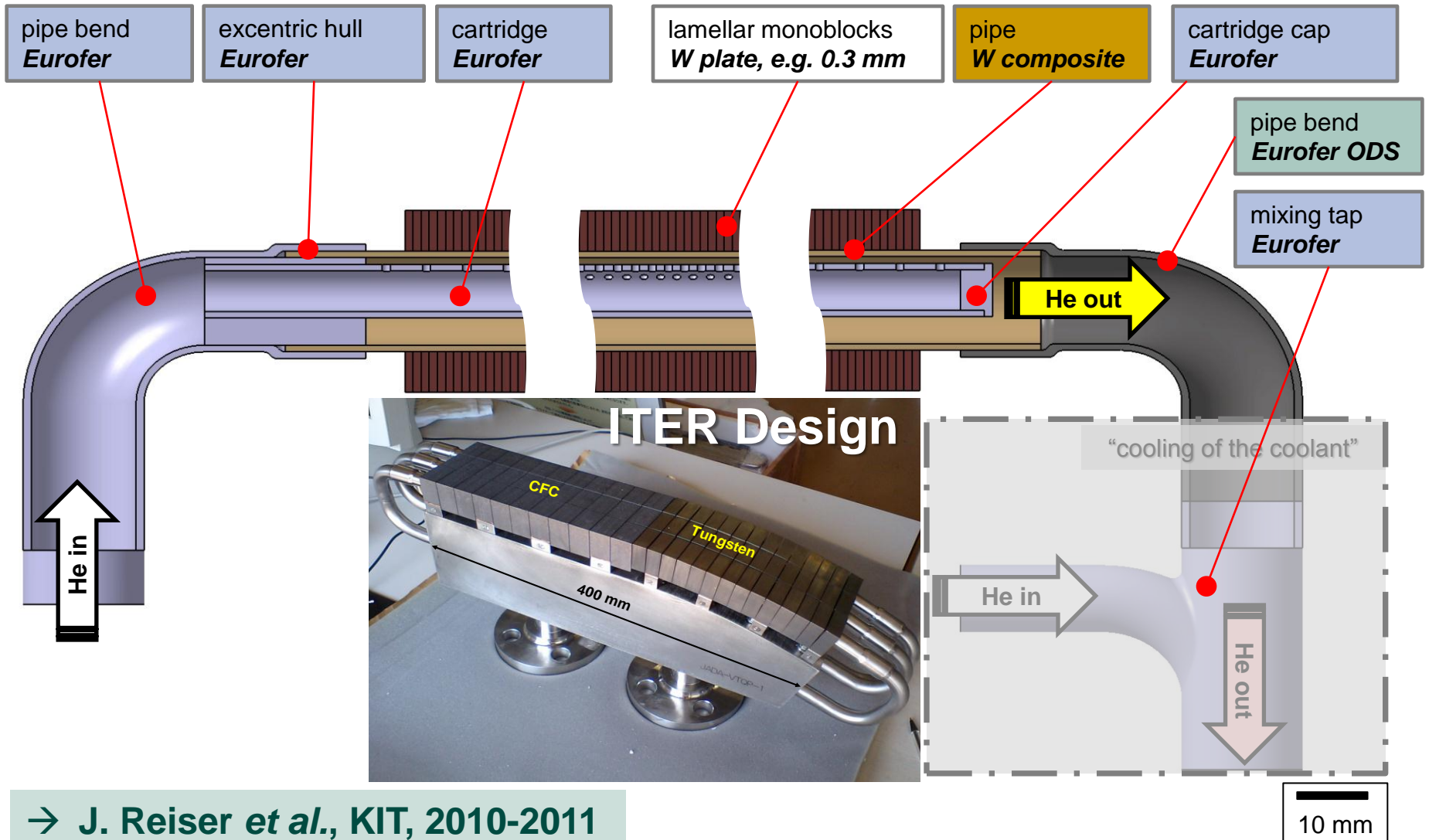
+ “Double Containment”

- Large Numbers:  $\sim 300\ 000$

- Many/Long Struct. W-W Joints

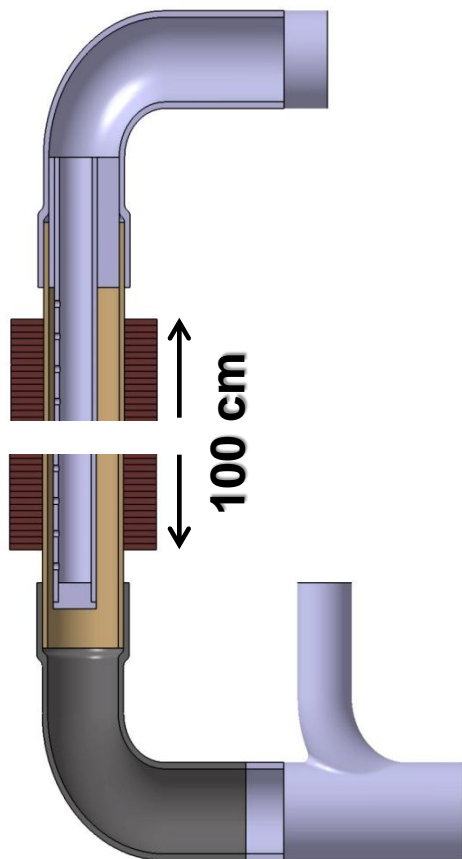
He temperature limited by steel  
(multiple jet cartridges)  
Ferritic ODS  $\rightarrow 750^\circ\text{C}$  ???  
Eurofer ODS, 9Cr ODS  $\rightarrow 650^\circ\text{C}$   
Eurofer 97, F82H  $\rightarrow 550^\circ\text{C}$

# PIPE/MONOBLOCK DESIGN, JET COOLING



→ J. Reiser *et al.*, KIT, 2010-2011

# PIPE/MONOBLOCK DESIGN, JET COOLING



Simple Design

“Easy Joints”

“Small Number of Parts”

Inexpensive



Low Temperatures for W

Low Performance

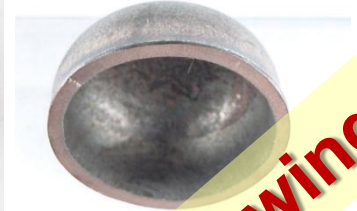
Speculative Pipe Material

He temperature limited by steel  
Eurofer ODS → 650°C (upper)  
Eurofer 97 → 350°C (lower)

# 3

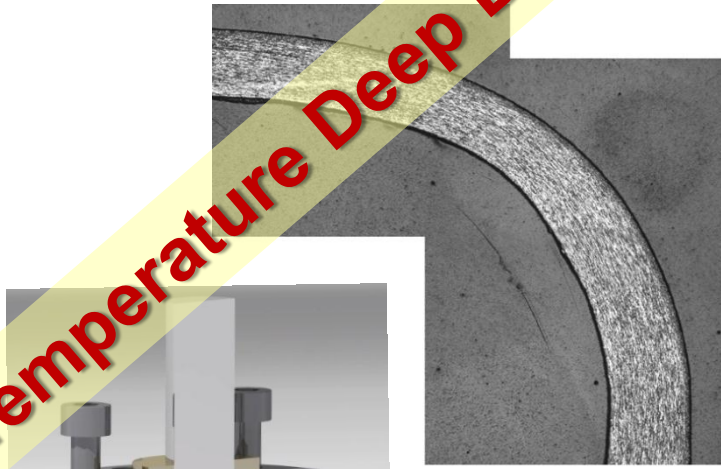
# IDENTIFICATION OF ISSUES

# FABRICATION



Machining: Turning, Milling, Grinding, ...

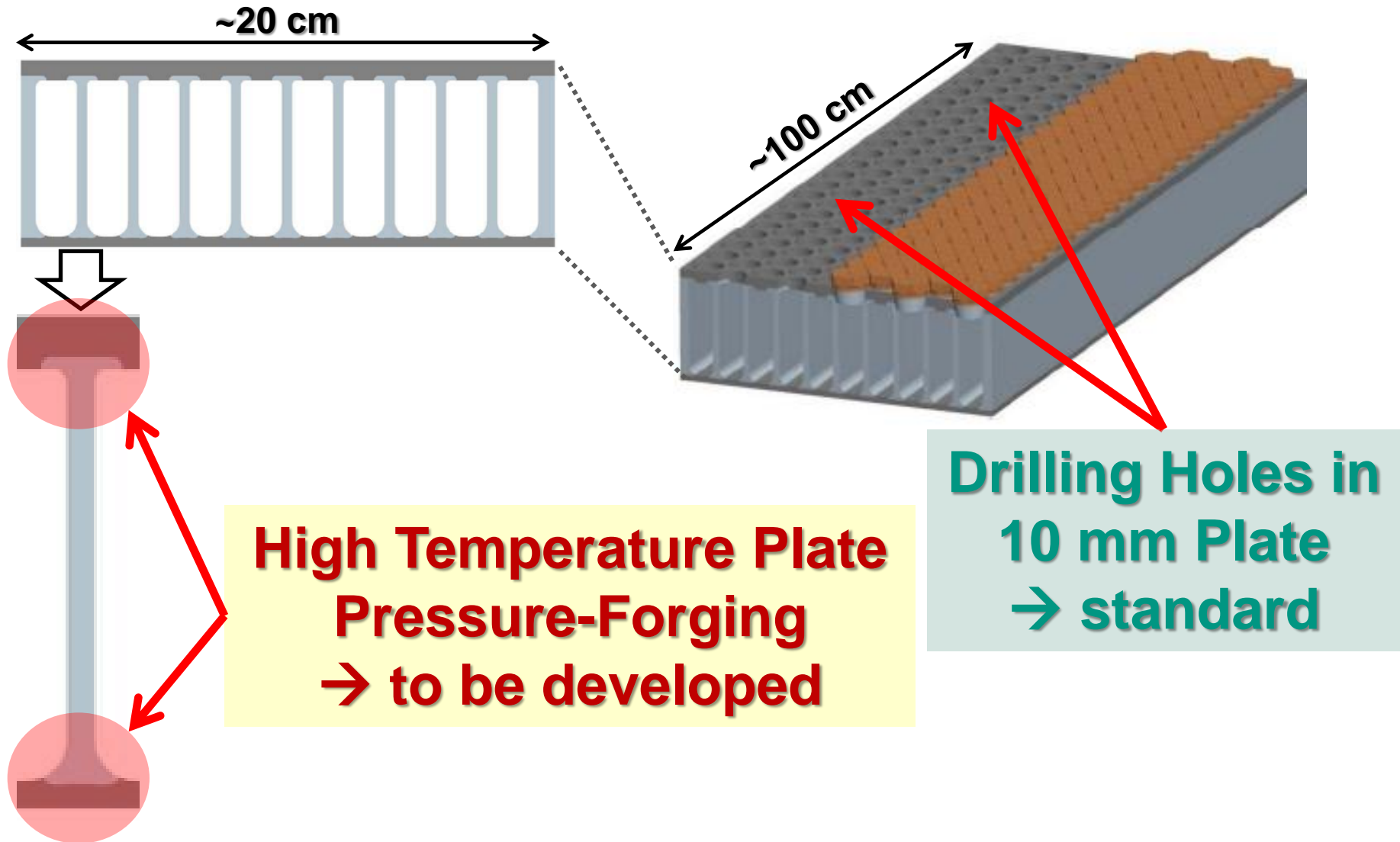
High Temperature Deep Drawing



1mm

P. Norajitra, J. Reiser, S. Baumgärtner *et al.*, KIT

# FABRICATION



**IMPORTANT: We have to consider joints for STRUCTURAL applications!!!  
Joining W tiles to W timbles is NOT considered as structural application!**

## Brazing Material for W-W Joints

Brazing temperature must be  $\gg 900-1200$  °C (operating temp.)

Brazing temperature must be  $< 1800$  °C → Grain growth

Formation of brittle compounds cannot be tolerated

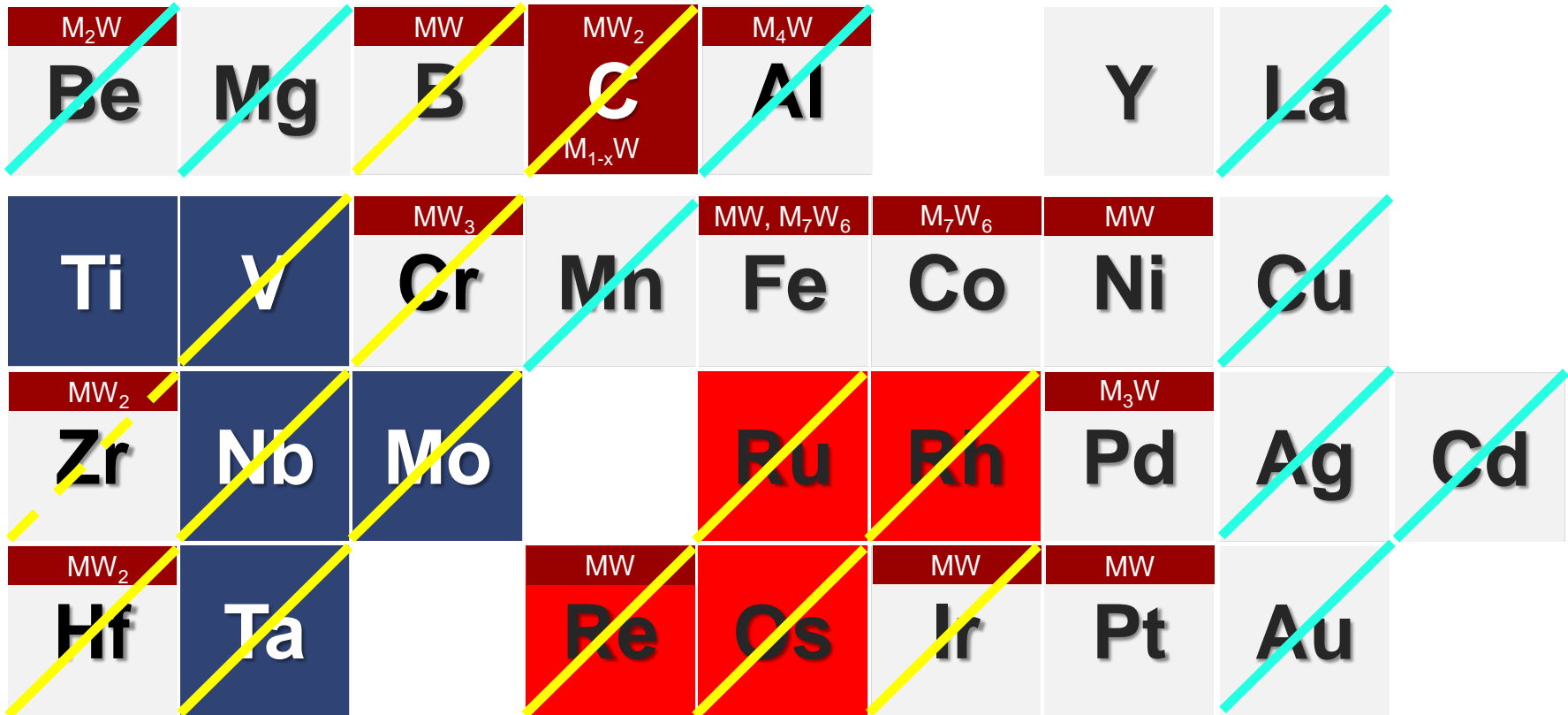
## Brazing Material for W-Steel Joints

Brazing temperature  $< 1100$  °C → Grain growth (in steel)

Brazing temperature must be  $\gg 550-750$  °C (operating temp.)

Formation of brittle compounds cannot be tolerated

# BRAZING W→W



W Insoluble

Intermetallic Phases

W Rich Line Compounds

Solid Solution

$T_m > 1800^\circ$

$T_m < 1400^\circ$



# BRAZING MATERIALS, W→W

1670°C	<b>Ti</b>	<740°C: Difficult, ... ?	
1520°C	<b>Y</b>	Strong <1570°C: Difficult, ... ?	
1850°C	<b>Zr</b>	<2160°C: W → ZrW <1700°C: Brittle Joint <860°C: Zr → ZrW <sub>2</sub>	
1550°C	<b>Pd</b>	<1800°C: Expensive, ... ? <900°C: intermetallic Pd <sub>3</sub> W ???	
1770°C	<b>Pt</b>	<2400°C: Very expensive, ... ? phase Pt <sub>3</sub> W	
1540°C	<b>Fe</b>	<1700°C: μ phase Fe <sub>7</sub> W <sub>6</sub> (Fe,W) <sub>4</sub> <1000°C: Laves phase Fe <sub>2</sub> W	
1500°C	<b>Co</b>	<1700°C: μ phase Co <sub>7</sub> W <sub>6</sub> (Co,W) <sub>4</sub> <1000°C: Laves phase Co <sub>3</sub> W	
1450°C	<b>Ni</b>	<1000°C: peritectoid intermetallics NiW <950°C: peritectoid intermetallic Ni <sub>4</sub> W	

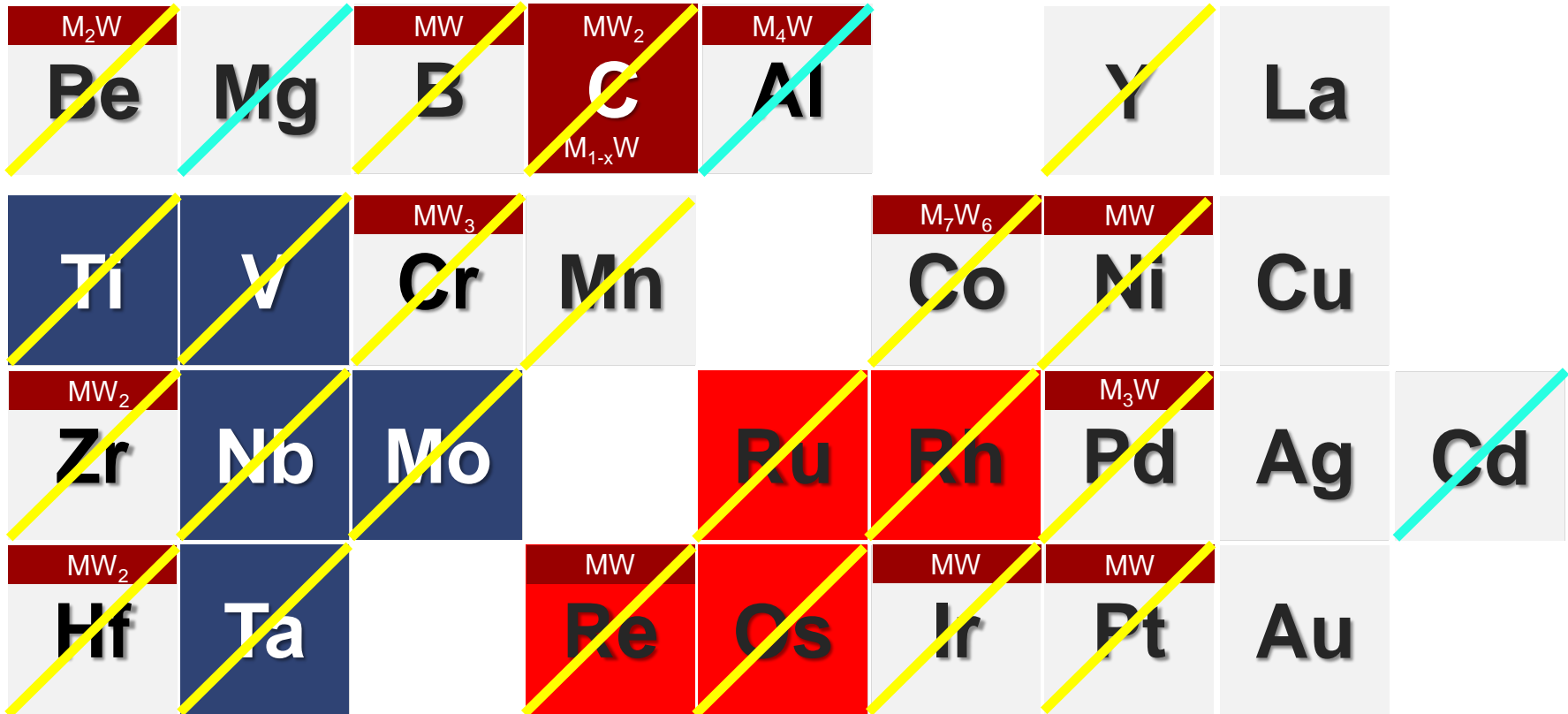
→ T. Hirai, 2008

**Brittle Joints**

W, Ni, Fe, Co  
Intermetallic phases

WL10

# BRAZING W → STEEL



W Insoluble

Intermetallic Phases

W Rich Line Compounds

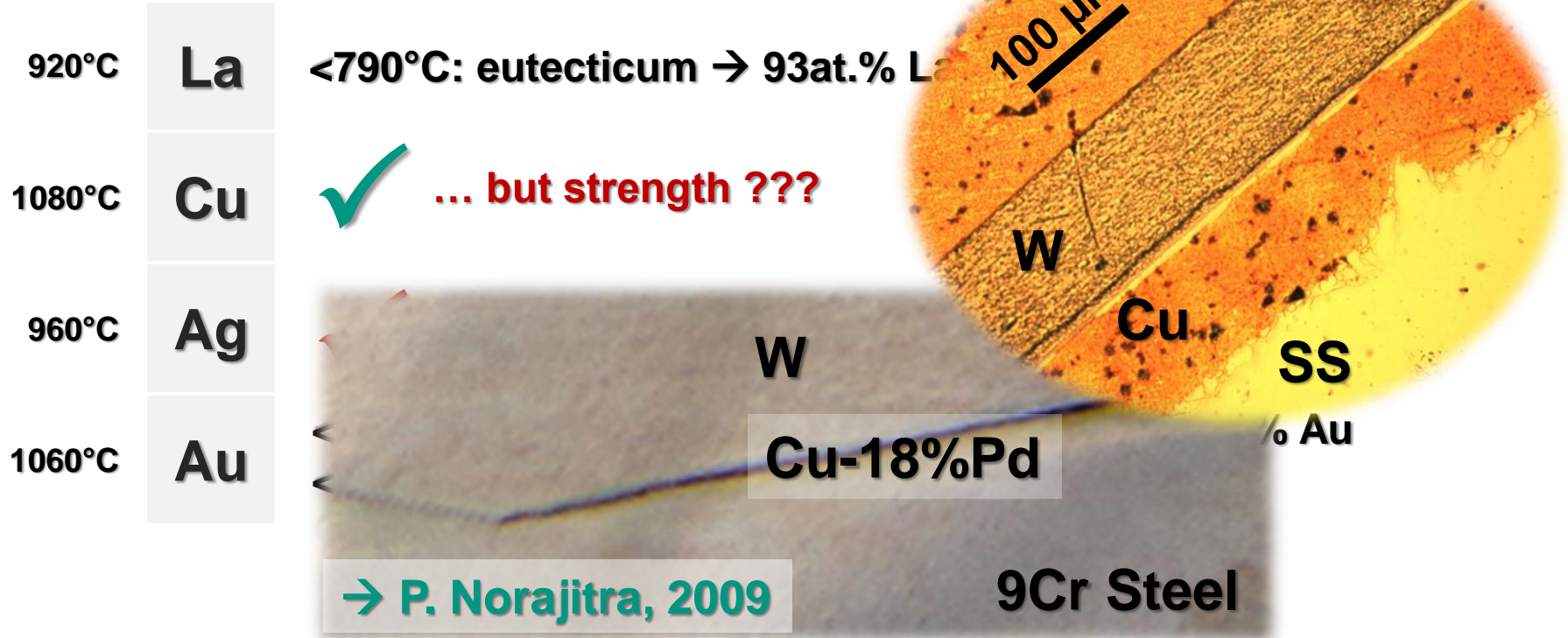
Solid Solution

$T_m > 1200^\circ$

$T_m < 900^\circ$

# BRAZING MATERIALS, W → STEEL

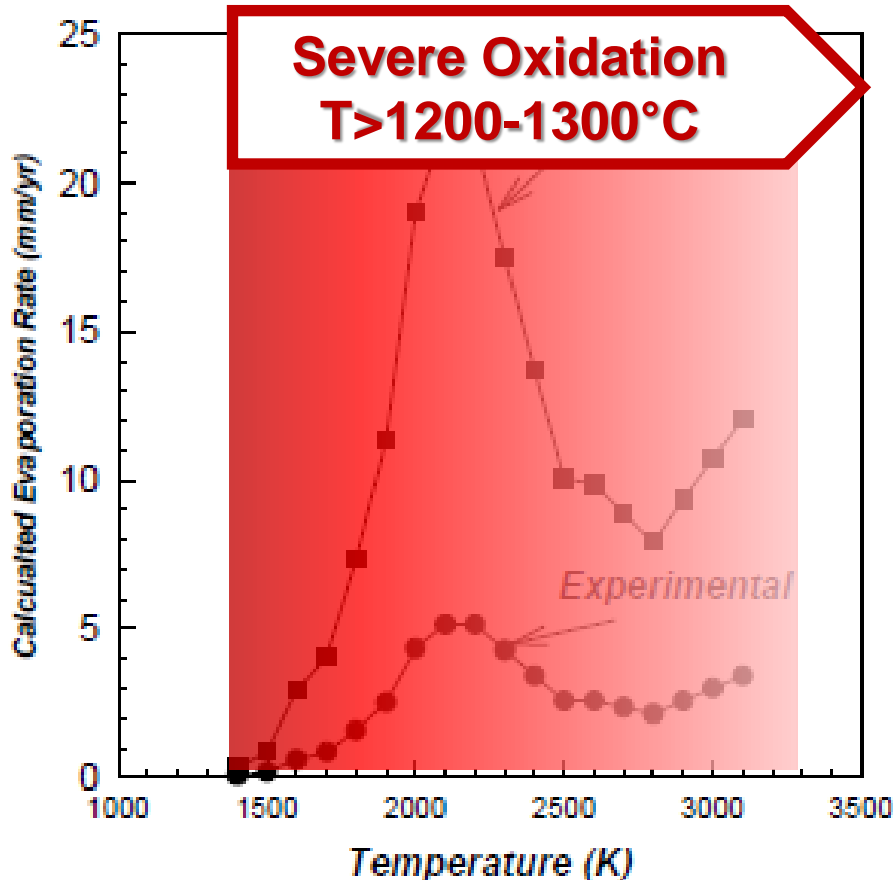
→ J. Reiser, 2011



**CONCLUSION: Copper has to be used as sealing rather than as a braze material !!!**

# ENVIRONMENT → OXIDATION

**WO<sub>3</sub> yellow, T<sub>m</sub>=1470°C, 7200 kg/m<sup>3</sup>, volatile in vacuum**

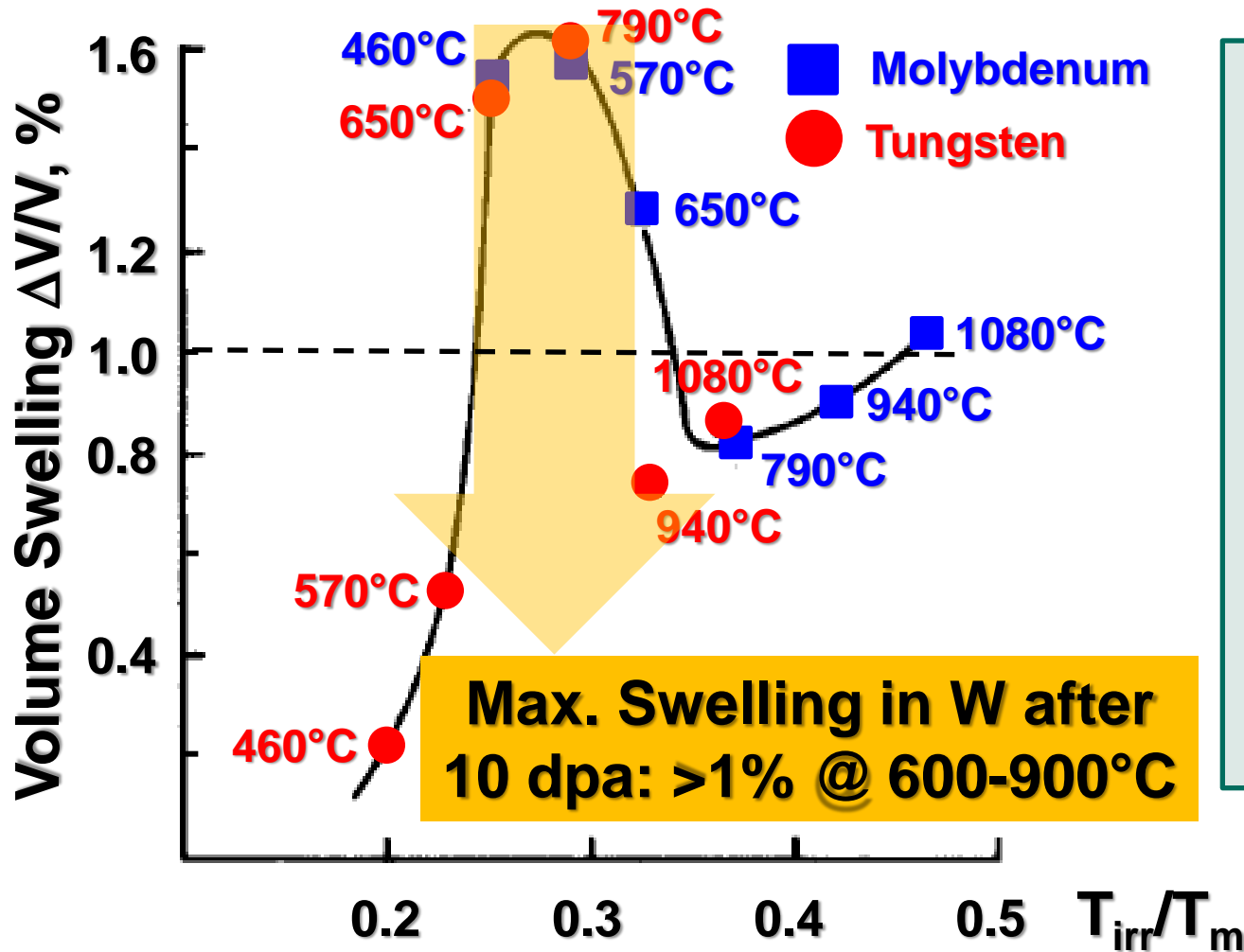


## CONCLUSION

For tungsten operating at 50 atm. He coolant, at 0.1 ppm oxygen, the upper temperature is estimated at 1200-1300°C.

→ N.M. Ghoniem, 1998

# IRRADIATION EFFECTS → SWELLING



**EBR-II**

$E_n > 1 \text{ MeV}$   
 $1 \times 10^{22} \text{ n/cm}^2$

$E_n > 0.1 \text{ MeV}$   
 $1.6 \times 10^{22} \text{ n/cm}^2$

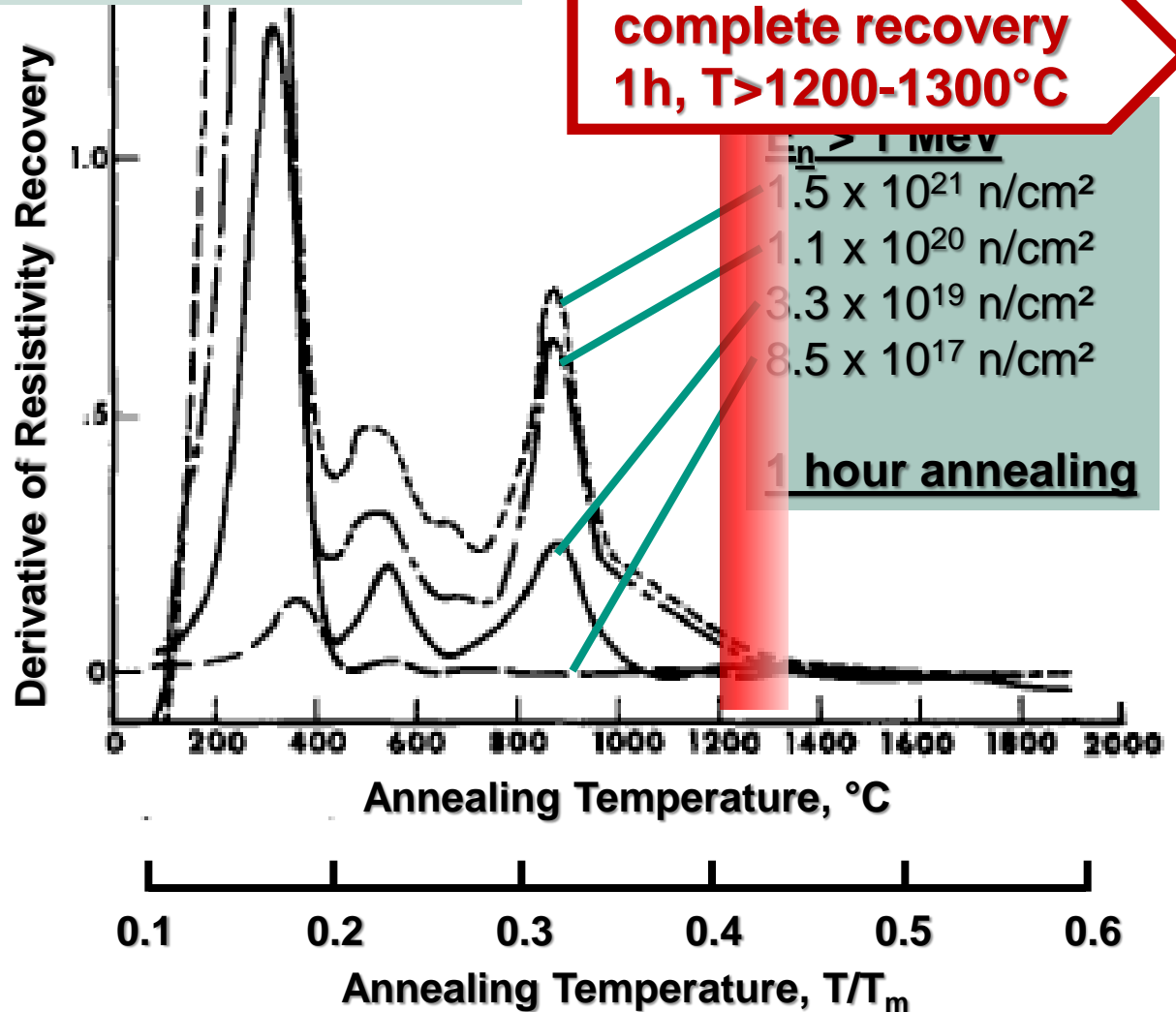
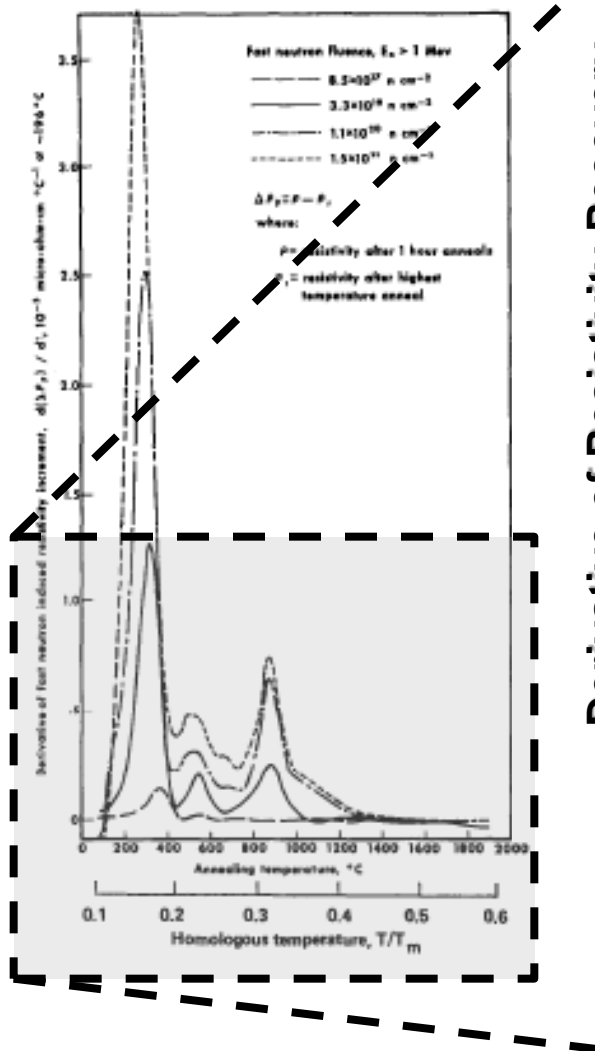
→ 29 dpa in Mo

→ 9.6 dpa in W

→ F. Lee, J. Matolich, J. Moteff, JNM 62 (1976) 115-117

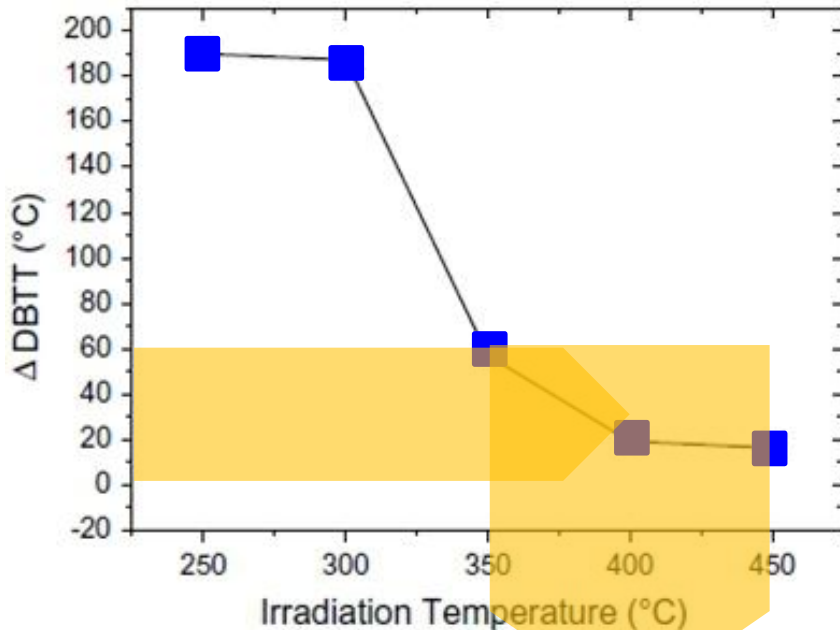
# IRRADIATION EFFECTS → RECOVERY

→ L.K. Keys, J. Moteff, JNM 34 (1970) 260-280



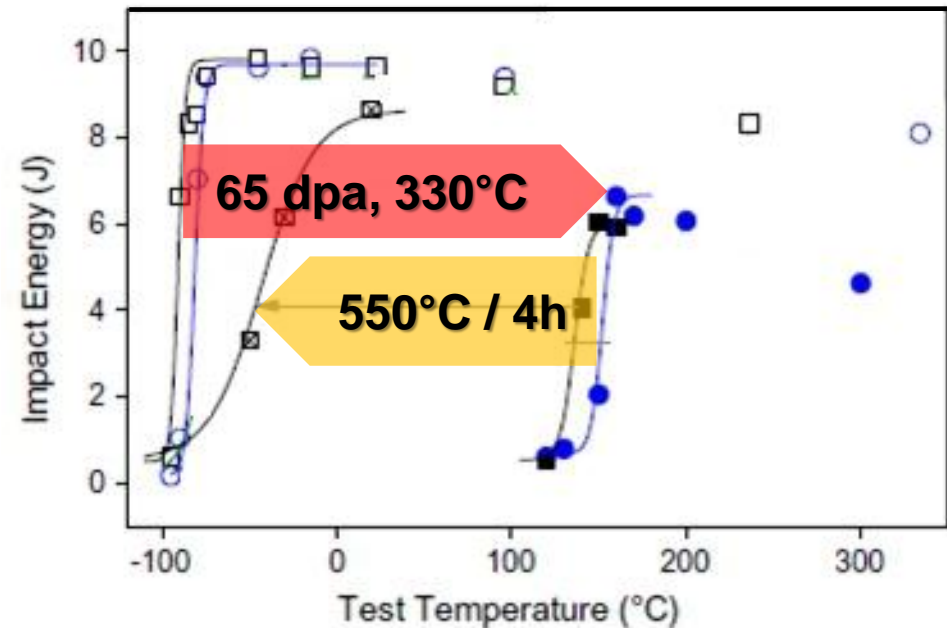
# IRRADIATION EFFECTS → EMBRITTLEMENT

**EUROFER:** In-service irradiation embrittlement after ~10 dpa



**Possible Operating Temperature  $T_{op} > 350^{\circ}\text{C}$**

**EUROFER:** Recovery of 65 dpa irradiation embrittlement

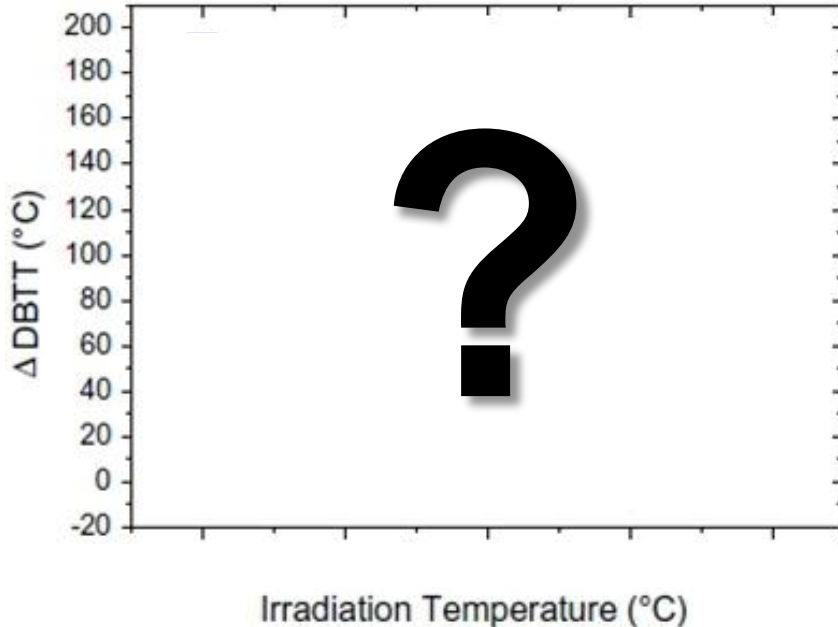


**Possible Recovery Temp.**  
 $T_{rec} > 550^{\circ}\text{C}$

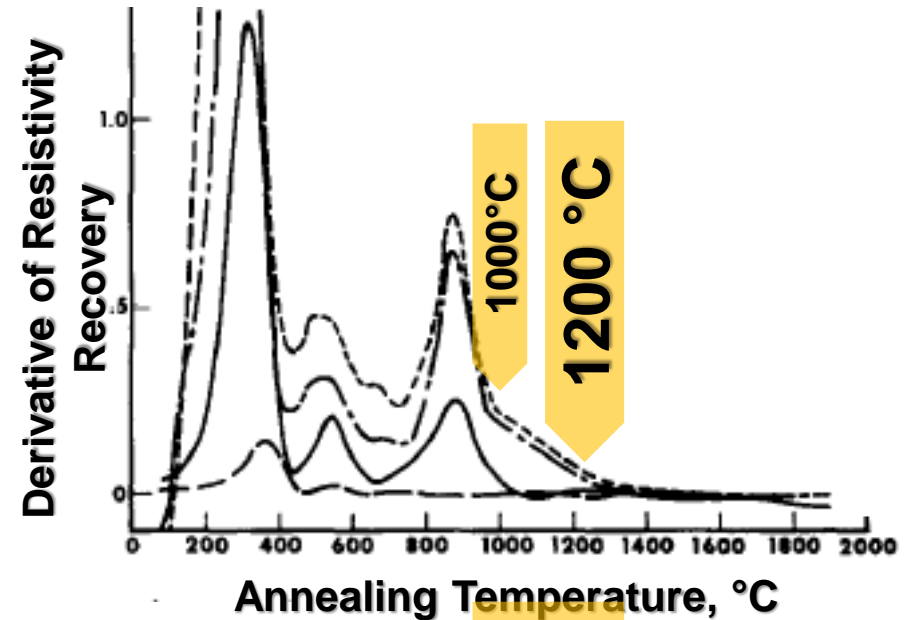
→ E. Gaganidze *et al.*, KIT

# IRRADIATION EFFECTS → EMBRITTLEMENT

**TUNGSTEN:** In-service irradiation embrittlement after 10-20 dpa



**Tungsten:** Recovery of ~2 dpa stage IV irradiation hardening



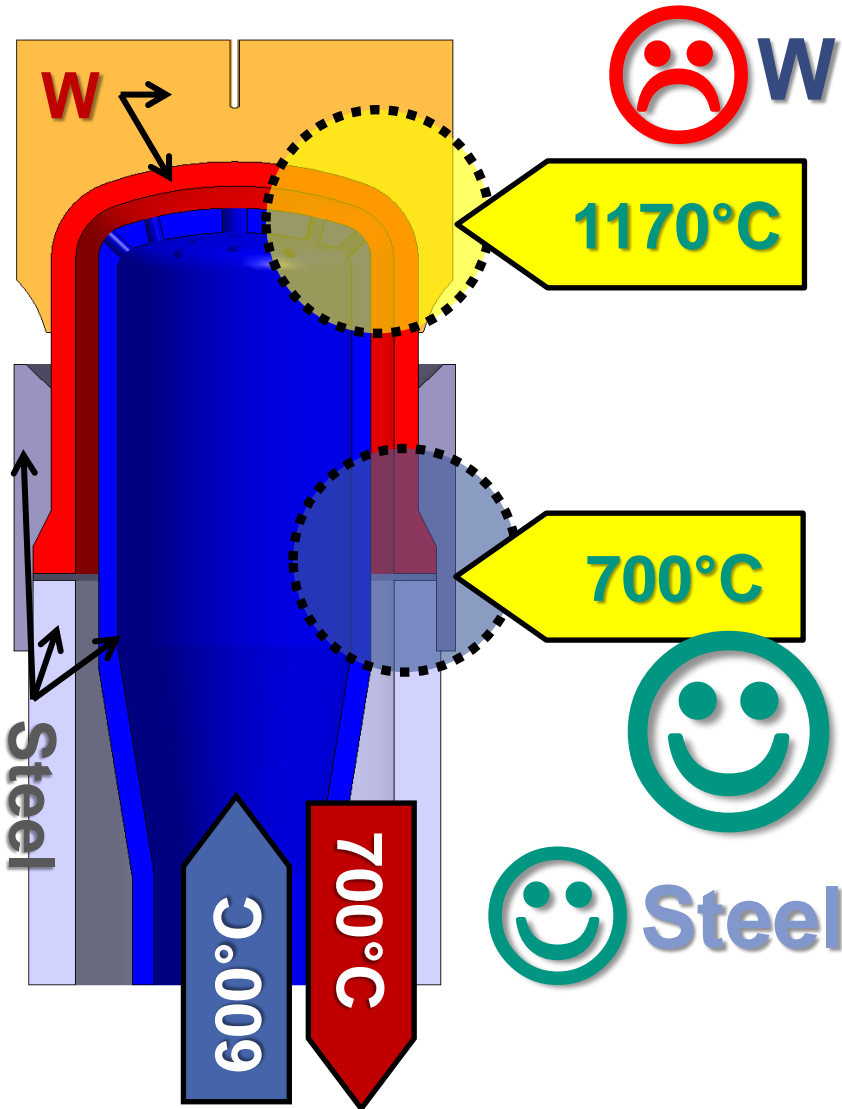
**Possible Operating Temp.**  
 $T_{op} > 800^{\circ}\text{C} \dots 1000^{\circ}\text{C}$



# 4

# MATERIAL MEETS DESIGN

# MATERIALS / DESIGN WINDOW → FINGER



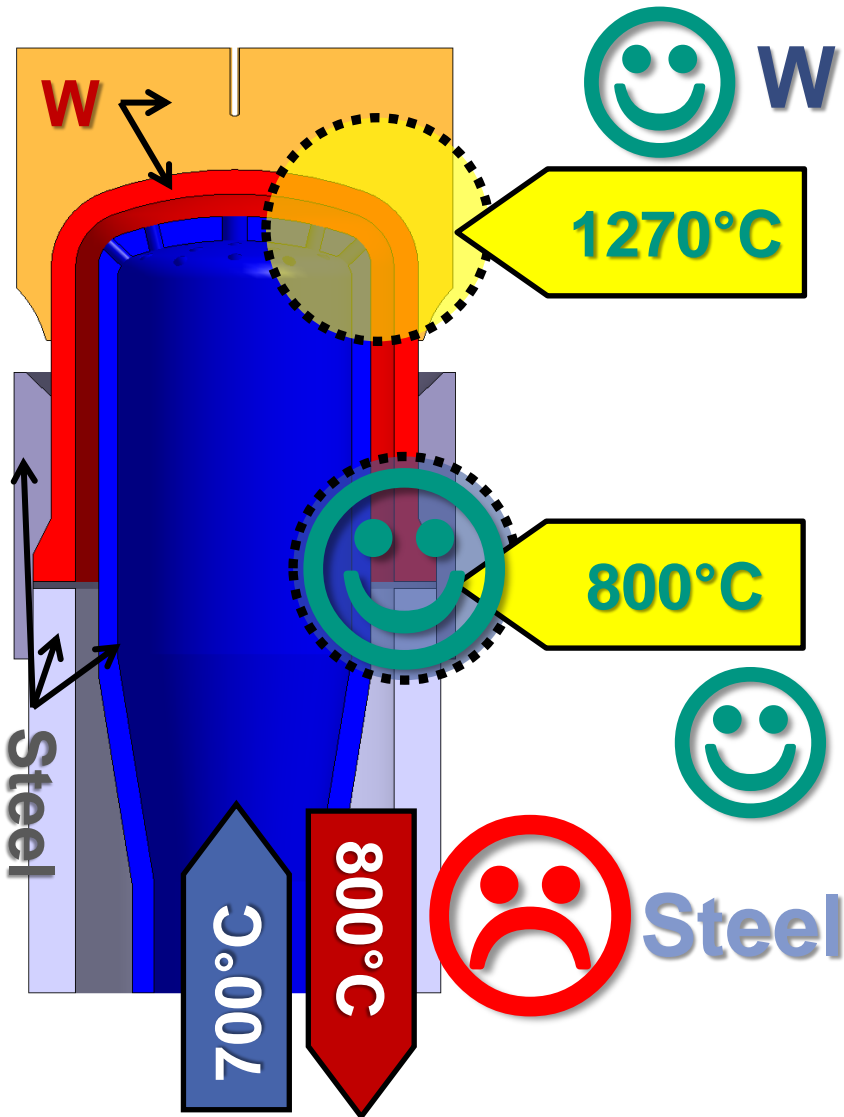
Oxidation	→	OK
Swelling ~3%	→	?
Embrittlement	→	OK
Grain Growth	→	? (ODS)

Swelling ~5%	→	?
Embrittlement	→	<b>NO GO (?)</b>

Brazing (Cu)	→	OK (...)
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Embrittlement	→	OK
Strength, ...	→	? ( <b>ODS</b> )

# MATERIALS / DESIGN WINDOW → FINGER



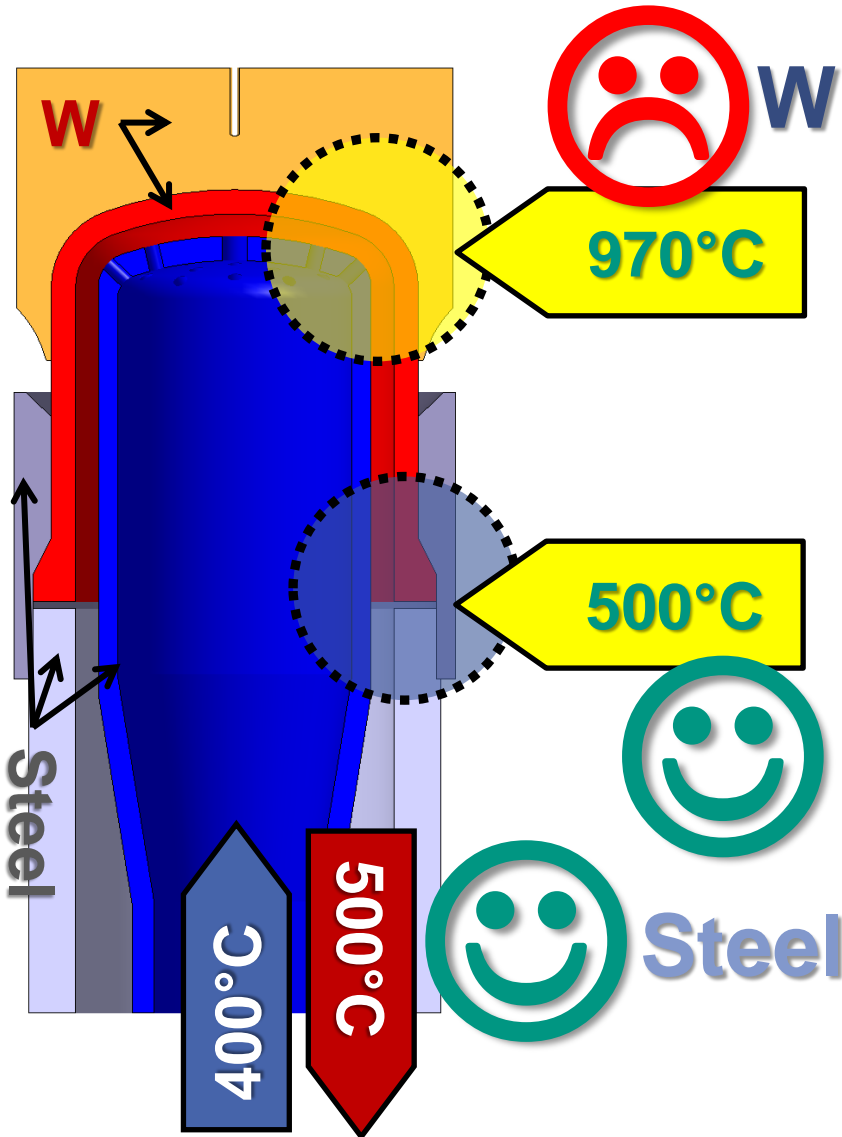
Oxidation	→	OK
Swelling ~3%	→	?
Embrittlement	→	OK
Grain Growth	→	ODS

Swelling ~5%	→	?
Embrittlement	→	OK (tbc)

Brazing (Cu)	→	OK (...)
--------------	---	----------

Embrittlement	→	OK
Strength, ...	→	ODS ???

# MATERIALS / DESIGN WINDOW → FINGER



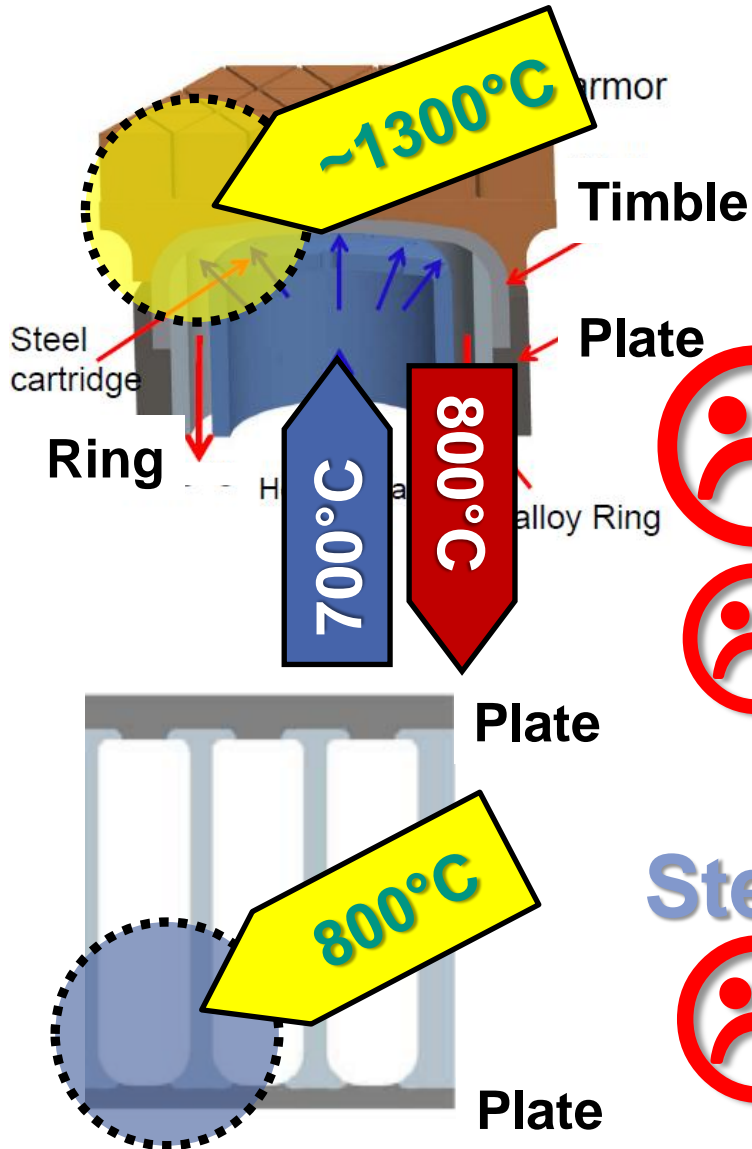
Oxidation	→	OK
Swelling <3%	→	OK (?)
Embrittlement	→	OK
Grain Growth	→	OK

Swelling <2%	→	OK (?)
Embrittlement	→	<b>NO GO</b>

Brazing (Cu)	→	OK (...)
--------------	---	----------

Embrittlement	→	OK
Strength, ...	→	OK

# MATERIALS / DESIGN WINDOW → PLATE



**W**

Oxidation	→	OK
Swelling $\sim 3\%$	→	???
Embrittlement	→	OK
Grain Growth	→	ODS

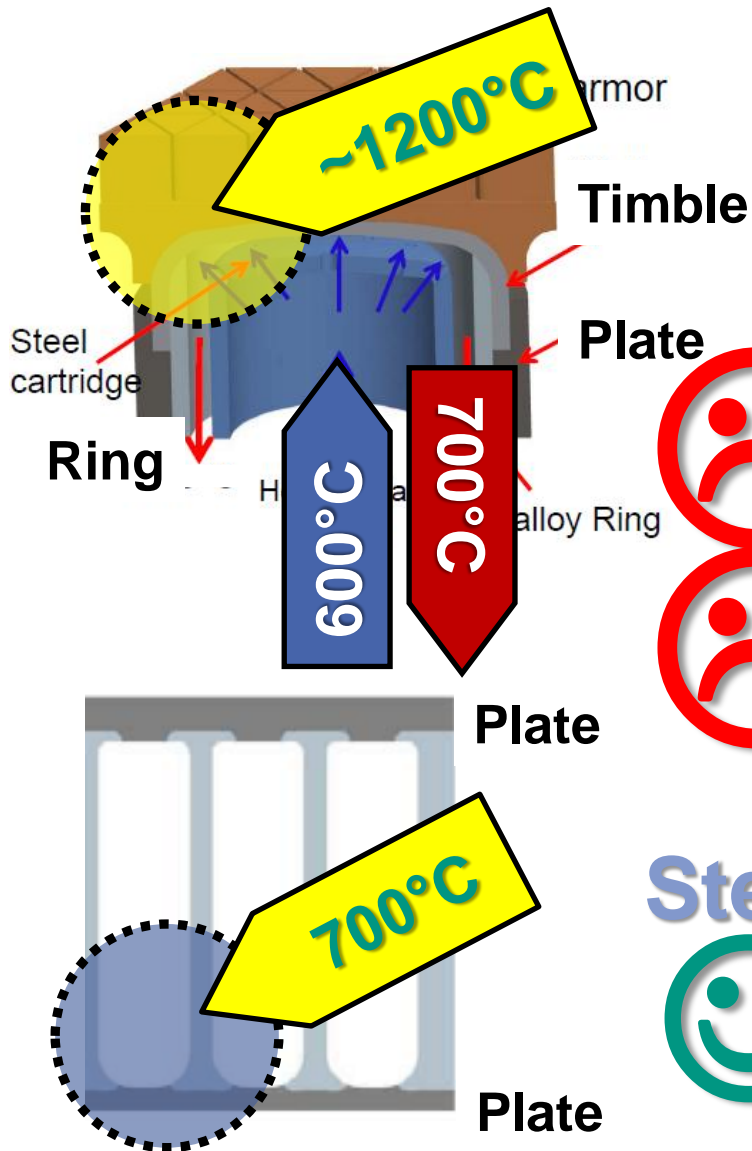
**Brazing W→W** → Pd, Pt ???

Swelling $\sim 5\%$	→	?????
Embrittlement	→	OK (tbc)

**Steel**

Embrittlement	→	OK
Strength, ...	→	ODS ???

# MATERIALS / DESIGN WINDOW → PLATE



**W**

Oxidation	→	OK
Swelling ~3%	→	???
Embrittlement	→	OK
Grain Growth	→	? (ODS)

Brazing W→W	→	Pd, Pt ???
-------------	---	------------

Swelling ~5%	→	?????
Embrittlement	→	NO GO (?)

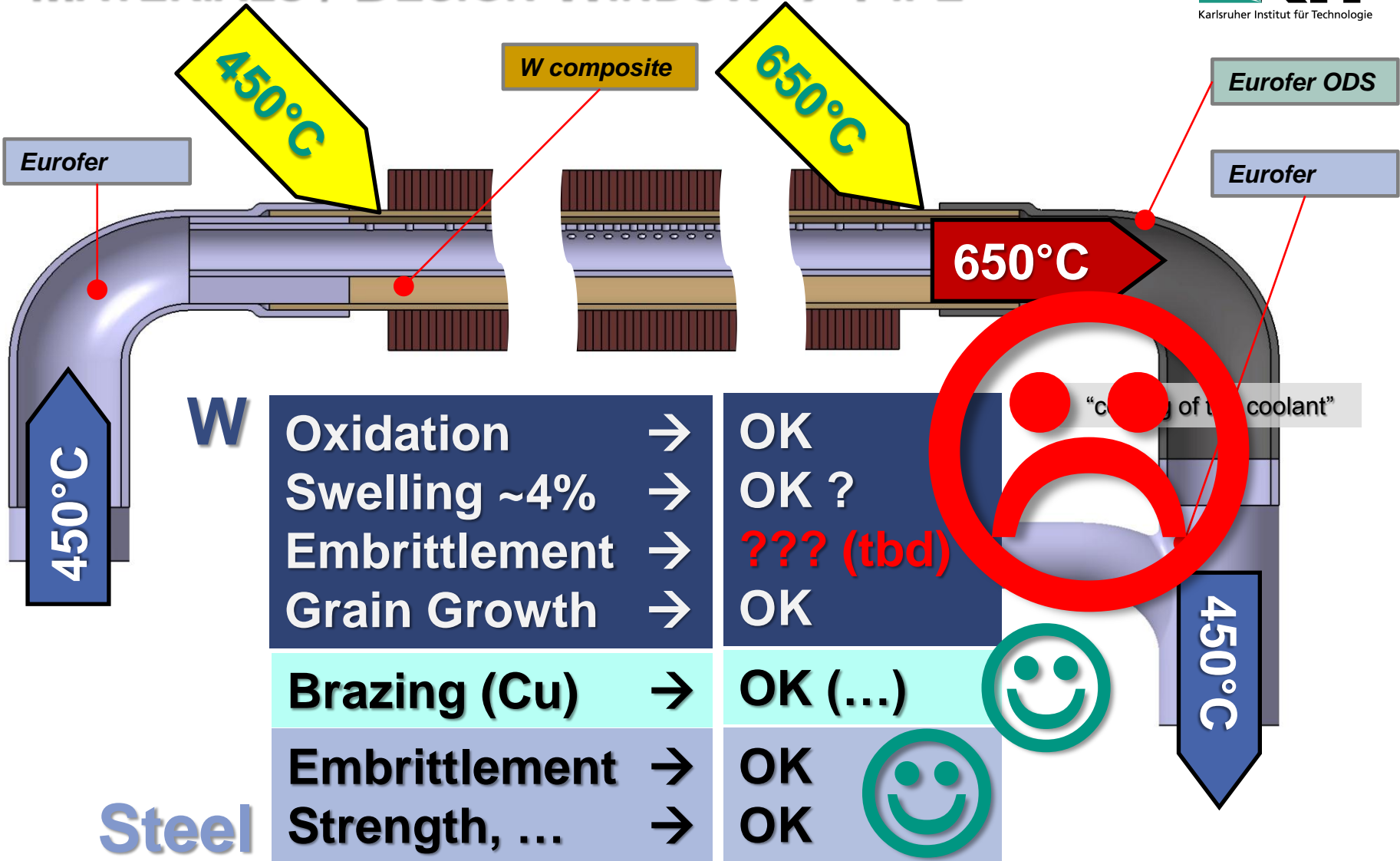


**Steel**



Embrittlement	→	OK
Strength, ...	→	? (ODS)

# MATERIALS / DESIGN WINDOW → PIPE



# 5

# SUMMARY AND PATH FORWARD



# SUMMARY

→ Thin plates (<4 mm) of pure W (including small amounts of grain stabilizers, if necessary) are the most suitable semi-finished products for structural applications !

→ The microstructure has to be adapted to the contour of the component (depending on the fabrication process to be developed) !

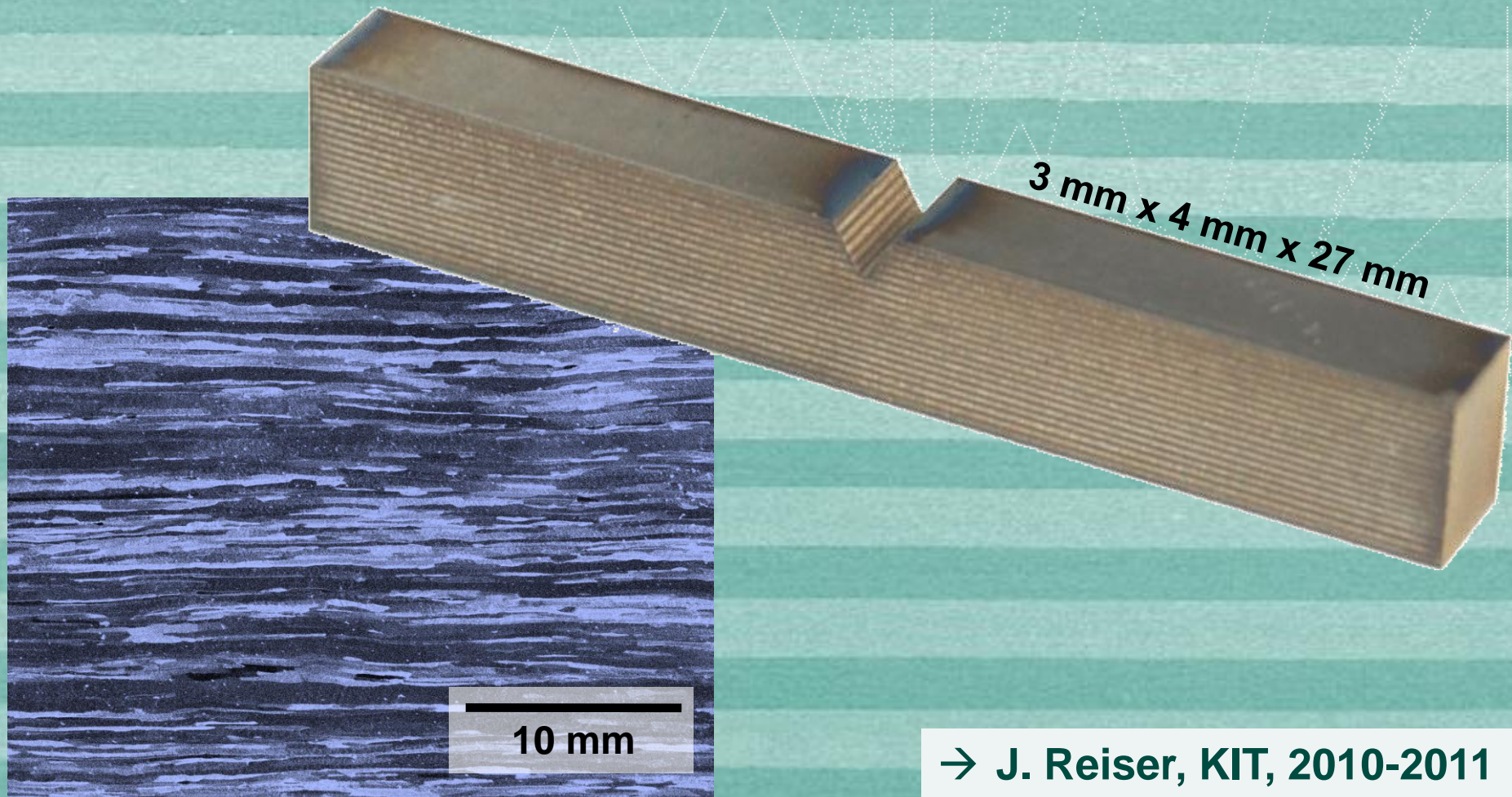
→ Coatings can be used as brazing material for W-steel joints, but needs additional strengthening by desing !

→ Suitable structural W-W joints are not yet demonstrated and characterized ! → Pt, Pd, ...?

→ W irradiation data needed for design (determination of lowest possible operating temperature) !!!

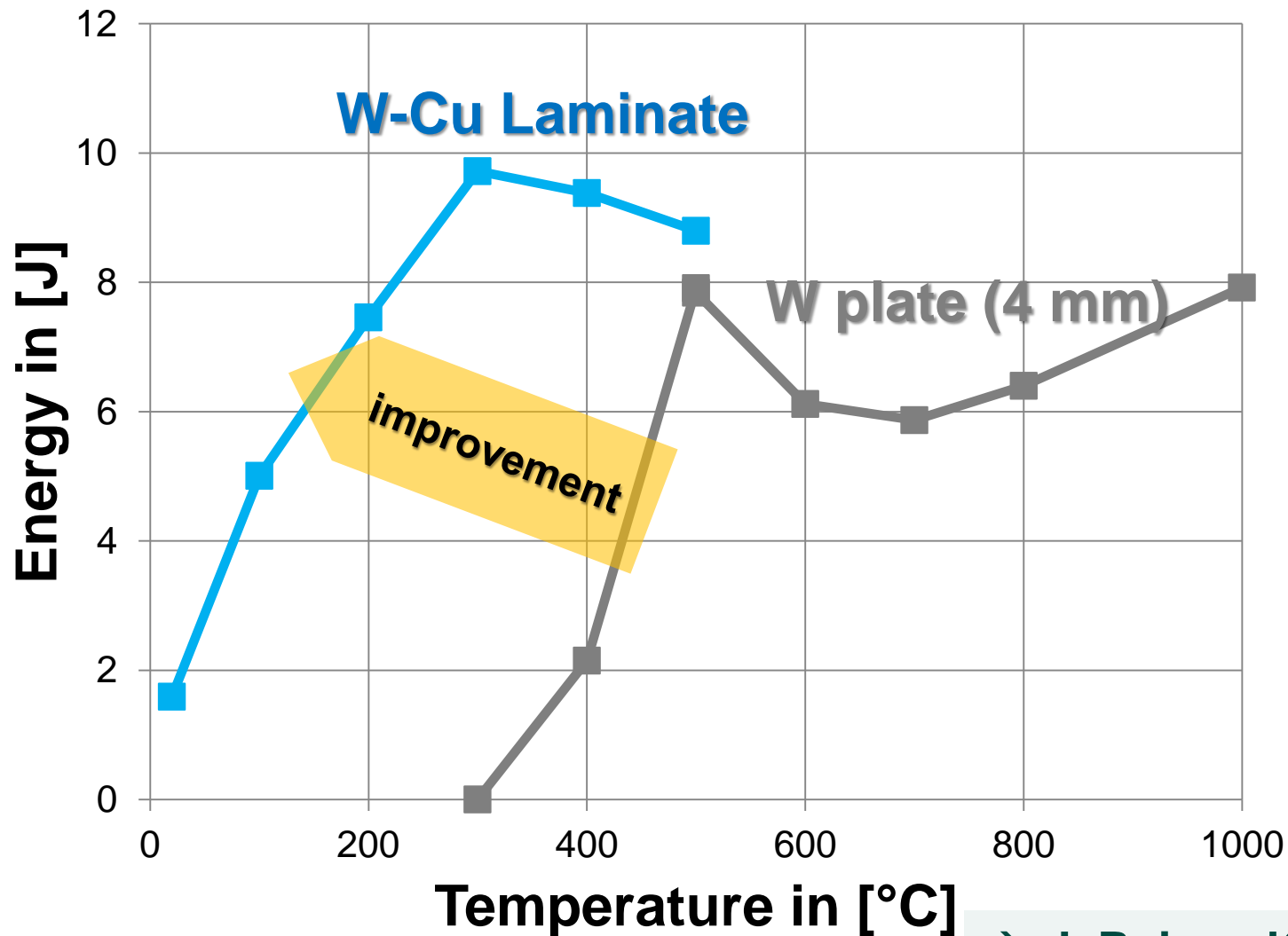


## W Laminate Material



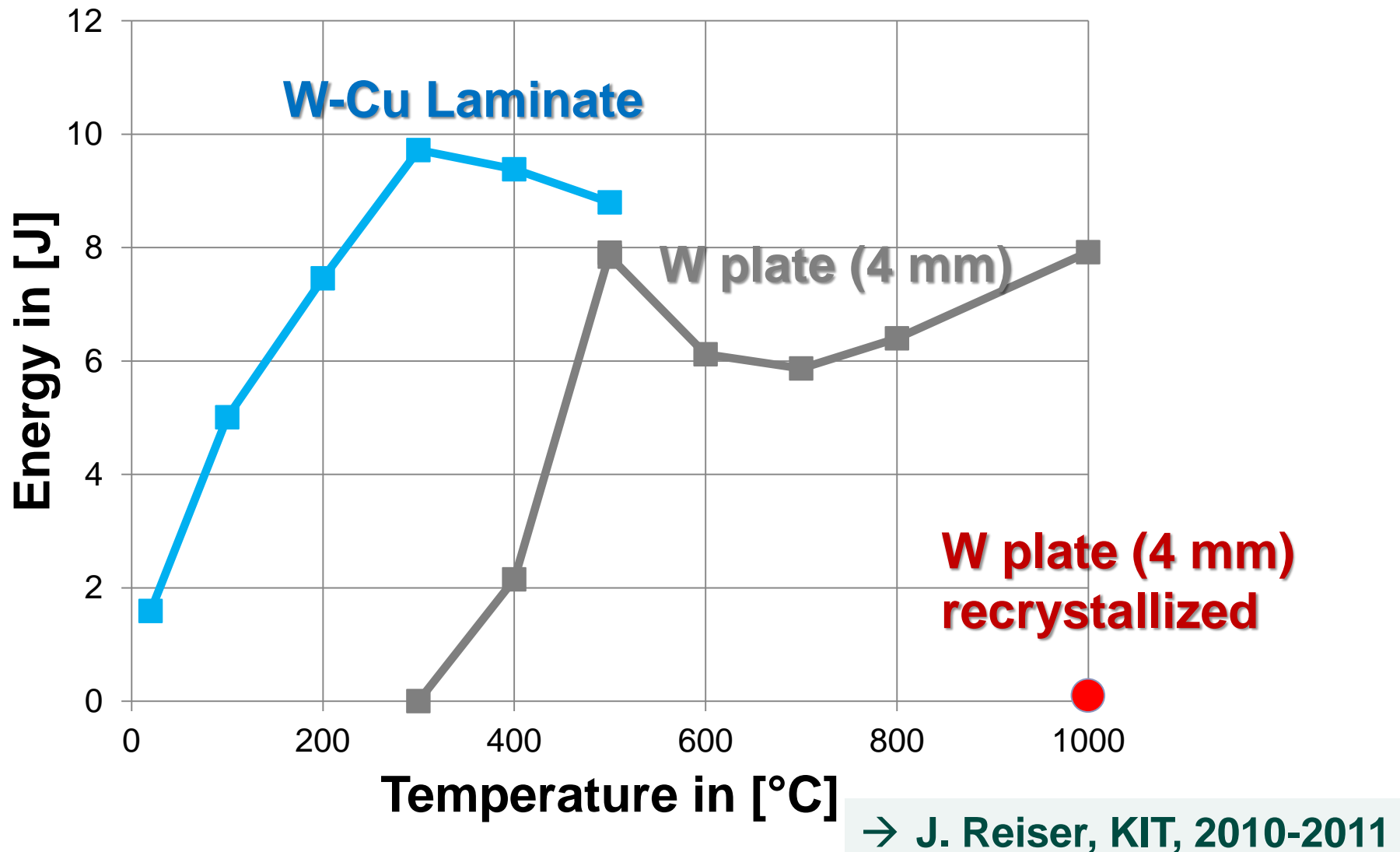
→ J. Reiser, KIT, 2010-2011

# PATH FORWARD → TUNGSTEN ALTERNATIVES

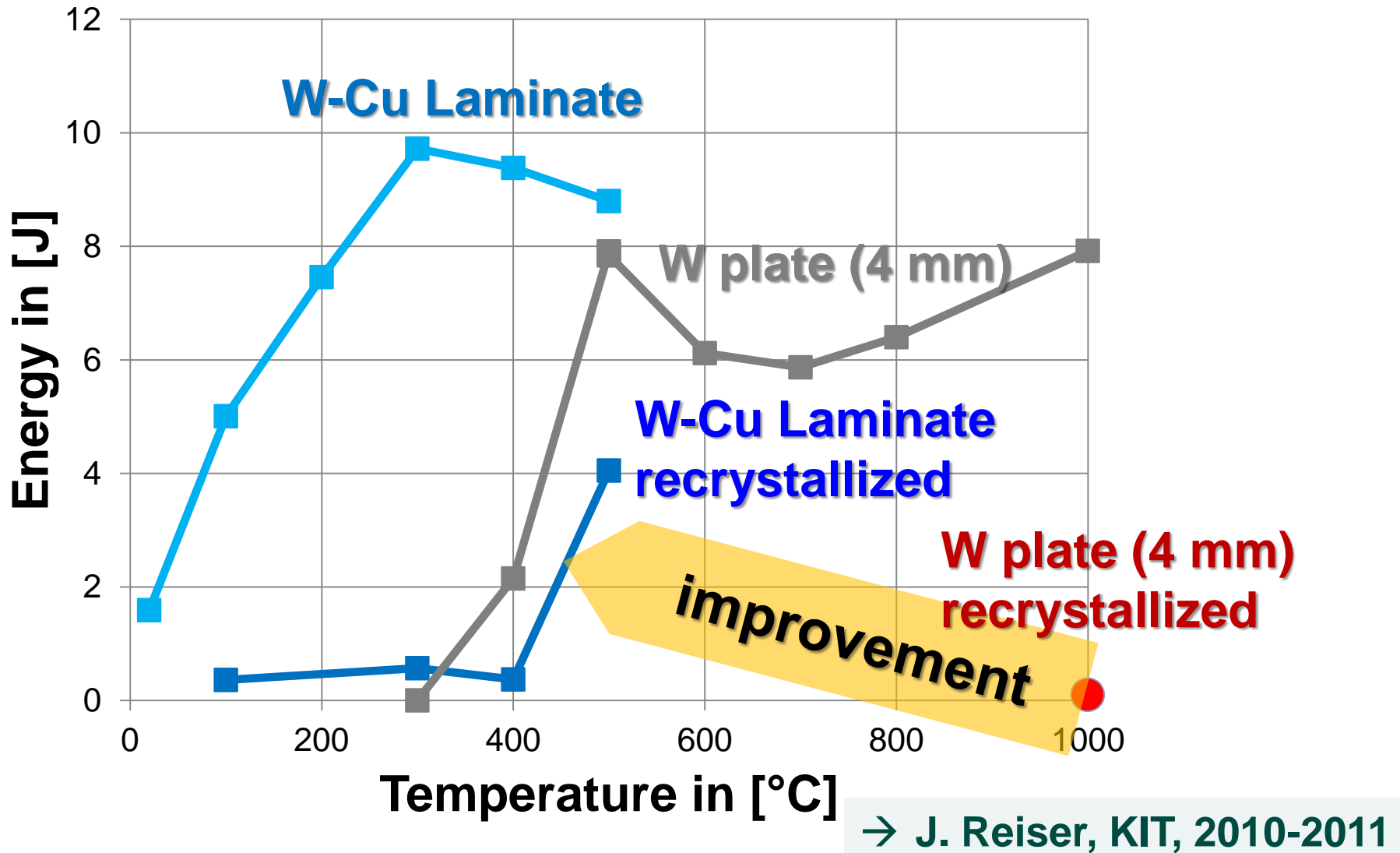


→ J. Reiser, KIT, 2010-2011

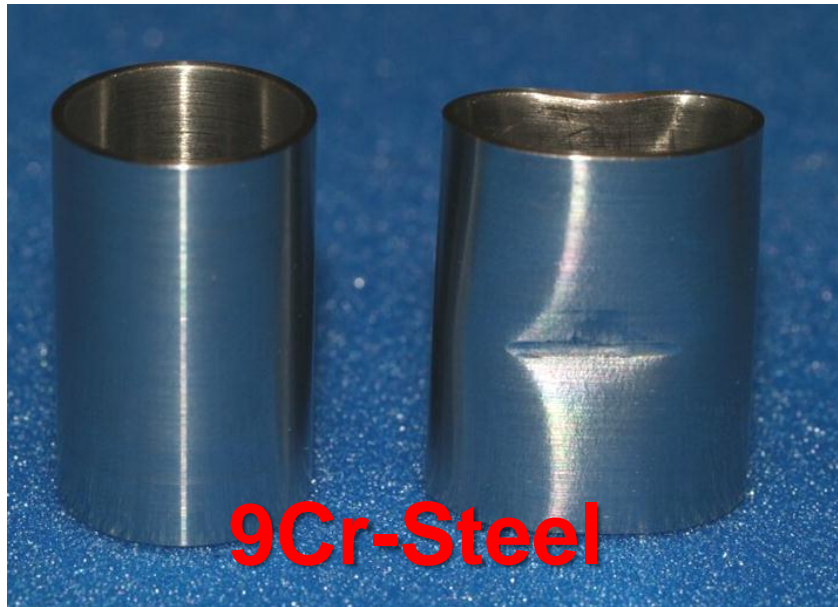
# PATH FORWARD → TUNGSTEN ALTERNATIVES



# PATH FORWARD → TUNGSTEN ALTERNATIVES



# PATH FORWARD → TUNGSTEN ALTERNATIVES



# THE ULTIMATE DIVERTOR → GENERIC DESIGN

