

# Divertor from the technology perspective

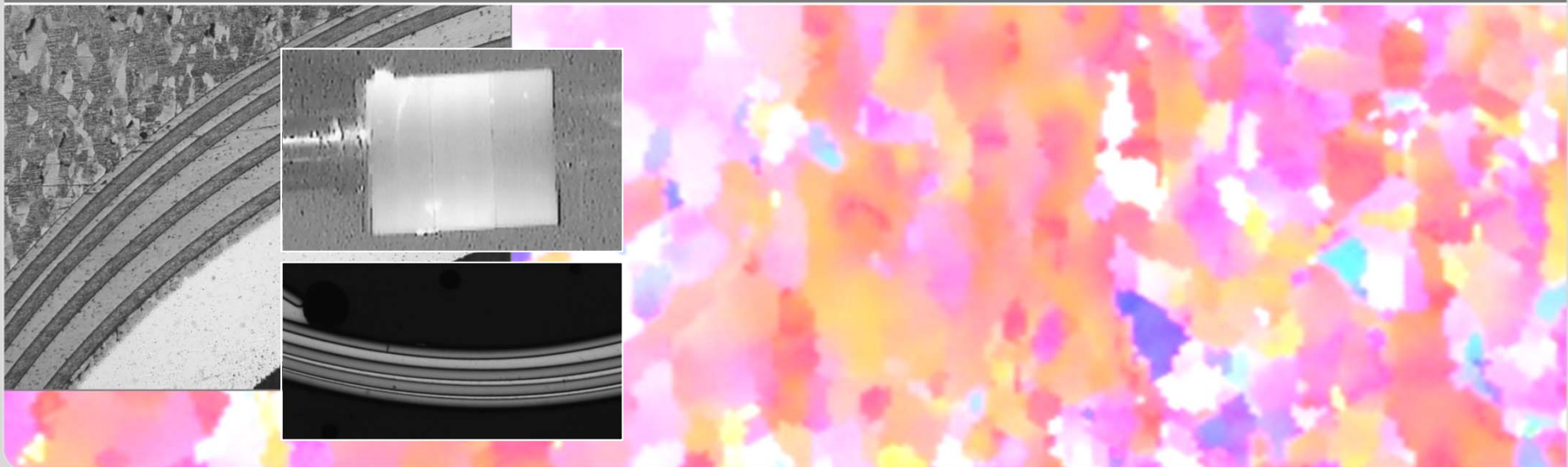
**J. Reiser<sup>1</sup>, M. Rieth<sup>1</sup>, B. Dafferner<sup>1</sup>, A. Hoffmann<sup>2</sup>**

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**1<sup>st</sup> IAEA DEMO program workshop, 15-18 October 2012**

INSTITUTE FOR APPLIED MATERIALS, APPLIED MATERIALS PHYSICS

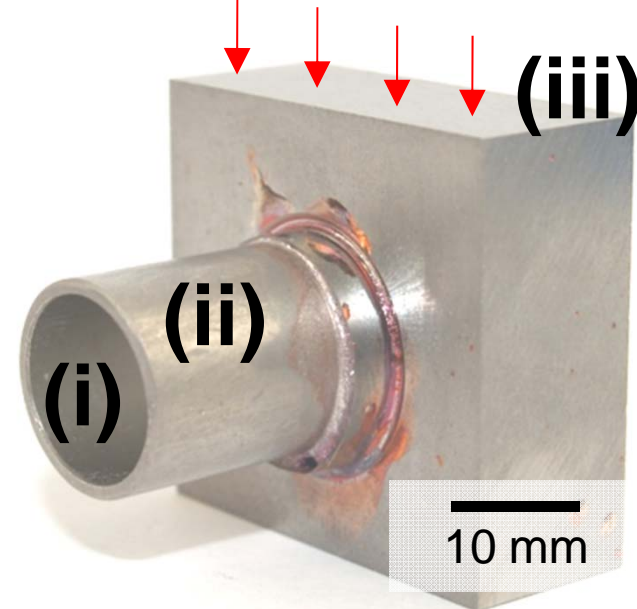


## Definition of the “divertor”

- Definition of the divertor: pipe, surrounded by tungsten
  - (i): type of coolant?
  - (ii): structural material for the pipe?
  - (iii): armour material? → tungsten
- Question: What amount of heat can we remove with a specific combination of (i) coolant and (ii) structural material?

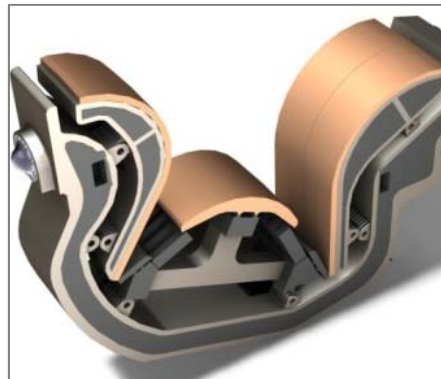


picture: PLANSEE SE



# Content

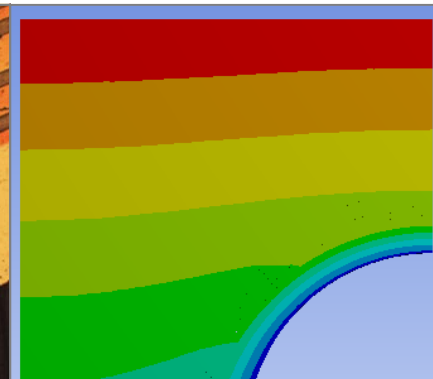
- Introduction
- The tungsten laminate project
- Matrix of coolant and structural material
- Divertor for DEMO: our proposals
- 
- Appendix (material issues)



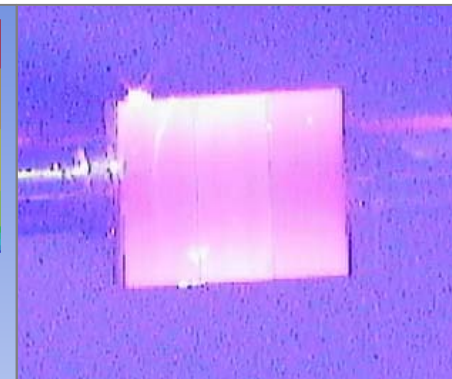
introduction



W-laminate



matrix



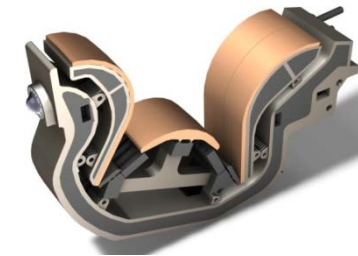
our proposals

# Introduction

- requirements on a DEMO divertor: survive 2 fpy
  - high heat flux:
    - 5 MW/m<sup>2</sup> (plasma physical minimum)
    - 7 MW/m<sup>2</sup> (continuous burning plasma → long term)
    - DEMO: **10 MW/m<sup>2</sup>** (pulsed operation → short term) with peaks due to plasma instabilities up to 20 MW/m<sup>2</sup>
  - neutron load → structural material
    - W structure: max. 1.9 dpa / fpy [1]
    - steel or Cu cooling structure: max. 5.9 dpa / fpy

- References:

- [1] M.R. Gilbert, S.L. Dudarev, S. Zheng, L.W. Packer and J.-Ch. Sublet, An integrated model for materials in a fusion power plant: transmutation, gas production, and helium embrittlement under neutron irradiation, Nucl. Fusion 52 (2012).



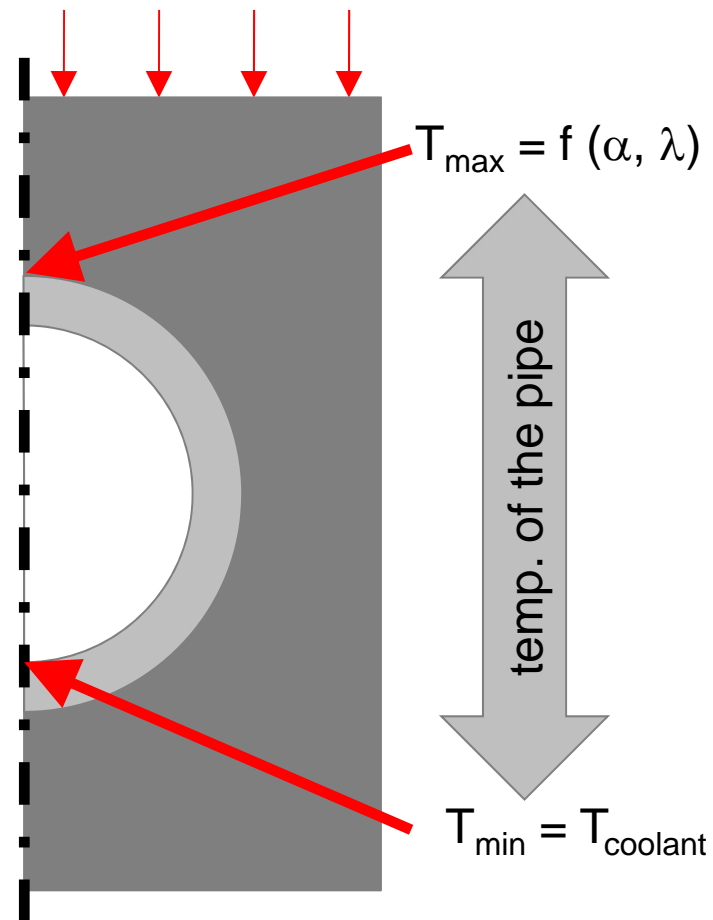
picture: ITER



picture: PLANSEE

# Introduction

## ■ How to deal with the heat load?



$\lambda$ : thermal conductivity, [W/(m\*K)]

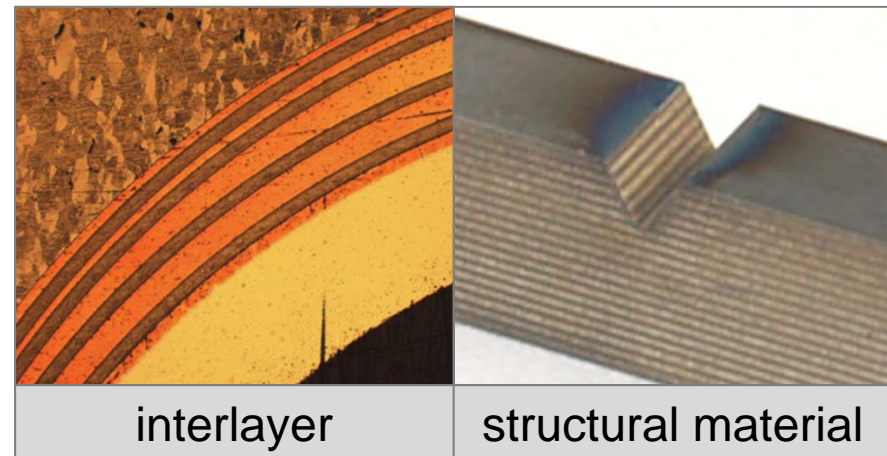
CuCrZr:	305 (at RT)
austenitic steel, 316Ti:	15 (at RT)
RAFM, Eurofer:	30 (at 500°C)
W:	180 (at RT)

$\alpha$ : heat transfer coefficient, [kW/(m<sup>2</sup>\*K)]

water:	100	swirl, hypervapotron
helium:	30	jet impingement

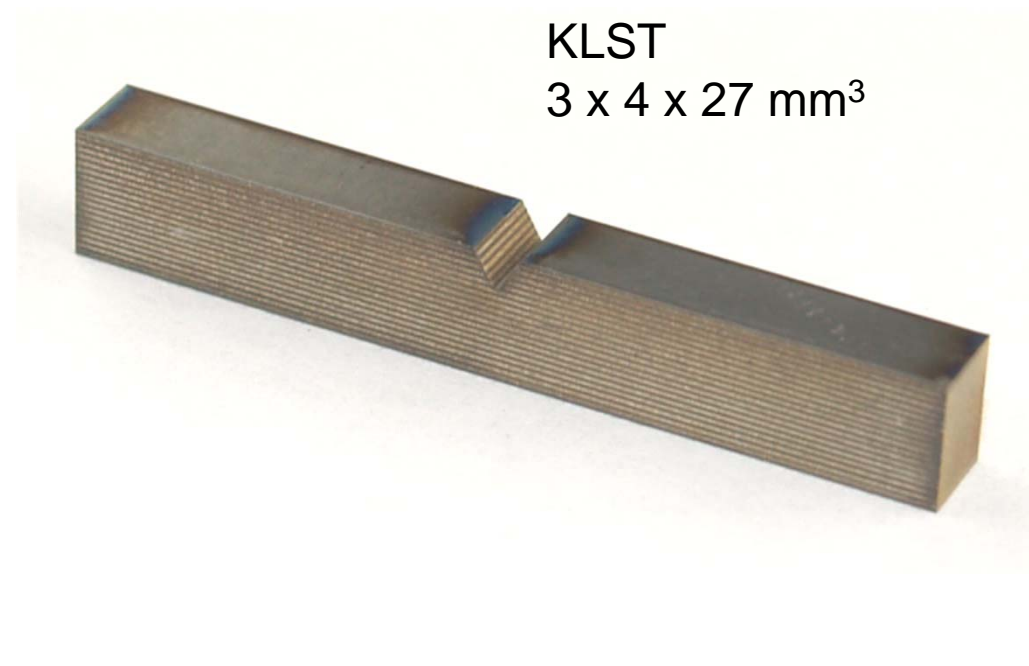
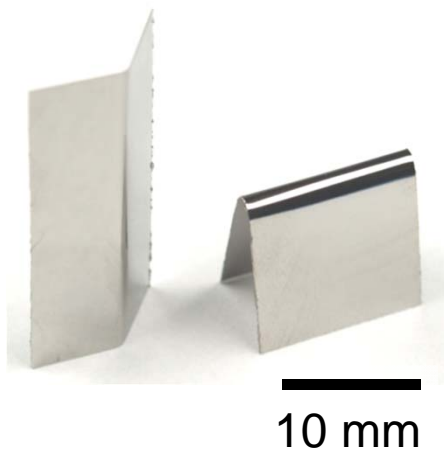
# Content

- Introduction
- **The tungsten laminate project**
  - Interlayer between steel and tungsten
  - **Structural material**
- Matrix of coolant and structural material
- Divertor for DEMO: our proposals
- 
- Appendix (material issues)



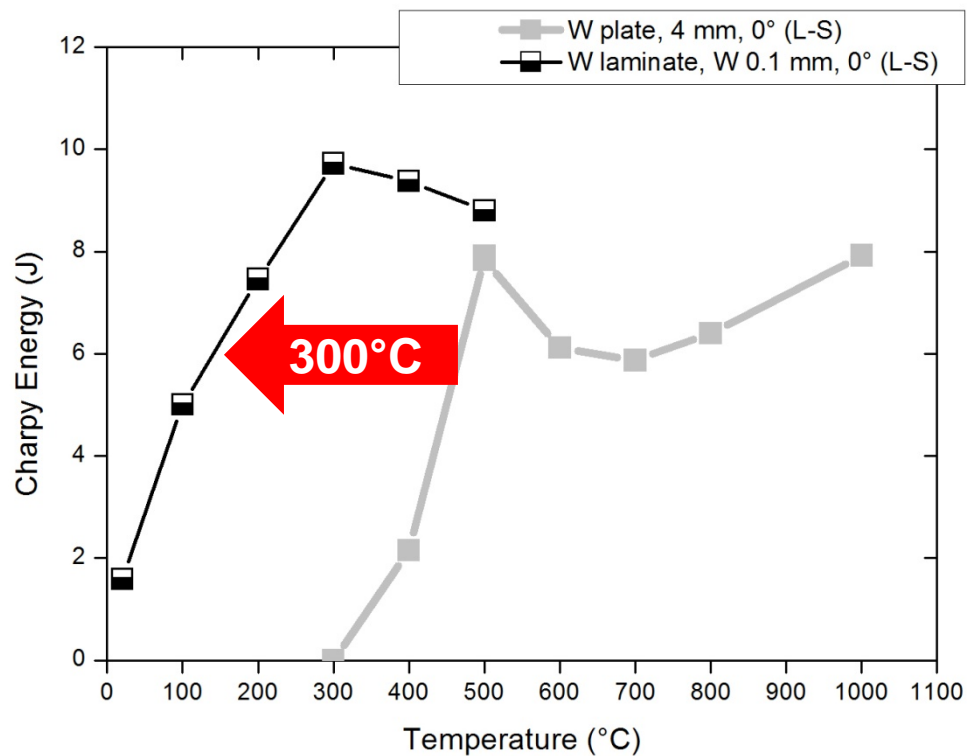
## The W-laminate project

- Do we succeed to transfer the ductile properties of a W-foil to the bulk?
- How can W-laminates be used for divertor applications?



## The W-laminate project: Charpy tests

- Can the ductile properties of a foil be transferred to the bulk?
  - as-received condition: improvement of 300°C

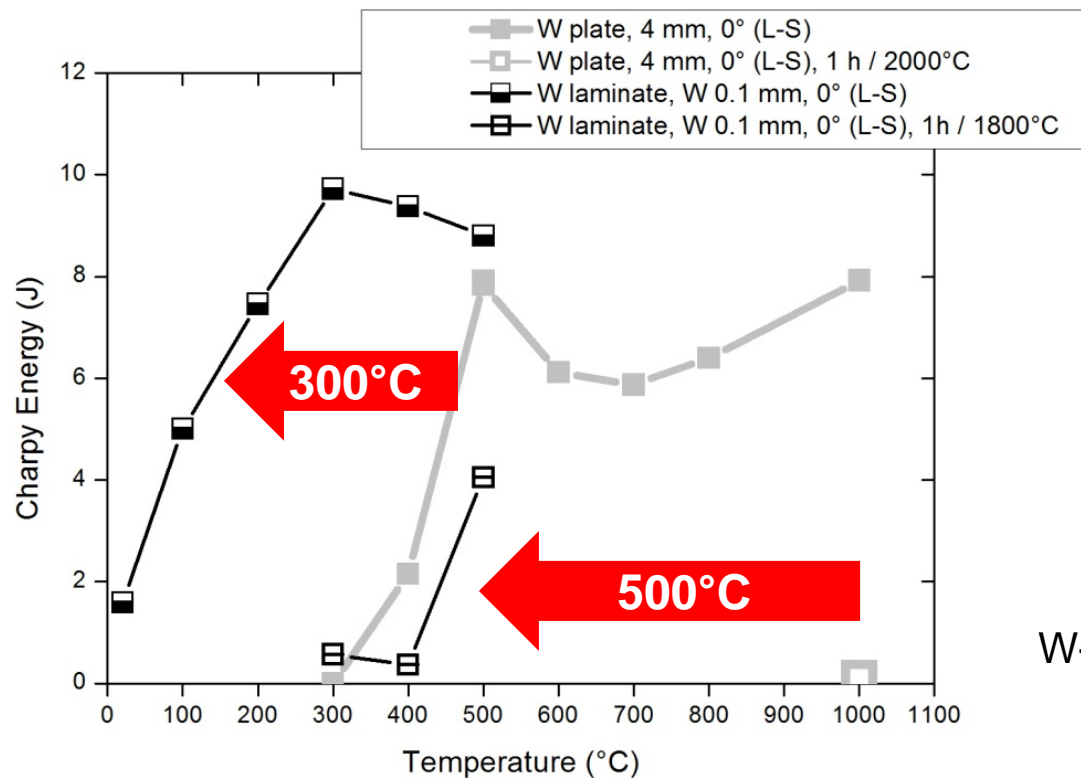


W-laminate made of Cu-alloy



## The W-laminate project: Charpy tests

- Can the ductile properties of a foil be transferred to the bulk?
  - as-received condition: improvement of 300°C
  - recrystallized condition: improvement of 500°C



W-laminate made of Cu-alloy

# The W-laminate project: pipes

- How can we produce a tungsten pipe?



15 mm

rod



Cu-alloy, 780°C



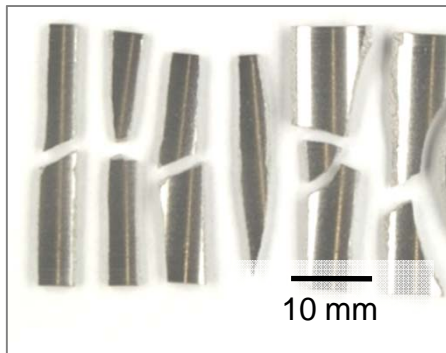
Cu, 1085°C



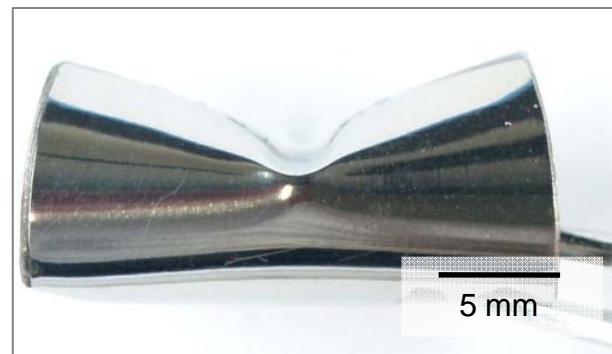
Ti, 1670°C



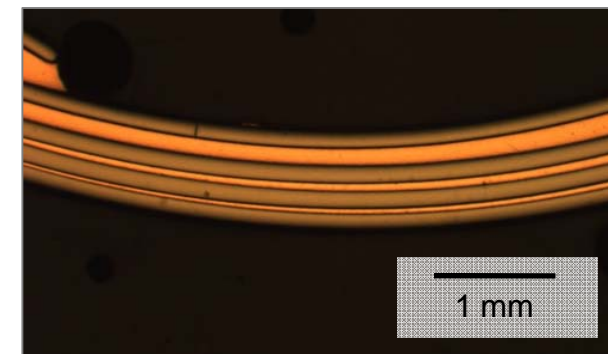
Zr, 1855°C



W rod, Charpy at 300°C



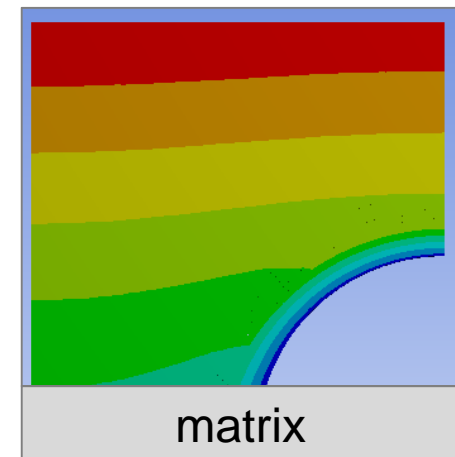
W-laminate-pipe, Charpy at 300°C



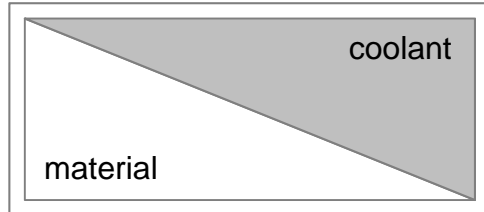
W-laminate-pipe, optical micrograph

# Content

- Introduction
- The tungsten laminate project
- **Matrix of coolant and structural material**
  - **What amount of heat can be removed by which combination of (i) structural material and (ii) coolant?**
- Divertor for DEMO: our proposals
- 
- Appendix (material issues)



# Matrix: material and coolant



H <sub>2</sub> O, 10 bar RT – 50 °C $\alpha = 100 \text{ kW}/(\text{m}^2 \cdot \text{K})$ swirl, hyperv.	H <sub>2</sub> O, 100 bar, 100°C – 120 °C $\alpha = 100 \text{ kW}/(\text{m}^2 \cdot \text{K})$ swirl, hyperv.	H <sub>2</sub> O, 160 bar 275°C – 325°C $\alpha = 100 \text{ kW}/(\text{m}^2 \cdot \text{K})$ swirl, hyperv.	He, 100 bar 400°C – 600°C $\alpha = 30 \text{ kW}/(\text{m}^2 \cdot \text{K})$ jet impingement
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CuCrZr	$\lambda_{RT} = 305$ W / (m * K)
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20 MW/m <sup>2</sup>			
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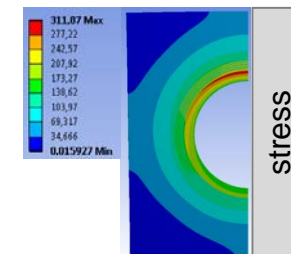
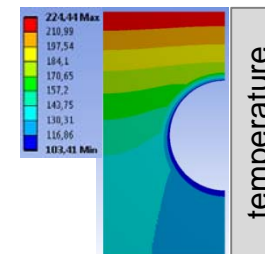
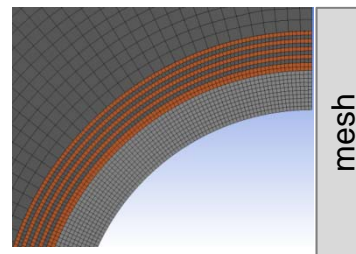
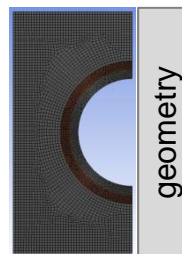
steel	Aust. steel, e.g. 316Ti	$\lambda_{RT} = 15$ W / (m * K)
	RAFM, e.g. Eurofer	$\lambda_{500^\circ\text{C}} = 30$ W / (m * K)

5 MW/m <sup>2</sup>	5 MW/m <sup>2</sup>	-	-
-	-	-	1 MW/m <sup>2</sup>

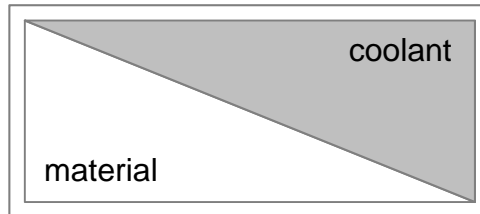
W*	W-Laminate* (W-Cu)	$\lambda_{RT, L} = 240$ $\lambda_{RT, II} = 285$
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-	-	-	10 MW/m <sup>2</sup>
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\*: neutrons are not considered



# Matrix: material and coolant



H<sub>2</sub>O, 10 bar  
RT – 50 °C  
 $\alpha = 100 \text{ kW}/(\text{m}^2 \cdot \text{K})$   
swirl, hyperv.

H<sub>2</sub>O, 100 bar,  
100°C – 120 °C  
 $\alpha = 100 \text{ kW}/(\text{m}^2 \cdot \text{K})$   
swirl, hyperv.

H<sub>2</sub>O, 160 bar  
275°C – 325°C  
 $\alpha = 100 \text{ kW}/(\text{m}^2 \cdot \text{K})$   
swirl, hyperv.

He, 100 bar  
400°C – 600°C  
 $\alpha = 30 \text{ kW}/(\text{m}^2 \cdot \text{K})$   
jet impingement

CuCrZr

 $\lambda_{RT} = 305$   
W / (m \* K)
20 MW/m<sup>2</sup>

steel

Aust. steel,  
e.g. 316Ti
 $\lambda_{RT} = 15$   
W / (m \* K)
RAFM,  
e.g. Eurofer
 $\lambda_{500^\circ\text{C}} = 30$   
W / (m \* K)

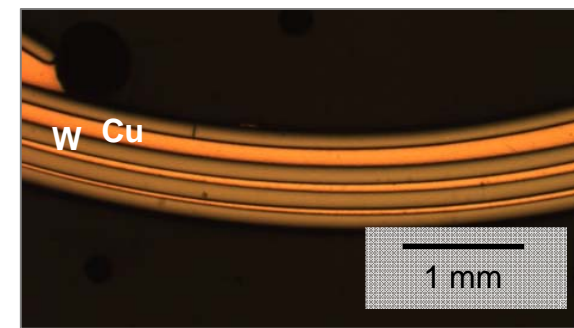
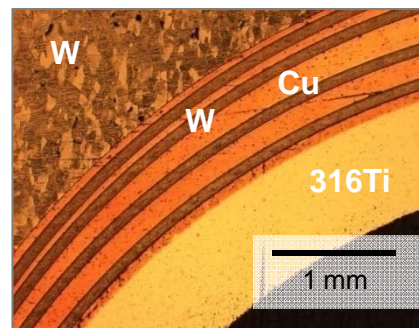
**W-laminate** used as **transition piece** between steel pipe and W armour

W\*

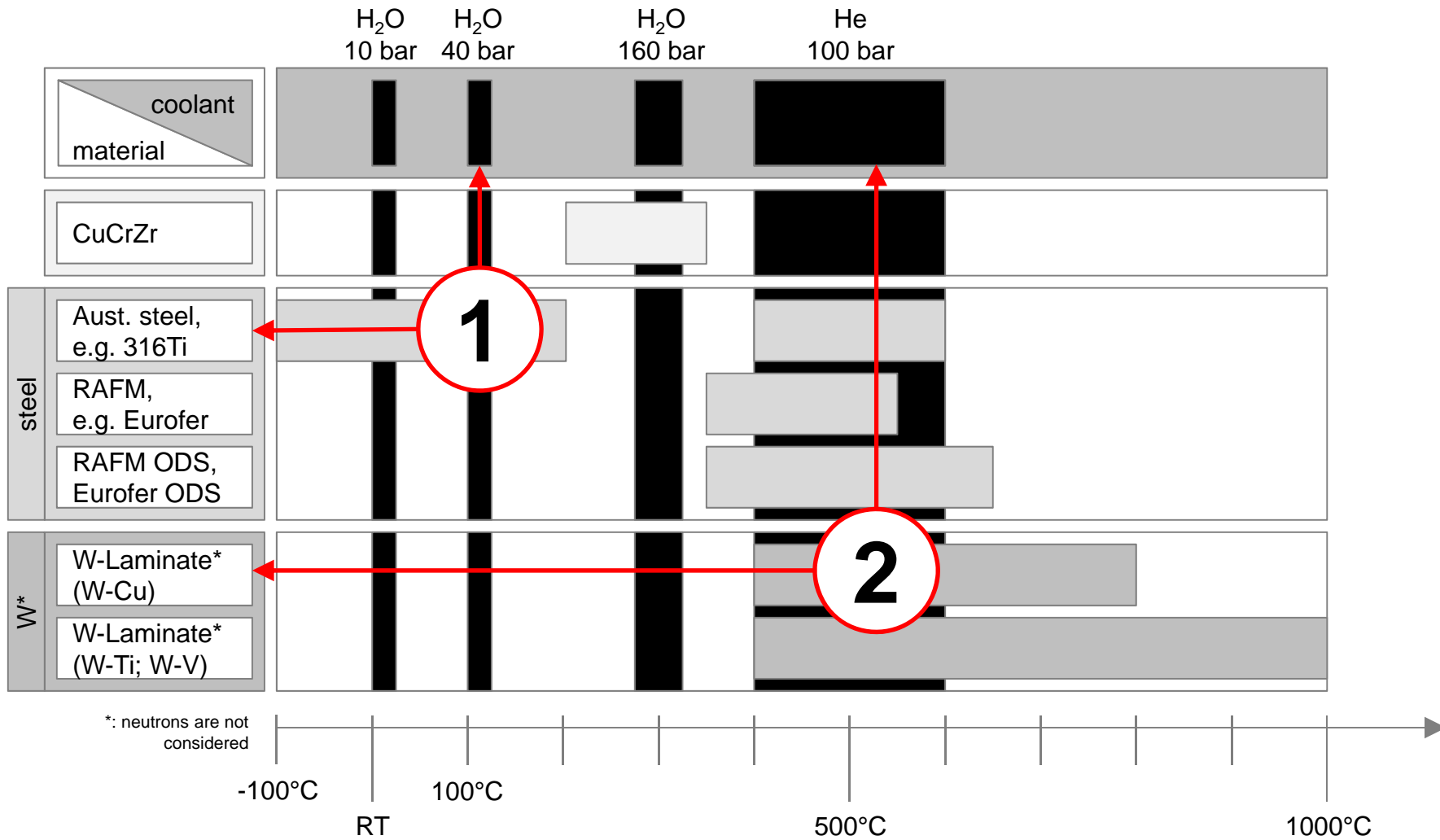
W-Laminate\*  
(W-Cu)
 $\lambda_{RT, L} = 240$   
 $\lambda_{RT, II} = 285$ 

**W-laminate** used as a **structural material**

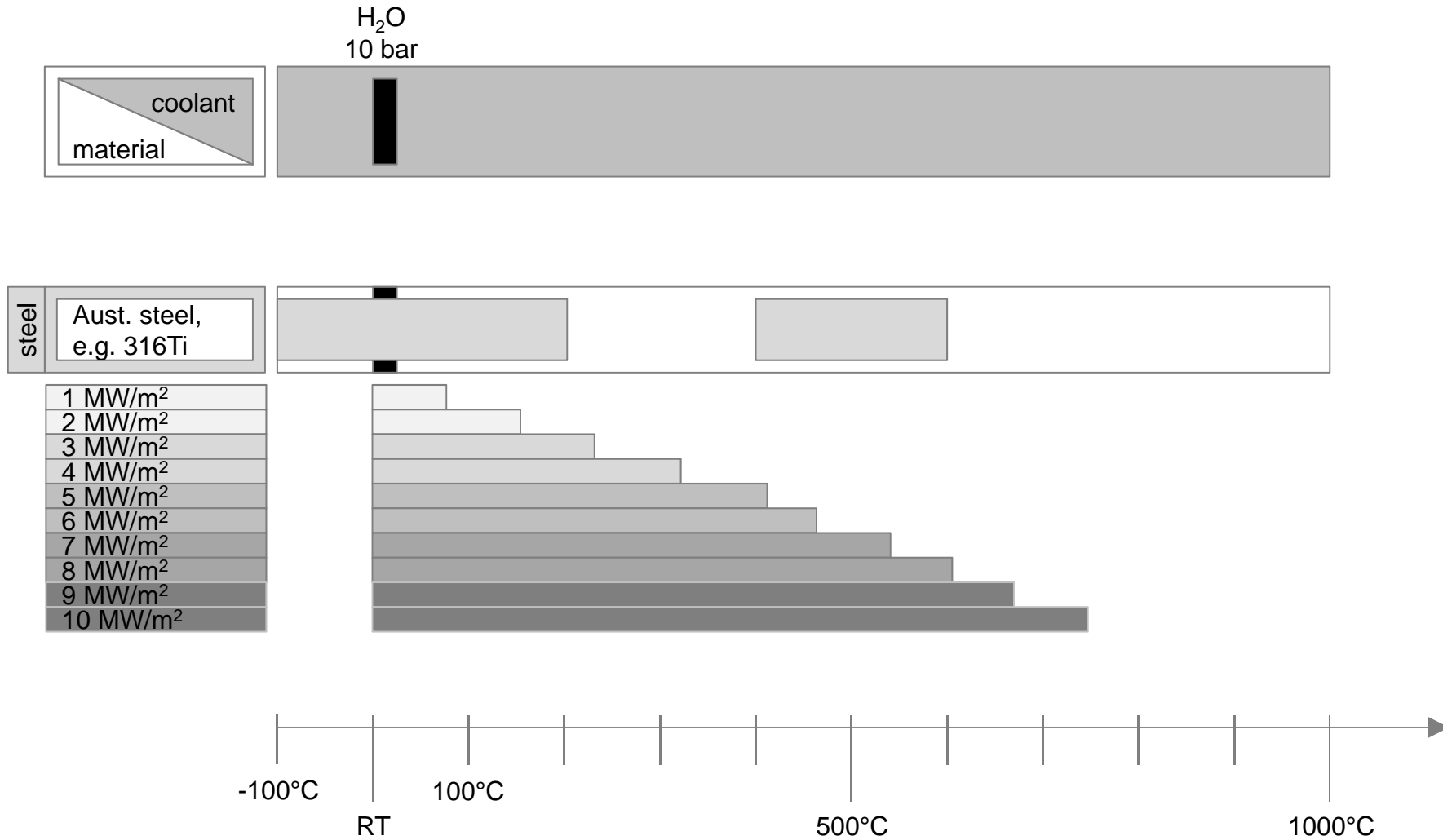
\*: neutrons are not  
considered



# Matrix: material and coolant

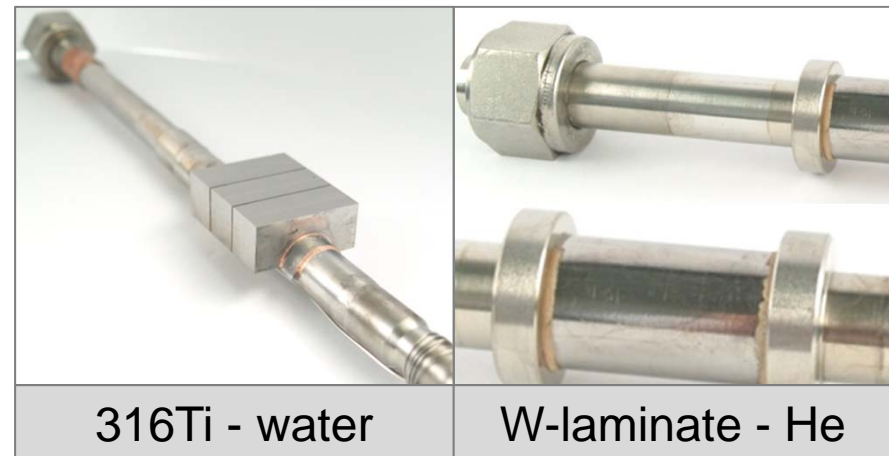


# Matrix: material and coolant



# Content

- Introduction
- Matrix of coolant and structural material
- The tungsten laminate project
- **Divertor for DEMO: our proposals**
  - Austenitic steel – water coolant
  - Tungsten laminate – helium coolant
- 
- Appendix (material issues)





# Divertor for DEMO: our proposals 1

- our proposal 1:
  - material: austenitic steel (316Ti)
  - coolant: water (100°C – 120°C, 40 bar)
  - result of simulation: 5 MW/m<sup>2</sup>
- state of the art: until now it was not possible to join an austenitic steel pipe with the tungsten armour (different thermal expansion coef.  $\alpha$ )
- our idea: use a tungsten laminate as a transition piece

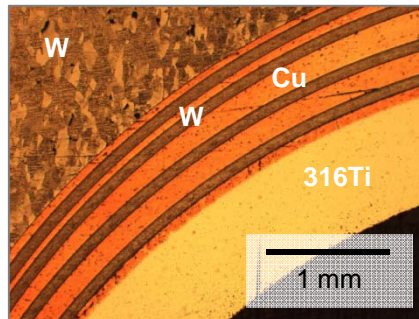
## The team:

- fabrication Rieth, Reiser (KIT)
- NDT Huber, Zabernig (PLANSEE SE)
- HHF testing Greuner, Böswirth (IPP)  
Pintsuk (FZJ)  
Ghidrsa (KIT)

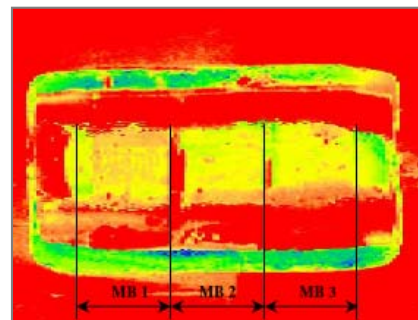


# Divertor for DEMO: our proposals 1

- HHF tests, GLADIS, IPP:
  - water, RT, 10 m/s, 1.13 l/s
  - beam 20 s on 40 s off
- **result of test: 100 cycles, 6 MW/m<sup>2</sup>, no residual damage**
- next steps:
  - use swirl → improvement of  $\alpha$  up to 100 [kW/(m<sup>2</sup>\*K)]
  - HHF tests at 10 MW/m<sup>2</sup>



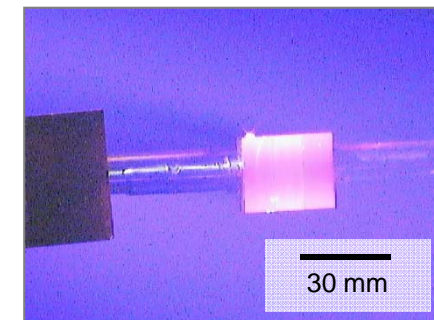
W-laminate as a transition piece



non-destructive testing,  
PLANSEE SE



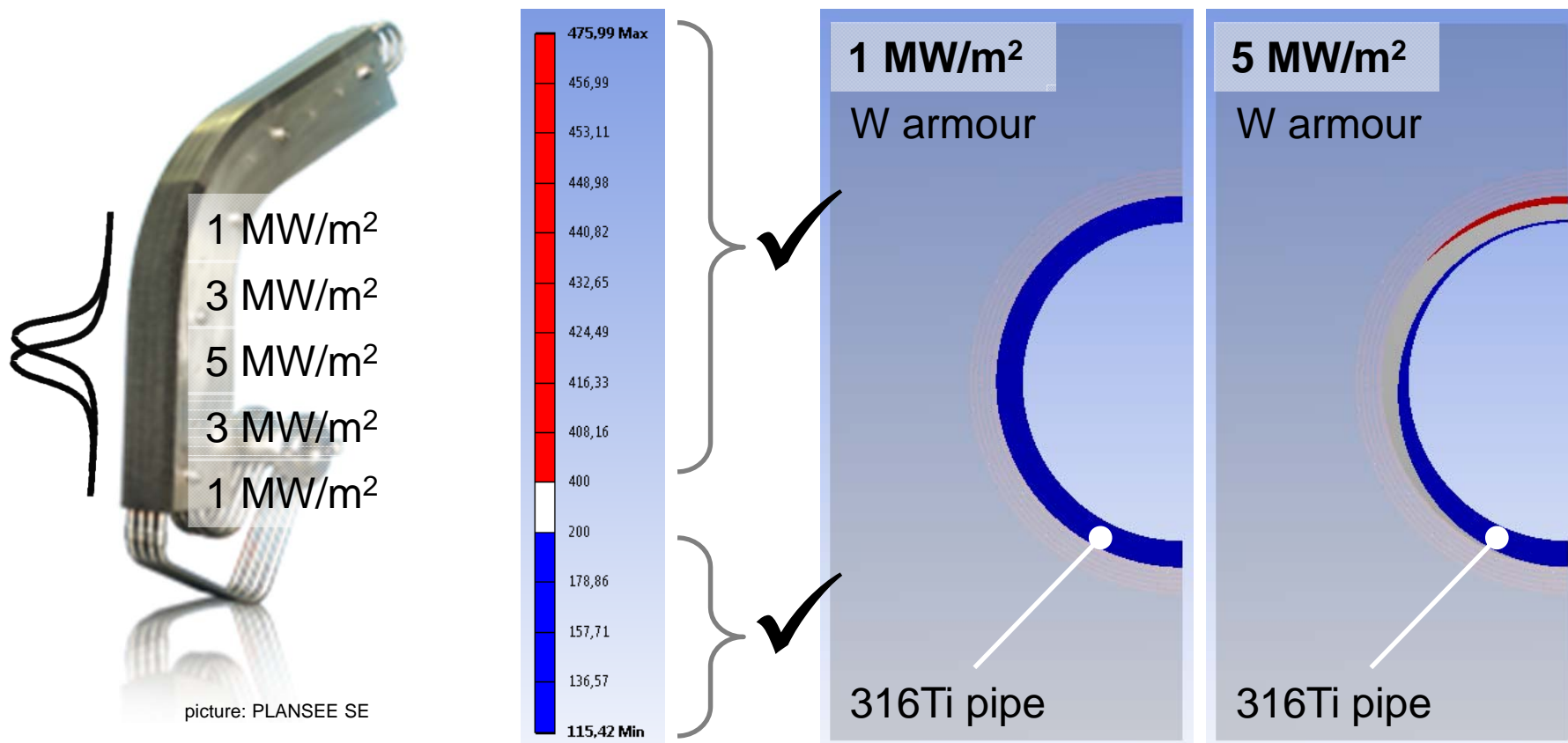
GLADIS, IPP, Garching



Test: 100 Zyklen, 6 MW/m<sup>2</sup>

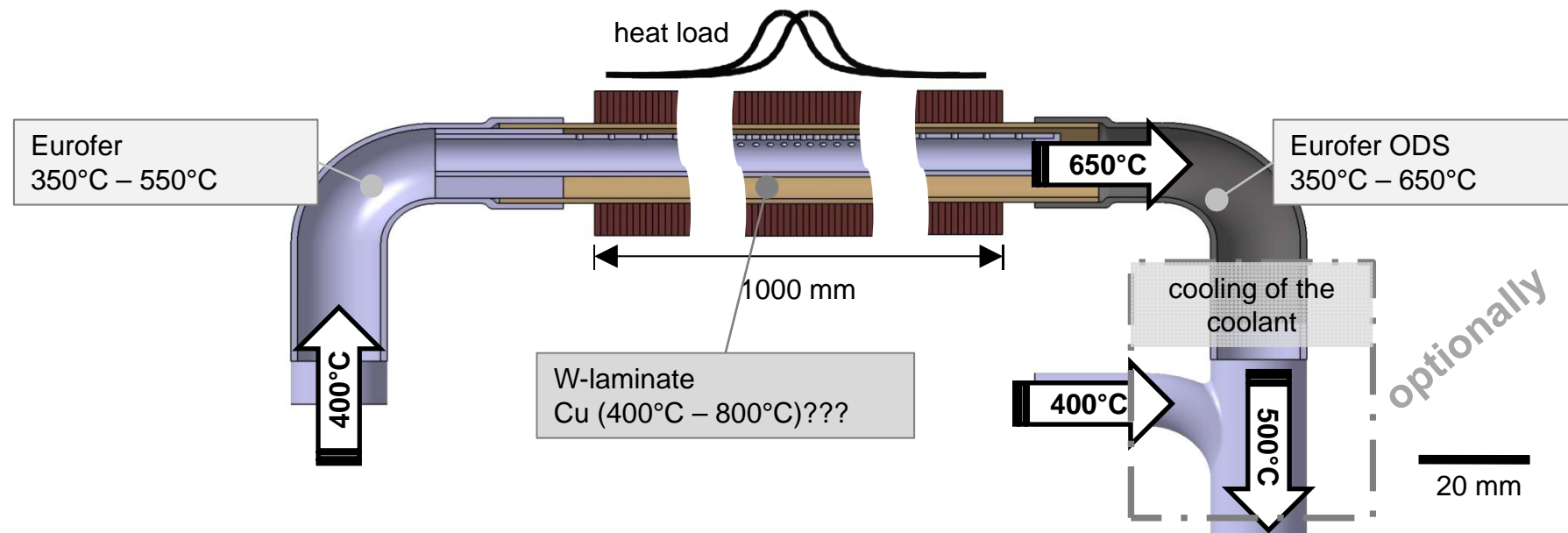
# Divertor for DEMO: our proposal 1

- austenitic steel (e.g. 316), coolant: water (100°C – 120°C, 40 bar):
  - operation window: up to 200°C and from 400°C – 600°C



## Divertor for DEMO: our proposals 2

- our proposal 2:
  - material: W-laminate pipe (with Cu brazing)
  - coolant: helium (400°C – 600°C, 100 bar)
  - result of simulation: 10 MW/m<sup>2</sup>
- state of the art: until now there were no tungsten pipes available
- our idea: use W-laminate pipe as structural material



## Divertor for DEMO: our proposals 2



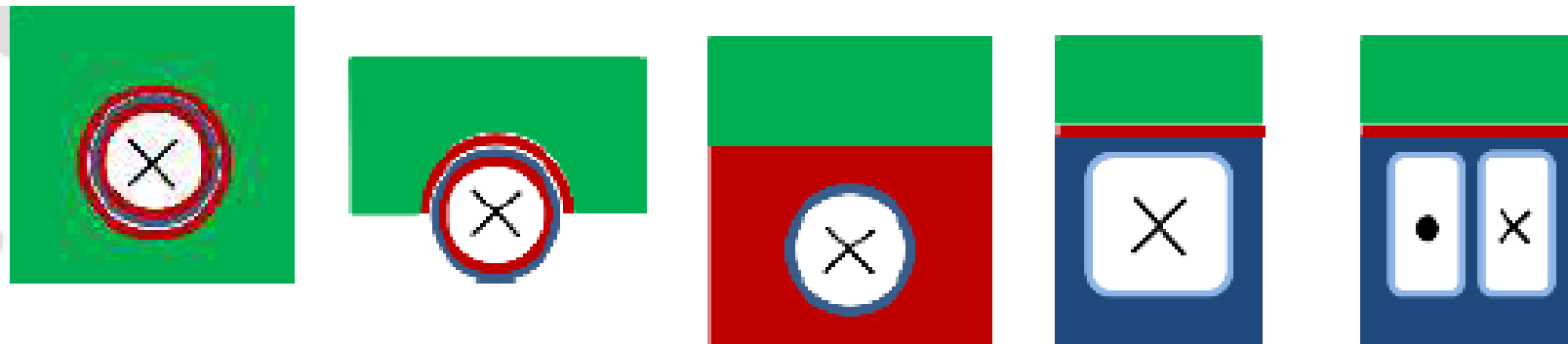
# Outlook (I/II)

W-laminates	Material tests	Pipe tests
<p><b>W-foil</b></p> <ol style="list-style-type: none"> <li>1) W</li> <li>2) WVM (W-0.005 wt.% K)</li> </ol> <p><b>interlayer</b></p> <ol style="list-style-type: none"> <li>1) Cu (<math>T_{\text{melting}} = 1085^{\circ}\text{C}</math>)</li> <li>2) Ti (<math>T_{\text{melting}} = 1670^{\circ}\text{C}</math>) <math>\rightarrow</math> allotropy</li> <li>3) V, or V4Cr4Ti (<math>T_{\text{melting}} = 1910^{\circ}\text{C}</math>) <math>\rightarrow</math> Kirkendall effect</li> </ol> <p><b>joining</b></p> <ol style="list-style-type: none"> <li>1) brazing</li> <li>2) hot pressing / diffusion bonding</li> </ol>	<ol style="list-style-type: none"> <li>1) properties after 1000 hours at <math>1000^{\circ}\text{C}</math></li> <li>2) irradiation tests (<b>ORNL, Oak Ridge, Y. Katoh, L. Snead, et al.</b>)</li> </ol>	<p>1) burst tests at <math>600^{\circ}\text{C}</math></p> <p><b>Joint to steel</b></p> <ol style="list-style-type: none"> <li>1) thermal fatigue tests (RT – <math>600^{\circ}\text{C}</math>)</li> </ol>



## Outlook (II/II)

- KIT-CCFE cooperation:  
E. Surrey, T. Barrett, W. Timmis, C. Waldon, M. Porton,...
- Workshop on water cooled divertors:
  - Mai 2012: CCFE
  - August 2012: KIT
  - next: March 2013: CCFE
- Plans and ideas: e.g. double-walled pipes



# Summary

- Introduction
  - Requirements for a DEMO divertor
  - Temperature distribution
- The tungsten laminate project
  - Interlayer between steel and tungsten
  - Structural material
- Matrix of coolant and structural material
  - What amount of heat can be removed by which combination of (i) coolant and (ii) structural material?
- Divertor for DEMO: proposals
  - Austenitic steel – water coolant
  - Tungsten laminate – helium coolant
- Appendix (material issues)



# Thank you for your attention

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Plansee Metall GmbH,  
University of Oxford,  
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Oak Ridge National Laboratory, and  
our colleagues from IAM (KIT).

