



#### Oxidation of zirconium alloys in mixed atmospheres containing nitrogen

#### Martin Steinbrück, Karlsruhe Institute of Technology, Institute for Applied Materials

EFC Workshop "Beyond Single Oxidants", 19-21 September 2012, Frankfurt/M., Germany

Institute for Applied Materials, IAM-AWP / Program NUKLEAR



KIT – University of the State of Baden-Wuerttemberg and National Research Center of the Helmholtz Association

### Karlsruhe Institute of Technology

Founded in 2009

#### = FZK research center (1956) + University Karlsruhe (1825)

#### = 9000 employees

#### = 23 000 students



#### **Motivation**



- Zirconium alloys are used as cladding materials in nuclear reactors worldwide
- Especially advanced cladding alloys (e.g. M5<sup>®</sup>, ZIRLO<sup>™</sup>) exhibit excellent mechanical and corrosion properties during operation till high burnup
- But, at high temperature, existing during LOCA and severe accidents, strong oxidation occurs, causing:
  - Cladding degradation
  - Hydrogen release
  - Energy release
- Oxidizing atmospheres:
  - Steam
  - 🗖 Air
  - Nitrogen
  - Mixtures of them

after - failure of RPV







#### **Specimens**



2-cm cladding segmentsBoth-side oxidation allowed



#### Composition (approx., main alloying elements)

| Element | Zircaloy-4 | D4  | M5    | E110  | ZIRLO  |
|---------|------------|-----|-------|-------|--------|
| Nb      | -          | -   | 1     | 1     | 1      |
| Sn      | 1.5        | 0.5 | 0.01  | -     | 1      |
| Fe      | 0.2        | 0.5 | 0.05  | 0.008 | 0.11   |
| Cr      | 0.1        | 0.2 | 0.015 | 0.002 | < 0.01 |



## Test rig with thermal balance and mass spectrometer









 Release of hydrogen and heat
Hydrogen either released to the environment or absorbed by Zr metal



## Hydrogen detonation in Fukushima Dai-ichi NPPs ...







### **Oxidation in steam (oxygen)**



- Most textbooks: Parabolic kinetics of HT oxidation of Zr alloys determined by the diffusion of oxygen through growing oxide scale
- Most LOCA and SFD codes use parabolic oxidation correlations



## Calculated oxide thickness during oxidation of Zry at 1200°C in steam





#### **Breakaway oxidation**

- Loss of protective properties of oxide scale due to its mechanical failure.
- Breakaway is caused by phase transformation from pseudo-stable tetragonal to monoclinic oxide and corresponding change in density up to ca. 1050°C.
- Critical times and oxide thicknesses for breakaway strongly depend on type of alloy and boundary conditions (ca. 30 min at 1000°C and 8 h at 600°C).
- During breakaway significant amounts of hydrogen can be absorbed (>40 at.%, 7000 wppm) due to local enrichment of H<sub>2</sub> in pores and cracks near the metal/oxide boundary ("hydrogen pump").









## Correlation of H absorption and oxide morphology





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# In-situ investigation by neutron radiography of hydrogen uptake during oxidation of Zry in steam





### **Oxidation in atmospheres containing nitrogen**



- Air ingress reactor core, spent fuel pond, or transportation cask
- Nitrogen in BWR containments (inertization) and ECCS pressurizers
- Prototypically following steam oxidation and mixed with steam

#### Consequences:

- <u>Significant heat release</u> causing temperature runaway from lower temperatures than in steam
- <u>Strong degradation of cladding</u> causing early loss of barrier effect
- <u>High oxygen activity</u> influencing FP chemistry and transport











### **Oxidation of Zr alloys in N<sub>2</sub>, O<sub>2</sub> and air**







# Oxidation of Zr alloys in N<sub>2</sub>, O<sub>2</sub> and air





**14** 21.09.2011

### **Consequences of air ingress for cladding**





1 hour at 1200°C in steam



#### 1 hour at 1200°C in air



## Loss of barrier effect of cladding

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### **Mechanism of air oxidation**



- Diffusion of air through imperfections in the oxide scale to the metal/oxide boundary
- Consumption of oxygen
- Remaining nitrogen reacts with zirconium and forms ZrN
- ZrN is re-oxidized by fresh air with proceeding reaction associated with a volume increase by 48%
- Formation of porous and nonprotective oxide scales



1 – initially formed dense oxide  $ZrO_2$ 2 – porous oxide after oxidation of ZrN 3 – ZrO<sub>2</sub> / ZrN mixture 4 –  $\alpha$ -Zr(O)



### **Experiments on mechanism of nitrogen attack**







### **Reaction of ZrO<sub>x</sub> with nitrogen**









#### 19 21.09.2011 Martin Steinbrück



## Nitride formation under local and global oxygen starvation conditions





Local oxygen starvation: Formation and re-oxidation of nitride phase at metal-oxide phase boundary



<u>Global oxygen starvation:</u> Pre-oxidation in steam and subsequent reaction in pure nitrogen

Nitride formation only in the absence of oxygen in the gas phase and in the presence of oxygen in the solid phase!



### **Oxidation in mixed steam-air atmospheres**



Zry-4, 1 hour at 1200°C



Increasing degradation with raising content of air in the mixture



### **Oxidation in mixed steam-nitrogen atmosphere**



#### 1 hour at 1000 °C in steam



#### 1 hour at 1000 °C in 50/50 steam/N<sub>2</sub>



- Strong effect of nitrogen on oxidation and degradation
- Nitrogen acts like a catalyst (NOT like an inert gas)
- Enhanced hydrogen source term by oxidation in mixtures containing nitrogen



#### **Oxidation of Zr alloys in various atmospheres**





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### Conclusions



- The usually applied parabolic correlation for the hightemperature oxidation of zirconium alloys are not valid under all conditions
- Breakaway has to be taken into account at temperatures below 1100°C especially for slow transients and long duration scenarios
- Nitrogen is not an inert gas under the conditions of a nuclear accident
- Zirconium nitride ZrN is formed when (1) oxygen is absent in the atmosphere <u>and</u> (2) oxygen is present in the solid phase
- Hydrogen produced by oxidation in steam is released to the environment (explosion risk) and absorbed by the remaining metal (degradation of mechanical properties)









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#### Phase diagram Zr - O







#### Phase diagram Zr - H







### Reaction of $\alpha$ -Zr(O) with nitrogen



#### 1200 °C, 6.5 wt% O



