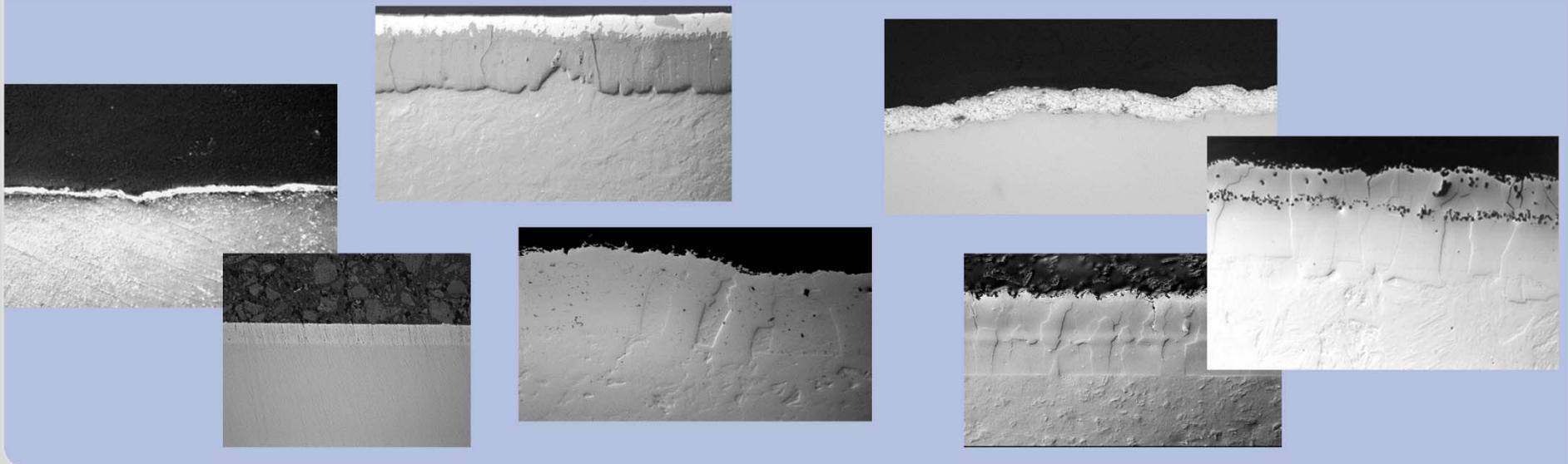


# Evaluation of Coating Processes for the Development of Aluminum-based Barriers for Fusion Applications

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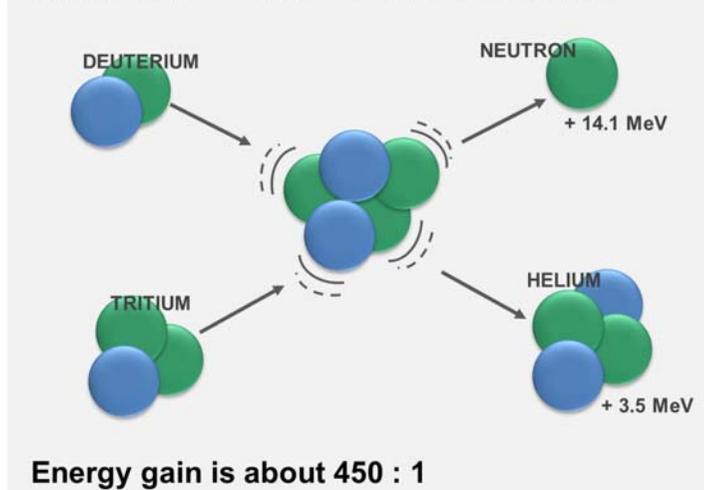
# Advanced processes for T-permeation and corrosion barriers

## Outline

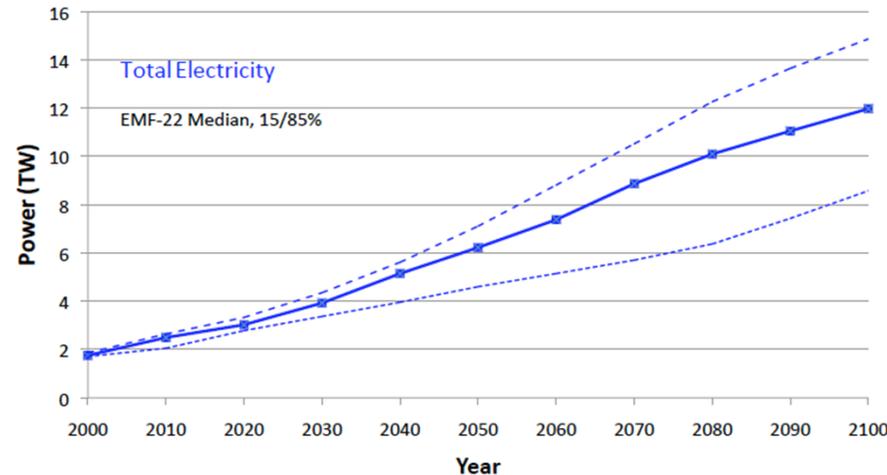
- Applications for Nuclear Fusion
  - T-permeation and/or anti-corrosion barriers for liquid breeder blanket concepts in ITER and future Fusion Power Reactors
    - ▶ Why **Al-based** barriers?
- Overview of previous coating activities → Hot-dip-aluminization process
- New electrochemical Al coating processes
  - Al deposition from organic aprotic electrolytes (ECA)
  - Al deposition from ionic liquids + metal salt (ECX)
- Conclusions

# Nuclear Fusion as an long-term Option for the Worldwide Energy Demand

Deuterium – Tritium Fusion Reaction

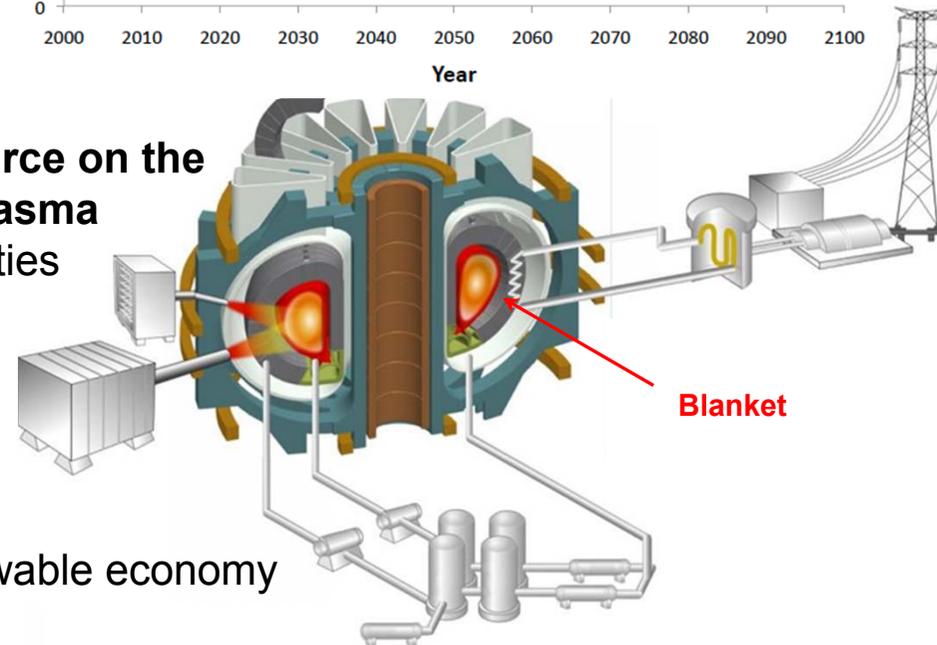


Worldwide energy demand is rising continuously



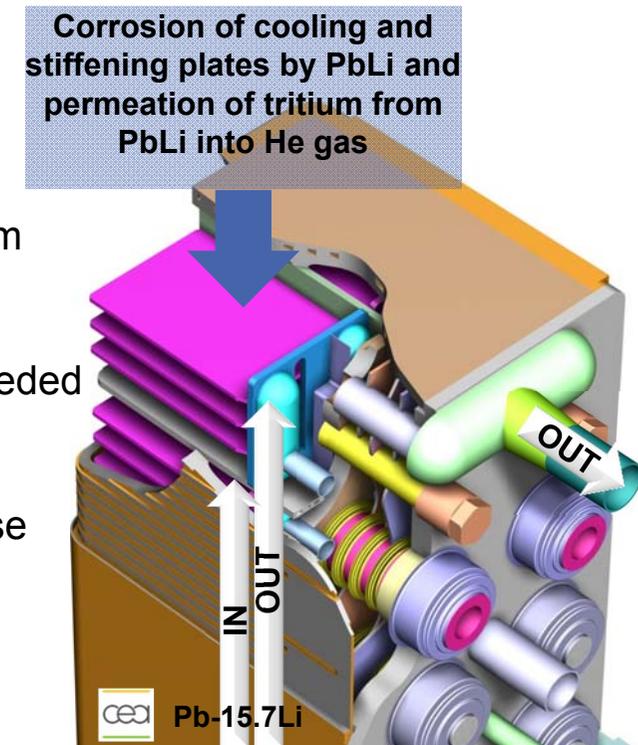
## Development of a new primary energy source on the basis of a magnetically confined fusion plasma

- Favorable environmental and safety properties
- Unit size 2 – 5 GWth / 1 – 2 GWe
  - Size of present base load power plants
- Potential fusion applications
  - Base load for large cities
  - Energy intensive industries
  - High temperature process heat in a renewable economy



# The He-PbLi blanket concept for ITER: Application of T-permeation and/or anti-corrosion barriers

- Deuterium (D) is highly available, e. g. in sea water
- Tritium (T) is naturally “not really“ available, but
  - produced in CANDU reactors by  $(n, \gamma)$  reaction on deuterium
  - **and bred by nuclear reactions from Lithium**  
 ${}^6\text{Li} (8\%) + n \rightarrow \text{T} + \text{He} + 4.8 \text{ MeV} \rightarrow$  enrichment is needed  
 ${}^7\text{Li} (92\%) + n \rightarrow \text{T} + \text{He} - 2.87 \text{ MeV}$
- Worldwide, many fusion reactor concepts are designed to use lithium in different chemical form
  - as solid breeder, e.g.  $\text{Li}_4\text{SO}_4$ ,  $\text{Li}_2\text{O}$
  - as liquid metal, e.g. pure Li or Pb-15.7Li ( $T_m = 235^\circ\text{C}$ )



Barriers  
are required!

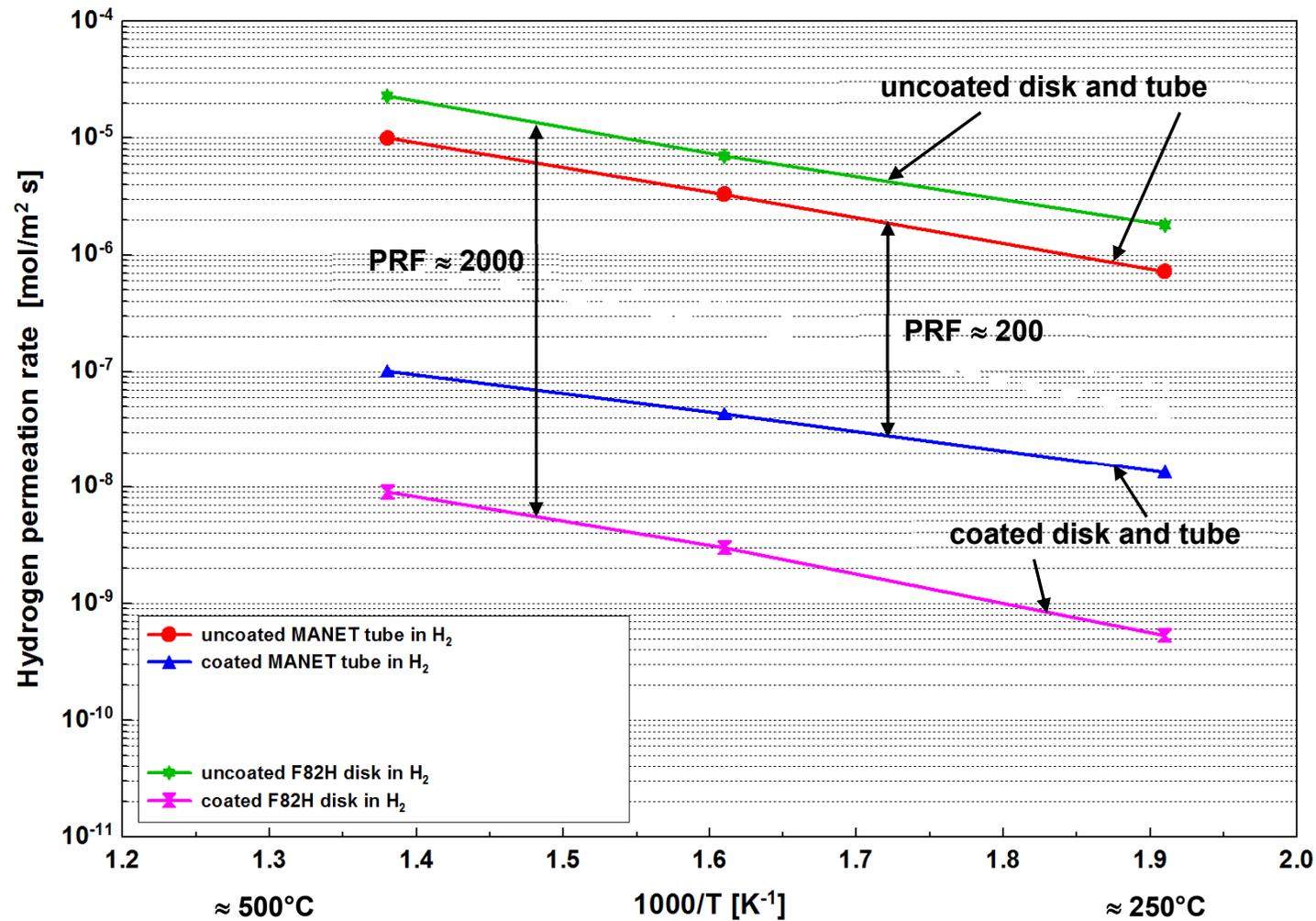
# Structure and technical requirements for an Al-based T-permeation and/or corrosion barrier



## Requirements for a tritium permeation barrier

- Reduction of T-permeation by a factor of <100 in Pb-15.7Li (1000 in gas phase)
- Self-healing of (mechanically) damaged layer must be thermodynamically possible in Pb-15.7Li (re-oxidizing)
- Long-term corrosion resistant in Pb-15.7Li up to ca. 550°C
- High content of low activation elements
- No negative influence on mechanical properties of the steel due to the coating process
- The coating process must be of industrial relevance

# Permeation data of Al-coated FM-steels in H<sub>2</sub>



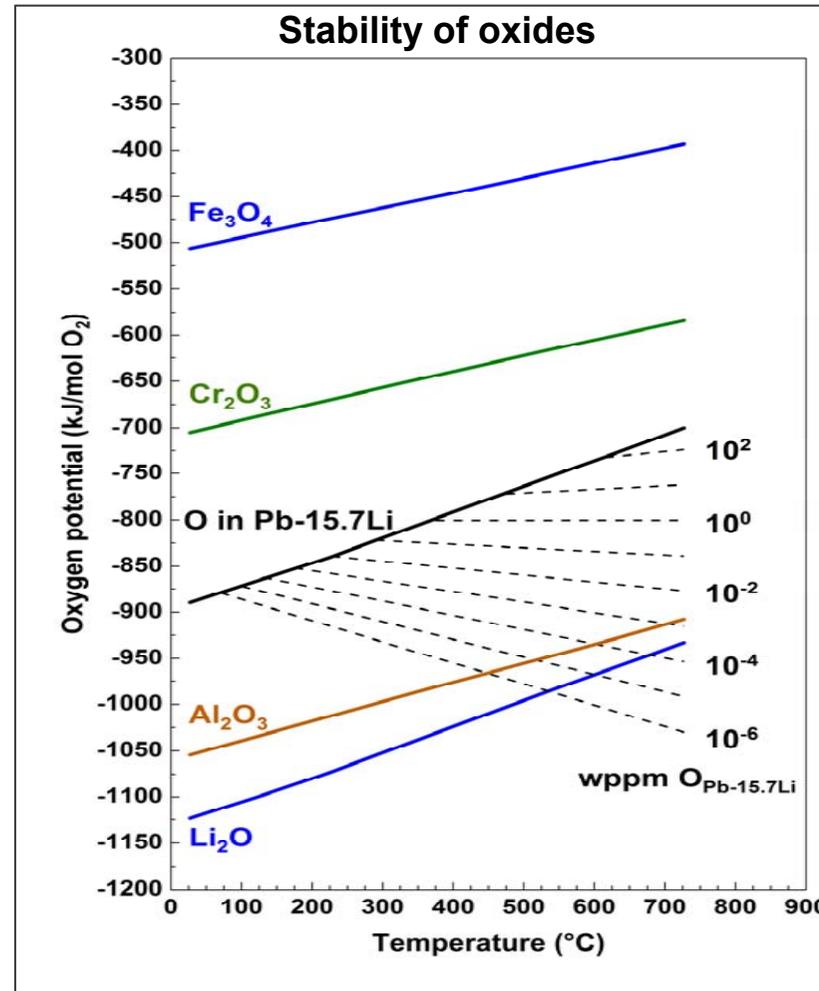
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# Thermodynamics of Al/Al<sub>2</sub>O<sub>3</sub>-based T-permeation barriers



# Structure and technical requirements for an Al-based T-permeation and/or corrosion barrier

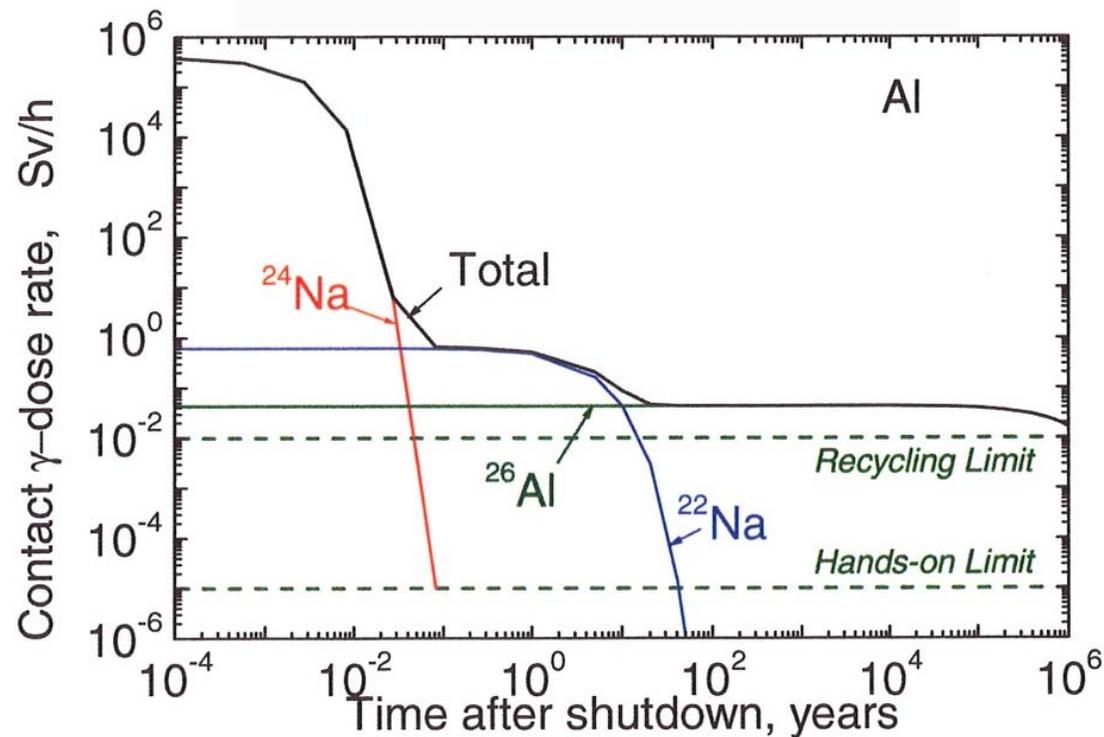


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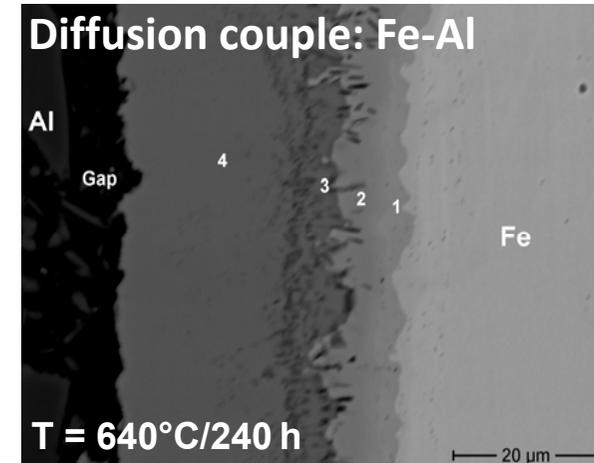
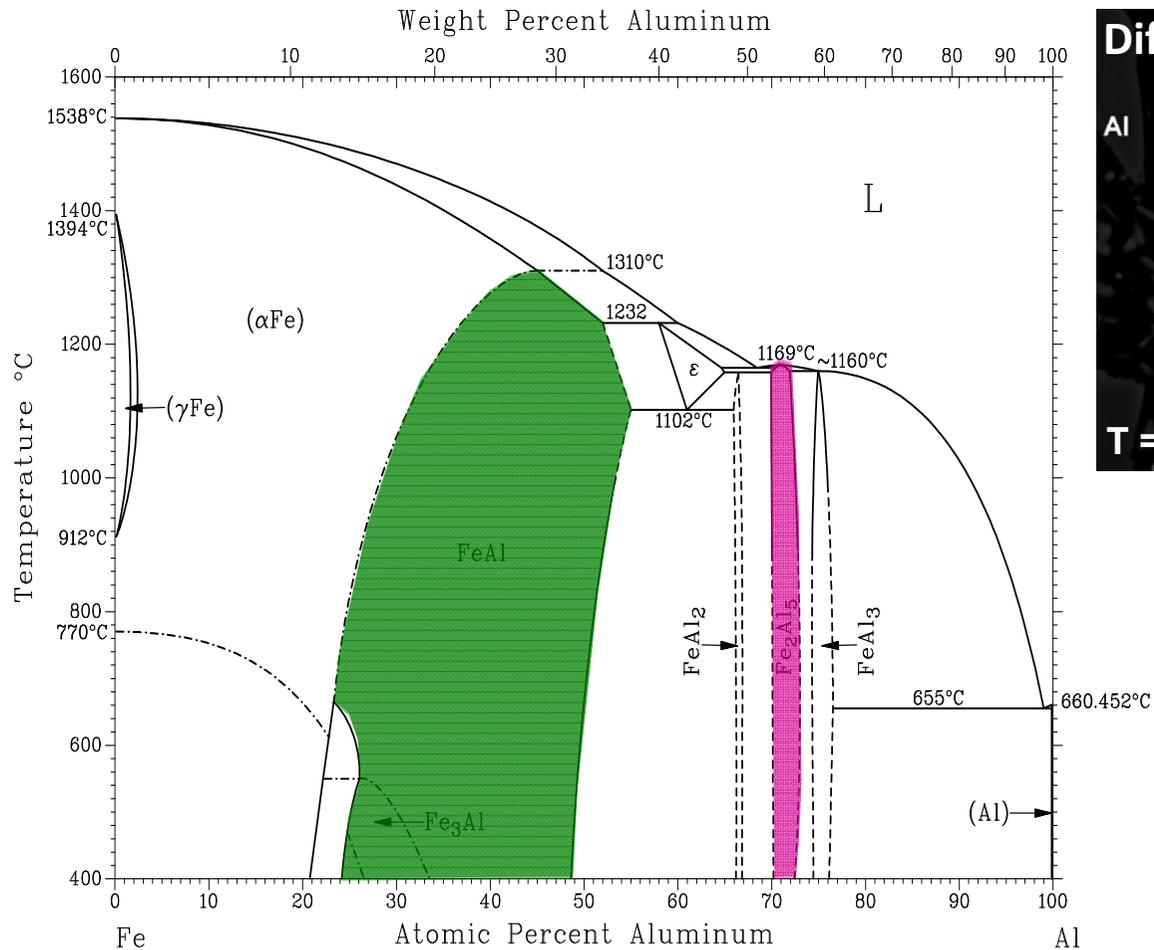
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# Activation of Al for Al-based barriers in a “fusion irradiation environment”

## Aluminium irradiation for 2 years



# Al-based coatings: The Fe-Al phase diagram



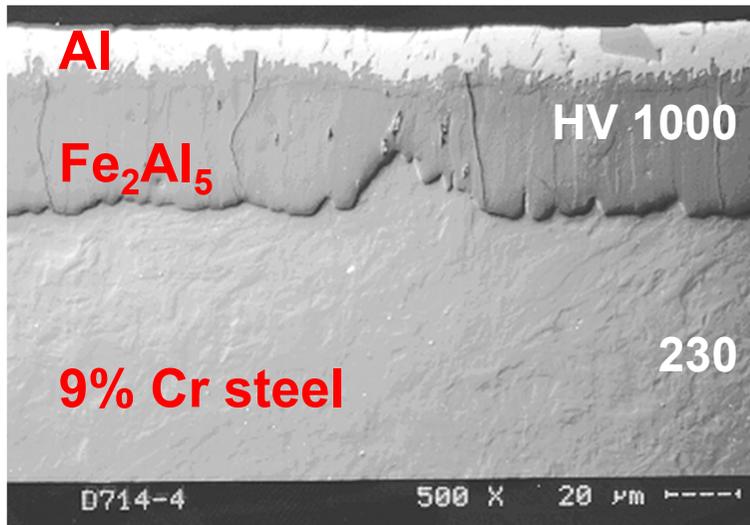
- 1: Fe<sub>3</sub>Al
- 2: FeAl
- 3: FeAl<sub>2</sub>
- 4: Fe<sub>2</sub>Al<sub>5</sub>

# Hot-Dip aluminizing process

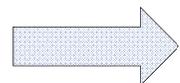
Parameters for hot dipping are:

Temperature  $T_{\text{dip}} = 700^{\circ}\text{C}$ , dipping time of 30 s in Ar-5% $\text{H}_2$

Microstructure of hot dipped surface

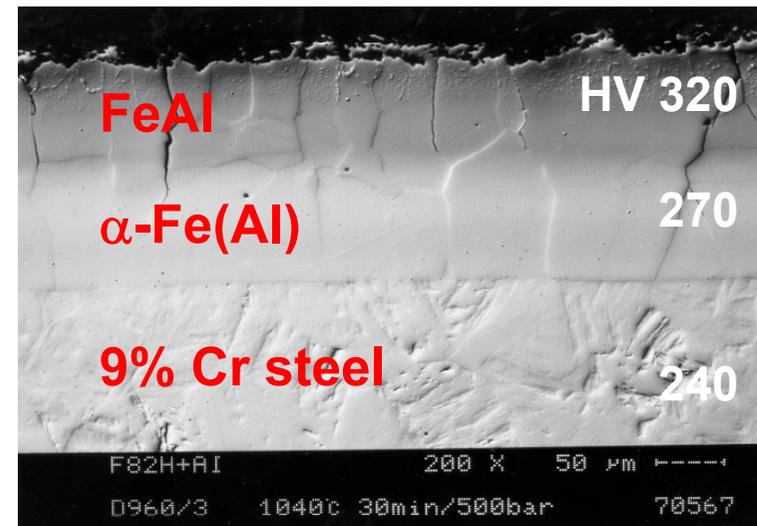


The alloyed surface layer consists of brittle  $\text{Fe}_2\text{Al}_5$ , covered by solidified Al



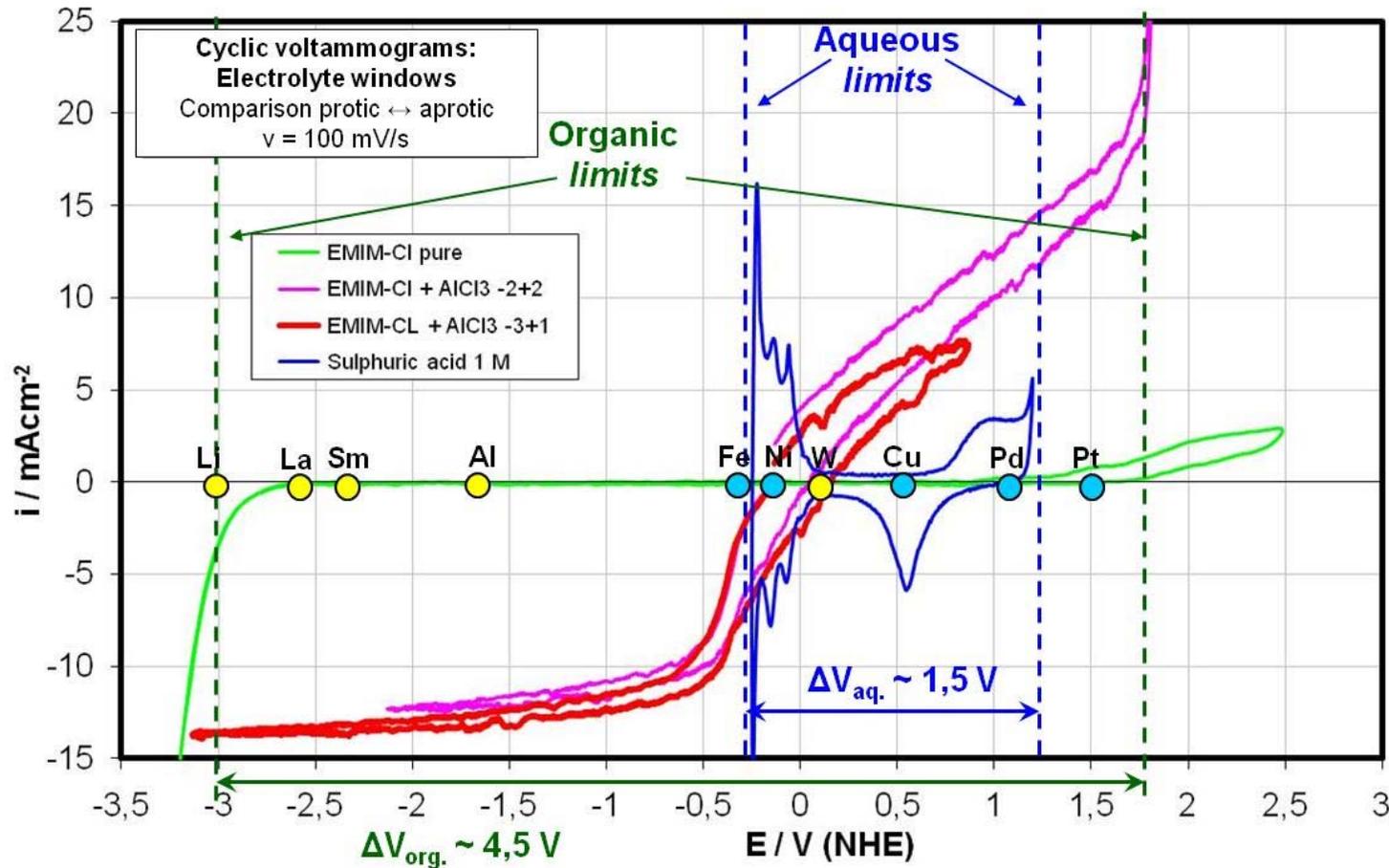
Al-enriched layer is too thick  $\rightarrow$  too much Al in the near-surface region

Microstructure after heat treatment



Heat treatment at  $980^{\circ}\text{C} / 0.5 \text{ h} + 760^{\circ}\text{C} / 1.5 \text{ h}$  and an applied pressure of  $>250 \text{ bar}$  (HIPing) reduces porosity and transforms the brittle  $\text{Fe}_2\text{Al}_5$ -phase into the more ductile phases FeAl and  $\alpha\text{-Fe(Al)}$

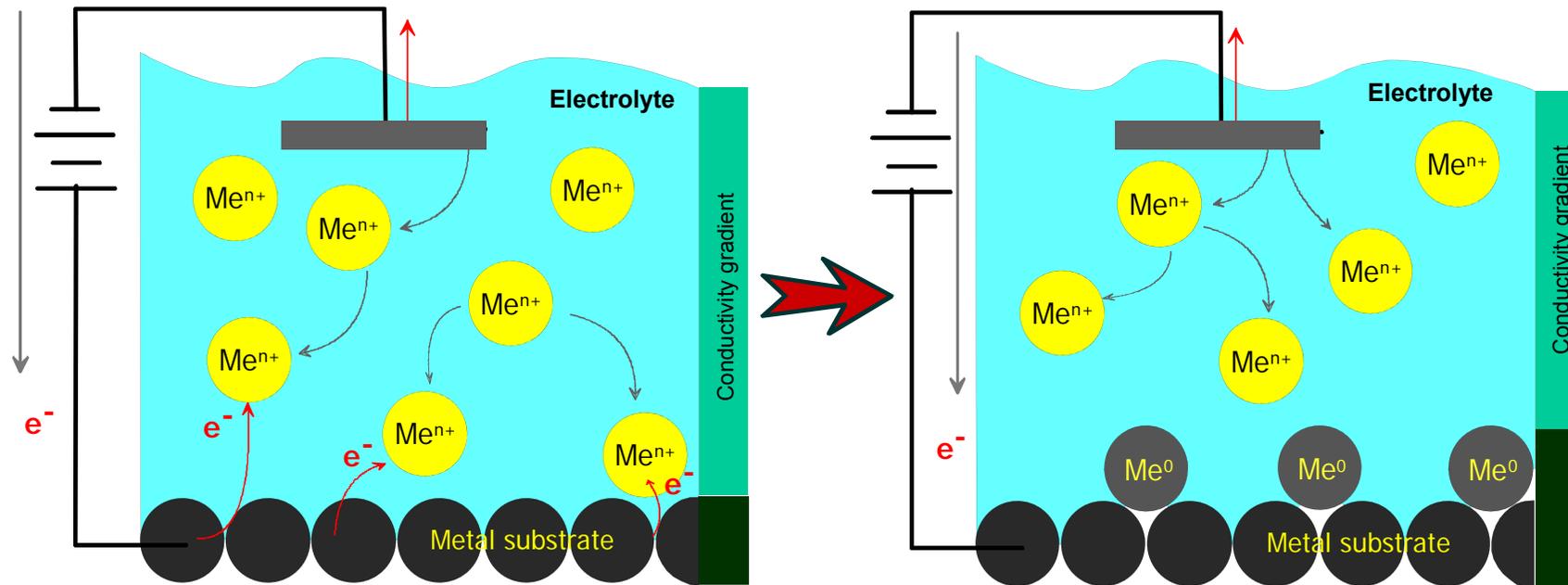
# Electrochemistry for coating application



## EC measurements of protic and aprotic metal deposition systems

# Electrochemical deposition for barriers/coatings

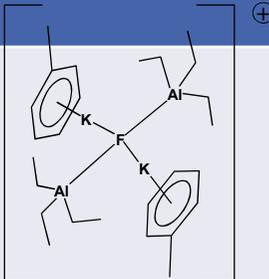
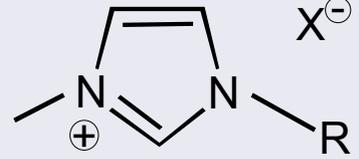
## - advantages of galvanic coatings -



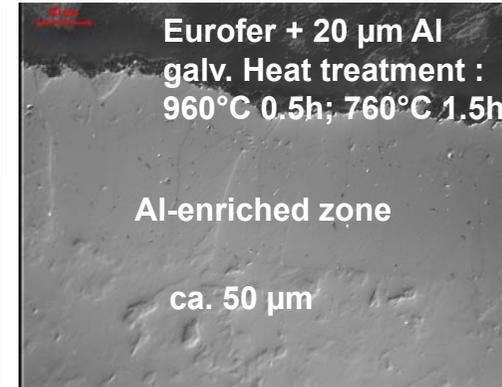
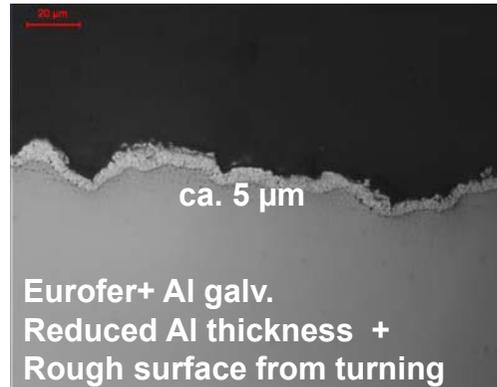
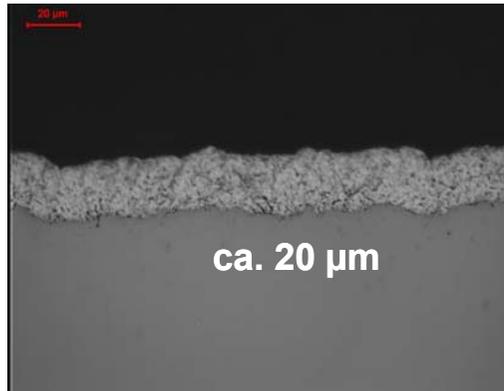
- By **anodic** dissolution, metal removal takes place without any mechanical stresses and at “low” temperatures

- **No gradients**  $\Delta T$ ,  $\Delta p$  (and resulting forces) between
  - electrolyte medium and metal surface
  - metal surface and metal bulk
- ▶ no local heating as in EDM working
- ▶ no mechanical load (no residual stresses)

# Electrochemical aluminium deposition - properties of organic aprotic electrolyte systems -

Solvens		Toluol, Xylol Diisopropylether	Quarternay Amin salts e. g. Ethylimidazolium chloride
Ionic solubility of solvens		No	Yes
Al-carrier system		KF·2Al(R) <sub>3</sub> R = C <sub>n</sub> H <sub>2n+1</sub> mit n= 2-6	AlCl <sub>3</sub>
Temperature		100°C	RT ... 200°C
Reactivity	Water	extremly high	modest
	Air	extremly high	low
	Temperature	modest	Stable up to 300°C
Toxicology   biodegrability		Aromates: ++/--	Amines: -/+
Max. conductivity [mS/cm]		19,5	22,0
		<b>ECA</b>	<b>ECX</b>
		Al-Alkyl- Acryl-Complex in Toluol resp. Alkylether	Al <sup>3+</sup> + 3 Cl <sup>-</sup> → EMIM-AlCl <sub>4</sub>
			

# Development of electrochemical Al coating Process, toluol-based (ECA)



## Process specifics

Organic electrolyte, Al-alkyle, under cover gas  
Deposition temperature ca. 100°C, rate  $\approx$  12  $\mu\text{m}/\text{h}$   
More complex geometries can be coated; even inside tubes

EUROFER (wt.-%)	8.82 Cr	0.47 Mn	0.20 V	1.09 W	0.13 Ta	-- Mo	0.11 C	0.02 Ni
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## Result of ECA development

- Electrochemical coating **applicable** to functional scales in TBM's
- Barrier function tested in corrosion, successfully
- **Salt-based processes have to be developed** for higher compositional flexibility
- Reason: Electro-negativity of refractory metals and unique behavior

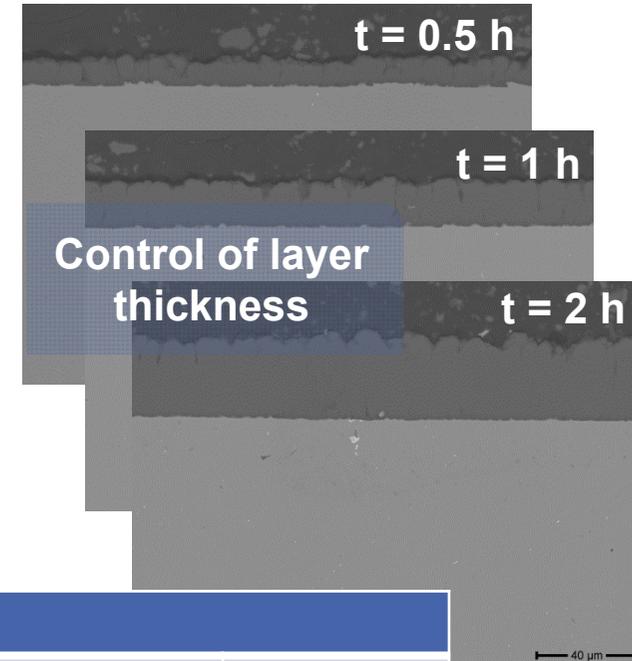
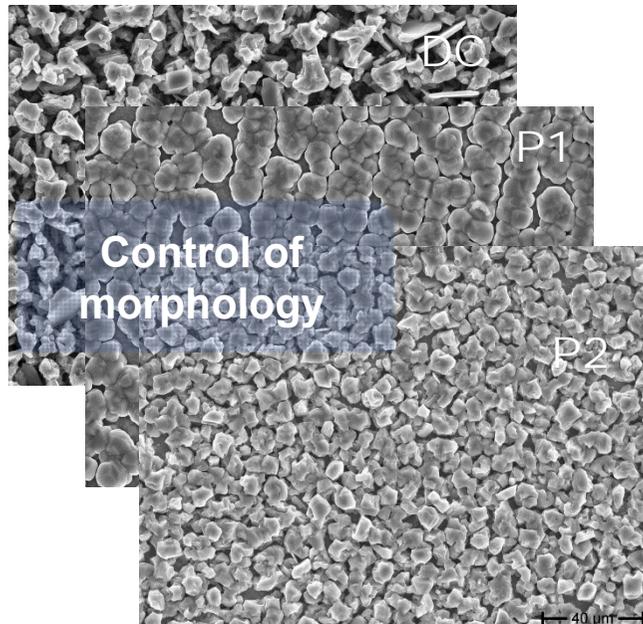


# Development of coatings as corrosion T-permeation barriers (ECX)

Development of electrochemical aluminum coating process based on ionic liquids (ECX)

Advantages of ECX process based on ionic liquids:

- Improved flexibility compared to ECA
- Improved security (inflammable, not volatile) compared to ECA
- Deposition parameters are customizable to produce coatings with specific properties (thickness, deposition rate, morphology)
- Controllable layer thickness (compared to HDA)

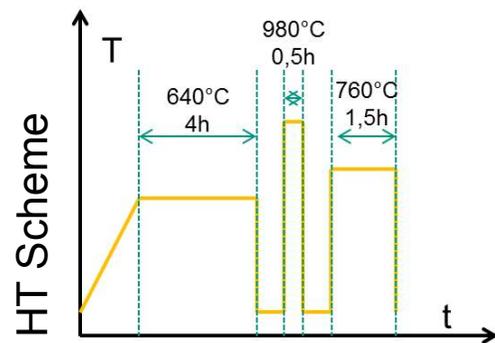


Deposition Parameters			
Parameter	DC	P1	P2
$j_m$	20 mA/cm <sup>2</sup>	20 mA/cm <sup>2</sup>	20 mA/cm <sup>2</sup>
$j_p$	-	80 mA/cm <sup>2</sup>	25 mA/cm <sup>2</sup>
$t$	30 min	30 min	30 min
$f$	-	1 s <sup>-1</sup>	1 s <sup>-1</sup>
$\Theta$	100 %	25 %	80 %

# Heat treatment of Al layers for corrosion and T-permeation barriers

## Treatment of Al coatings produced by ECX

- Heat treatment necessary to convert Al coatings to desired protective Fe-Al scales for corrosion protection and T-permeation



After deposition



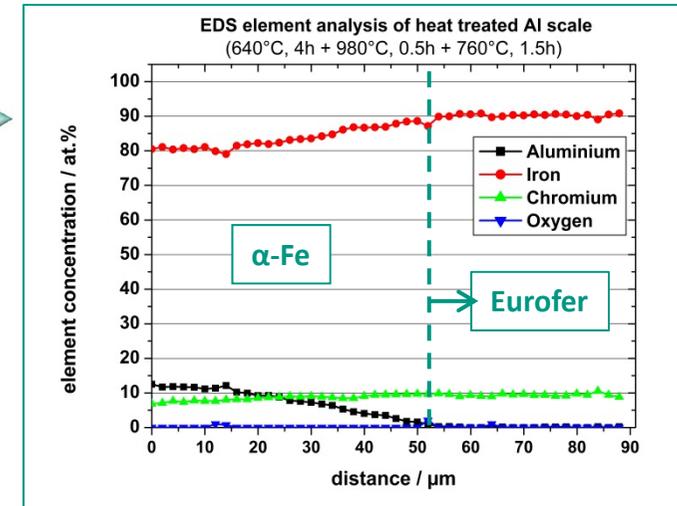
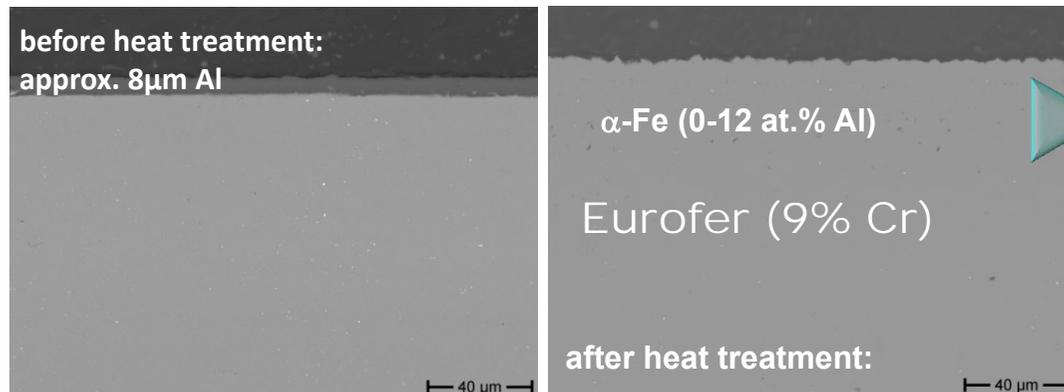
After HT



- Homogeneous conversion of Al coatings and formation desired Fe-Al scales on 1.2210 steel
- No delamination visible

# Heat treatment of Al layers for corrosion and T-permeation barriers

## Treatment of Al coatings produced by EDX process (Lewis acidic IL)



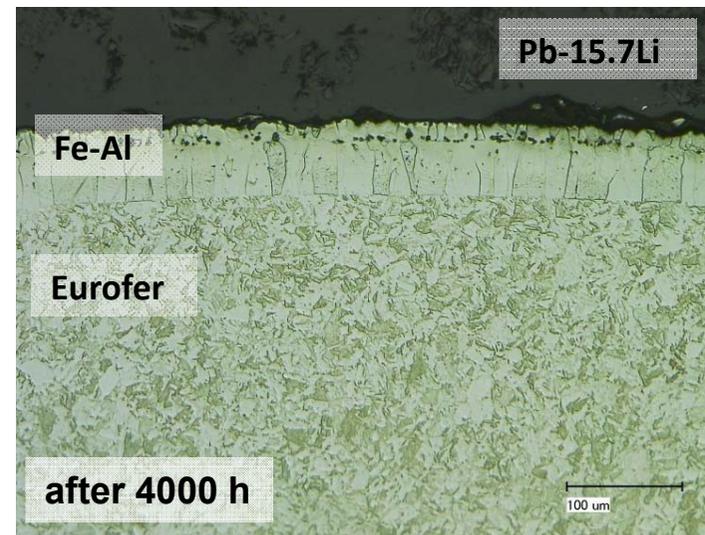
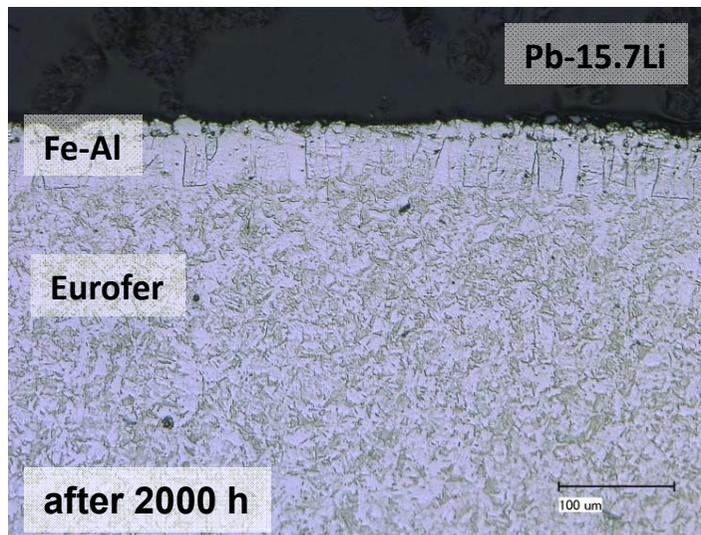
- Heat treatment under Ar atmosphere (preventing of strong surface oxidation) + additional annealing step at 640°C (4h)
- Relatively smooth surface after heat treatment
- Layer thickness after heat treatment: approx. 50  $\mu\text{m}$  (center)

### Actual work:

- Ongoing examination of deposition parameters:
  - Adhesion to the substrate, reproducibility, influence on coating properties
  - Influence of sample geometry
- Optimization of heat treatment parameters (depending on parameters during ECX process)

# Development of electrochemical aluminum coating processes (corrosion tests in Pb-15.7Li for ECX process)

- Barriers produced by ECX process:
  - Corrosion protection of Eurofer in flowing Pb-Li is shown for “short-term“ exposure times up to 4.000h
  - Remaining protective scale thickness after 4000 h:  $>50 \mu\text{m}$
  - Radial mass loss: ca.  $10 \mu\text{m}$  → **corrosion rate ca.  $20 \mu\text{m}/\text{year}$**
  - Homogeneous corrosion attack of the scale itself → No formation of plateaus (!) visible as in the case scales produced by ECA process



# Conclusions

- **Barriers**, based on Fe-Al/ $\text{Al}_2\text{O}_3$ , are appropriate to fulfill the requirements for T-permeation reduction and corrosion protection in liquid PbLi.
- **Hot-dip aluminizing** is an excellent tool to investigate the formation of aluminide layers on FM-steels (interdiffusion). But HDA coatings have drawbacks because of the high Al content in the surface
  - ▶ high activation under neutron irradiation:  $^{26}\text{Al}$   
and the low flexibility for coating of complex-shaped parts.
- Electrochemical deposition processes like **ECX** have shown their applicability for manufacturing of thin Al coatings with **high reproducibility**, even for complex geometries.
- The development of appropriate **heat treatments** has to be further optimized, followed by new permeation tests in H-, D- and finally T- environments.
- The new electrochemical Al-based coatings have also a high potential in other energy applications at elevated temperatures and aggressive environments.