Modeling of the QUENCH-14 bundle experiment using ASTECv2.0R2p2

Heinrich Muscher[(1)] Petar Kaleychev[(2)], Juri Stuckert[(1)]

(1) KIT; (2) SEEL Techn. Univ. Sofia; ***presented at NUTECH-2014,***

Int. Conf. on Development & Apps of Nuclear Technologies in Warsaw on 22.9.2014

by H. Muscher

Introduction

- The series of QUENCH experiments investigate the H_2 source term resulting from the water injection into an uncovered core of LWR as well as the high temperature behavior of core materials under transient conditions
- The aim is to present the results of the QUENCH-14 modeling by the ASTEC code to the Polish and foreign NUTECH community. Both KIT Karlsruhe and Techn. Univ. Sofia are adopting the ASTEC code for modeling several QUENCH experiments.

The QUENCH-14 experiment

In the QUENCH-14 experiment, the effect of **M5**® cladding material on bundle oxidation and core *re-flooding* was investigated, in addition to the former QUENCH-06 test that used **Zry-4**. The bundle configuration of QUENCH-14 with 1 unheated rod, 20 heated rods, and 4 corner rods was identical to the design of QUENCH-06.

The QUENCH-14 test was conducted in principle with the same protocol as QUENCH-06, so that the effects of the change of cladding material could be observed more easily (a "one-parameter" investigation).

QUENCH-6 was already modeled using ICARE/CATHARE in the frame of the ISP-45 (Benchmark Exercise)

QUENCH-14 facility

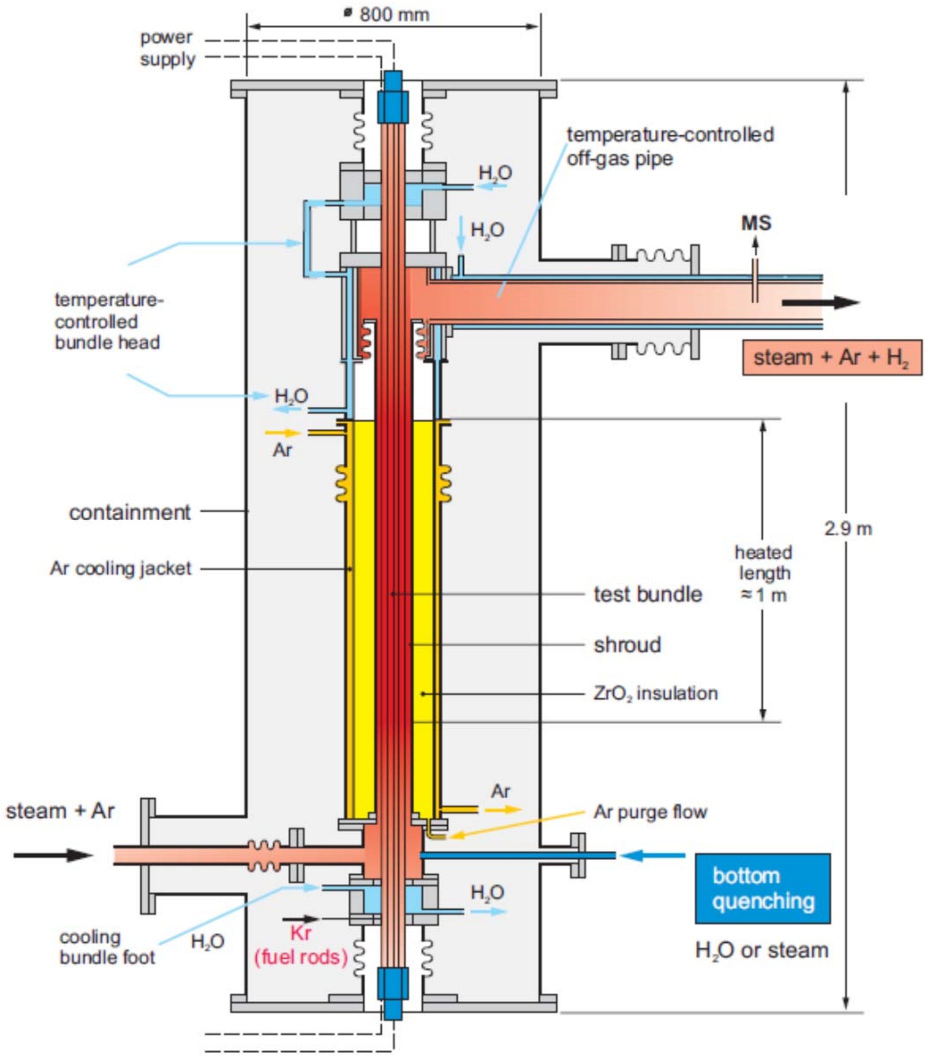
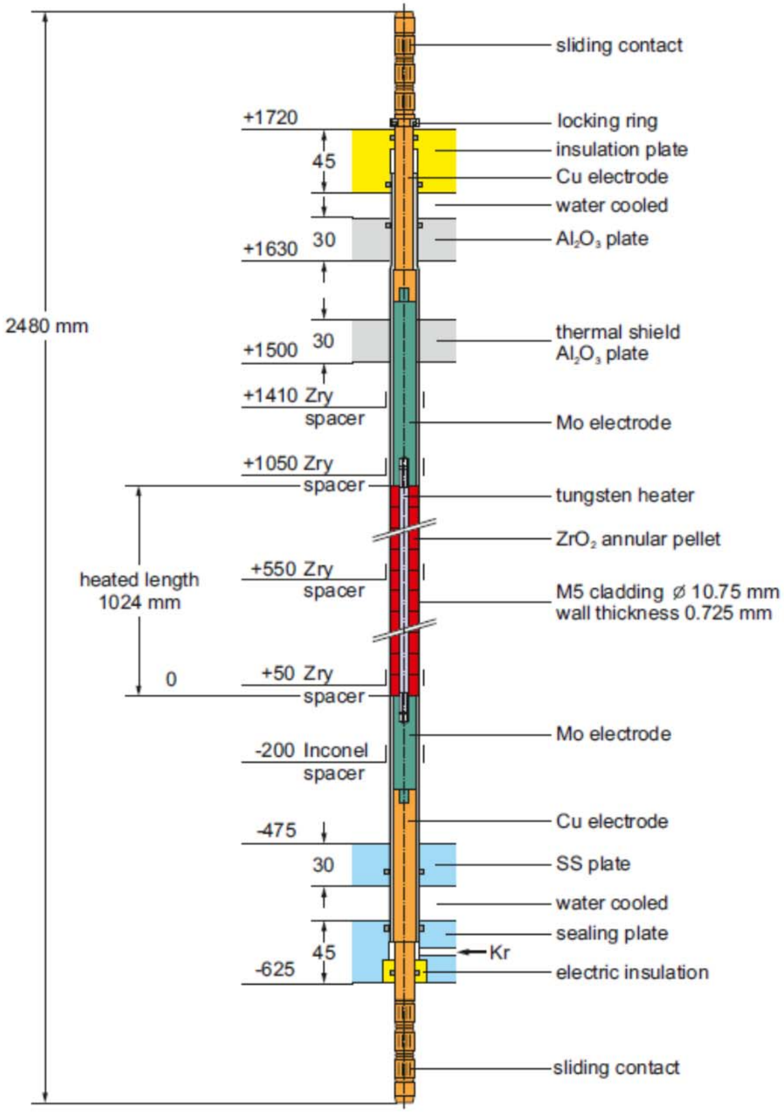


Fig.1 QUENCH-14 Test section

The test section is enclosed by a safety containment. Superheated steam from the SG and super heater together with Ar enter test bundle at the bottom. Ar, steam and H_2 produced in the Zr-$H_2O_{(g)}$ reaction flow upwards inside the bundle and from the outlet at the top through a water-cooled off-gas pipe to the condenser, where the remaining steam is separated from the non-condensable gases Ar and H_2.

QUENCH-6/-14 bundle



Fuel rod simulator

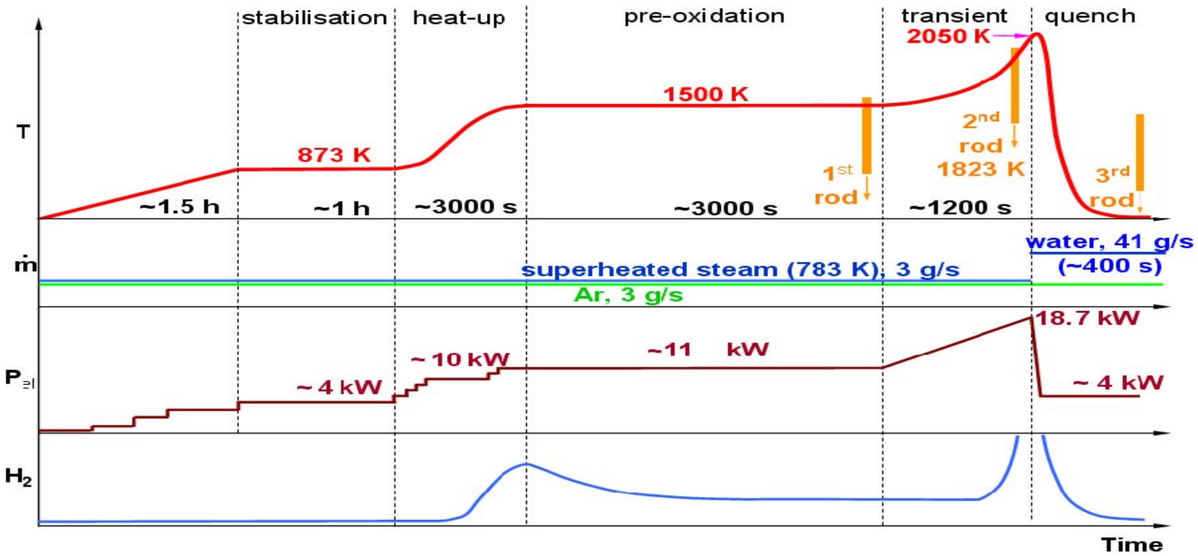
The test bundle is made up of 21 fuel rod simulators and of 4 corner rods. The fuel rod simulators are held in their positions by 5 grid spacers, 4 of Zry-4, and one of Inconel 718 in the lower bundle zone.

The rod cladding of the heated and unheated fuel rod simulator is M5® (product of AREVA)

The max. total power during the Q-14 test was 19 kW. About 40 % of it being released into the inner rod circuit (8 fuel rod simulators); 60 % in the outer one (12 fuel rod simulators).

The test bundle is surrounded by a 3.25 mm thick shroud (80 mm ID) made of Zry-4 with a 37 mm thick ZrO_2 fiber insulation and an annular cooling jacket made of Inconel 600 (inner tube) and SS (outer tube).

QUENCH-14 test phases



Heatup to ~873 K. Facility check.

Phase I Stabilization at ~873 K.

Phase II Heat-up with ~0.3-0.6 K/s until ~1500 K is reached.

Phase III Pre-ox of the bundle in a mix flow of 3 g/s of $H_2O_{(g)}$ superheated to 783K & 3 g/s Ar for ~3000 s; peak temp. of ~1500 K =const. Withdrawal of the corner rod B at the end of that Phase.

Phase IV Transient heat-up with 0.3…2.0 K/s from ~1500 to ~2050 K in the same flow conditions. Withdrawal of the corner rod D ~30 s before quench starts.

Phase V Quenching of the test bundle using a high flow of ~41 g/s of $H_2O_{(l)}$.

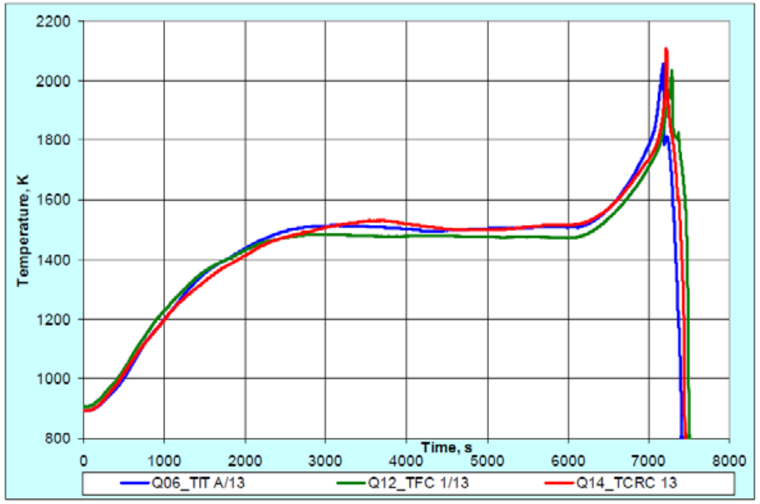
QUENCH-14 ID tuning

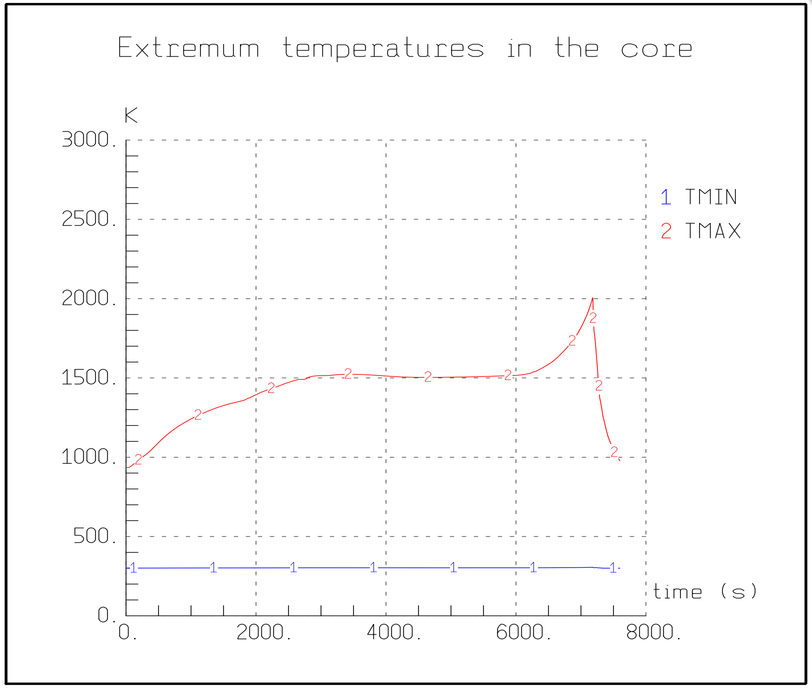
To change the QUENCH-06 ID according to the exp. conditions of QUENCH-14:

- For the temp. range (1073–1673) K, the M5® oxidation kinetics data proposed after the SET measurements at KIT (M. Große) were taken. For the temp. range (1674- 2050) K the existing data for Zry-4 were used instead that of M5® since the needed –M5® values are not available
- El. power histories for both sub circuits of heated rods were changed in accordance to Q-14 experimental results.
- Visualization: 3 figures were additionally produced: the H_2 rate [kg/s]; layer thickness evolution of the cladding [µm] vs. time and the cladding layer thicknesses [µm] for given rod elevation / according ASTEC structures were developed by S. Bertusi

By all these implementations, changes/ improvements in the QUENCH-14 IDs -both for ASTECv2.0R2p2 and ASTECv1.3R2 several runs were performed, allowing a comparison of the results given by the older and newer ASTEC-versions, respectively.

Results using ASTECv2.0R2p2





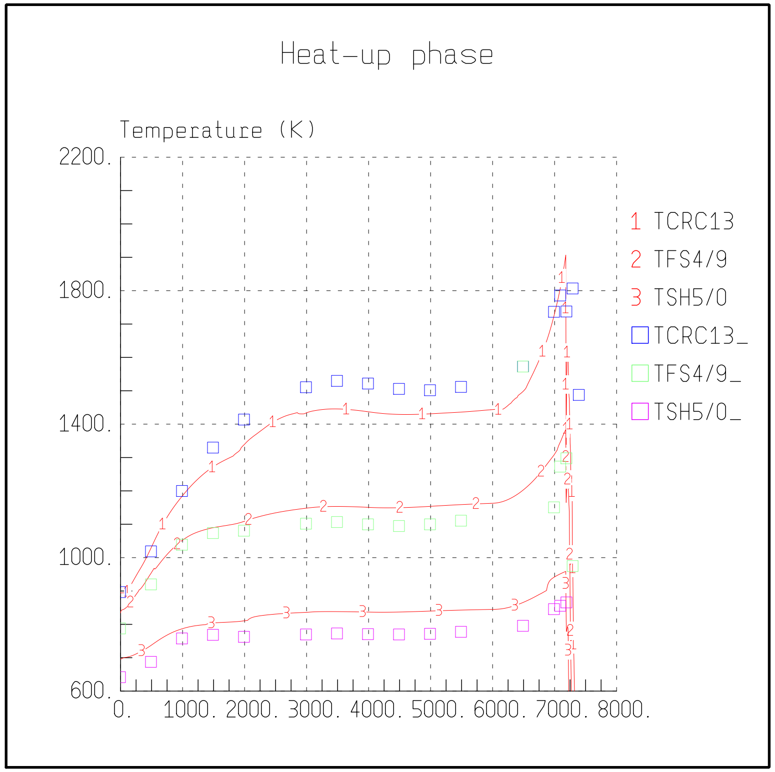
Temp. histories – experimental data

According temperatures - ASTECv2.0R2p2

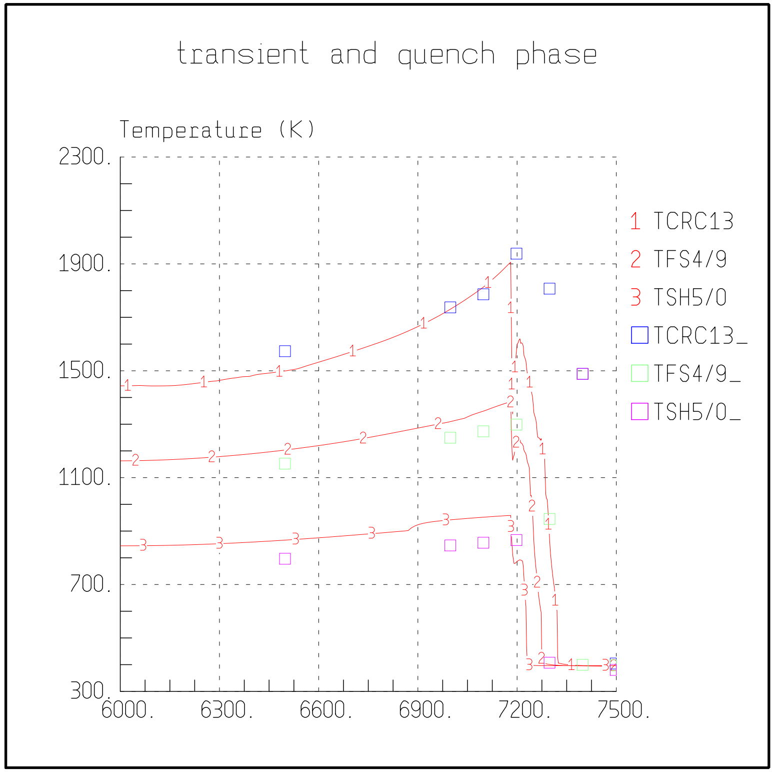
Calculated max. temp. (*right side*) is close to the exp. Q-14 data at "hottest" elevation of 950 mm (*left*), the but max. calculated value just before quenching is ca 2000 K in comparison to 2150 K for the exp.

This lower max-value may be explained with the ox correlation for Zry-4 used for the highest temp-s.

Results of ASTECv2.0R2p2: temp. histories



Rod temp. – heat-up phase



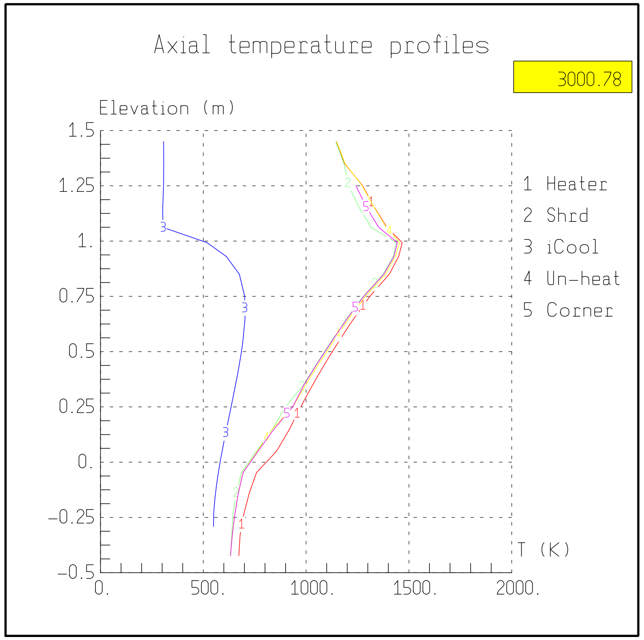
Rod temp. – transient & quench phases

Rod temp. histories for 3 rods were calculated: for the unheated central fuel rod (TCRC13), for one heated rod from the inner ring (8 rods) (TFS4/9) and for one heated rod from the outer ring of 12 rods (TSH5/0).

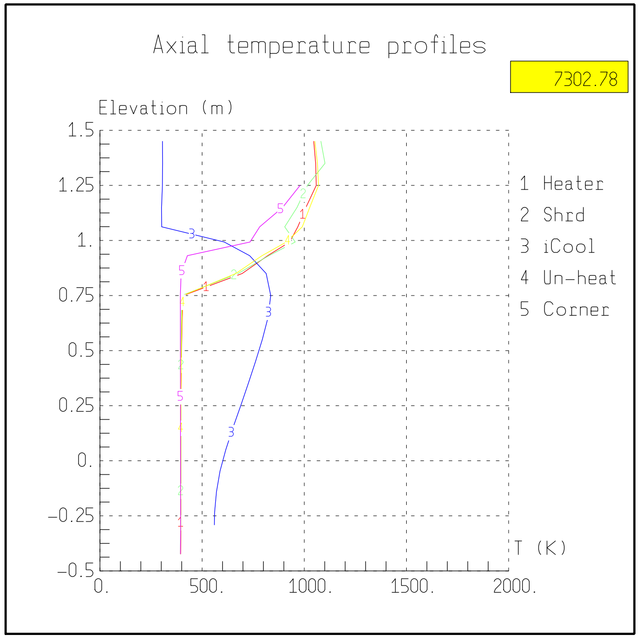
The highest temp.-s were calculated for the inner rod TCRC13, where the max. value of about 1900 K is found just before quench. For the same time the temp. of TFS4/9 is about 1500 K ; the temp. of rod TSH5/0 is 900 K.

There is an acceptable difference of about 100 K for all of the three rods in comparison to the exp. Q-14 data.

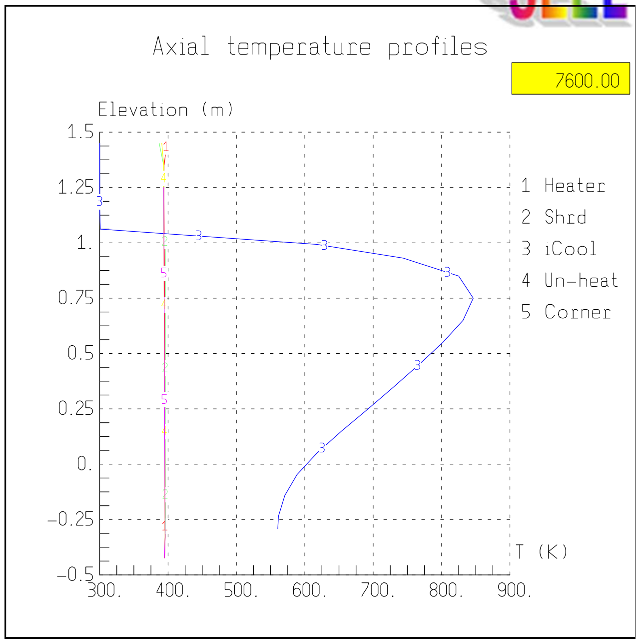
ASTECv2.0R2p2-results: some axial temp. profiles



Axial temp profiles –start of the pre-ox phase, 3000 s



Axial temp. profiles on the end of reflood, 7300 s, beginning of quenching

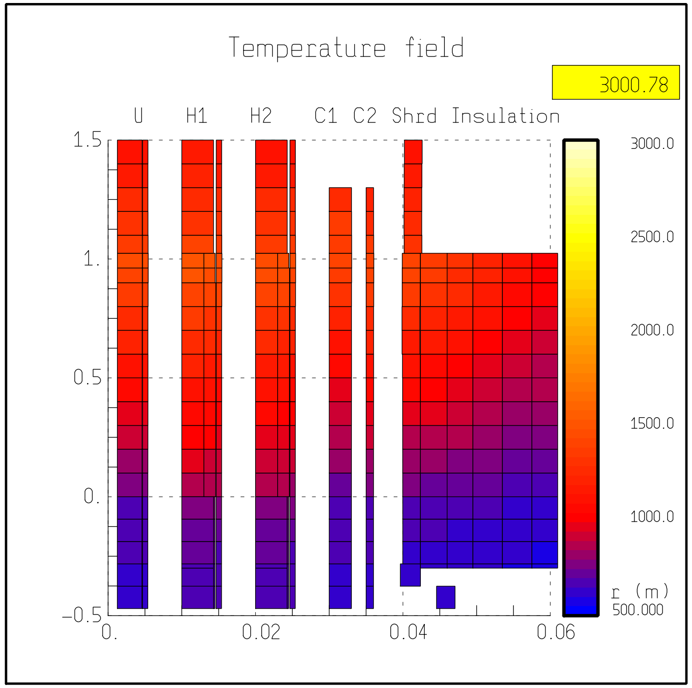


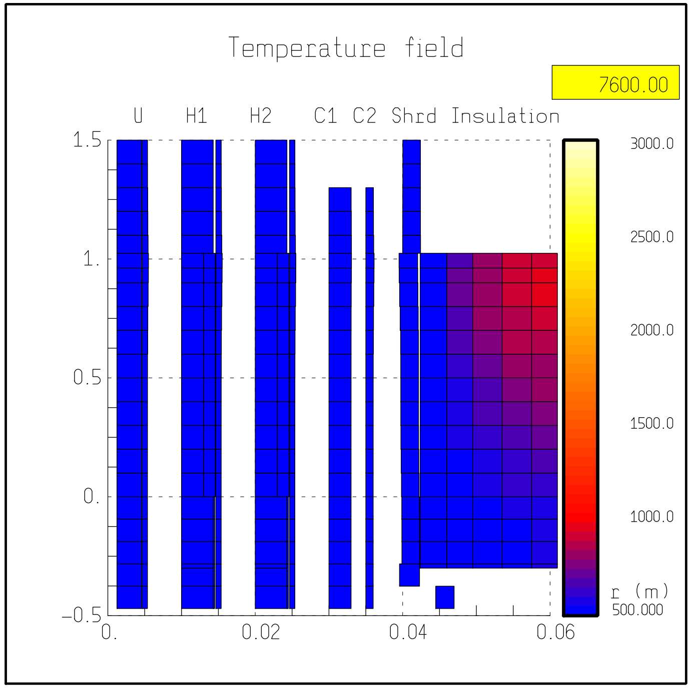
Axial temp profiles on the end of test, 7600 s

The axial temp. profiles from the beginning till the quench phase are similar for the heated rod, the shroud, the unheated and the corner rod. They are higher in comparison to the temp. of the cooling jacket. The highest temp. is calculated for the heated rod in the height of about 950 mm, exactly as it was in the Q-14 experiment.

After the beginning of the quench phase, the temp.-s of the heated, unheated and the corner rods as well as that of the shroud start to decrease (here τ=7300s) in correspondence to the rapid increase of the quench water level. In the end of the calc., the highest temp.-s at levels down to 1 m were calculated over the cooling jacket with a max. detected at a height ca. 750 mm (τ=7600 s). At heights up to 1 m the temp.-s of the heated rod, shroud, the unheated and the corner rod remain higher in comparison to the temp. of the cooling jacket.

Results of ASTECv2.0R2p2: nodalization



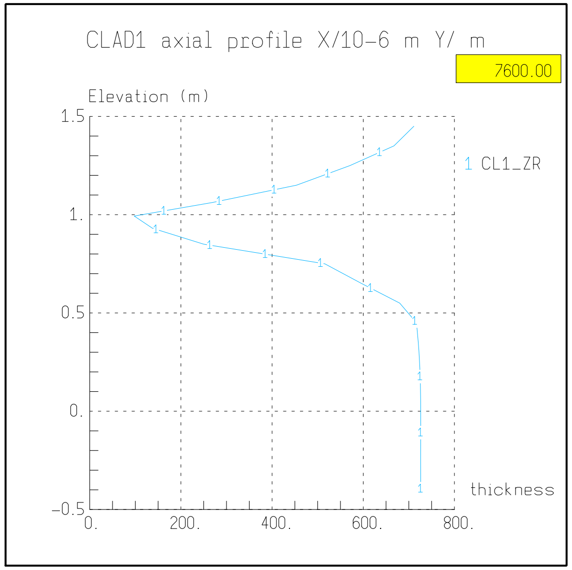


ASTEC- temp. field in the beginning of pre-ox phase (3000 s)

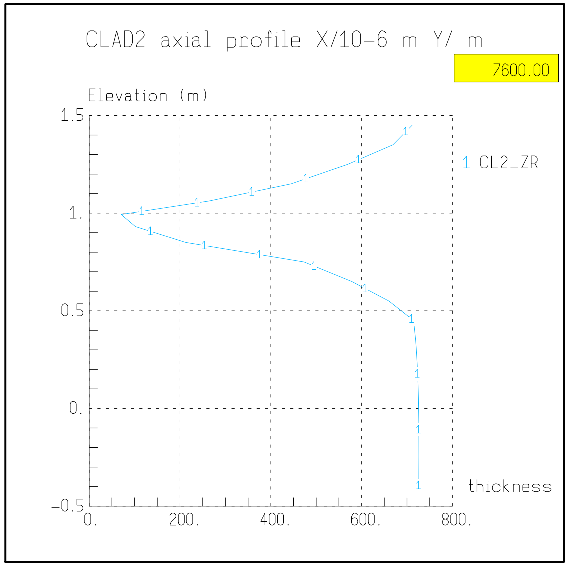
Temp field at the end of experiment (7600 s)

The temp. fields for the central rod (U), one of the heated rods from inner ring (H1), one heated rod from the outer ring (H2), two corner rods (C1 and C2), shroud and insulation. The highest temp. before quenching are calculated for height of ca. 950 mm. In the end of the calculation (at 7600 s) the highest temp. are calculated over the insulation at height around 750 mm and above.

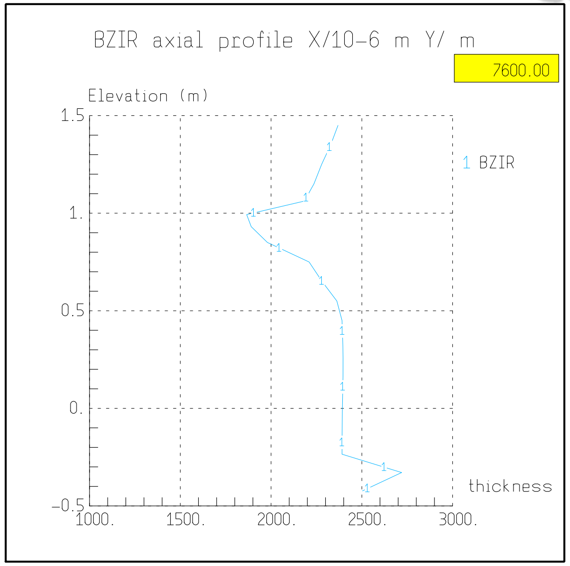
Results of ASTECv2.0R2p2: oxide layer



Oxide thickness profile, 7600 s,
unheated rod - ASTEC



Oxide thickness profile, 7600 s,
inner ring rod - ASTEC



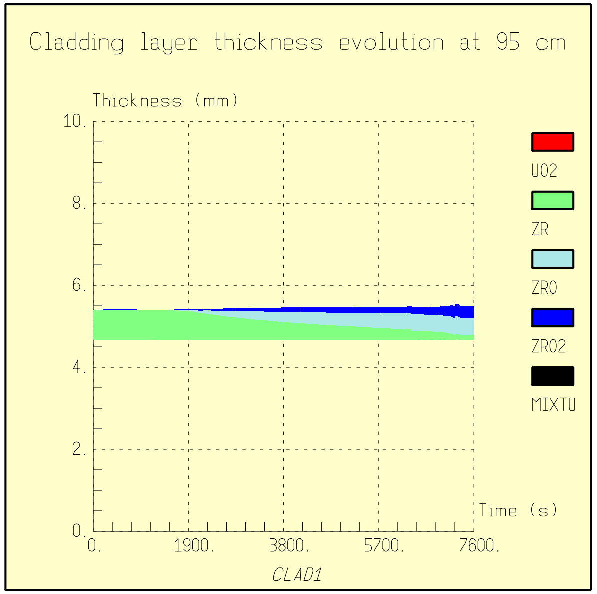
Oxide thickness profile, 7600 s,
Shroud - ASTEC

The max. oxide thickness calc. by ASTEC for the central unheated rod *(Fig. left, CLAD1*), is ca. 630 µm at a height around 950 mm in comparison to 860 µm at the same height from the Q-14 exp. At the same height, approx. equal (around 650 µm) is the max. layer thickness for inner ring rod (*CLAD2*). For the rod from the outer ring, the max. oxide thickness is about 630 µm at the height of ca. round 950 mm. In the shroud *(BZIR) the* calculated oxide thickness is of ca 650 µm: is similar to the exp. value of 590 µm.

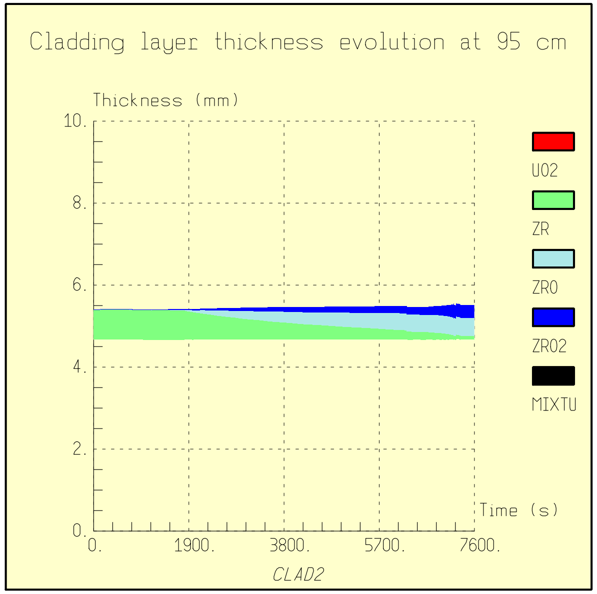
In all the fig-s depletion of the metal– layers is visualized (abs. value being equal to the oxide thicknesses)

•

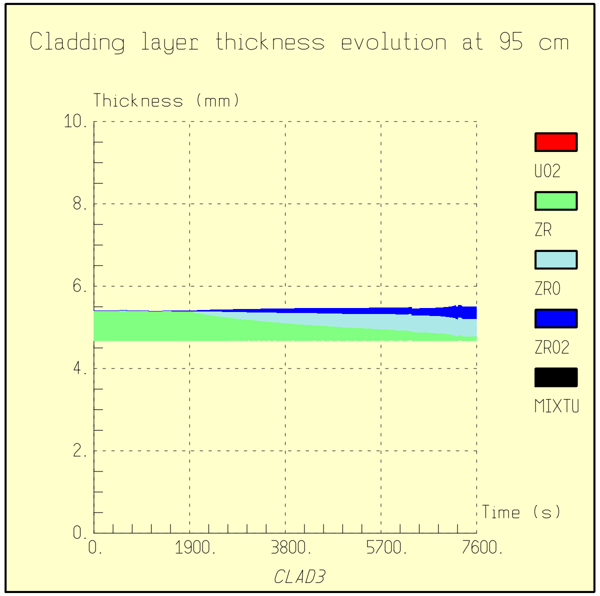
ASTECv2.0R2p2 results: formation of α-Zr(O) and ZrO_2 cladding layers



Cladding layer thickness evolution, 950 mm, unheated rod - ASTEC



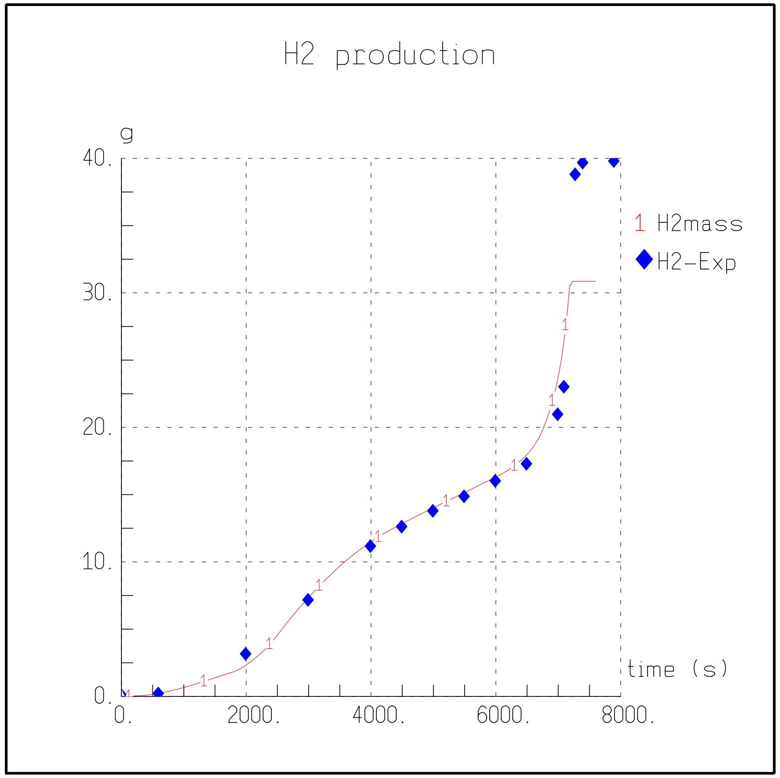
Cladding layer thickness evolution, 950 mm, inner ring rod - ASTEC



Cladding layer thickness evolution, 950 mm, outer ring rod - ASTEC

According to the height of max. calculated oxide thickness, which was at 950 mm, the cladding layer thickness evolution for the whole time of the Q-14 exp. was modeled. In the end of calc. the fraction ratio of α-Zr(O) becomes the largest one for all the 3 cases – unheated rod, inner ring and outer ring rod, on the second place – the fraction of ZrO_2 and in the end - the Zr contribution. In the case of inner ring rod oxidation one can postulate that the according oxide thicknesses (α-Zr(O) and ZrO_2) are only a little bit larger than in the cases of the unheated rod *(left)* and outer ring rod oxidation *(right).*

Results of ASTECv2.0R2p2: hydrogen release



H_2 prod. – Q-14 exp. data vs. an ASTEC -line

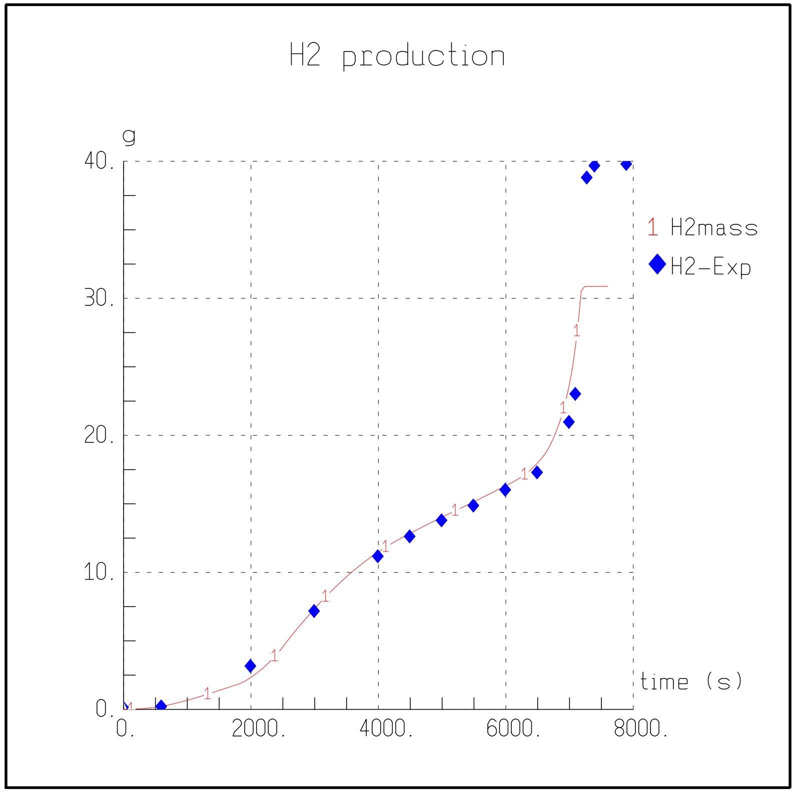
The calculated H_2 production by ASTECv2.0R2p2 is about 32 g (40 g in the Q-14 experiment).

The results obtained by ASTEC are close to the exp. data in the phases before quench. Because at the high temp.-s range (1674-2050) K data of Zry-4 instead of M5 were used (mentioned two times above), the obtained results for H_2 prod. at quench itself are under-estimated.

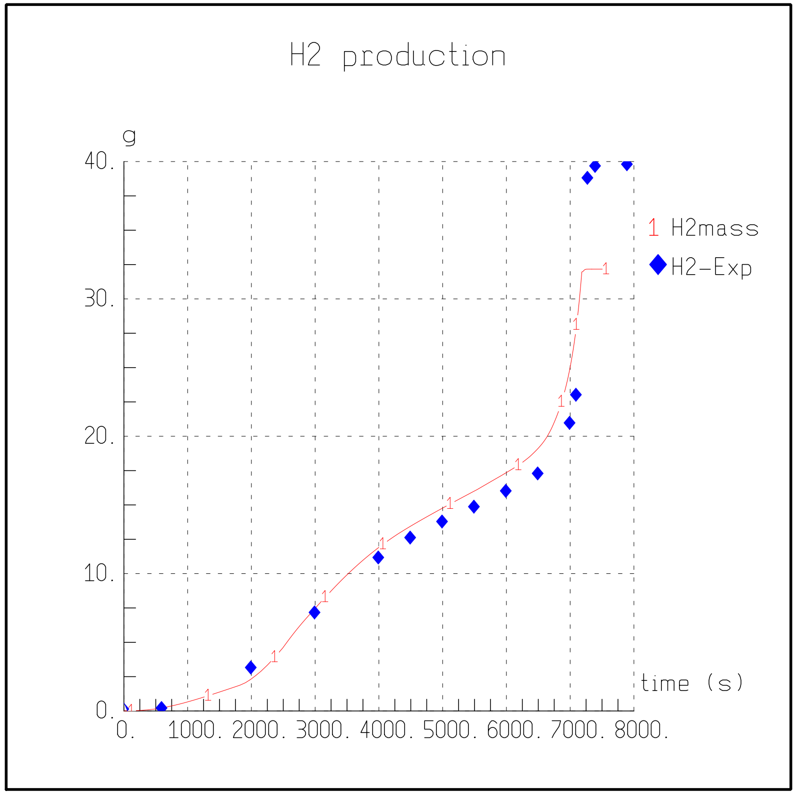
Discussion of other possible reasons for that: - up till now no modeling of important phenomena like

1) **H_2 abs. & release by the cladding material,**
2) **Melt oxidation in-between cladding & pellets;**
3) **formation of a quite thick (non-uniform?) oxide layer at the inner cladding surface in the region of melt formation.**

Comparison of ASTECv2.0R2p2 and ASTECv1.3R2



Q-14: H_2 production
exp. data vs. ASTEC**v2.0R2p2** modeling



Q-14: H_2 production
exp. data vs. modeling with the old ASTEC**v1.3** version

In the case of ASTECv1.3R2 for the Q-14 calc. ***(Fig. left)*** **the obtained H_2 masses are overestimated in the pre-ox phase and underestimated in the quench phase by the same reason as in the case of the ASTECv2.0R2p2 calc. mentioned above. The calc. integral H_2 prod. Given by ASTECv1.3 - 35 g in comparison to the 40 g coming directly from the experiment.**

Conclusions

- The adapted ASTEC input decks for QUENCH-14 led to calculation results which are similar to experimental data. This is encouraging for our future activities. The newest version of the ASTECv2.1 code (still under development) will surely give us a further chance for even more accurate modeling of the Quench-phenomena.

- Concerning our QUENCH-14 approach: after getting some technical assistance from IRSN, the following important aspects of the QUENCH-14 process were modeled :
- 1) the position of the hottest zone in the test bundle,
- 2 the generation of H_2 in the different phases of the experiment,
- 3) the thicknesses of the oxide layers both over time and height of the rod bundle .

Although some little differences in the validation of the Q-14 modeling results towards experiment exist (especially for the QUENCH phase itself) one can be optimistic looking for the next stage of modeling – i.e. the QUENCH-10 and especially QUENCH-16 modeling.

Acknowledgement

The MODELING OF THE QUENCH-14 test was performed in framework of the European SARNET program with financial support from the HGF /KIT/ NUKLEAR.

Thank you for your attention

http://www.iam.kit.edu/wpt/english/471.php/
http://quench.forschung.kit.edu/

Addendum: a quick look QUENCH test matrix

Test	Quench medium / Injection rate	Temp. at onset of flooding	Max. ZrO_2 before transient	Max. ZrO_2 before flooding	Max. ZrO_2 after test	H_2 production before / during cooldown	Remarks, objectives
QUENCH-00 Oct. 9 - 16, 97	Water 80 g/s	≈ 1800 K			completely oxidized		commissioning test
QUENCH-01 February 26, 98	Water 52 g/s	≈ 1830 K	312 µm		500 µm at 913 mm	**36 / 3**	pre-oxidized cladding
QUENCH-02 July 7, 98	Water 47 g/s	≈ 2400 K			completely oxidized	**20 / 140**	COBE: no additional pre-oxidation
QUENCH-03 January 20, 99	Water 40 g/s	≈ 2350 K			completely oxidized	**18 / 120**	no additional pre-oxidation
QUENCH-04 June 30, 99	Steam 50 g/s	≈ 2160 K	82 µm		280 µm	**10 / 2**	slightly pre-oxidized cladding
QUENCH-05 March 29, 2000	Steam 48 g/s	≈ 2020 K	160 µm		420 µm	**25 / 2**	pre-oxidized cladding
QUENCH-06 Dec. 13 2000	Water 42 g/s	≈ 2060 K	207 µm	300 µm	670 µm	**32 / 4**	OECD-ISP 45
QUENCH-07 July 25, 2001	Steam 15 g/s	≈ 2100 K	230 µm		completely oxidized	**66 / 120**	COLOSS: B_4C
QUENCH-09 July 3, 2002	Steam 49 g/s	≈ 2100 K			completely oxidized	**60 / 400**	COLOSS: B_4C, steam starvation, very high T
QUENCH-08 July 24, 2003	Steam 15 g/s	≈ 2090 K	274 µm		completely oxidized	**46 / 38**	reference to QUENCH-07 (without B_4C)
QUENCH-10 July 21, 2004	Water 50 g/s	≈ 2200 K	514 µm	613 µm (at 850 mm)	completely oxidized	**48 / 5**	LACOMERA: air ingress
QUENCH-11 Dec 08, 2005	Water 18 g/s	≈ 2040 K		170 µm	completely oxidized	**9 / 132**	LACOMERA: boil-off
QUENCH-12 Sept 27, 2006	Water 48 g/s	≈ 2100 K	160 µm, breakaway	300 µm, breakaway	completely oxidized	**34 / 24**	ISTC: VVER
QUENCH-13 Nov. 7, 2007	Water 52 g/s	≈ 1820 K		400 µm	750 µm	**42 / 1**	SARNET: Ag/In/Cd (aerosol)
QUENCH-14 July 2, 2008	Water 41 g/s	≈ 2100 K	170 µm	470 µm	840 µm	**34 / 6**	M5® cladding
QUENCH-15 May 27, 2009	Water 48 g/s	≈ 2100 K	145 µm	320 µm	630 µm	**41 / 7**	ZIRLO™ cladding