



# Neutronic Performance Issues of the Breeding Blanket Options for the European DEMO Fusion Power Plant

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## Outline



- Background
- Breeder blanket concepts for DEMO
- Neutronic characteristics of blanket concepts
- Requirements for breeding and shielding
- Methodological approach for DEMO nuclear analyses
- Tritium breeding potential
- Shielding performance issues
- Conclusions

## Background



- European Fusion Roadmap
  - *Realization of fusion as energy source for electricity by 2050 (Fusion Power Plant to providing electricity to the grid)*
- “Horizon 2020” research framework programme
  - *Conceptual design of a fusion power demonstration plant (DEMO)*
  - *Power Plant Physics and Technology (PPPT) Project organized within the EUROfusion Consortium for the Development of Fusion Energy <sup>(1)</sup>*
- DEMO power plant
  - *Relies on technically mature breeder blanket providing Tritium for self-sufficiency and producing heat for conversion into electricity*
  - *Four different design concepts are under investigation for DEMO <sup>(2)</sup>*
  - ⇒ ***Evaluation of nuclear performance for assessing potential and suitability for DEMO at an early development phase***

<sup>(1)</sup> G. Federici, Keynote 2

<sup>(2)</sup> L. V. Boccaccini, Oral 1A

## Breeder Blanket Concepts for DEMO

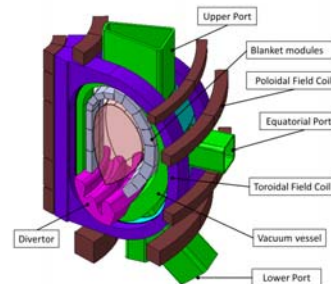


### Common Design Features

#### “DEMO 2014” configuration

- 16 Toroidal Field Coils (TFC)
  - ⇒ *Torus sectors of 22.5 ° with 3 outboard and 2 inboard segments*
- Multi Module Segmentation (MMS) scheme for blanket arrangement and maintenance
- Back Supporting Structure (BBS) acting as mechanical support and hosting main manifolds
- Vacuum vessel with integrated shielding function for protection of TFC over plant lifetime (6 full power years)
- Available radial space for blanket modules: 80 cm inboard, 130 cm outboard.
- Designed for peak values of Neutron Wall Loading (NWL): 1.15 MW/m<sup>2</sup> (inboard), 1.35 MW/m<sup>2</sup> (outboard)

Major radius (m)	9.0
Minor radius (m)	2.25
Plasma elongation	1.56
Plasma triangularity	0.33
Plasma peaking factor	1.7
Fusion power (MW)	1572
Net electric power (MW)	500
Average NWL (MW/m <sup>2</sup> )	1.07

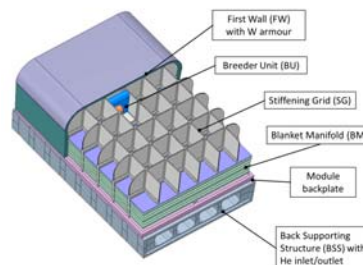


## Helium Cooled Pebble Bed (“HCPB”) Blanket



- **HCPB 2014 MMS blanket design:**  
6 blanket modules both at inboard and outboard.
- **Blanket module:** Steel box made of Eurofer with U-shaped First Wall (FW), stiffening grid (SG) with breeder units (BU), a box manifold with a back wall, two caps at the top and the bottom, and integrated BSS.
- **Li<sub>4</sub>SiO<sub>4</sub> ceramics** as breeder with <sup>6</sup>Li enriched to 60 at% and **Beryllium** as neutron multiplier.
  - ⇒ *Filled in the form of pebble beds in the space between the cooling/stiffening plates.*
- **Coolant:** High pressure (8 MPa) He gas for cooling of BU, FW, and box structure.

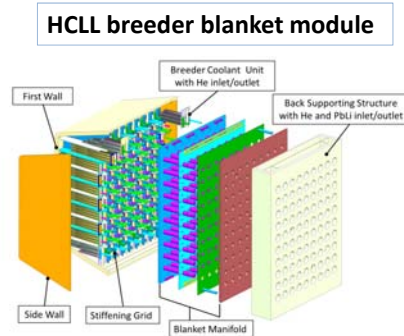
### HCPB breeder blanket module



## Helium Cooled Lithium Lead (“HCLL”) Blanket



- **HCLL MMS blanket design:**  
7 blanket modules inboard, 8 outboard.
- **Blanket module:** Eurofer steel box with stiffening grid similar to HCPB box design
  - ⇒ Open space filled with PbLi eutectic alloy for Tritium breeding
  - ⇒ Insertion of Coolant Units for cooling of PbLi
  - ⇒ Complex manifold scheme for circulation of PbLi (T extraction) and He gas (coolant)
- **Pb-15.8Li** eutectic alloy as breeder (90 at% <sup>6</sup>Li enrichment) and neutron multiplier.
- **Coolant:** High pressure (8 MPa) He gas for cooling of the breeder and the structure.



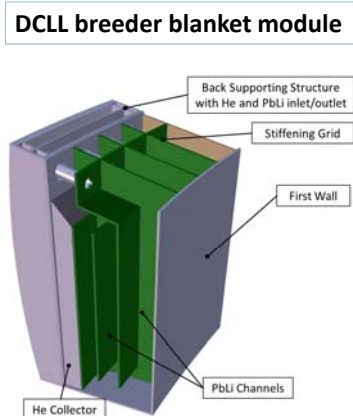
*J. Aubert et al, P2.034, Status on DEMO Helium Cooled Lithium Lead Breeding Blanket Thermo- Mechanical Analyses*

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## Dual Coolant Lithium Lead (“DCLL”) Blanket



- **DCLL MMS blanket design:**  
7 blanket modules inboard, 8 outboard
- **Blanket module:** Eurofer steel box with large sized coolant channels with thin flow channel inserts and attached BSS with integrated manifolds for He and PbLi.
- **Pb-15.8Li** eutectic alloy as breeder (90 at% <sup>6</sup>Li enrichment) and neutron multiplier.
- **Coolant:** High pressure (8 MPa) He gas for cooling of the Eurofer structure including FW, PbLi for the breeder zone.



*I. Palermo et al, P3.051, Neutronic Analyses of the Preliminary Design of a DCLL Blanket for the EUROfusion DEMO Power Plant*

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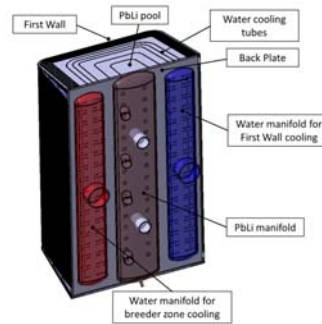
## Water Cooled Lithium Lead (“WCLL”) Blanket



- **WCLL MMS blanket design:**  
7 blanket modules inboard, 8 outboard
- **Blanket module:** Eurofer steel box with first wall, caps, back wall, stiffening grid and space for LiPb (“pool”), coolant tubes, back supporting structure with inlet/outlet pipes for water and PbLi.
- **Pb-15.8Li** eutectic alloy acting as breeder (90 at% <sup>6</sup>Li enrichment), neutron multiplier and Tritium carrier.
- **Coolant:** Pressured water (15.5 MPa) flowing in small double-walled cooling pipes.
- *Original WCLL breeder blanket design by CEA (J. Aubert et al.), now continued under responsibility of ENEA (A. Del Nevo et al.)*

### WCLL breeder blanket module

2015 design



P. A. Di Maio et al, P1.038, Optimization of the Breeder Zone Cooling Tubes of the DEMO Water-Cooled Lithium Lead Breeding Blanket

## Neutronic Characteristics of Blanket Designs



	HCPB	HCLL	DCLL	WCLL
Breeder material	Li <sub>4</sub> SiO <sub>4</sub>	Pb-15.8Li	Pb-15.8Li	Pb-15.8Li
<sup>6</sup> Li enrichment	30- 60 at%	90 at%	90 at%	90 at%
Neutron multiplier	Be	Pb (in PbLi)	Pb (in PbLi)	Pb (in PbLi)
Effect on neutronics	<b>moderating</b>	<i>non moderating</i>	<i>non moderating</i>	<i>non moderating</i>
Coolant	He	He	He, PbLi	H <sub>2</sub> O, PbLi
Effect on neutronics	<i>none</i>	<i>none</i>	<i>non moderating</i>	<i>(a bit) moderating</i>
Structural material	Eurofer	Eurofer	Eurofer	Eurofer
Effect on neutronics	<b>absorbing</b>	<i>absorbing</i>	<i>absorbing</i>	<i>absorbing</i>
Dominating material and reactions	Be, elastic scattering, (n,2n)	Pb, elastic scattering, (n,2n)	Pb, elastic scattering, (n,2n)	Pb, elastic scattering, (n,2n)
Effect on spectrum, flux and absorptions	<i>soft, enhanced parasitic and useful absorptions, low flux</i>	<i>fast, high neutron flux</i>	<i>fast, high neutron flux</i>	<i>partially moderated, lower flux</i>
Required breeder zone thickness	30 -50 cm	50 – 80 cm	50 -80 cm	50 - 80 cm

## DEMO Radial Build



- Available space must be sufficient to accommodate breeding blankets of any considered type and provide sufficient Tritium breeding.
  - ⇒ *Crucial for inboard side of DEMO where minimum space is available for the combined breeder/shield system.*
- Shielding of superconducting TFC (mainly) provided by VV with integrated shielding function:
  - ⇒ *5 cm thick steel plates at front and back, 47 cm space in between optimized for shielding (and providing thermal and structural-mechanical functions).*
- Radial space available to breeder blanket modules in DEMO:
  - 80 cm inboard, 130 cm outboard.
  - ⇒ *HCPB, HCLL, DCLL and WCLL breeder blanket modules including back supporting structure (BSS) and manifolds designed to fit to these dimensions.*
  - ⇒ *Includes space for BSS with inlet/outline piping of coolant and Tritium carrier (PbLi or He purge gas) and manifolds inside breeder modules.*
  - ⇒ *Pb-Li based blankets: manifolds carrying Pb-Li liquid metal contribute to Tritium breeding*

## Methodological approach for nuclear analyses



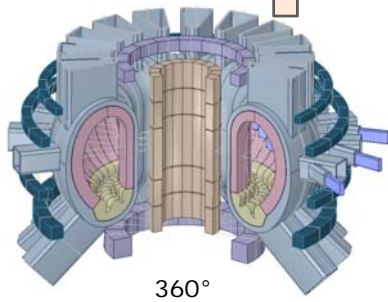
- Generic CAD neutronics model generated from DEMO Configuration Geometry Management (CGM) Model
  - ⇒ *Includes TFC, VV, divertor, blanket segment box, vessel ports, and plasma chamber, represented with “envelopes” without internal structure.*
  - ⇒ *Model converted to analysis model for MCNP/TRIPOLI-4 using the McCad conversion software*
- Resulting generic analysis model used for integration of specific HCPB, HCLL, DCLL and WCLL blankets.
  - ⇒ *CAD models provided by design teams for single blanket modules are converted and filled into empty blanket envelope of generic DEMO model.*
  - ⇒ ***HCPB, HCLL, DCLL and WCLL DEMO** models consistent with generic DEMO and specific blanket designs*
  - ⇒ ***HCPB:** KIT (P. Pereslavtsev), **HCLL:** CEA (J-C. Jaboulay), **DCLL:** Ciemat (I. Palermo), **WCLL:** ENEA (F. Moro)*
- Performance/optimisation analyses with MCNP (HCPB, DCLL, WCLL) and TRIPOLI (WCLL) and JEFF-3.1/3.2 nuclear data.

## DEMO Model Development



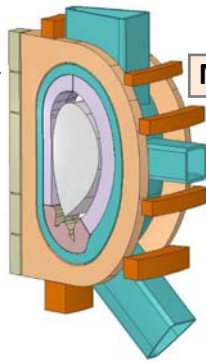
### Generic DEMO neutronics model

DEMO CGM model



360°

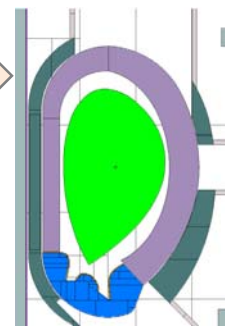
CAD



22.5°

McCad

MCNP



22.5°

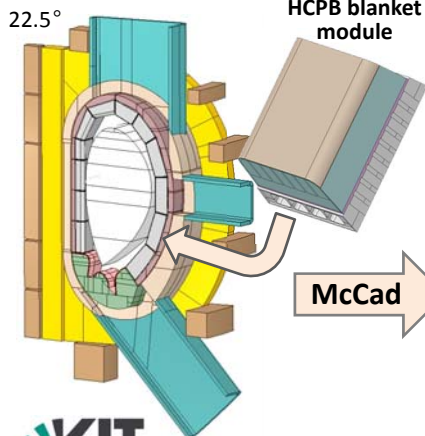


## HCPB DEMO Model Development



CAD neutronics model

- blanket module segmentation included -

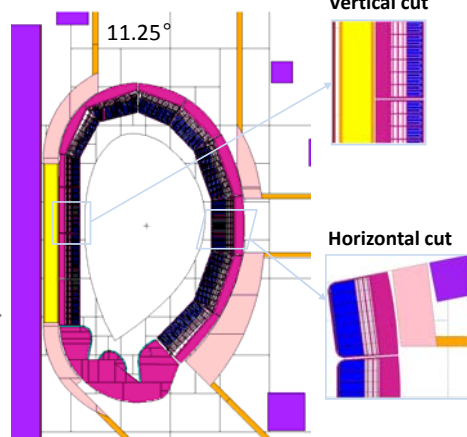


22.5°

HCPB blanket module

McCad

MCNP model



11.25°

Vertical cut

Horizontal cut

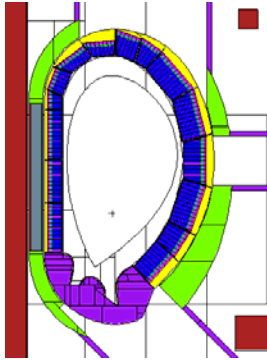
Blanket modules



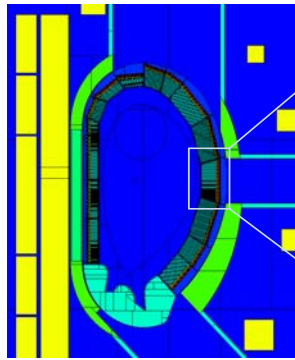
## HCLL DEMO Model



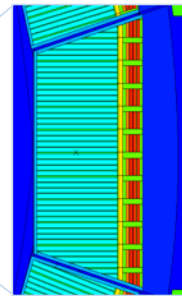
### MCNP model



### TRIPOLI model



### HCLL blanket module - vertical cut -

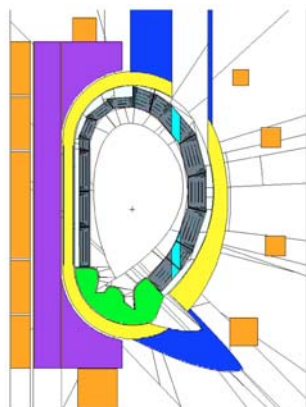


*J.-C. Jaboulay et al., P1.042, Nuclear Analysis of the HCLL Blanket Concept for the European DEMO using the TRIPOLI-4® Monte Carlo Code*

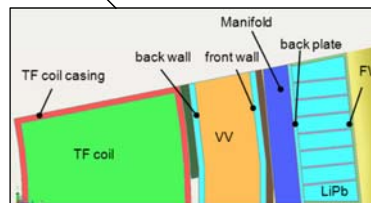
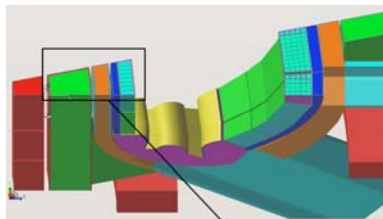
## WCLL DEMO Model



### MCNP model



### Cut-away view at torus mid-plane



### Horizontal cut at inboard mid-plane

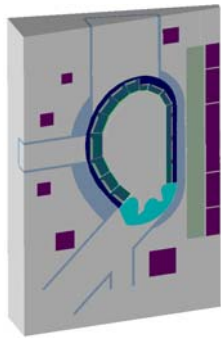




## DCLL DEMO Model

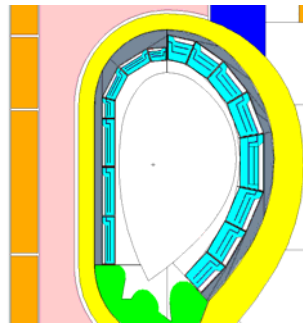


### MCAM model

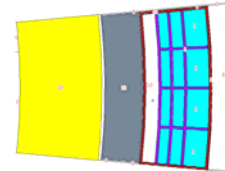


### MCNP model

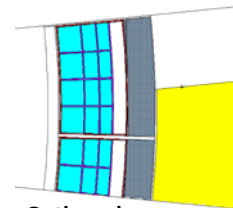
#### Vertical cut



#### Horizontal cuts at torus mid-plane



#### Inboard



#### Outboard



I. Palermo et al, P3.051, Neutronic Analyses of the Preliminary Design of a DCLL Blanket for the EUROfusion DEMO Power Plant

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## Tritium breeding potential



- DEMO requires **Tritium self-sufficiency**:  
 $\Rightarrow$  Net Tritium Breeding Ratio (TBR) > 1.0
- **DEMO design target**: TBR  $\geq$  1.10  
*(To be proven by 3D Monte Carlo calculation without blanket ports).*
- All blanket concepts show sufficient Tritium breeding capability as shown in previous studies/analyses.
- Design limitations adopted for the DEMO 2014 affect the TBR performance.
- Design improvements underway to achieve TBR design target for DEMO.

#### TBR performance for DEMO

	HCPB	HCLL	DCLL	WCLL
DEMO 2014 initial design	1.04	1.07	1.04	1.13
DEMO 2015 current design	1.12 – 1.15	1.09 – 1.11	1.13	1.13

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## Shielding performance issues



- Blanket/shield system must ensure sufficient protection of the super-conducting magnets  
 $\Rightarrow$  Limits for the radiation loads on the Toroidal Field Coils (TFC)

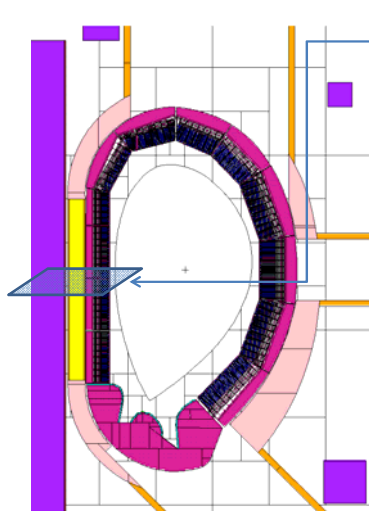
Total neutron fluence to epoxy insulator	$1 \cdot 10^{22} \text{ m}^{-2} \cong 10^7 \text{ Gray}$
Peak fast neutron fluence to the $\text{Nb}_3\text{Sn}$ super-conductor (*)	$1 \cdot 10^{22} \text{ m}^{-2}$
Peak displacement damage to Cu stabilizer between TFC warm-ups	$1 \cdot 10^{21} \text{ m}^{-2} \cong 0.5 \cdot 10^{-4} \text{ dpa}$
<b>Peak nuclear heating in winding pack</b>	<b><math>&lt; 0.05 \cdot 10^3 \text{ W/m}^3</math></b>

(\*) Results for DEMO conditions in a fast neutron flux limit of  $\cong 10^9 \text{ cm}^{-2}\text{s}^{-1}$

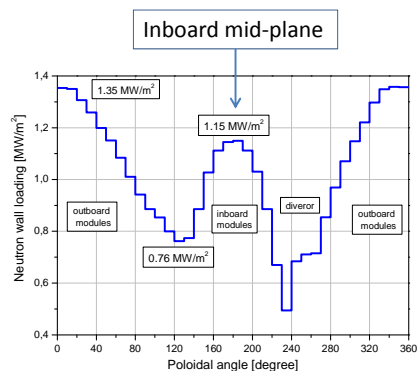
- Displacement damage accumulation of the vessel to be limited to prevent degradation of the stainless steel properties  
 $\Rightarrow 2.75 \text{ dpa limit for vacuum vessel made of austenitic steel}$
- Irradiation induced gas production accumulation to be limited to enable re-welding of components and connections/pipes made of steel ( 1 appm)  
 $\Rightarrow$  DEMO design goal: Re-welding only in areas where sufficient shielding can be provided

$\Rightarrow$  To be proven for DEMO inboard mid-plane where minimum space is available for shielding !

## Shielding calculations



Shielding calculations in torus mid-plane (inboard)

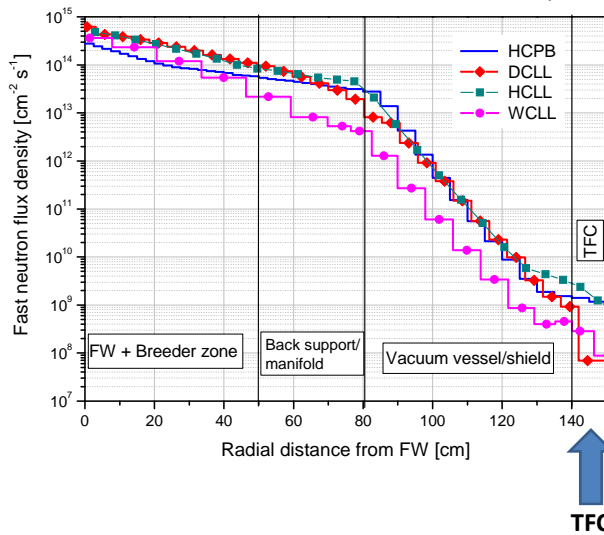


Poloidal distribution of Neutron Wall Loading (NWL) in DEMO

## Radial profile of fast neutron flux density



DEMO inboard torus mid-plane



Fast (>0.1 MeV) neutron flux densities [ $\text{cm}^{-2} \text{s}^{-1}$ ]

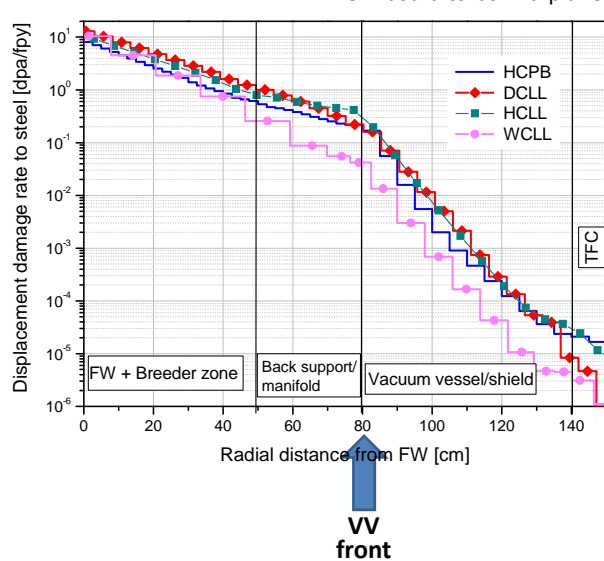
	FW	TFC front
HCPB	$2.8 \cdot 10^{14}$	$\approx 1.7 \cdot 10^9$
HCLL	$6.8 \cdot 10^{14}$	$\approx 2.4 \cdot 10^9$
DCLL	$6.2 \cdot 10^{14}$	$\approx 1.0 \cdot 10^8$
WCLL	$3.6 \cdot 10^{14}$	$\approx 5.3 \cdot 10^8$

Assumed DEMO limit at TFC front:  $\approx 10^9 \text{ cm}^{-2} \text{s}^{-1}$

## Radial profile of displacement damage in steel



DEMO inboard torus mid-plane



Displacement damage rate in steel [ $\text{dpa/fpy}^{(*)}$ ]

	FW	VV front
HCPB	8.1	0.22
HCLL	9.4	0.20
DCLL	10.4	0.15
WCLL	10.4	0.04

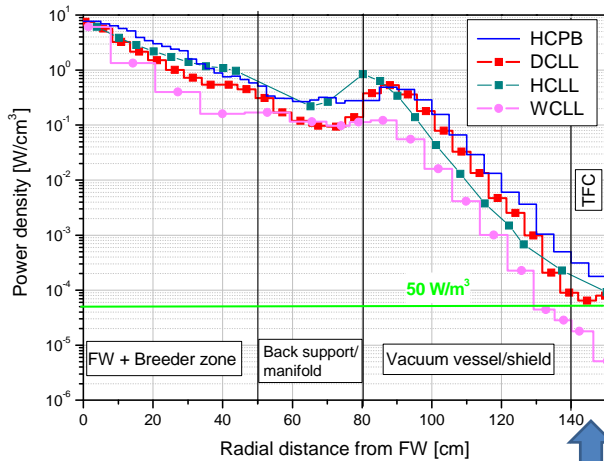
(\*)fpy = full power year

DEMO limit for VV : 2.75 dpa

## Radial profile of power density in steel



DEMO inboard torus mid-plane



Nuclear power density  
[W/cm<sup>3</sup>]

	FW	TFC front
HCPB	8.4	$\approx 3 \cdot 10^{-4}$
HCLL	6.4	$\approx 2 \cdot 10^{-4}$
DCLL	5.7	$\approx 9 \cdot 10^{-5}$
WCLL	6.1	$\approx 2 \cdot 10^{-5}$

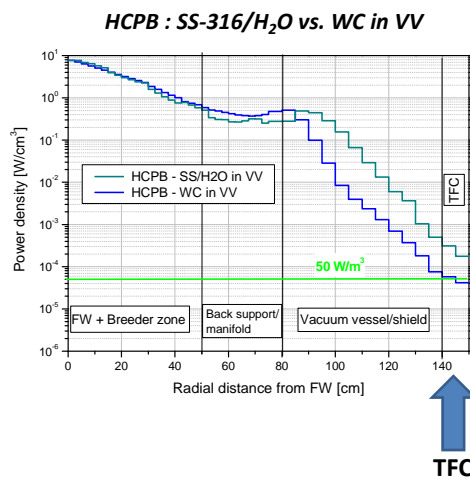
Recommended DEMO limit  
for TFC :  $5 \cdot 10^{-5} \text{ Wcm}^{-3}$

⇒ VV/shield composition: 80 % SS-316/20 % H<sub>2</sub>O

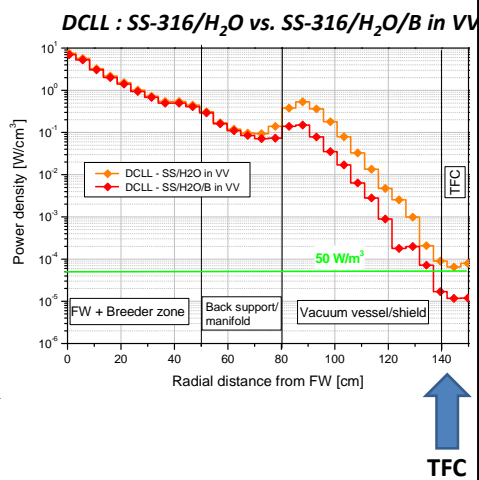
## Efficient shielding materials in VV



- Effect on nuclear heating profiles (inboard torus mid-plane) -



TFC



TFC

## Conclusions



### Nuclear performance of HCPB, HCLL, DCLL and WCLL for DEMO

- Tritium breeding potential
  - ✓ *Considered sufficient although initial 2014 design versions of HCPB, HCLL and DCLL require design improvements .*
  - ⇒ *Suitable measures shown to be sufficient to achieve  $TBR \geq 1.10$*
- Shielding performance
  - ✓ *Sufficient to protect the TFC from provided that efficient shielding materials including WC or borated water are utilized in the VV (HCPB, HCLL, DCLL).*
  - ✓ *WCLL does not require such materials provided the considered BSS/manifold configuration can be verified.*
  - ✓ *VV can be safely operated over anticipated DEMO lifetime of 6 fpy*