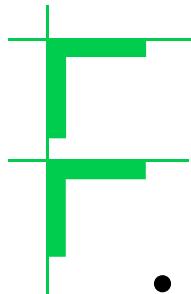


Invariance of the velocity field induced by a bubble rising steadily through liquid under variation of the gas-liquid density ratio

Martin Wörner

Forschungszentrum Karlsruhe, Institut für Reaktorsicherheit

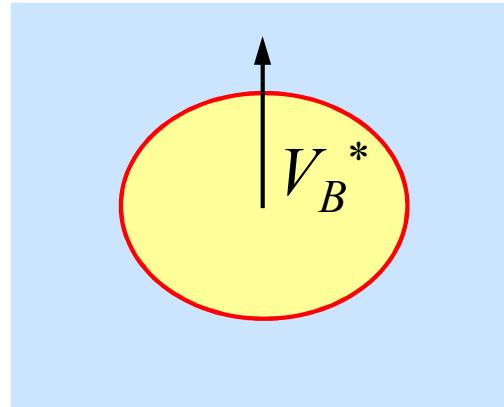
*German-Japanese Workshop on Multi-Phase Flow
Karlsruhe, Germany, August 26-27, 2002*



Motivation

- Buoyancy driven motion of single bubble in “infinite” liquid
 - Gas-liquid density ratio (Γ_ρ) is one of 5 dimensionless groups
- Direct Numerical Simulation (DNS) of two-phase flow
 - Numerical difficulties associated with low values of Γ_ρ
 - Usually a density ratio $\Gamma_\rho \approx 1/50$ is used instead of $1/1000$
- Objective
 - How is influence of gas-liquid density ratio on
 - bubble rise velocity
 - bubble shape
 - local motion in liquid and gas phase
 - Can results for $\Gamma_\rho = O(0.1)$ be transferred to $\Gamma_\rho = O(0.001)$?
 - Here: Investigation by 3D Volume-of-fluid computations

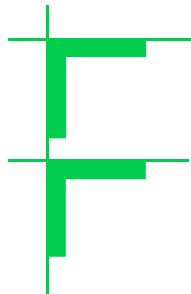
Dimensional equations in steady frame of reference



$$\nabla^* \cdot \mathbf{u}_c^* = 0, \quad \frac{\partial^* \rho_c^* \mathbf{u}_c^*}{\partial^* t^*} + \nabla^* \cdot \rho_c^* \mathbf{u}_c^* \mathbf{u}_c^* = -\nabla^* p_c^* + \mu_c^* \nabla^{*2} \mathbf{u}_c^* + \rho_c^* \mathbf{g}^*, \quad \mathbf{x}^* \in \Omega_c^*(t^*)$$

$$\nabla^* \cdot \mathbf{u}_d^* = 0, \quad \frac{\partial^* \rho_d^* \mathbf{u}_d^*}{\partial^* t^*} + \nabla^* \cdot \rho_d^* \mathbf{u}_d^* \mathbf{u}_d^* = -\nabla^* p_d^* + \mu_d^* \nabla^{*2} \mathbf{u}_d^* + \rho_d^* \mathbf{g}^*, \quad \mathbf{x}^* \in \Omega_d^*(t^*)$$

$$\left. \begin{aligned} \mathbf{u}_c^* &= \mathbf{u}_d^* = \mathbf{u}_i^* \\ (p_c^* - p_d^* + \kappa^* \boldsymbol{\sigma}^*) \mathbf{n}_i &= \left[\mu_c^* (\nabla^* \mathbf{u}_c^* + \nabla^* \mathbf{u}_c^{*\top}) - \mu_d^* (\nabla^* \mathbf{u}_d^* + \nabla^* \mathbf{u}_d^{*\top}) \right] \cdot \mathbf{n}_i \end{aligned} \right\} \mathbf{x}_i^* \in S_i^*(t^*)$$



Normalization of variables

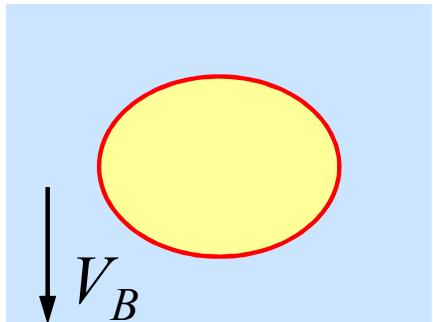
- **Reference scales**
 - length: sphere-equivalent diameter d_B^*
 - velocity: bubble rise velocity V_B^*
 - density: liquid phase density ρ_c^*
 - viscosity: liquid phase viscosity μ_c^*
- **Non-dimensional quantities**
 - $\mathbf{x} = \mathbf{x}^* / d_B^*$, $\mathbf{u}_c = \mathbf{u}_c^* / V_B^*$, $\mathbf{u}_d = \mathbf{u}_d^* / V_B^*$, etc.
 - $\rho_c = 1$, $\rho_d = \rho_d^* / \rho_c^* \equiv \Gamma_\rho$, $\mu_c = 1$, $\mu_d = \mu_d^* / \mu_c^* \equiv \Gamma_\mu$
 - $p_c \equiv \frac{p_c^* - \rho_c^* \mathbf{g}^* \cdot \mathbf{x}^*}{\rho_c^* V_B^{*2}}$, $p_d \equiv \frac{p_d^* - \rho_c^* \mathbf{g}^* \cdot \mathbf{x}^*}{\rho_c^* V_B^{*2}}$

Non-dimensional equations in moving frame of reference

$$\nabla' \cdot \mathbf{w}_c = 0, \quad \frac{\partial \mathbf{w}_c}{\partial t} + \nabla' \cdot \mathbf{w}_c \mathbf{w}_c = -\nabla' p_c + \frac{1}{Re_B} \nabla'^2 \mathbf{w}_c - \frac{d\mathbf{V}_B}{dt}, \quad \mathbf{z} \in \Omega'_c(t)$$

$$\nabla' \cdot \mathbf{w}_d = 0, \quad \Gamma_\rho \left(\frac{\partial \mathbf{w}_d}{\partial t} + \nabla' \cdot \mathbf{w}_d \mathbf{w}_d \right) = -\nabla' p_d + \frac{\Gamma_\mu}{Re_B} \nabla'^2 \mathbf{w}_d - \sqrt{\frac{E\ddot{o}_B^3}{MoRe_B^4}} \mathbf{n}_g - \Gamma_\rho \frac{d\mathbf{V}_B}{dt}, \quad \mathbf{z} \in \Omega'_d(t)$$

$$\left. \begin{aligned} & \mathbf{w}_c = \mathbf{w}_d = \mathbf{w}_i \\ & \left(p_c - p_d + \kappa \sqrt{\frac{E\ddot{o}_B}{MoRe_B^4}} \right) \mathbf{n}_i = \frac{1}{Re_B} \left[(\nabla' \mathbf{w}_c + \nabla' \mathbf{w}_c^\top) - \Gamma_\mu (\nabla' \mathbf{w}_d + \nabla' \mathbf{w}_d^\top) \right] \cdot \mathbf{n}_i \end{aligned} \right\} \mathbf{z}_i \in S_i'(t)$$



$$Re_B \equiv \frac{\rho_c^* d_B^* V_B^*}{\mu_c^*}, \quad E\ddot{o}_B \equiv \frac{g^* (\rho_c^* - \rho_d^*) d_B^{*2}}{\sigma^*}, \quad Mo \equiv \frac{(\rho_c^* - \rho_d^*) g^* \mu_c^{*4}}{\rho_c^{*2} \sigma^{*3}}$$

Steady non-dimensional equations in moving frame of reference

$$\begin{aligned}
 \nabla' \cdot \mathbf{w}_c &= 0, & \nabla' \cdot \mathbf{w}_c \mathbf{w}_c &= -\nabla' p_c + \frac{1}{Re_B} \nabla'^2 \mathbf{w}_c, & \mathbf{z} &\in \Omega'_c \\
 \nabla' \cdot \mathbf{w}_d &= 0, & \Gamma_\rho \nabla' \cdot \mathbf{w}_d \mathbf{w}_d &= -\nabla' p_d + \frac{\Gamma_\mu}{Re_B} \nabla'^2 \mathbf{w}_d - \sqrt{\frac{E\ddot{o}_B^3}{MoRe_B^4}} \mathbf{n}_g, & \mathbf{z} &\in \Omega'_d \\
 \mathbf{w}_c &= \mathbf{w}_d = \mathbf{w}_i \\
 \left(p_c - p_d + \kappa \sqrt{\frac{E\ddot{o}_B}{MoRe_B^4}} \right) \mathbf{n}_i &= \frac{1}{Re_B} \left[(\nabla' \mathbf{w}_c + \nabla' \mathbf{w}_c^\top) - \Gamma_\mu (\nabla' \mathbf{w}_d + \nabla' \mathbf{w}_d^\top) \right] \cdot \mathbf{n}_i & \mathbf{z}_i &\in S'_i
 \end{aligned}$$

Gas-liquid density ratio is without influence for

- limit $\Gamma_\rho \rightarrow 0$
- no internal circulation ($\mathbf{w}_d = 0$)

Momentum theorem

- Integration of disperse phase momentum Eq. over Ω'_d and application of Gauss-Ostrogradskii divergence theorem

$$\iint_{S'_i} \mathbf{n}_i \cdot \left\{ -\Gamma_\rho \mathbf{w}_d \mathbf{w}_d - \mathbf{I} p_d + \frac{\Gamma_\mu}{Re_B} [\nabla' \mathbf{w}_d + \nabla' \mathbf{w}_d^T] \right\} dS = \mathcal{V}_B \sqrt{\frac{E\ddot{o}_B^3}{MoRe_B^4}} \mathbf{n}_g$$

- At interface: $\Gamma_\rho \mathbf{n}'_i \cdot \mathbf{w}_d \mathbf{w}_d = \Gamma_\rho \mathbf{n}'_i \cdot \mathbf{w}_i \mathbf{w}_i = (\mathbf{n}'_i \cdot \mathbf{w}_i) \mathbf{w}_i = W_{i\perp} \mathbf{w}_i = 0$

⇒

$$\iint_{S'_i} \mathbf{n}_i \cdot \left\{ -\mathbf{I} p_d + \frac{\Gamma_\mu}{Re_B} [\nabla' \mathbf{w}_d + \nabla' \mathbf{w}_d^T] \right\} dS = \mathcal{V}_B \sqrt{\frac{E\ddot{o}_B^3}{MoRe_B^4}} \mathbf{n}_g$$

- If the bubble shape is independent of Γ_ρ then it is likely that this is also true for the bubble-driven liquid motion

TURBIT-VOF: Governing equations

$$\mathbf{x} = \frac{\mathbf{x}^*}{L_{ref}^*}, \quad \mathbf{u}_k = \frac{\mathbf{u}_k^*}{U_{ref}^*}, \quad t = \frac{t^* U_{ref}^*}{L_{ref}^*}, \quad \rho_k = \frac{\rho_k^*}{\rho_c^*}, \quad \mu_k = \frac{\mu_k^*}{\mu_c^*}, \quad P_k = \frac{p_k^* + p_0^* - \rho_c^* \mathbf{g}^* \cdot \mathbf{x}^*}{\rho_c^* U_{ref}^{*2}} \quad (k \in c, d)$$

$$\frac{\partial}{\partial t} \rho_m \mathbf{u}_m + \nabla \cdot \rho_m \mathbf{u}_m \mathbf{u}_m = -\nabla P + \frac{1}{Re_{ref}} \nabla \cdot \left[\mu_m \left(\nabla \mathbf{u}_m + \nabla \mathbf{u}_m^\top \right) \right] - (1-f) \frac{E\ddot{o}_{ref}}{We_{ref}} \frac{\mathbf{g}^*}{g^*} + \frac{a_{int} \kappa \mathbf{n}_i}{We_{ref}}$$

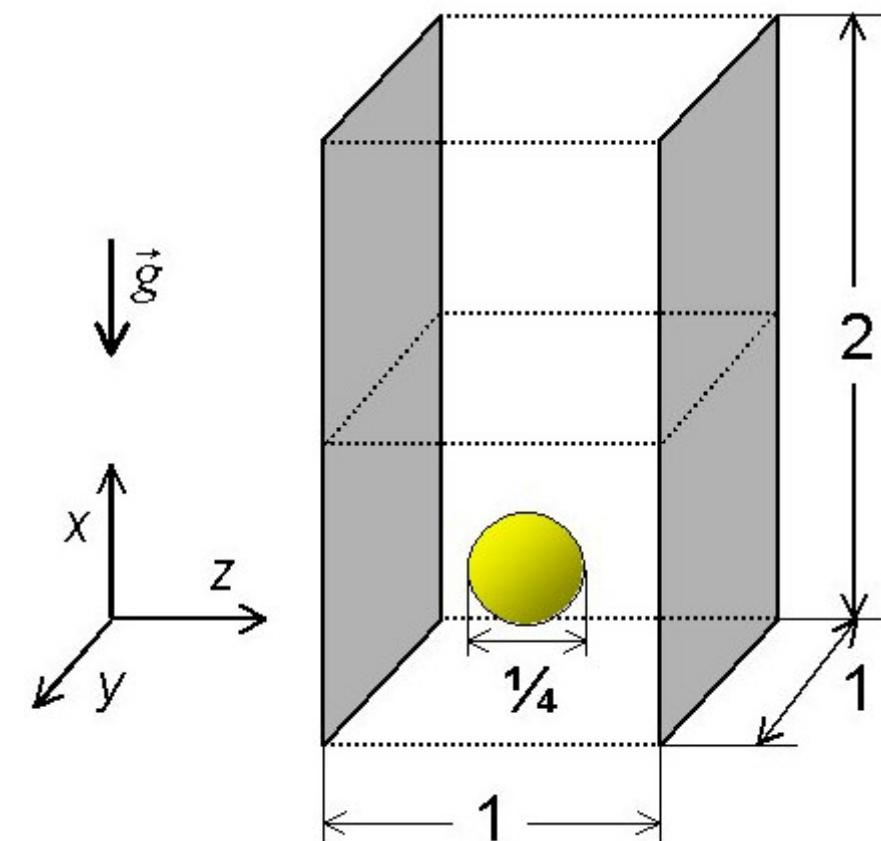
$$\boxed{\nabla \cdot \mathbf{u}_m = 0} \quad \boxed{\frac{\partial f}{\partial t} + \nabla \cdot f \mathbf{u}_m = 0} \quad (f \equiv \alpha_c, \quad 0 \leq f \leq 1) \quad \mathbf{u}_m \equiv \frac{1}{U_{ref}^*} \frac{f \rho_c^* \mathbf{u}_c^* + (1-f) \rho_d^* \mathbf{u}_d^*}{f \rho_c^* + (1-f) \rho_d^*}$$

$$\rho_m \equiv \frac{f \rho_c^* + (1-f) \rho_d^*}{\rho_c^*} = f + (1-f) \Gamma_\rho, \quad \mu_m \equiv \frac{f \mu_c^* + (1-f) \mu_d^*}{\mu_c^*} = f + (1-f) \Gamma_\mu$$

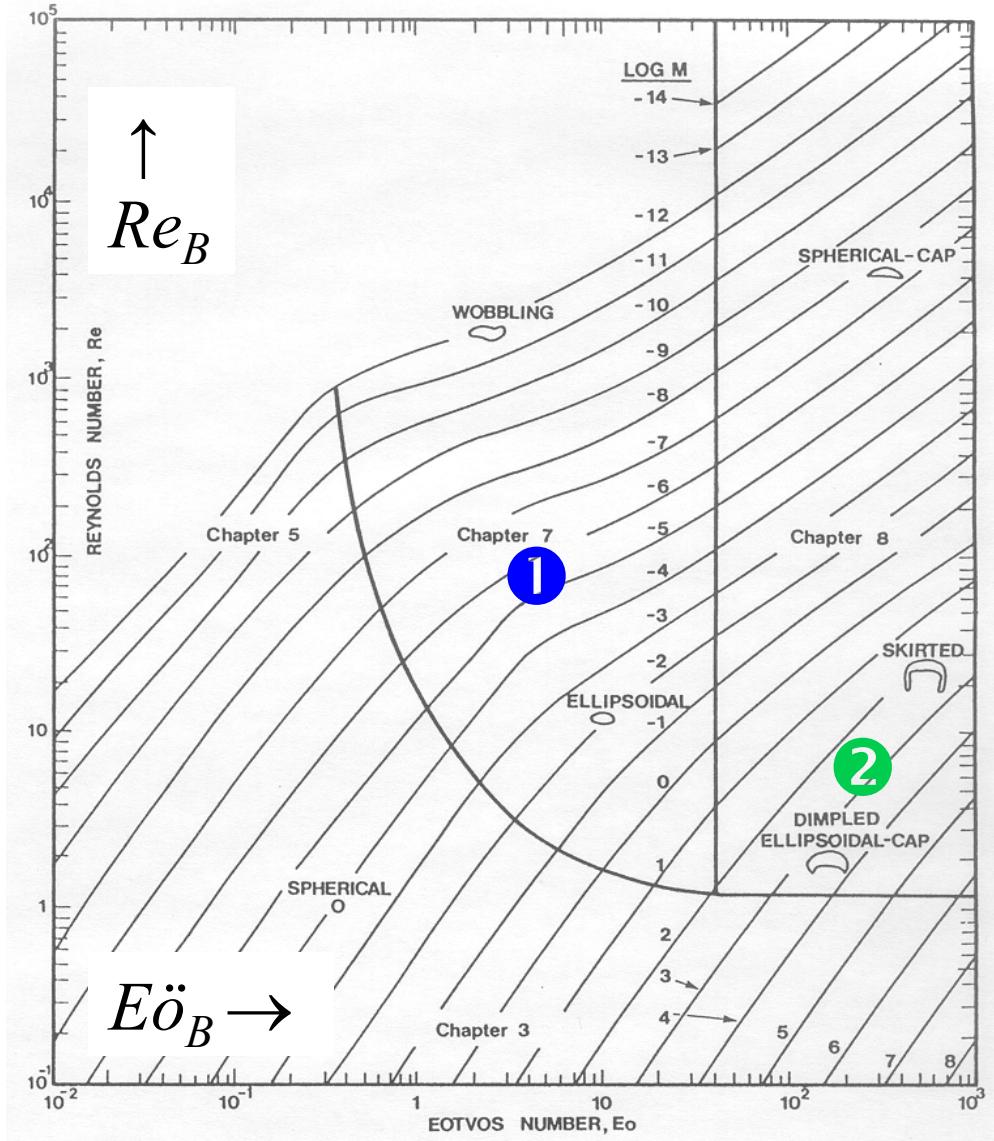
$$Re_{ref} \equiv \frac{\rho_c^* L_{ref}^* U_{ref}^*}{\mu_c^*}, \quad E\ddot{o}_{ref} \equiv \frac{(\rho_c^* - \rho_d^*) g^* L_{ref}^{*2}}{\sigma^*}, \quad We_{ref} \equiv \frac{\rho_c^* L_{ref}^* U_{ref}^{*2}}{\sigma^*} = \sqrt{\frac{MoRe_{ref}^4}{E\ddot{o}_{ref}}}$$

Computational set-up

- Domain: $2 \times 1 \times 1$
- Grid: $128 \times 64 \times 64$
- Bubble diameter: 0.25
(= 16 mesh cells)
- Gas holdup: $\approx 0.4\%$
- Boundary conditions
 - walls at $z = 0$ and $z = 1$
 - periodic in x and y
- Liquid & gas initially at rest



Bubble parameters



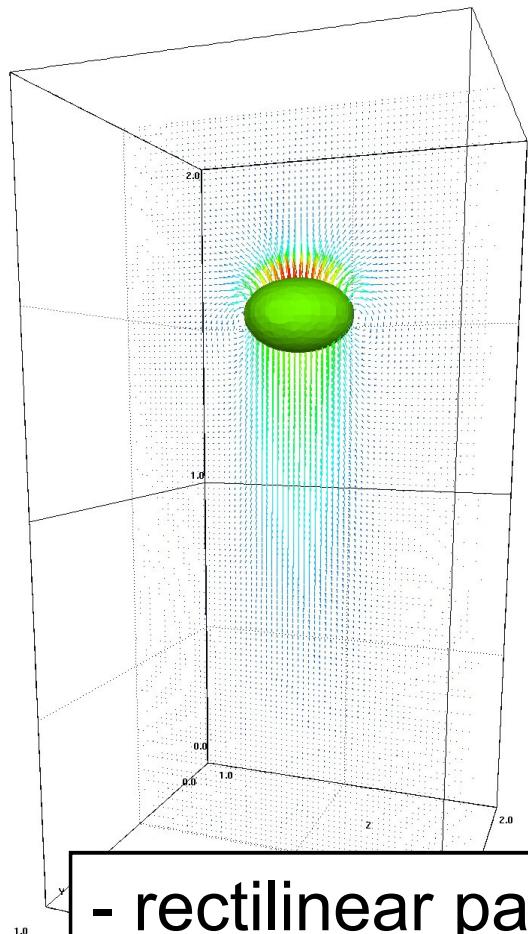
1 „medium“ Morton number ellipsoidal bubble

DNS for $\Gamma_\mu = 1$,
 $Mo = 3.09 \cdot 10^{-6}$, $Eo_B = 3.06$
 $\Gamma_\rho = 0.5, 0.2, 0.1, 0.02$

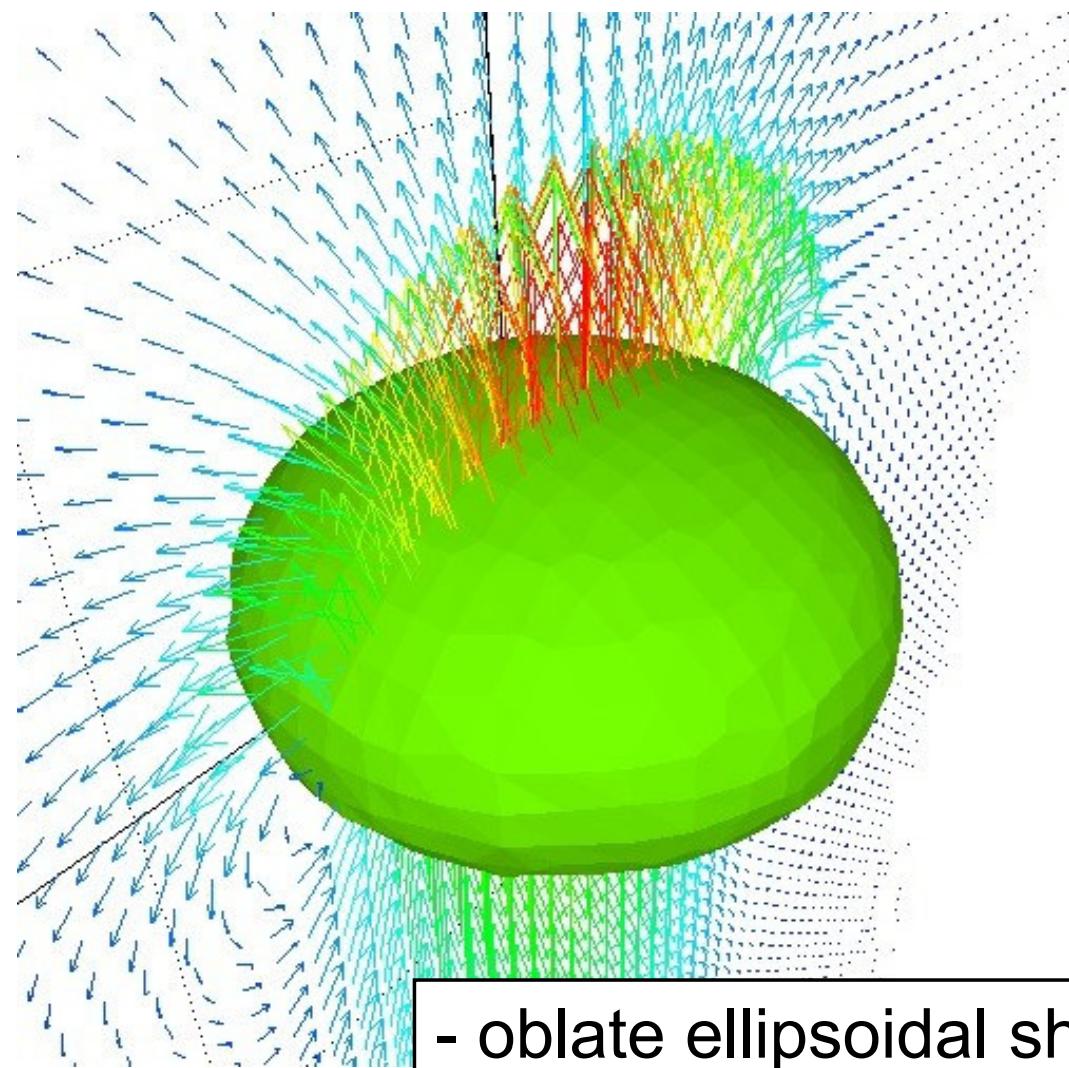
2 „high“ Morton number ellipsoidal cap bubble

DNS for $\Gamma_\mu = 1$,
 $Mo = 266$, $Eo_B = 243$
 $\Gamma_\rho = 0.5, 0.2, 0.1$

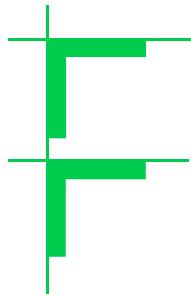
Flow visualizations case 1



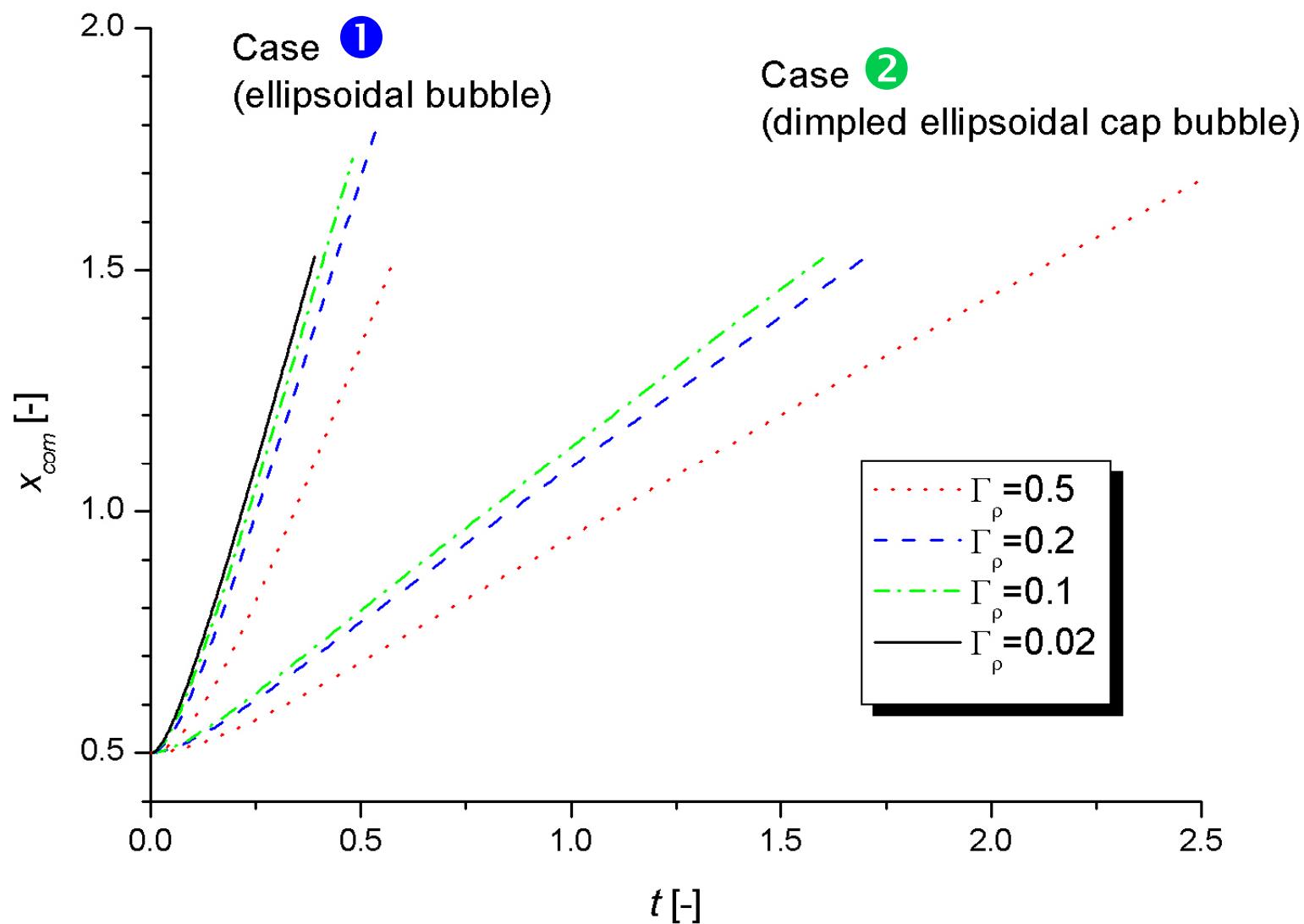
- rectilinear path
- closed wake



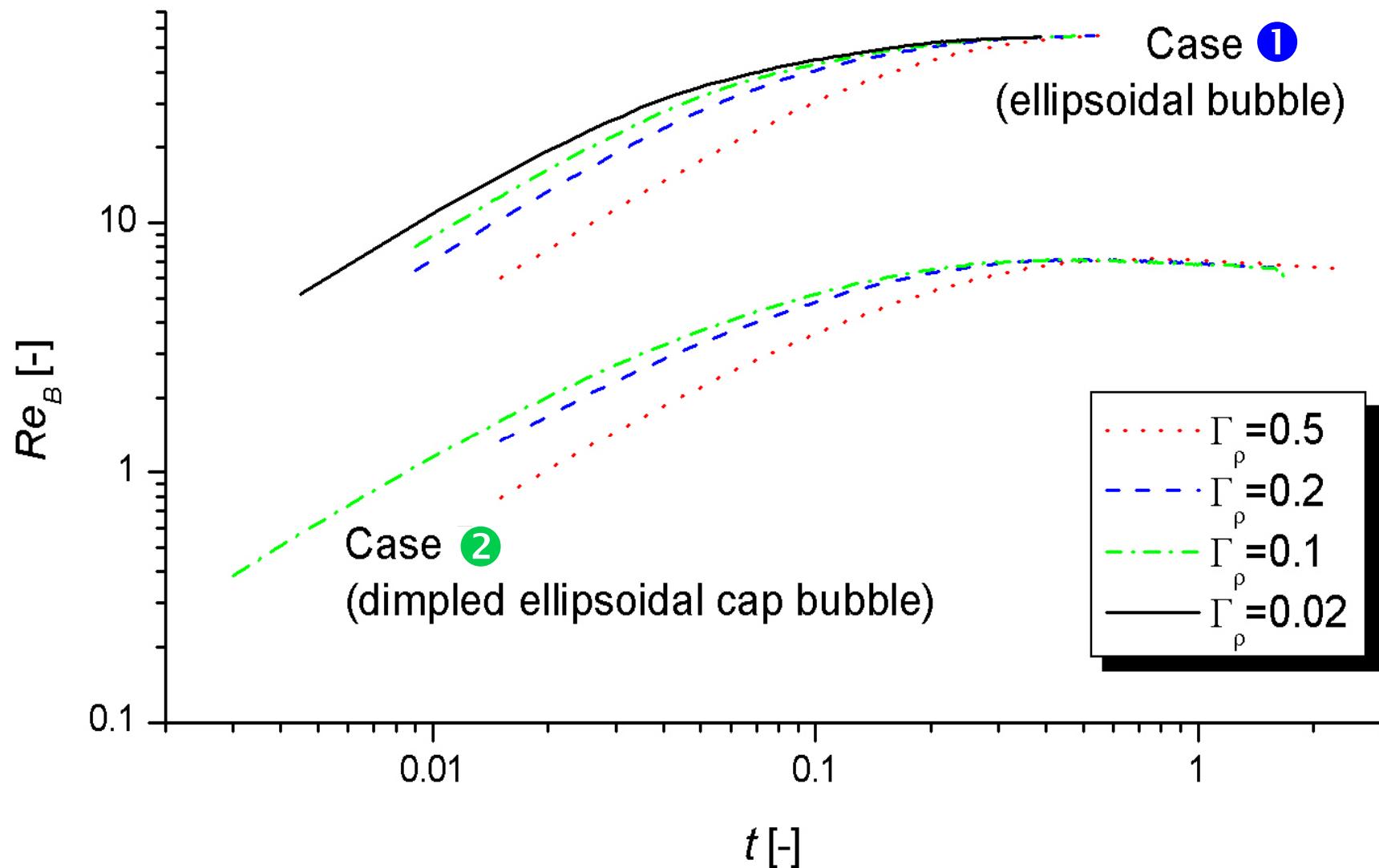
- oblate ellipsoidal shape



Time history of vertical bubble position



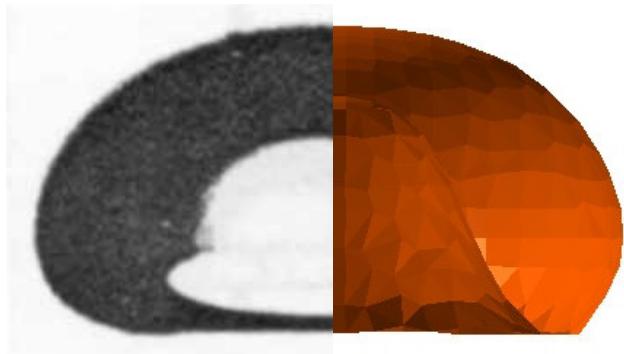
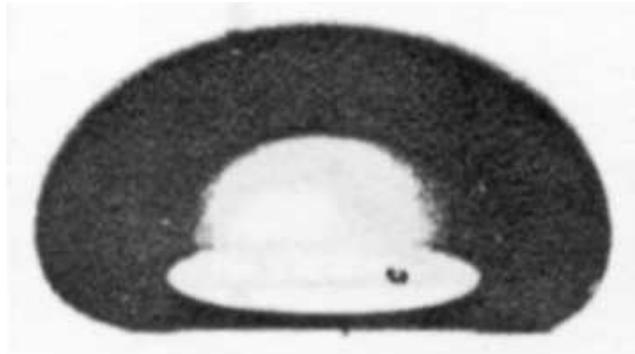
Time history of bubble Reynolds number



Comparison of bubble shape (case ②)

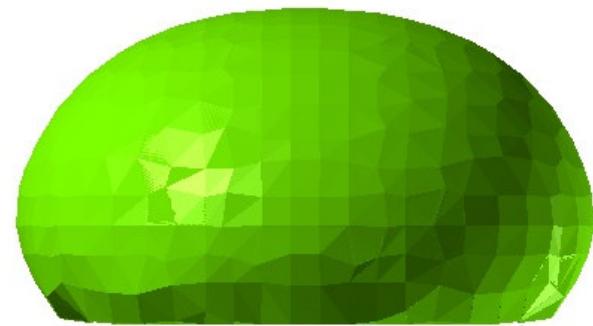
Experiment Bhaga & Weber*

$$(\Gamma_\rho \approx 0.0008, \Gamma_\mu \approx 10^{-5})$$

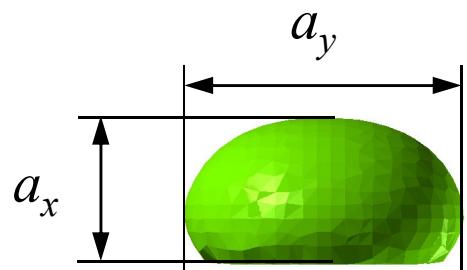


TURBIT-VOF

$$(\Gamma_\rho = 0.5, \Gamma_\mu = 1)$$



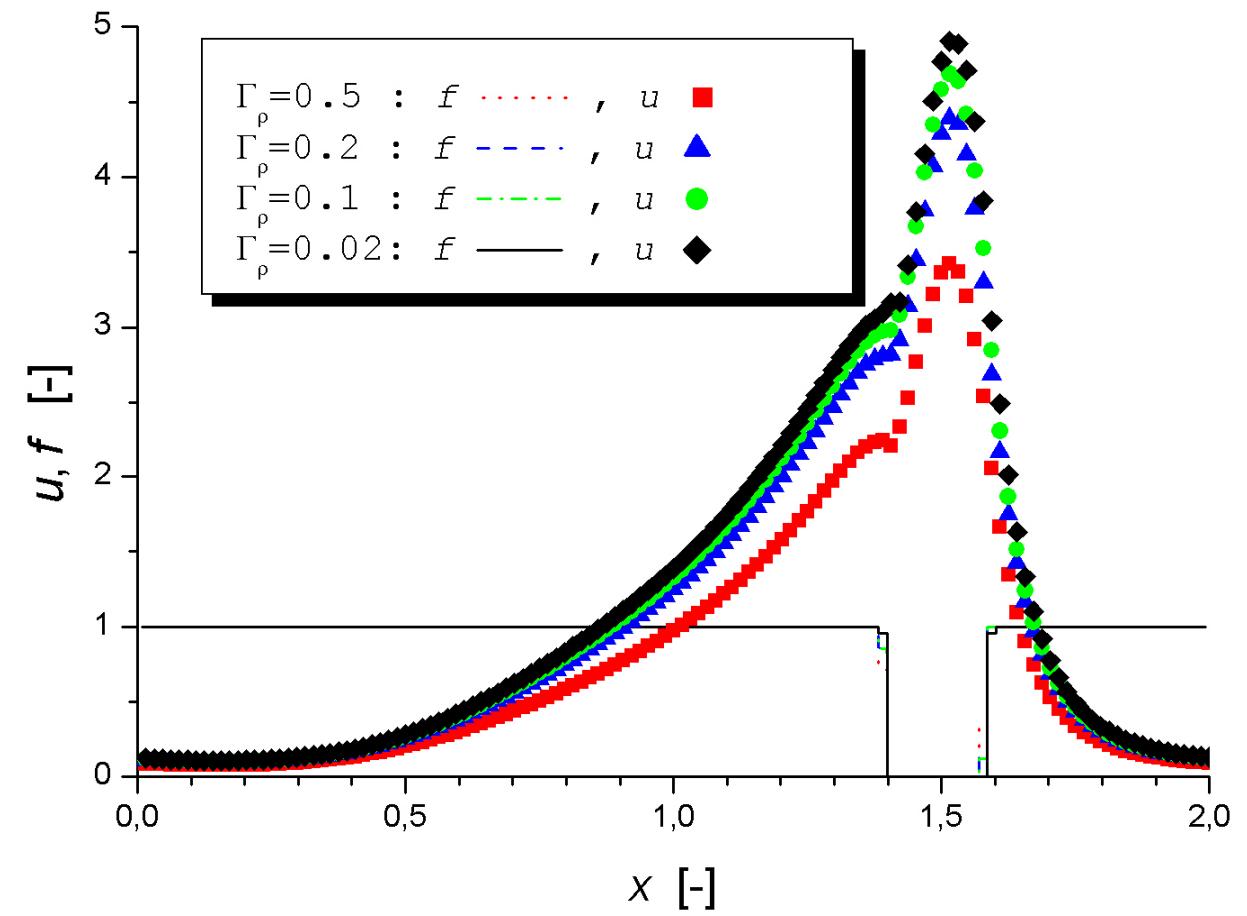
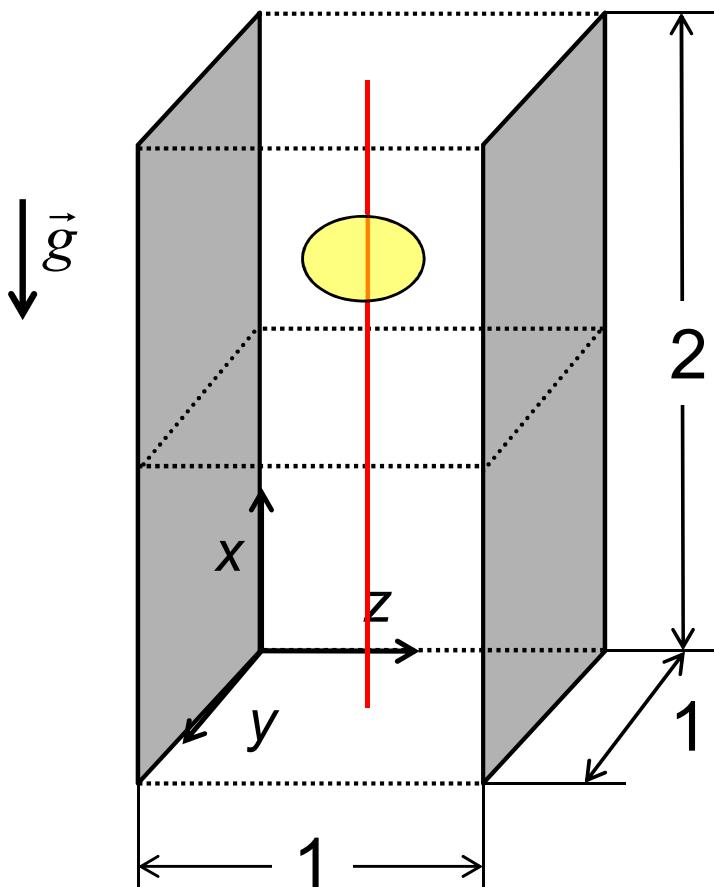
Influence of density ratio on bubble shape



Γ_ρ	Case ①			Case ②		
	a_x / a_y	a_x / a_z	a_y / a_z	a_x / a_y	a_x / a_z	a_y / a_z
0.5	0.648	0.659	1.017	0.538	0.556	1.033
0.2	0.652	0.665	1.021	0.528	0.544	1.030
0.1	0.658	0.669	1.016	0.528	0.543	1.029
0.02	0.658	0.666	0.998	-	-	-

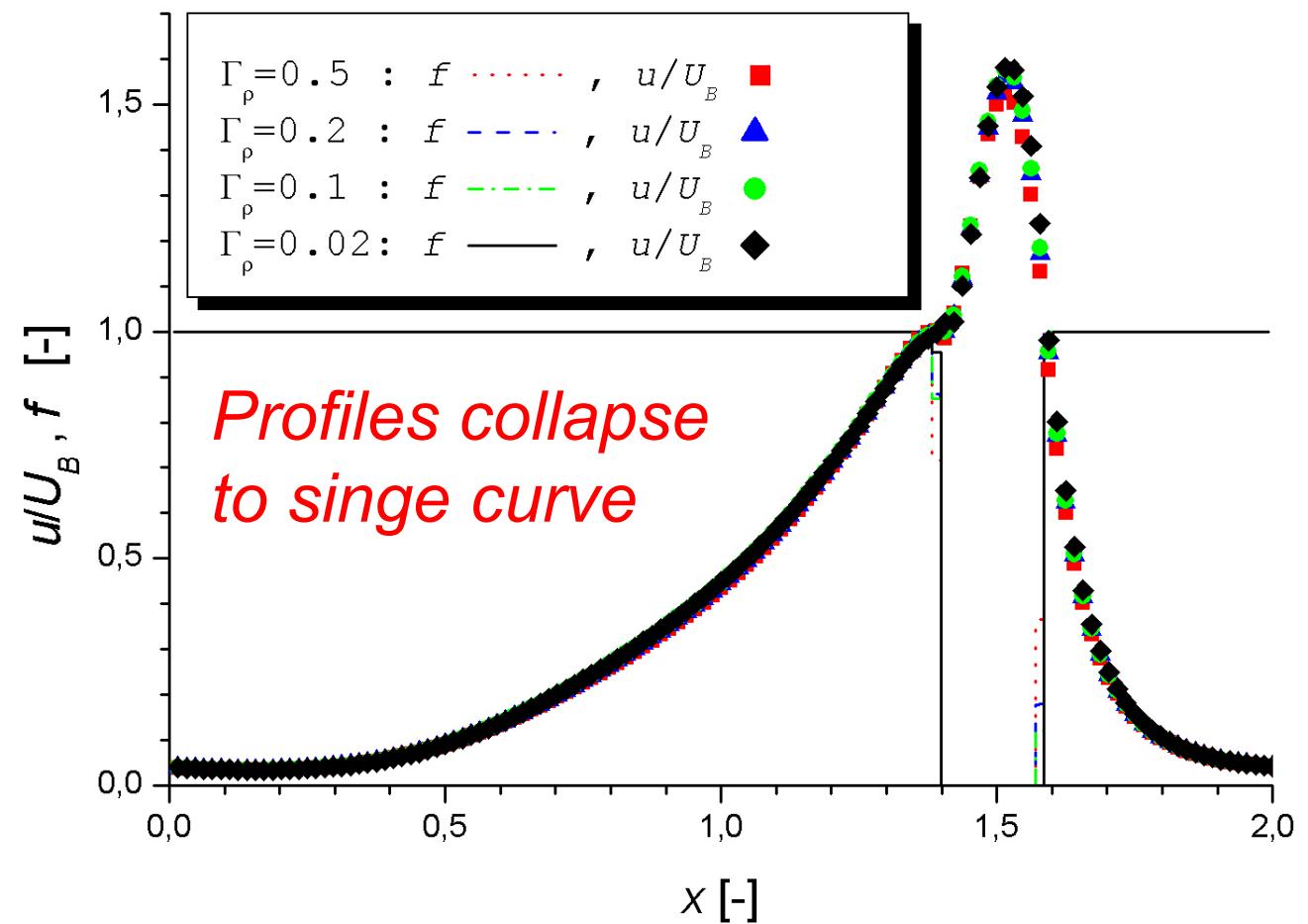
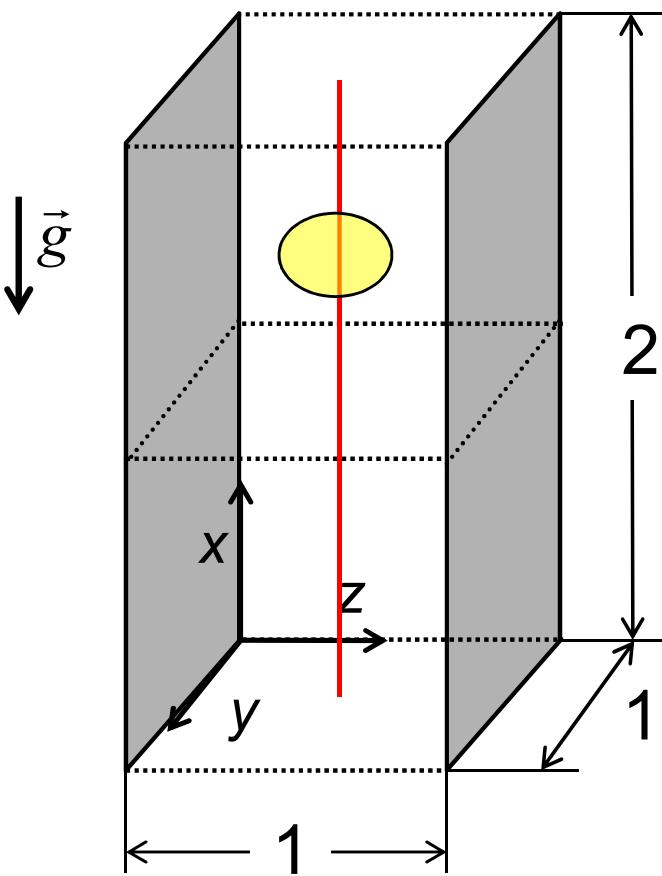
Local vertical velocity (case ①)

Comparison of profiles for instant t_C with $x_{com}(t_C) = 1.5$

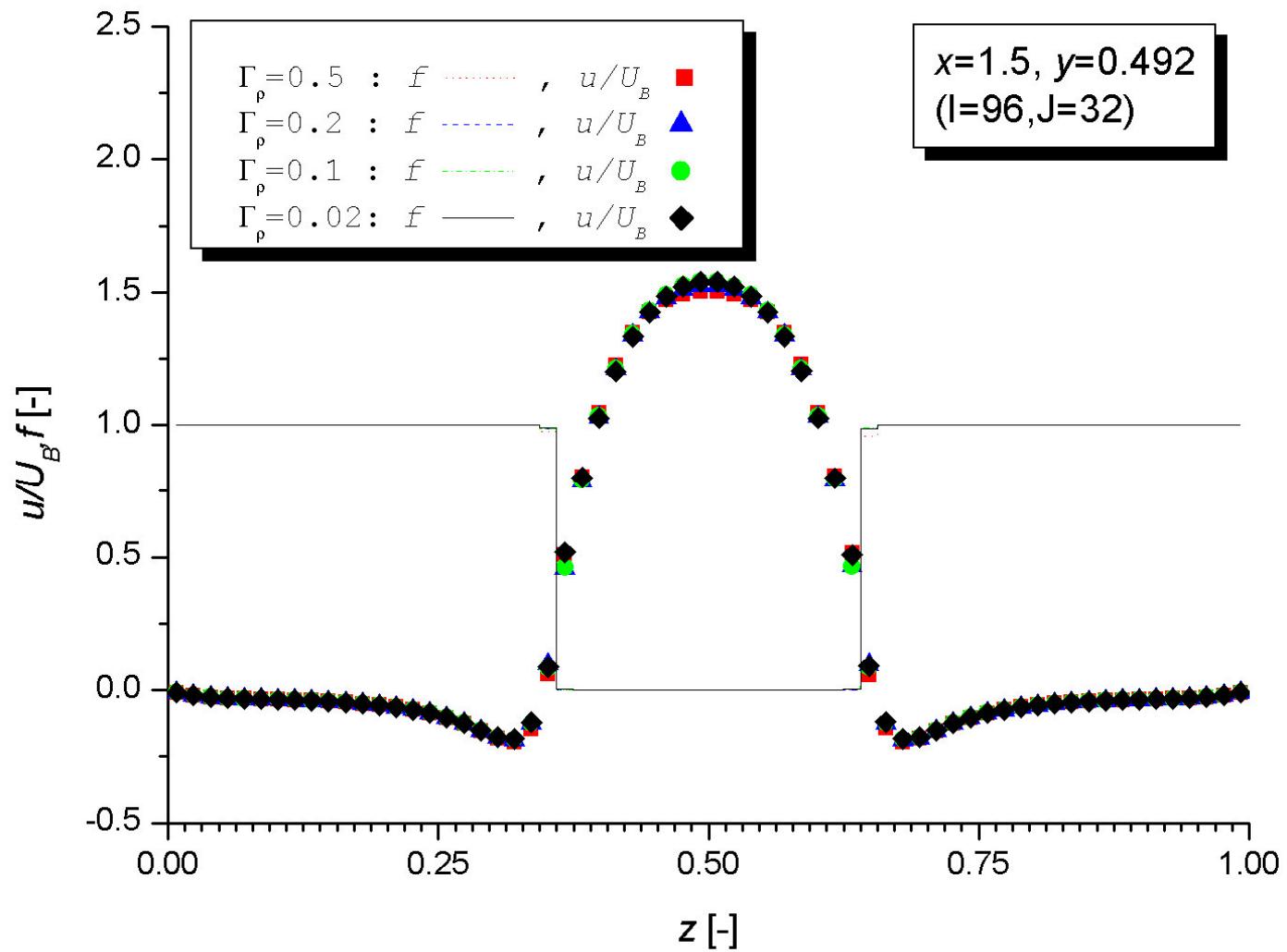
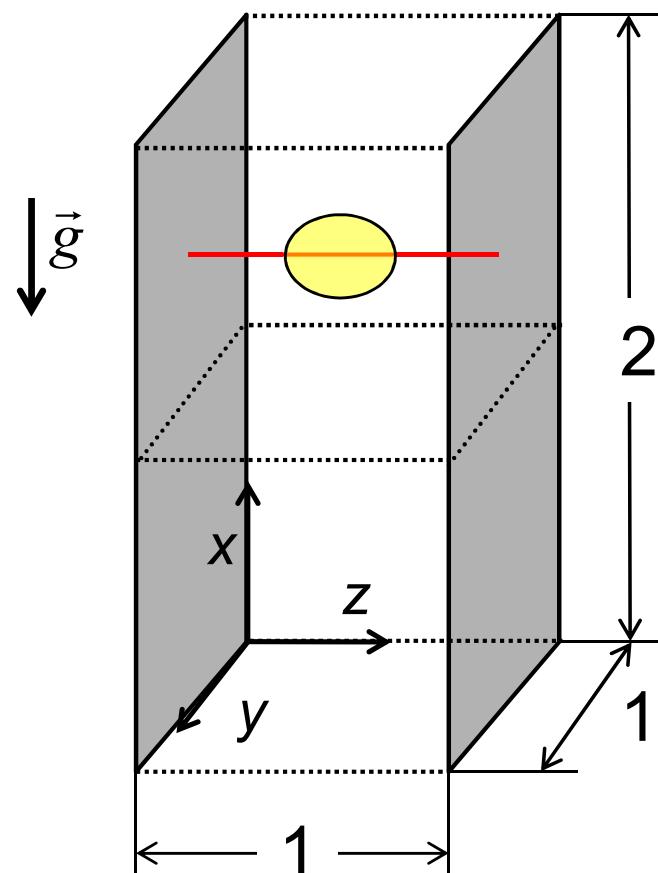


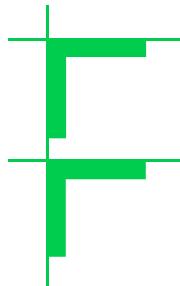
Local vertical velocity (case 1)

Normalization by respective bubble rise velocity U_B

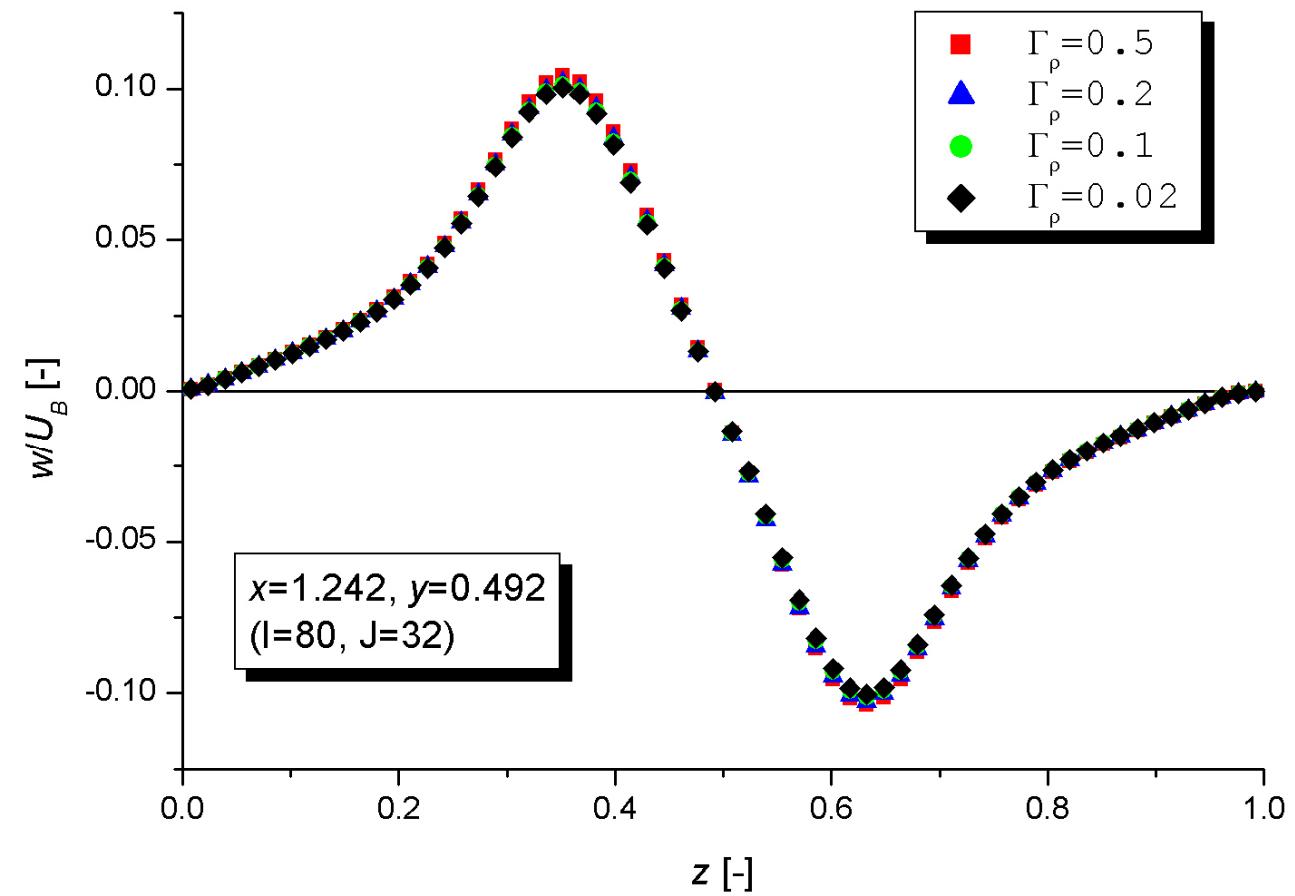
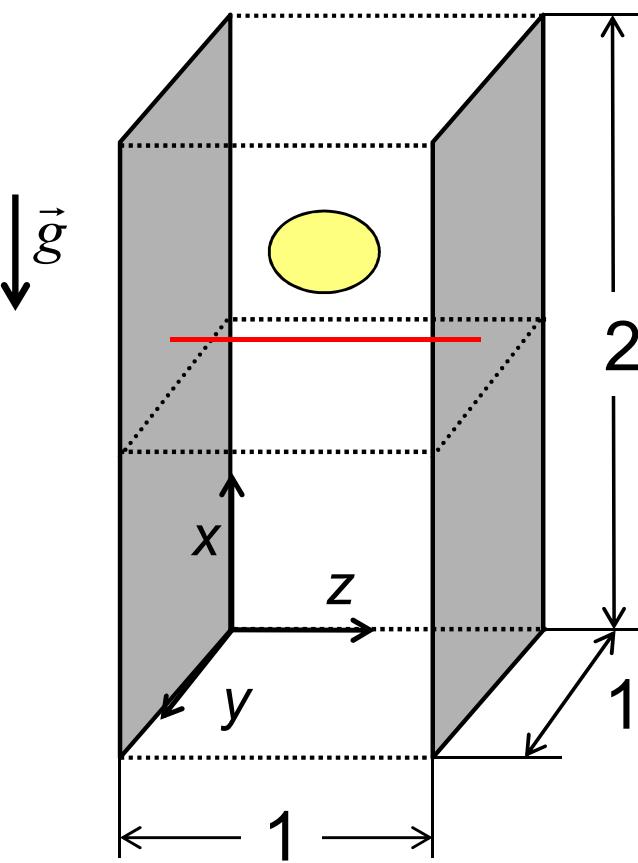


Local vertical velocity (case ①)

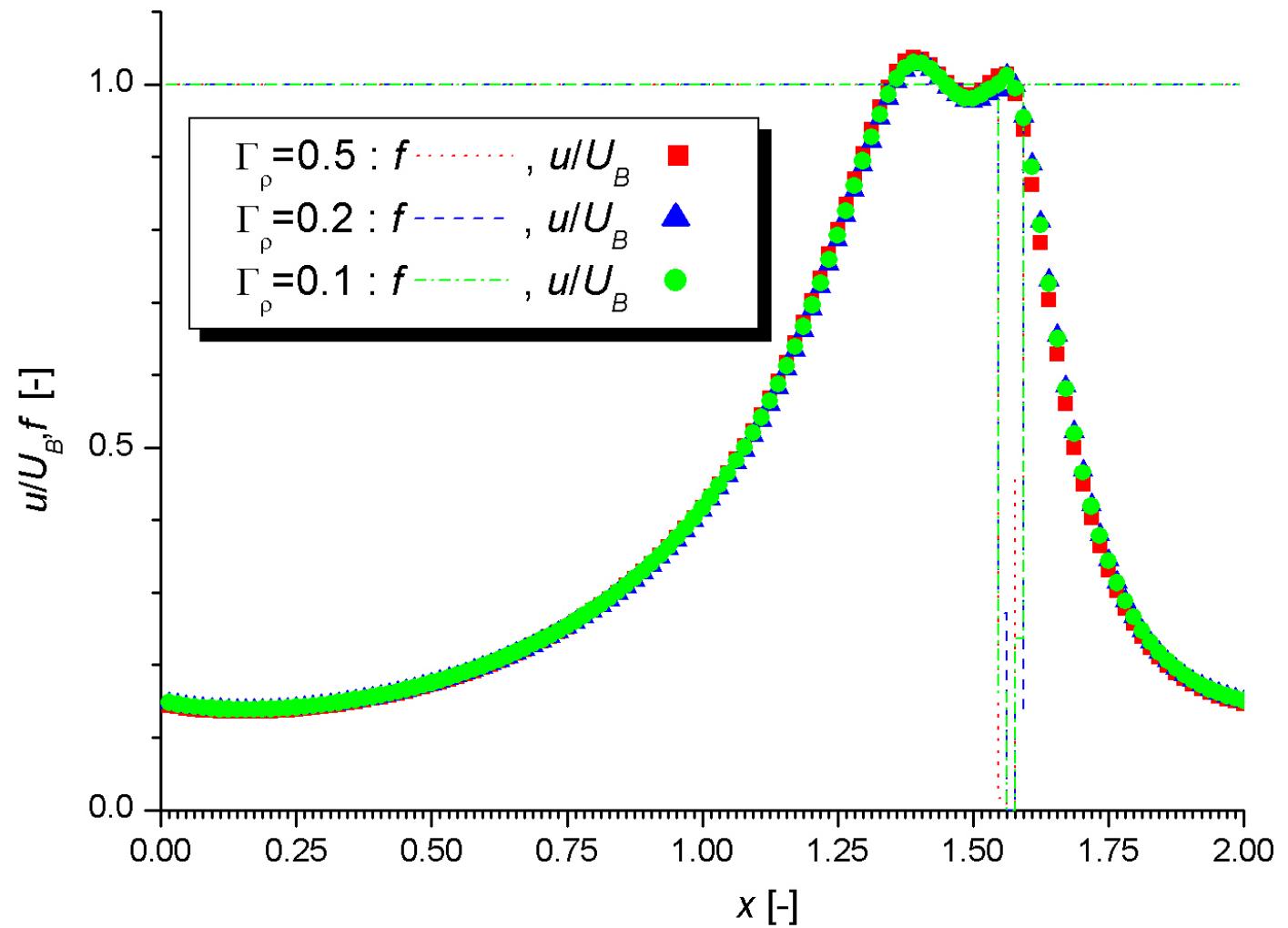
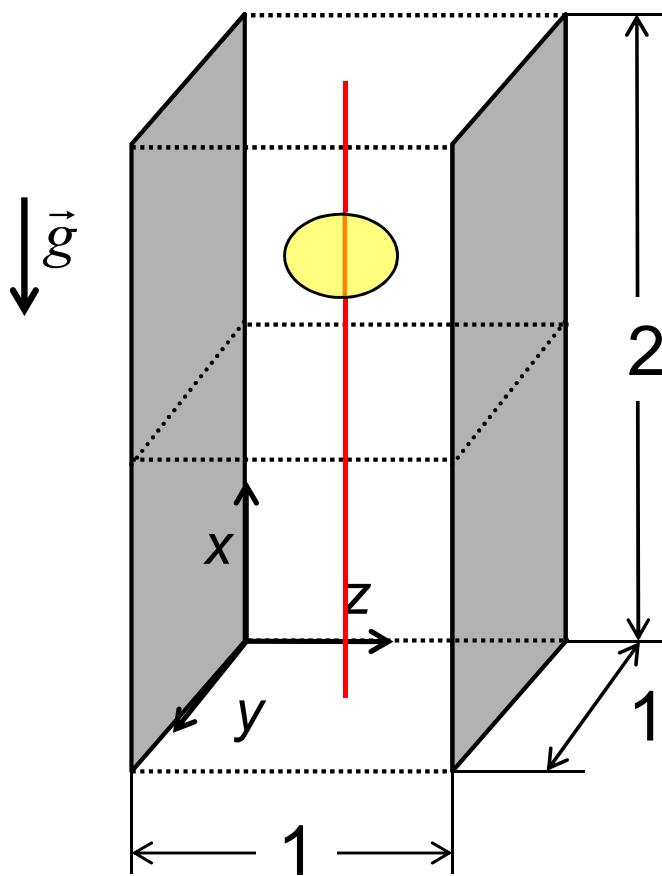


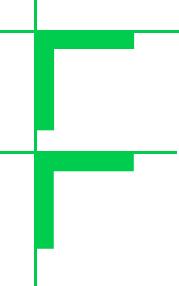


Local wall-normal velocity (case ①)



Local vertical velocity (case ②)





Conclusions

- DNS of ellipsoidal and ellipsoidal cap bubble for fixed values of $Eö_B$ and Mo but different density ratios Γ_ρ
- Steady bubble: shape, bubble Reynolds number, and liquid velocity field are virtually independent of Γ_ρ
 - ⇒ DNS results for steady bubbles obtained with $\Gamma_\rho = O(0.1)$ can be transferred to $\Gamma_\rho = O(0.001)$
- *Statistical models for bubble induced turbulence*
 - formulate models in terms of Eötvös and Morton number
 - utilize DNS data for model development and testing