

# **Numerical Study of Bubble Train Flow in a Square Vertical Mini-Channel: Influence of Length of the Flow Unit Cell \***

M. Wörner, B.E. Ghidersa, A.F. Shahab

Research Center Karlsruhe, Institute for Reactor Safety, Germany

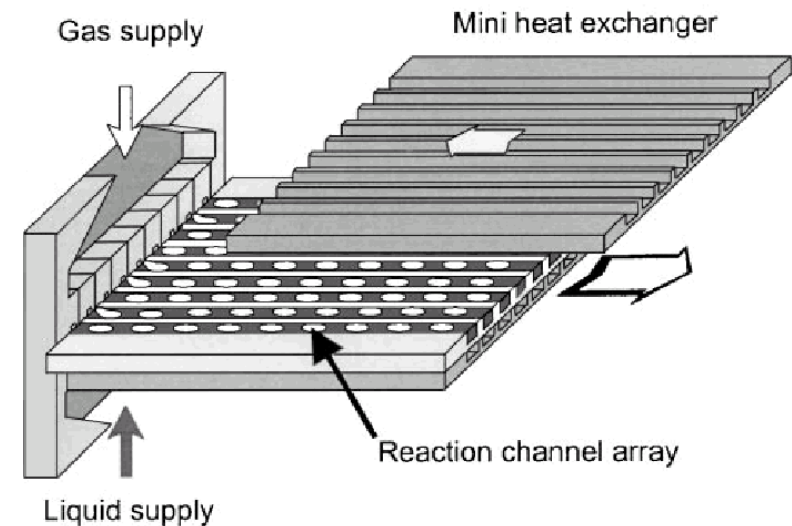
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\* Oral presentation by E. Laurien, University of Stuttgart, Germany

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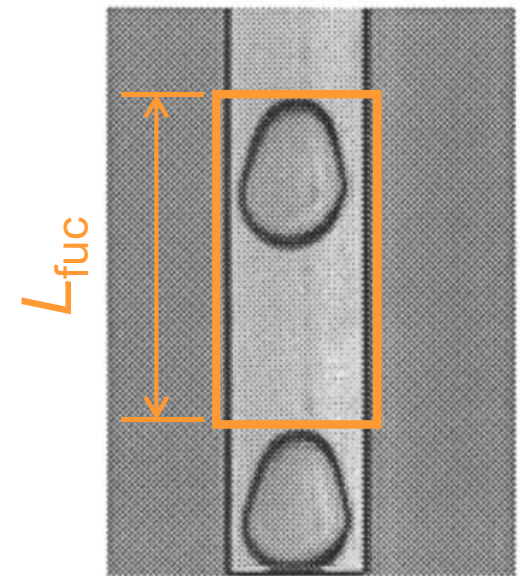
# Motivation

- Multi-phase chemical process engineering
  - Miniaturized devices offer certain advantages
    - High interfacial area per unit volume
      - ⇒ Enhanced heat and mass transfer
    - Defined interface geometry
      - ⇒ Numbering up instead of scaling up
    - Example:  
Micro bubble column\*
- Of interest: gas-liquid flow in single channel



# Objective

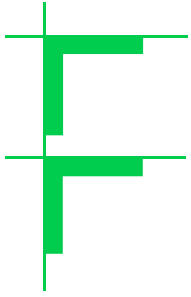
- Investigate gas-liquid flow in narrow channel numerically by volume-of-fluid method
- Verification by experiments of Thulasidas et al.\*
  - Square vertical channel  
cross section: 2 mm × 2 mm ( $W = 2$  mm)
  - Air bubbles in silicon oil
  - Bubbles of identical shape move with same velocity = “bubble train flow”
  - Flow is fully characterized by a single “flow unit cell” of length  $L_{\text{fuc}}$





# In-house code TURBIT-VOF

- Volume-of fluid method for interface tracking
  - Interface is locally approximated by plane (PLIC method)
- Governing equations for two incompressible fluids (see paper)
- Solution strategy
  - Projection method resulting in pressure Poisson equation
  - Explicit third order Runge-Kutta time integration scheme
- Discretization in space
  - Finite volume formulation for regular staggered grid
  - Second order central difference approximations



# Numerical set up

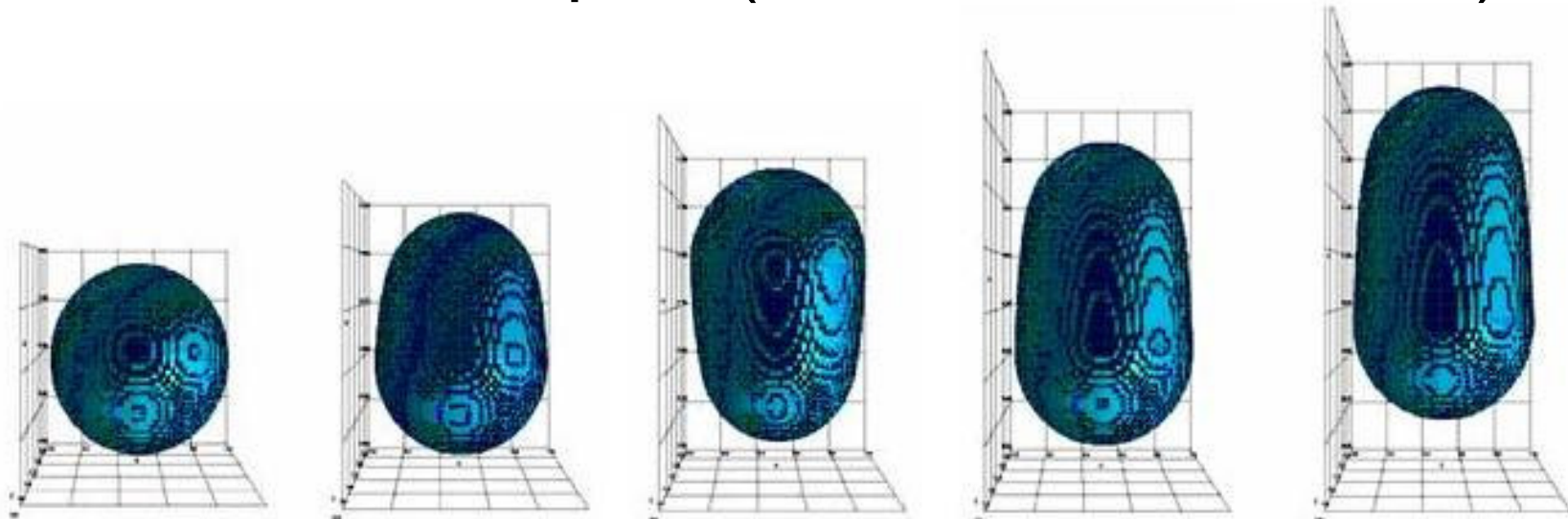
- Consideration of one flow unit cell
- Account for influence of trailing/leading unit cells by periodic boundary conditions in axial direction
- Length of flow unit cell,  $L_{\text{fuc}}$ , is input parameter
- Here: investigate influence of  $L_{\text{fuc}} / W$
- Flow is driven in vertical direction ( $y$ ) by specified axial pressure gradient and buoyancy

# Physical parameters

- Fluid properties Factor 10 higher than  $\rho$  and  $\mu$  of air

$\rho_l$	$\rho_g$	$\mu_l$	$\mu_g$	$\sigma$
957 kg/m <sup>3</sup>	11.7 kg/m <sup>3</sup>	0.048 Pa s	$1.84 \times 10^{-4}$ Pa s	0.022 N/m

- Initial bubble shapes\* (void fraction  $\varepsilon = 33\%$ )



- Simulations are started from gas and liquid at rest

\* Mathematical description see paper

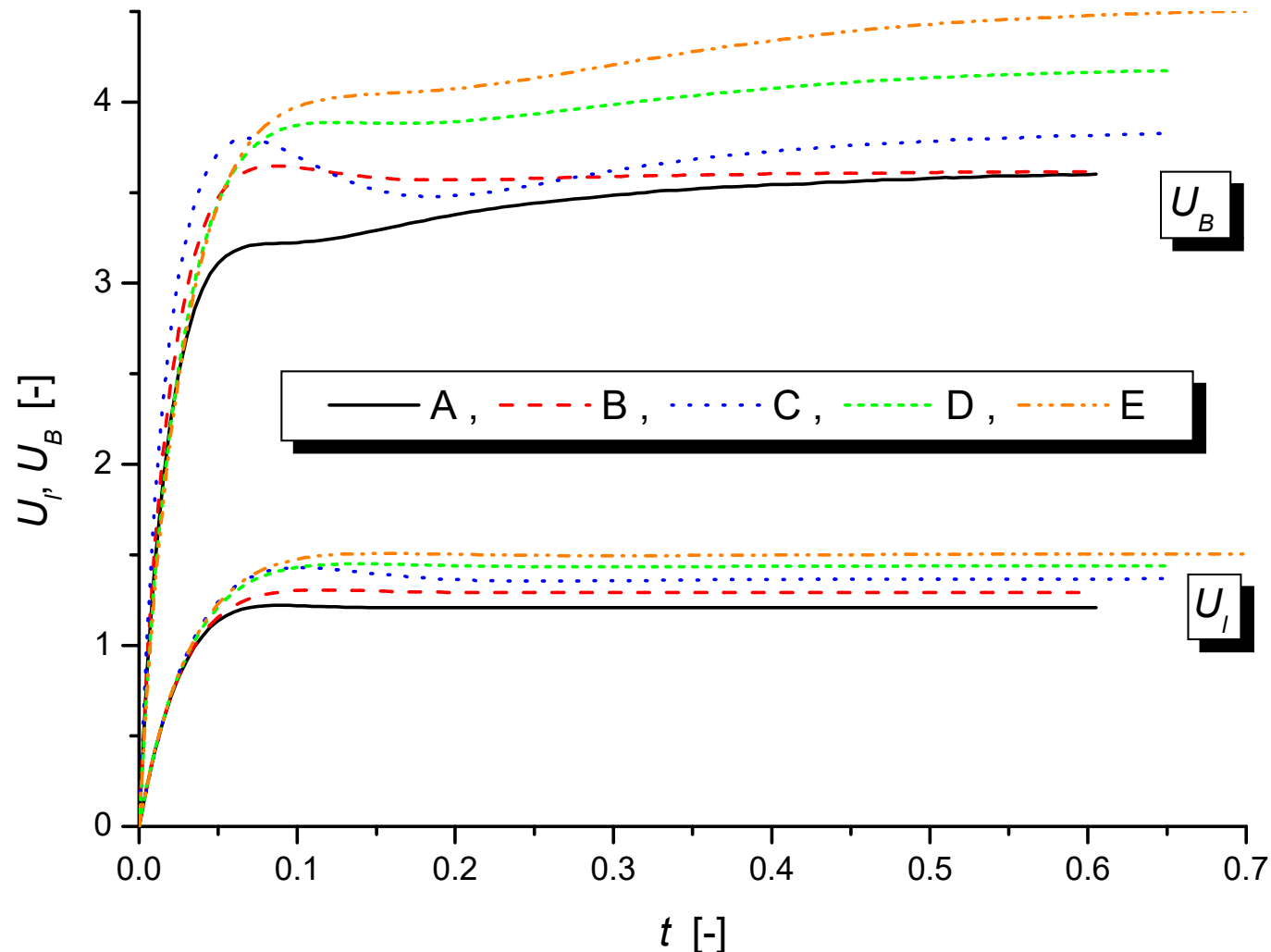


# Computational parameters

Case	$L_{\text{fuc}} / W$	Domain	Grid	Time steps
A1	1	$1 \times 1 \times 1$	$48 \times 48 \times 48$	24,000
A2	1	$1 \times 1 \times 1$	$64 \times 64 \times 64$	60,000
B	1.25	$1 \times 1.25 \times 1$	$48 \times 60 \times 48$	24,000
C	1.5	$1 \times 1.5 \times 1$	$48 \times 72 \times 48$	26,000
D	1.75	$1 \times 1.75 \times 1$	$48 \times 84 \times 48$	26,000
E	2	$1 \times 2 \times 1$	$48 \times 96 \times 48$	28,000

Results on both grids show only slight differences

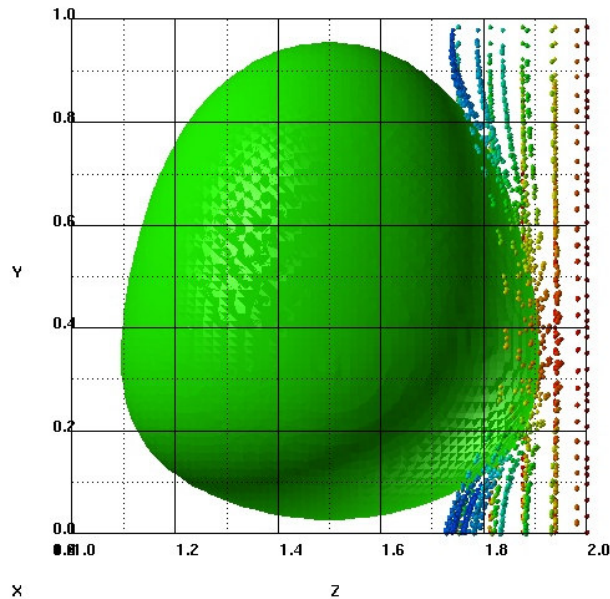
# Time history of mean velocities



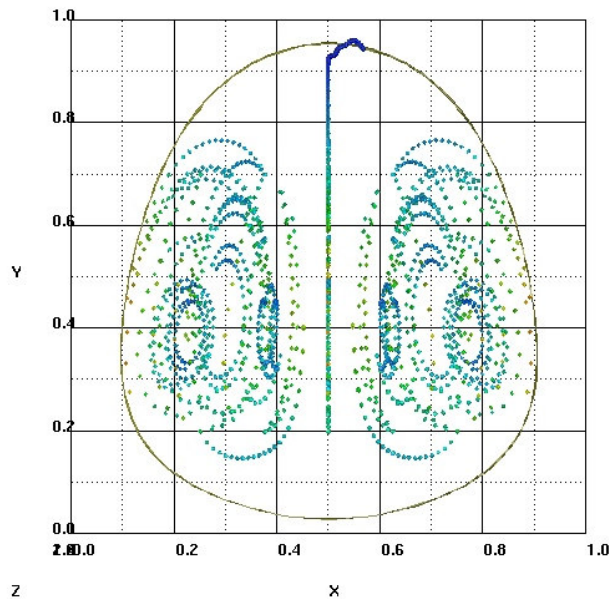
Steady state values of bubble velocity  $U_B$  and mean liquid velocity  $U_l$  increase with increasing length of the flow unit cell



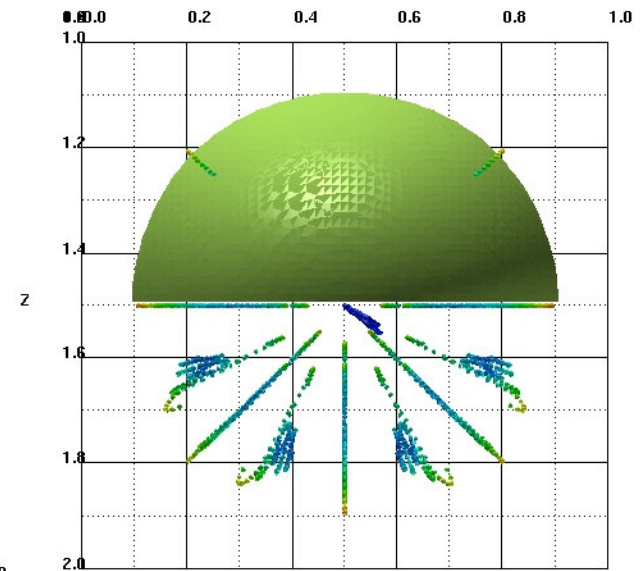
# Bubble shape and trajectories of mass less particles for case A



View from side

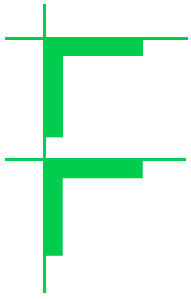


View from side



View from top

- Bubble has axisymmetric shape
- One large vortex inside the bubble
- Small azimuthal flow inside bubble

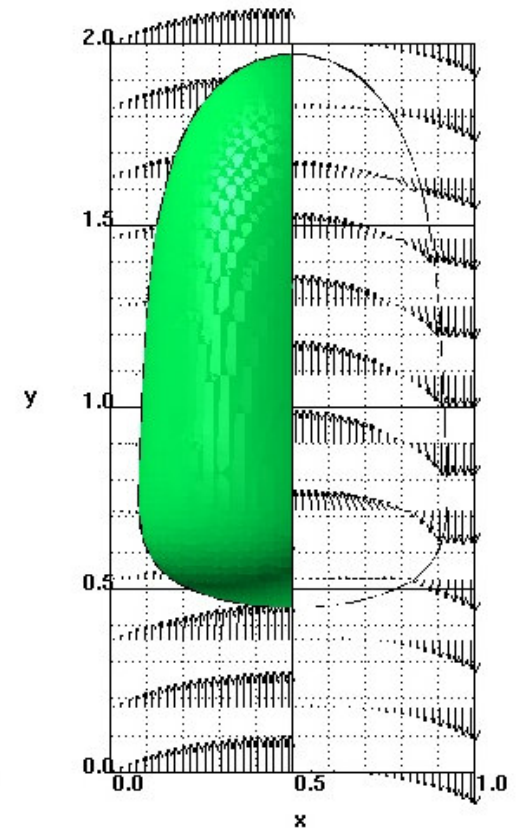
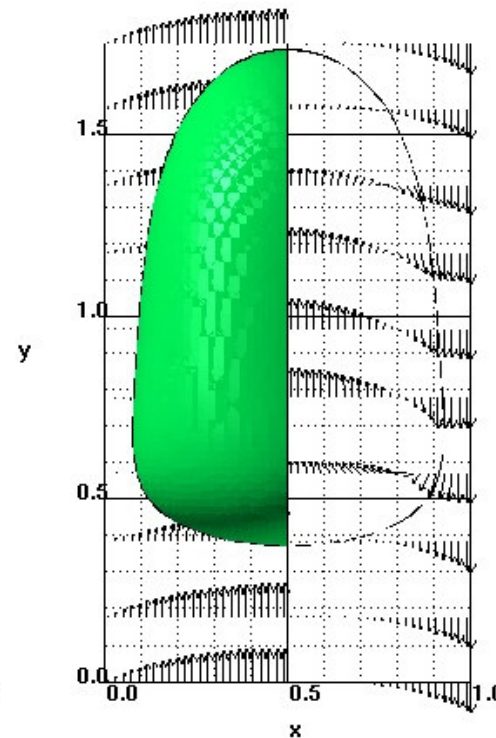
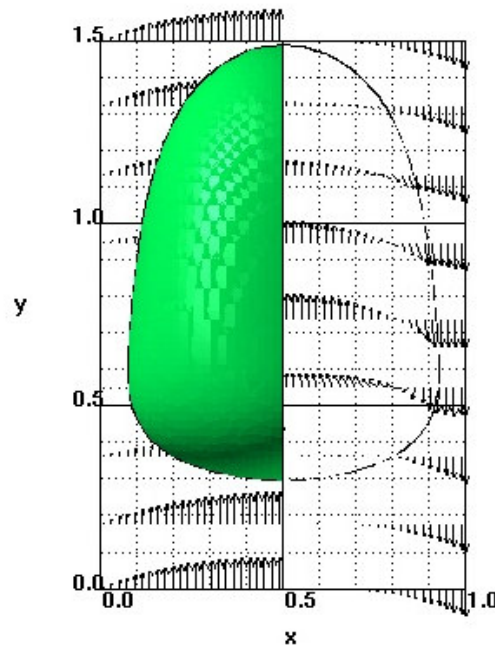
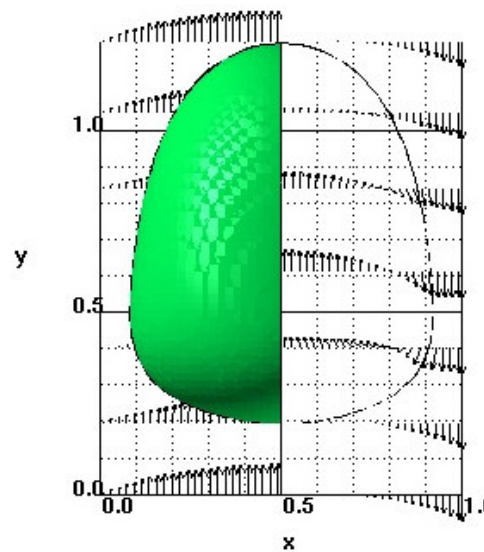
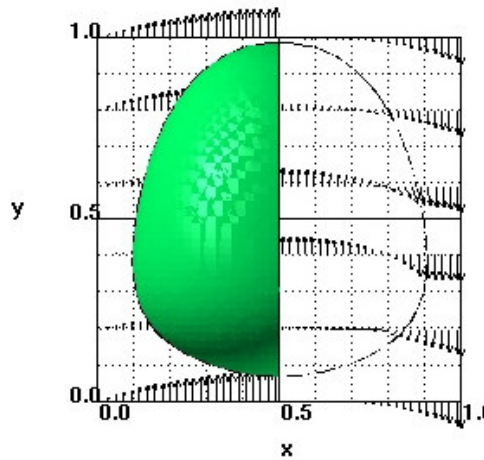


# Bubble shape and velocity field

## Velocity field in vertical mid-plane

Right half: frame of reference moving with bubble

Left half: fixed frame of reference



# Comparison with experiment

Non-dimensional bubble diameter

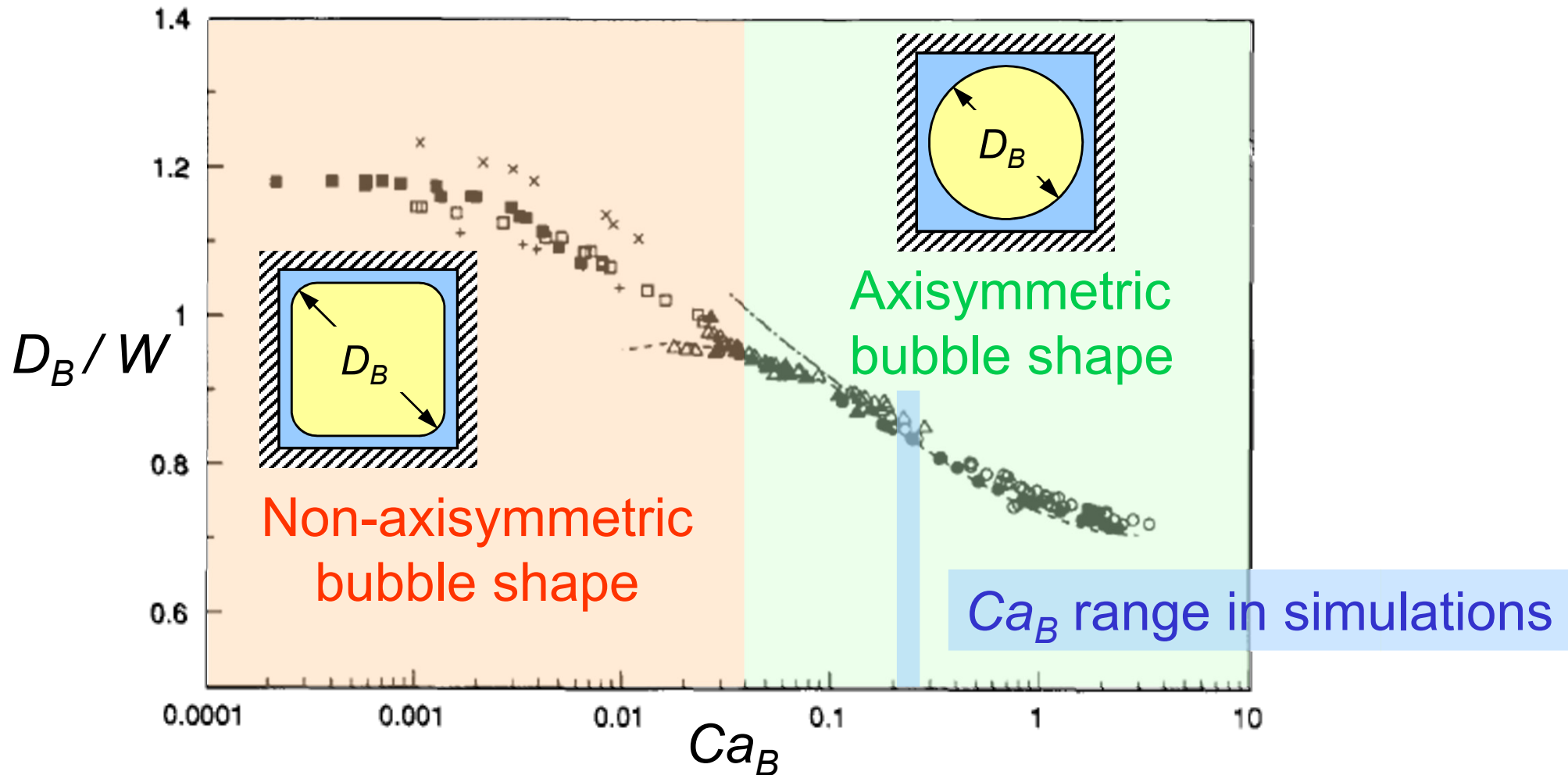
Relative velocity

Non-dimensional  $U_B$

Case	$L_{fuc} / W$	$Ca_B$	$D_B / W$	$(U_B - J_{total}) / U_B$	$U_B / J_{total}$
A	1	0.204	0.81	1.80	0.445
B	1.25	0.207	0.84	1.75	0.430
C	1.5	0.215	0.85	1.75	0.430
D	1.75	0.238	0.85	1.78	0.438
E	2	0.253	0.85	1.8	0.445
Experimental data*		correlated in terms of Capillary number $Ca_B \equiv \mu_l U_B / \sigma$			
		0.2 – 0.25	0.82 – 0.86	1.68 – 1.84	0.435 – 0.475

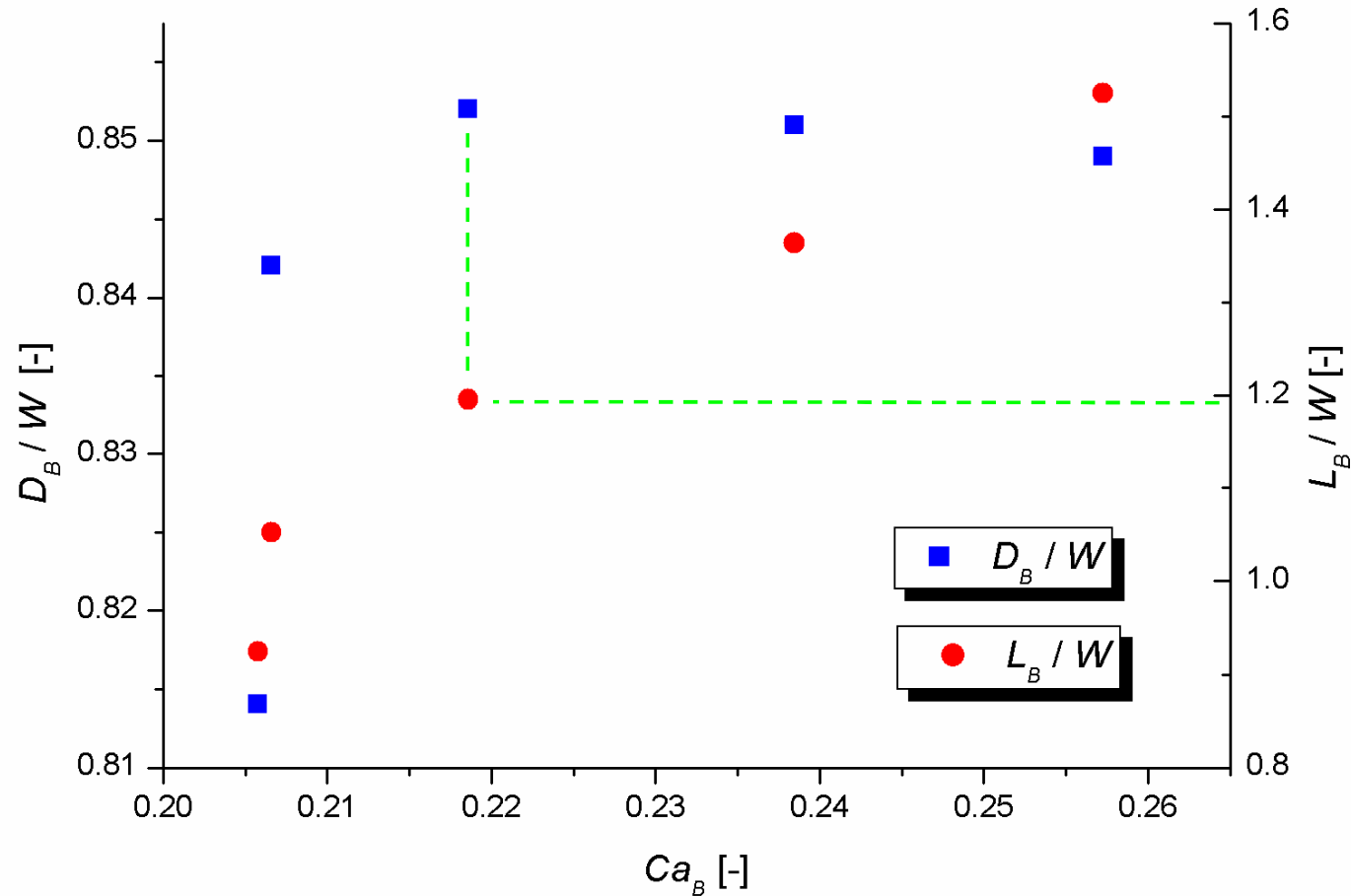


# $D_B$ measured along channel diagonal\*

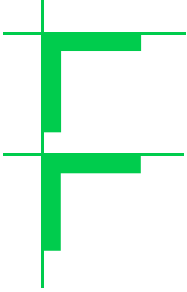


$\Rightarrow D_B/W$  decreases with increase of  $Ca_B$

# Bubble diameter in simulations



$D_B / W$  decreases with increase of  $Ca_B$  only if the bubble length  $L_B$  is larger than about 1.2 the channel width (this is the case in the experiments by Thulasidas et al.)



# Conclusions

- Numerical simulation of bubble train flow
  - Square vertical mini-channel of width  $W = 2$  mm
  - Investigation of influence of flow unit cell length
- Good agreement with experimental data from literature
- Dependence of bubble diameter on Capillary number
  - Regime I: increase of  $D_B$  with  $Ca_B$  for  $L_B < 1.2 W$
  - Regime II: decrease of  $D_B$  with  $Ca_B$  for  $L_B > 1.2 W$
  - From experiments so far only regime II is reported (long bubbles)