

Tungsten as a structural divertor material

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⁴Karlsruhe Institute of Technology, Institute of Nanotechnology, P.O. Box 3640, 76021 Karlsruhe, Germany

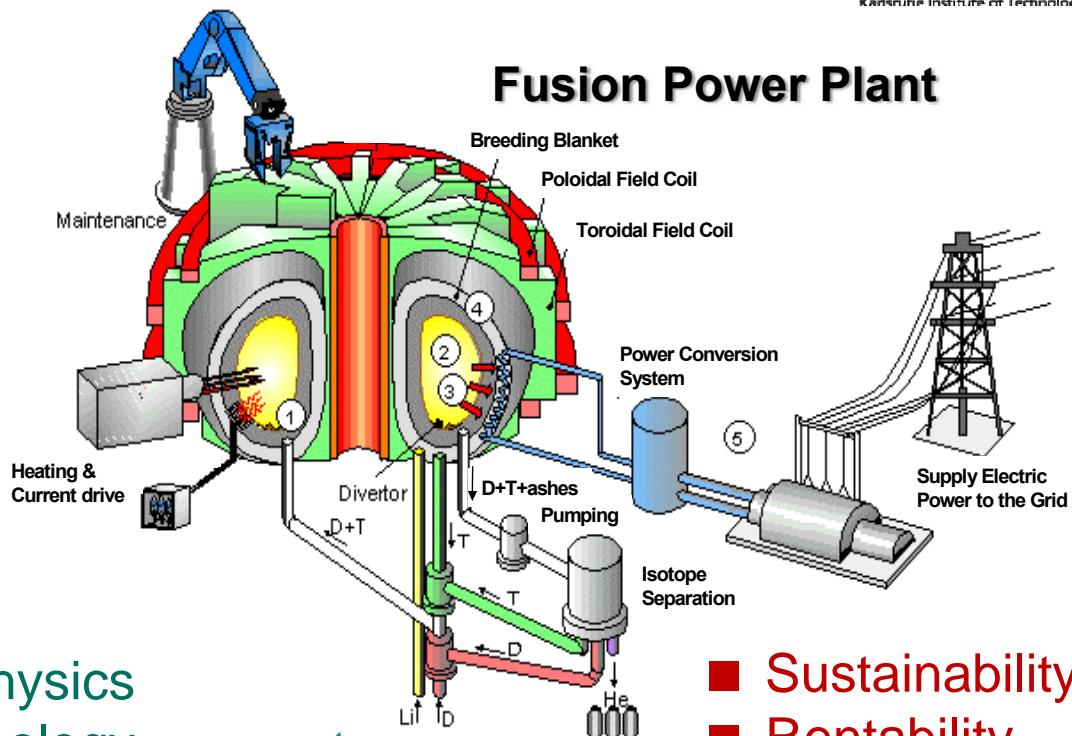
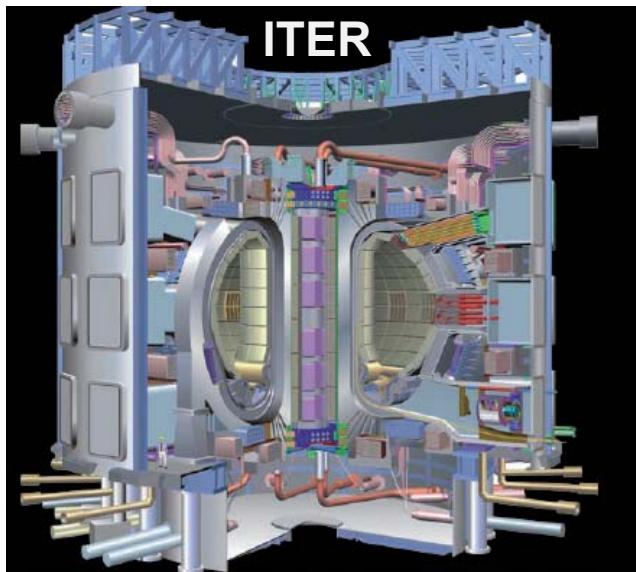
KARLSRUHE INSTITUTE OF TECHNOLOGY, INSTITUTE FOR MATERIALS RESEARCH



Contents

- Introduction
- Helium cooled divertor designs
- **Fracture behavior of tungsten materials under dynamic load**
 - Rods
 - Plates
- Conclusions

Where is the challenge?

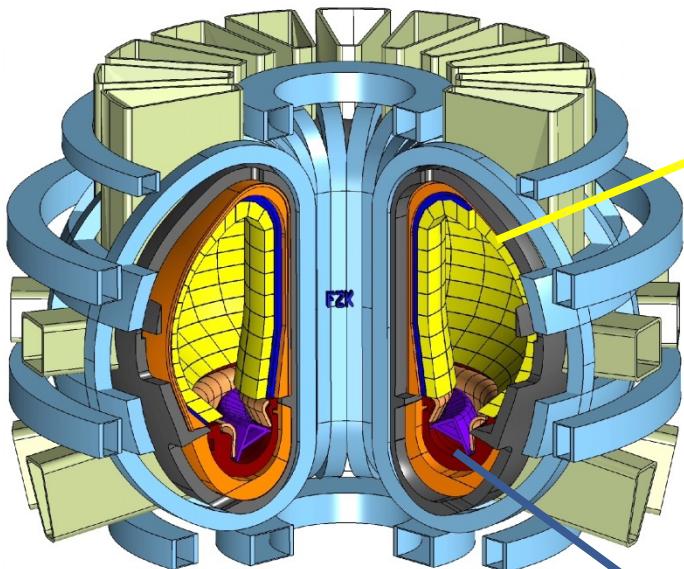


- Test device for plasma physics
- Safety → Standard technology

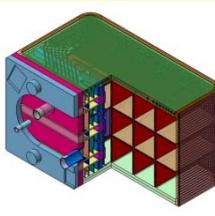
- Sustainability
- Rentability
- Safety
- Economy

complex superposition of intensive neutron/heat radiation and thermo-mechanical load/fatigue

High Heat Flux Components



DEMO



Blanket: $\leq 150 \text{ dpa/5 yrs}$, 2.5 MW/m^2

Reduced activation ferritic-martensitic steels

- **EUROFER (9Cr-WVTa)**
- EUROFER-ODS
- Ferritic ODS steels

350-550 °C

350-650 °C

350-750 °C ?

He cooled structure, liquid lithium or lithium-ceramics for tritium breeding → ~85 % power



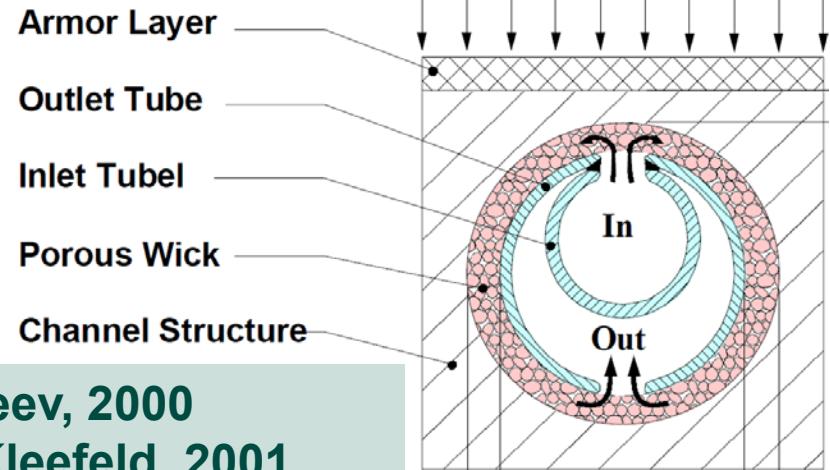
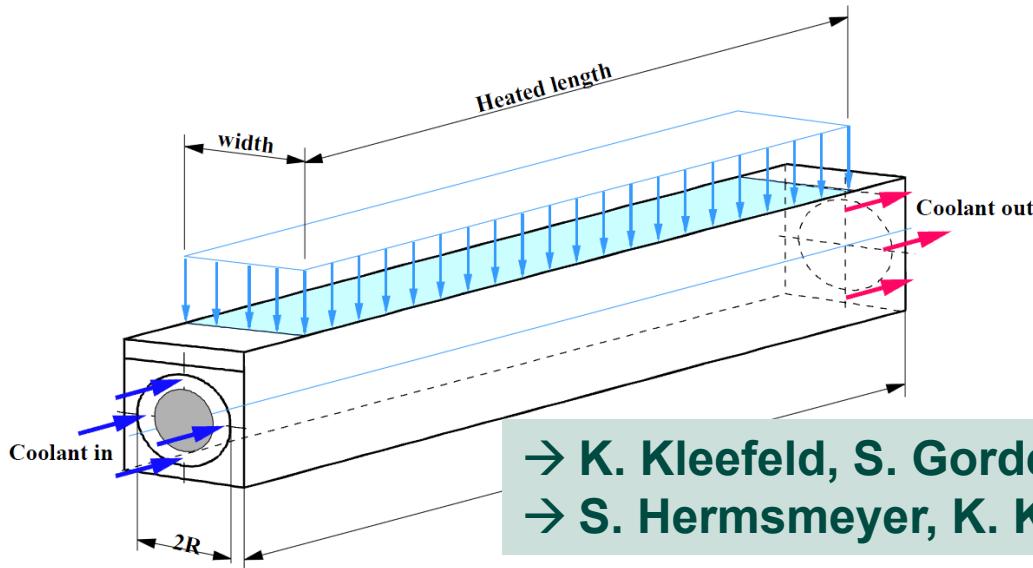
Divertor: $\sim 30 \text{ dpa/2 yrs}$, $5-10 \text{ MW/m}^2$

Materials unknown, tungsten ?

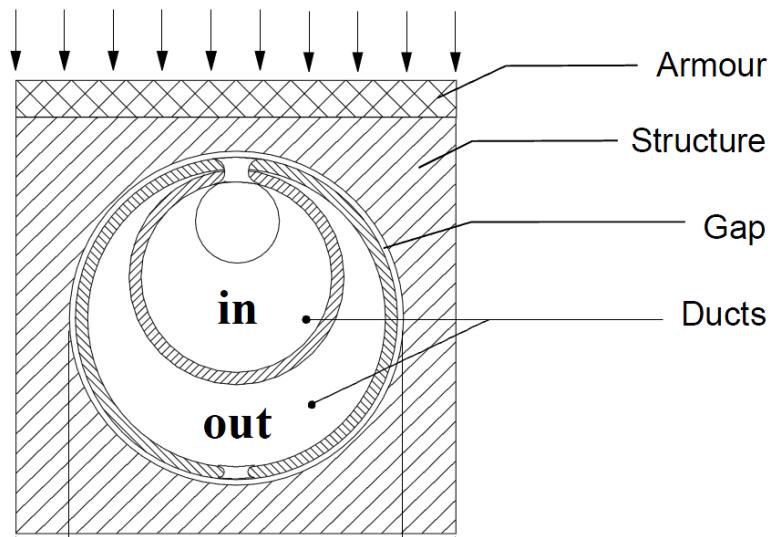
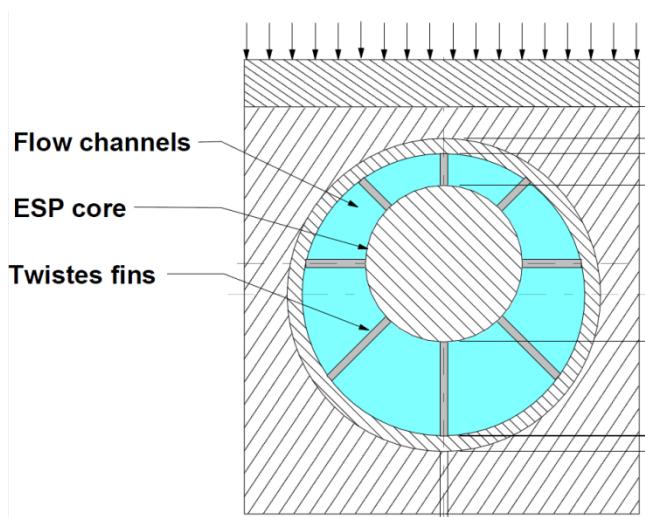
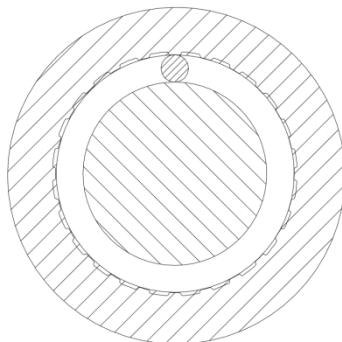
Operating temperature 350-1300 °C ?

Cooled tungsten shield to remove He and other particles from plasma → ~15 % power

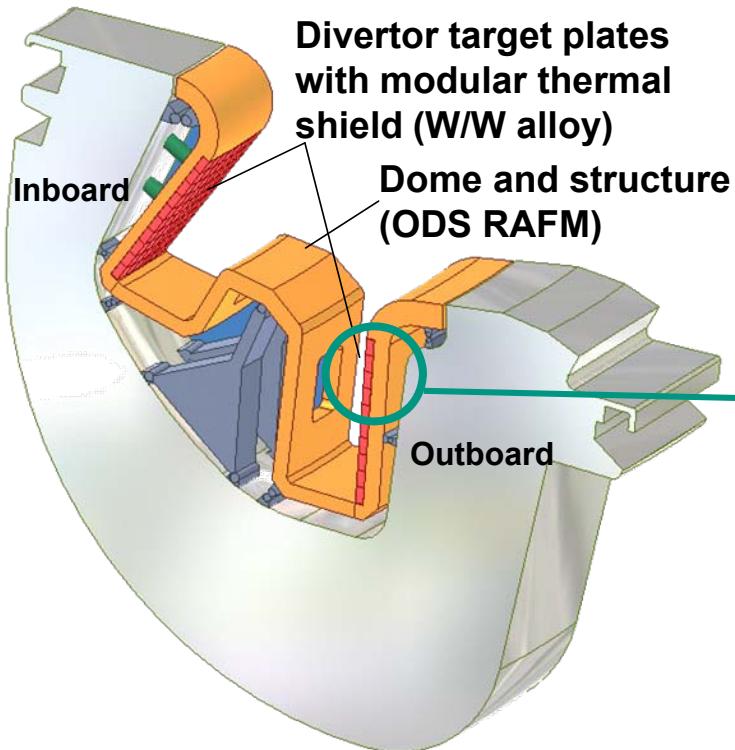
Tungsten & Helium, 5 MW/m² Concepts



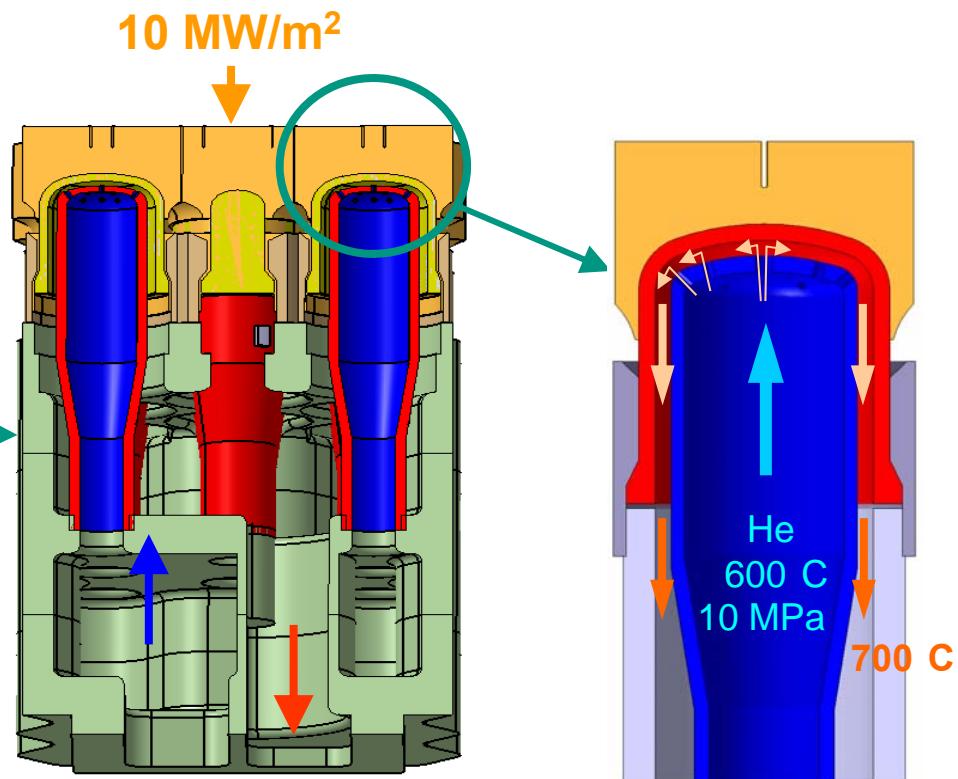
→ K. Kleefeld, S. Gordeev, 2000
→ S. Hermsmeyer, K. Kleefeld, 2001



Tungsten & Helium, 10 MW/m² Concepts



**Divertor
Cassette**

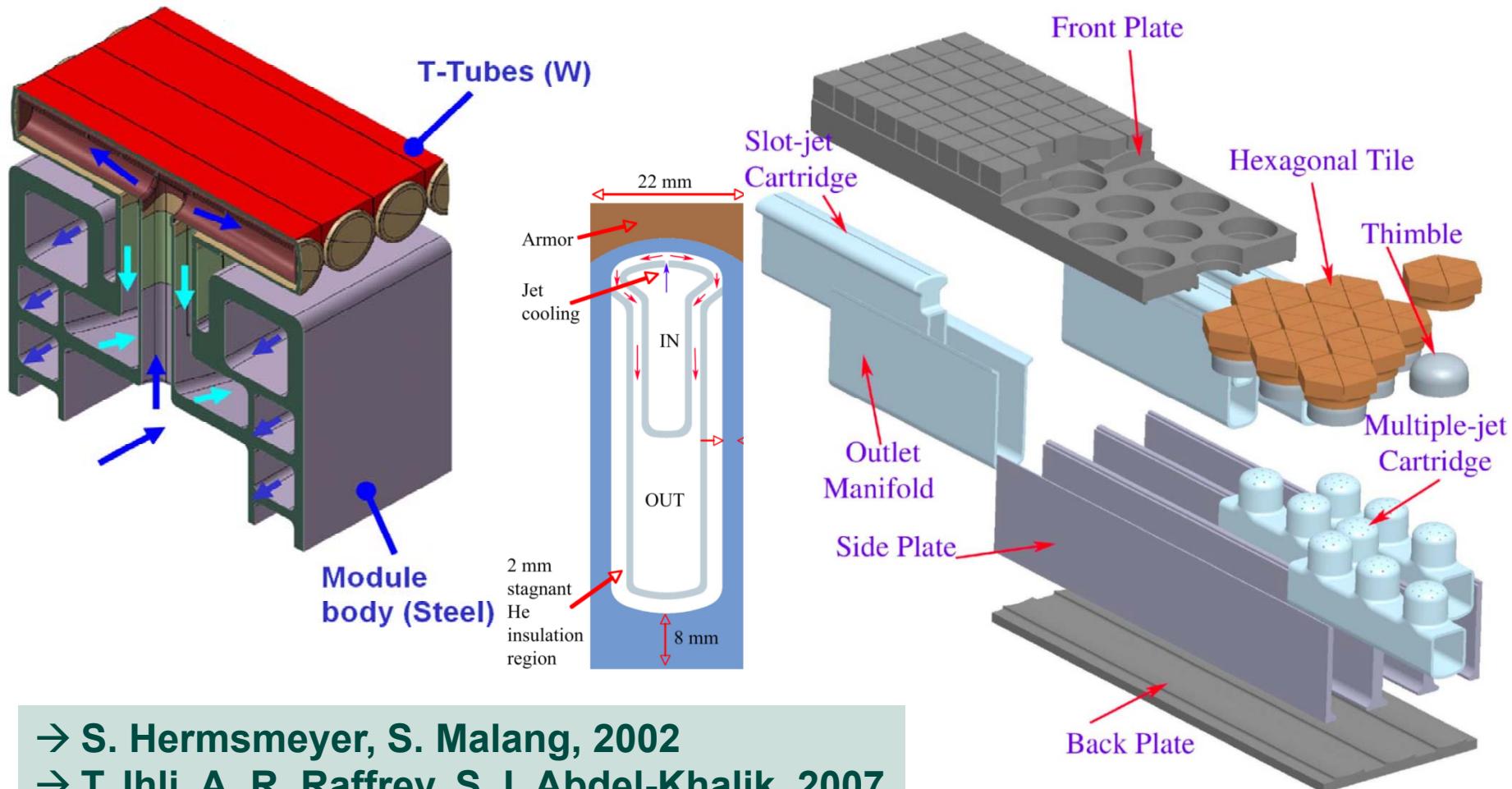


**9-Finger
Module**

Finger

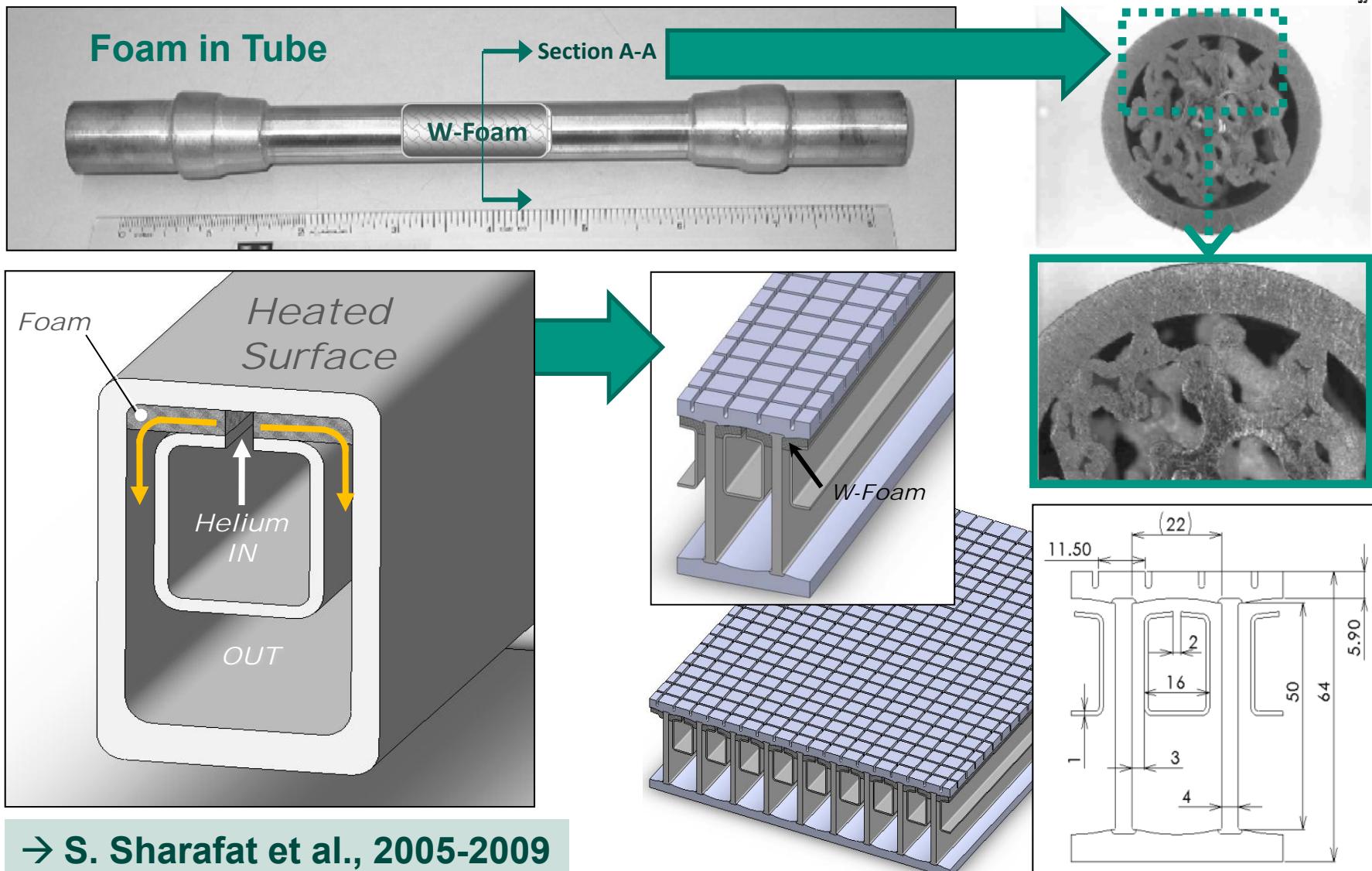
→ P. Norajitra et al., 2003-2009

Tungsten & Helium, 5-10 MW/m² Concepts



→ S. Hermsmeyer, S. Malang, 2002
→ T. Ihli, A. R. Raffrey, S. I. Abdel-Khalik, 2007
→ A. R. Raffrey, S. Malang et al., 2008

Tungsten & Helium, 10 MW/m² Concepts



→ S. Sharafat et al., 2005-2009

→ Pressurized pipes and cooling channels,
different cross-sections, caps, fittings, etc.

Facts

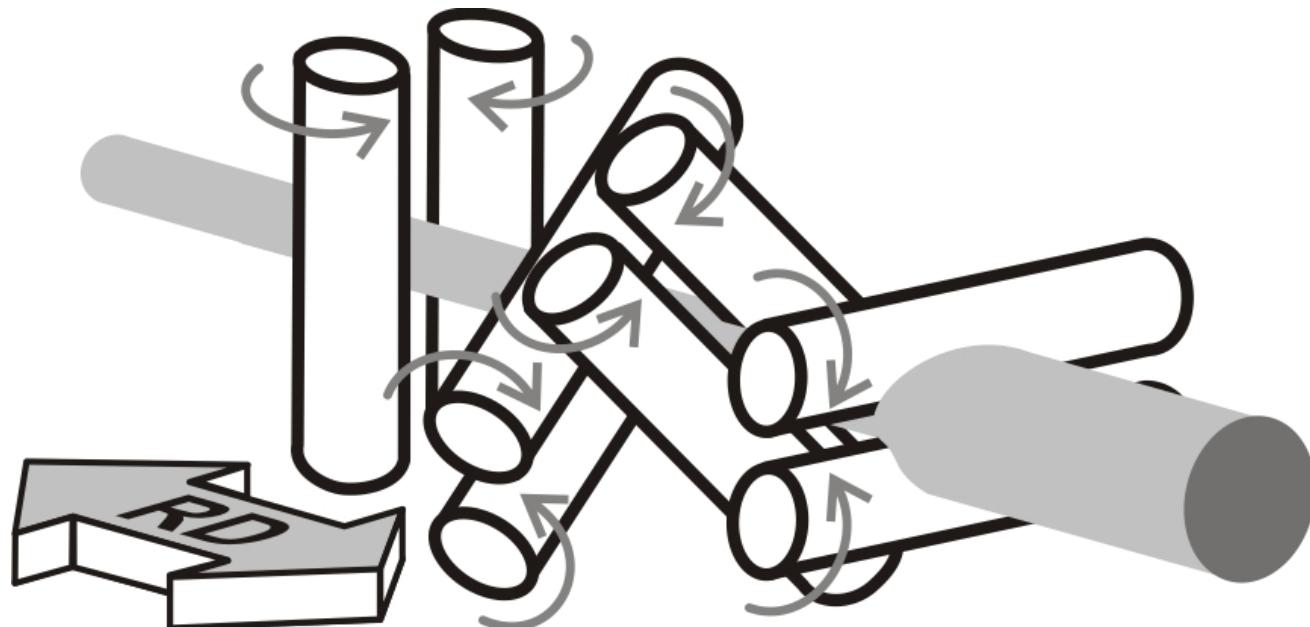
- Heat flux 5-10 MW/m²
- Various concepts
(experimental proof for finger module)
- Operating temperatures adaptable in a wide range

Drawbacks

- Brittleness of tungsten (even without irradiation)
- Unsolved fabrication issues (e.g. LA brazing, esp. under irradiation)

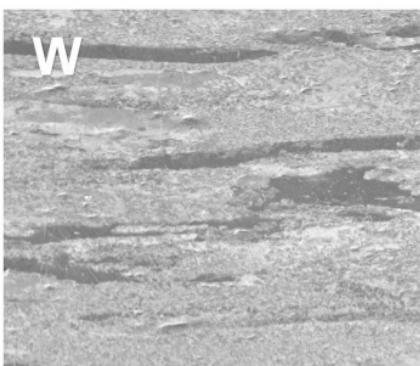
Fabrication of Half-finished Products

Rolling (or Swagging) of Rods



Microstructure Anisotropy

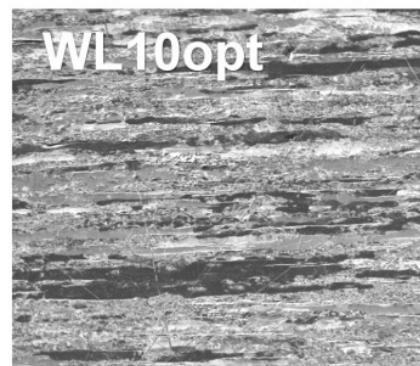
Rods: Metallography



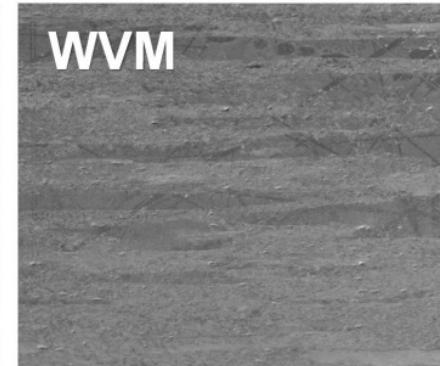
Ø6,9 mm | 91% | Rolling



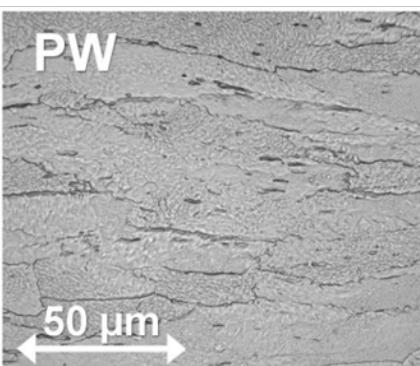
Ø6,9 mm | 91% | Rolling



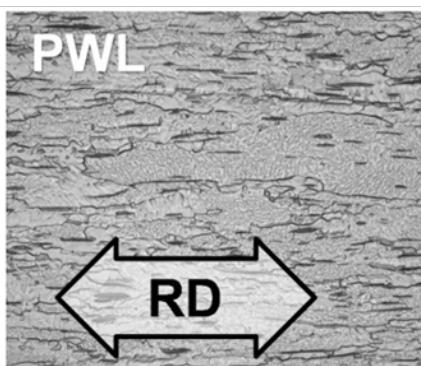
Ø6,9 mm | 94% | Swaging



Ø16 mm | 91% | Rolling



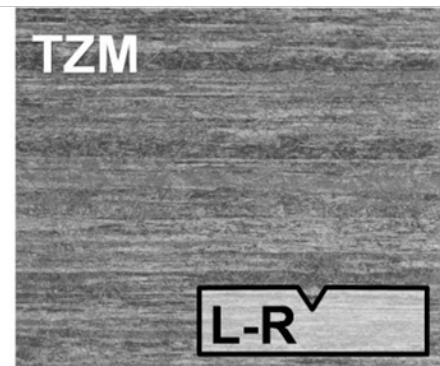
Ø20 mm | 93% | Swaging



Ø20 mm | 93% | Swaging



Ø10 mm | 81% | Rolling



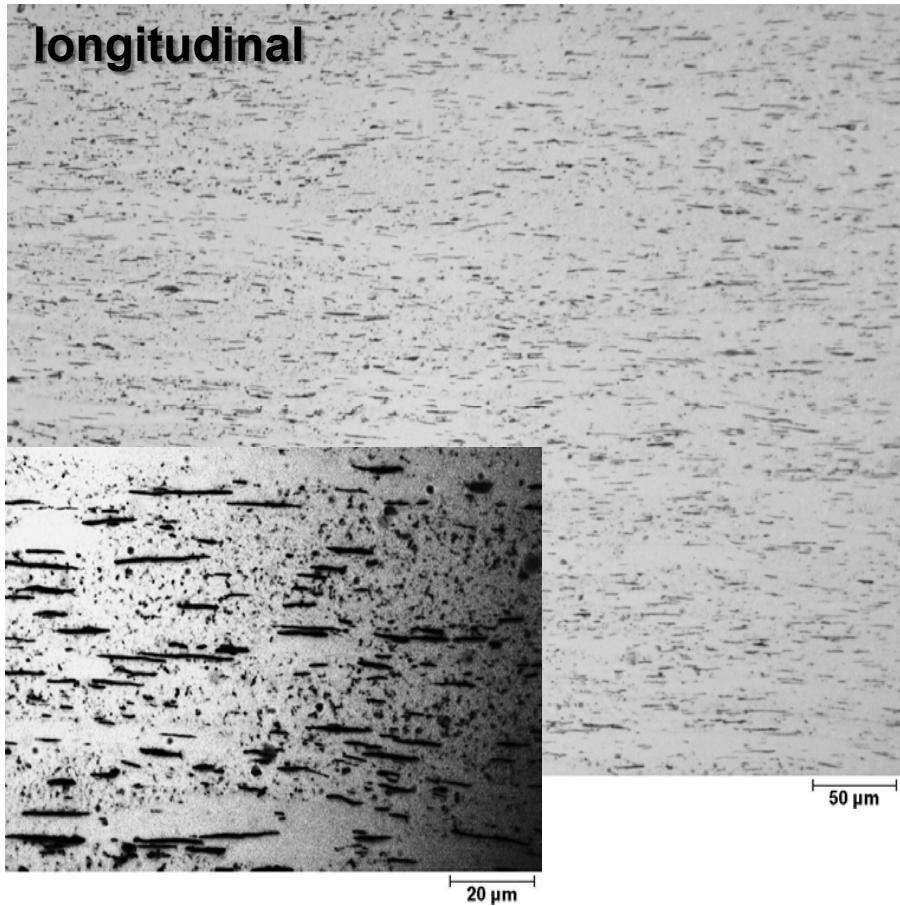
Ø7 mm | 91% | Sw+Rol

Microstructure Anisotropy, ODS Particles

WL10 Rod, Ø7 mm

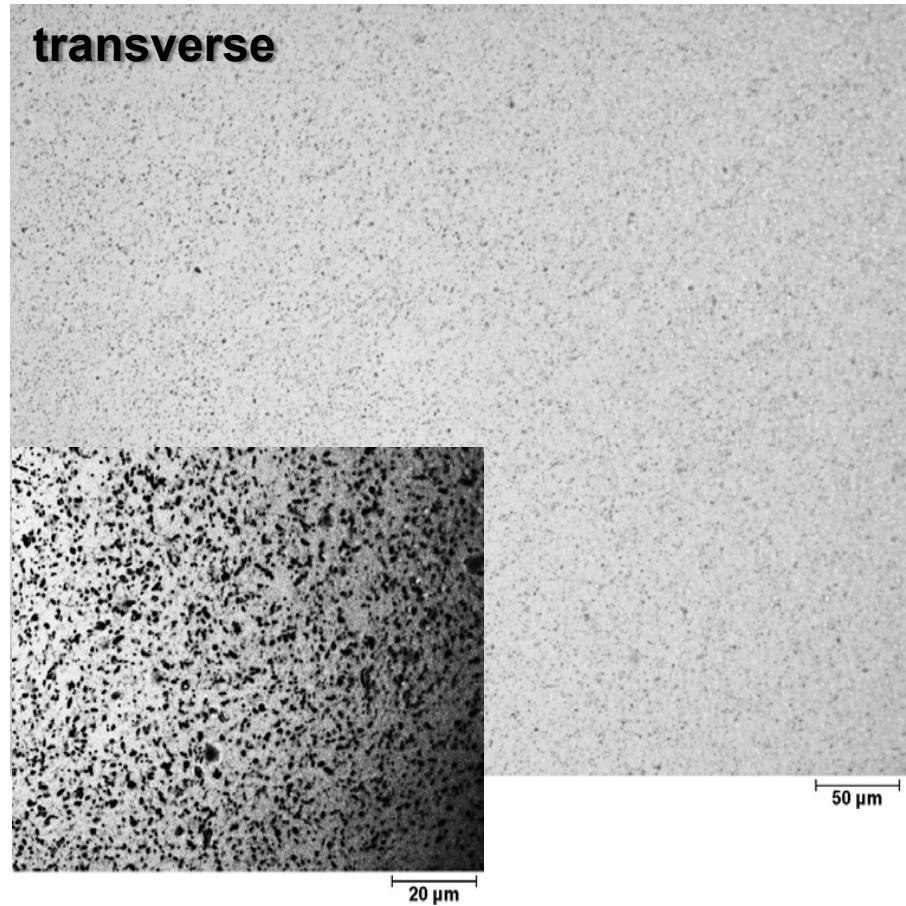


longitudinal



Rods: Metallography

transverse

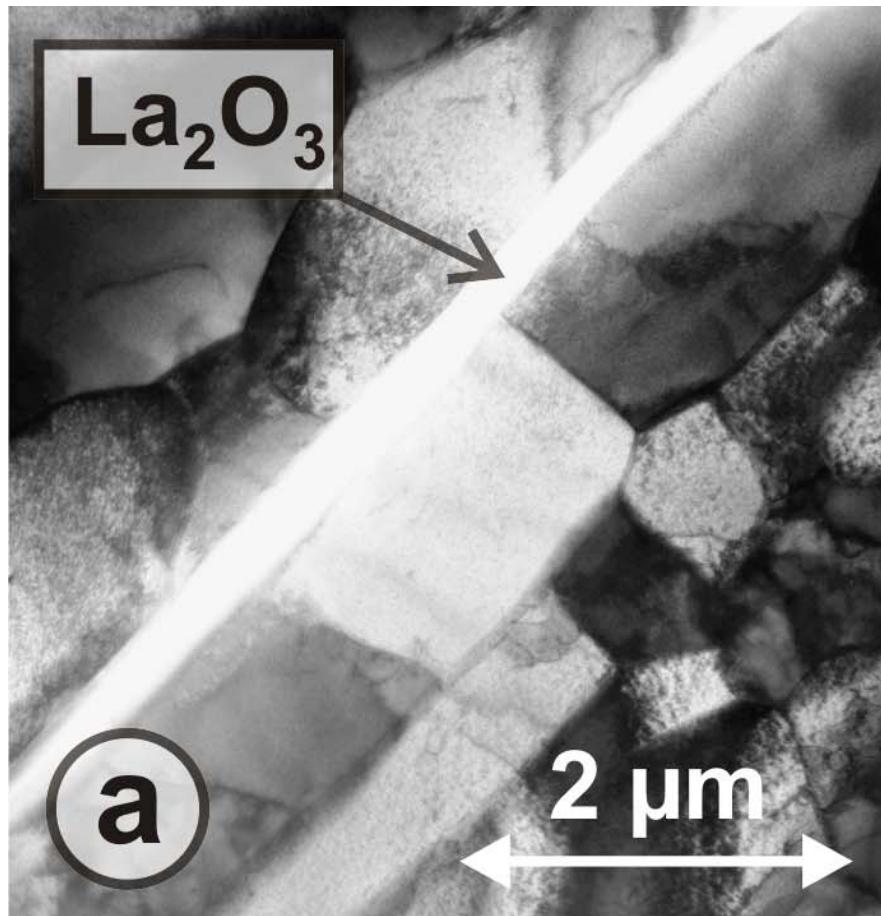


50 µm

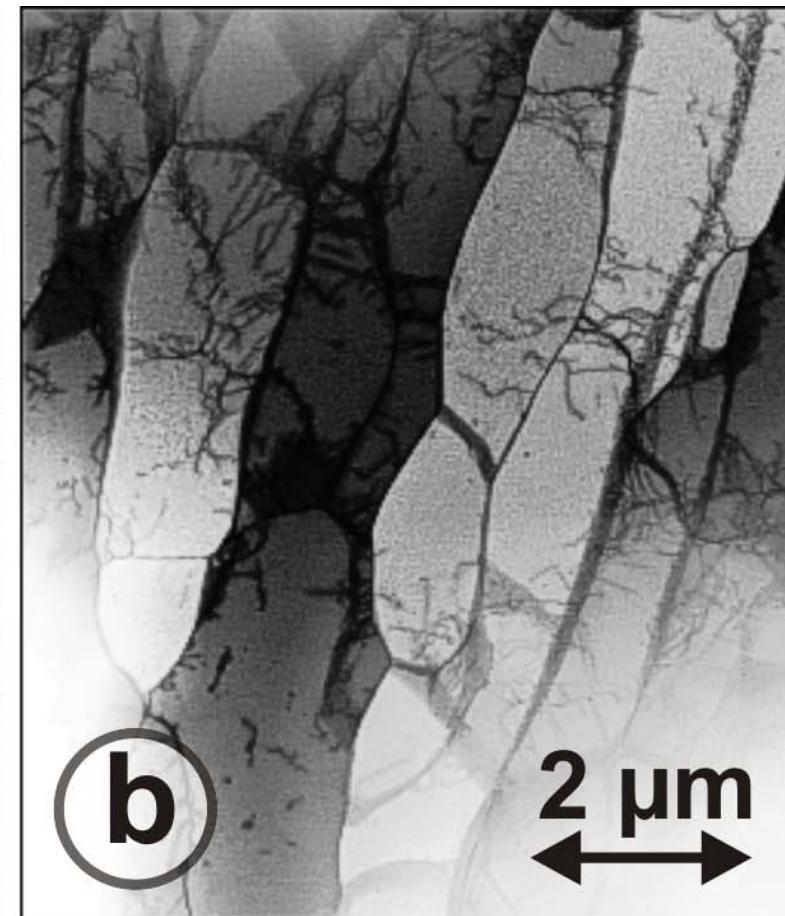
Microstructure Anisotropy

Rods: TEM

WL10 Rod, Ø7 mm

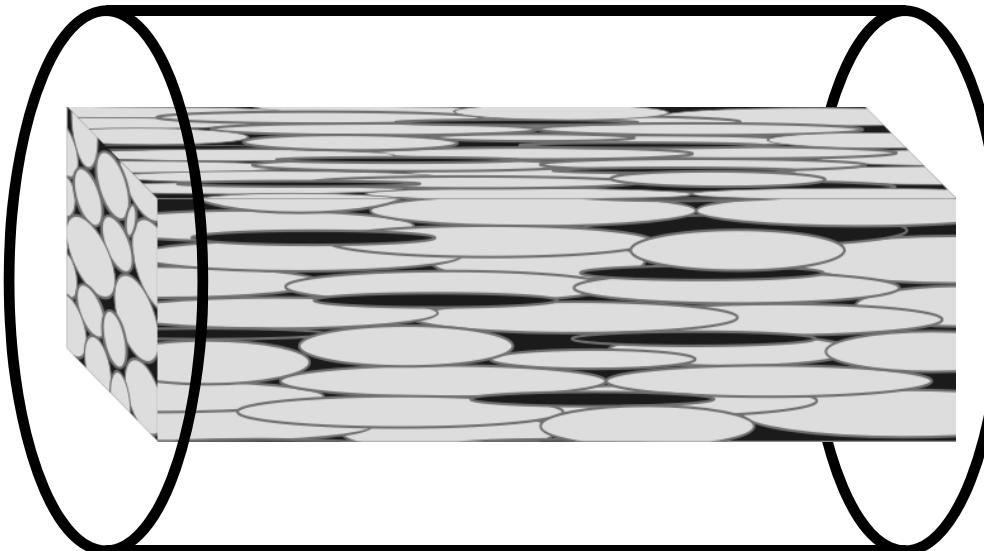


W Rod, Ø7 mm



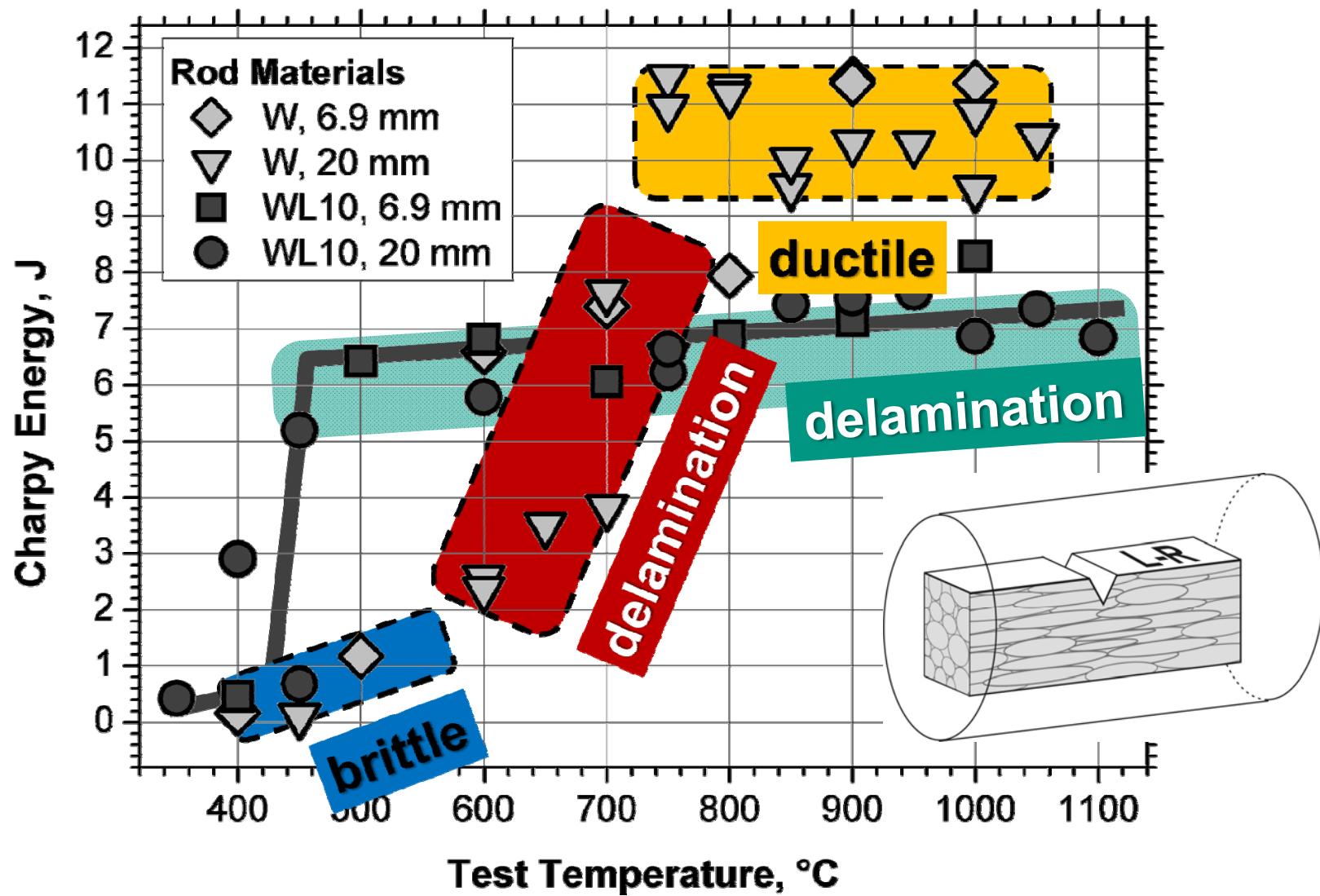
Microstructure Anisotropy

Rods

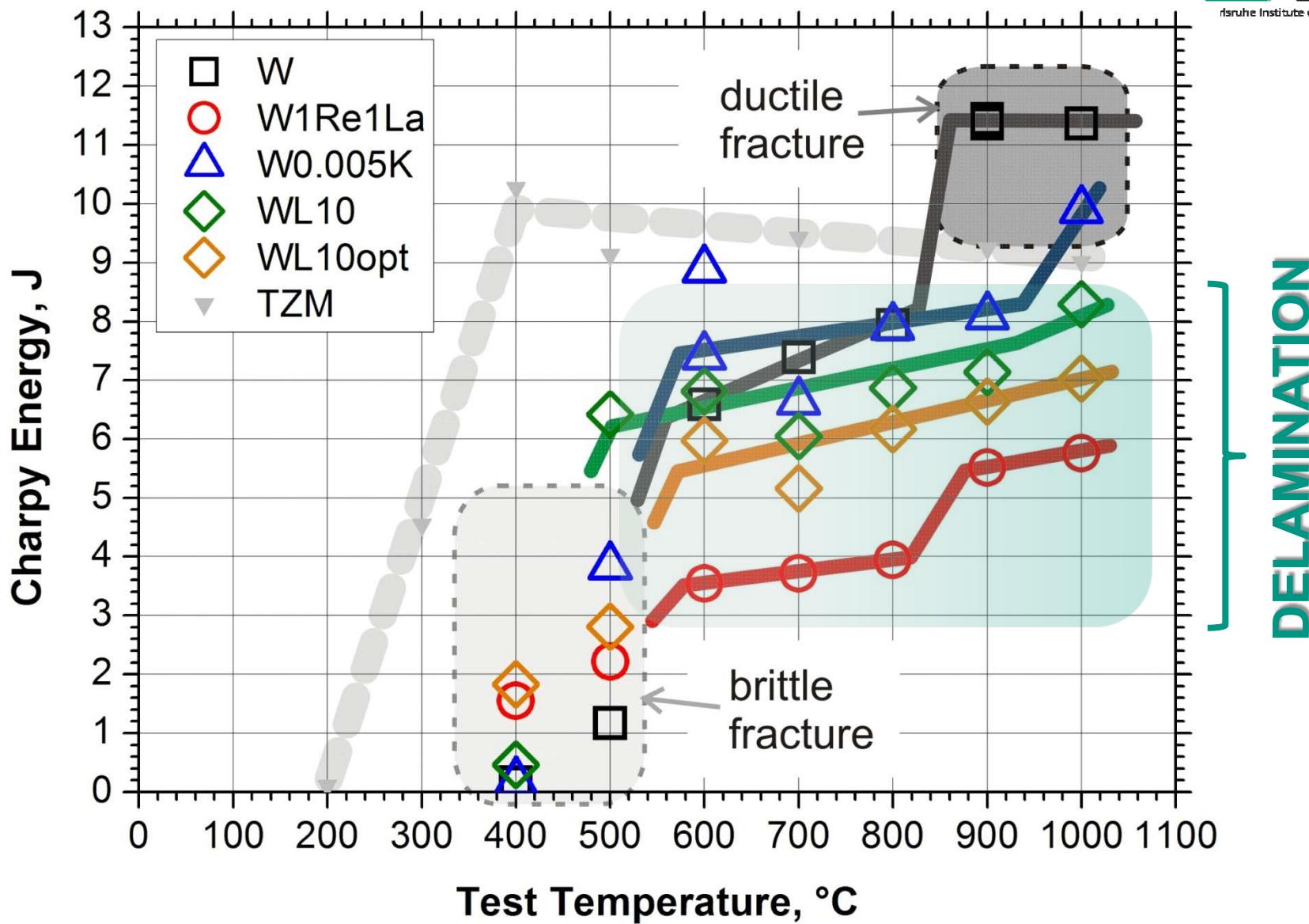


Bundle of „Fibres“

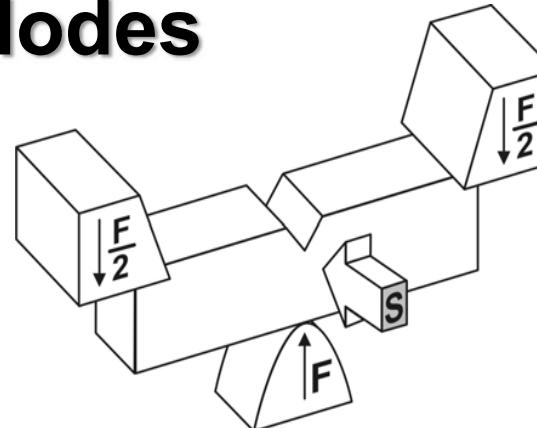
Rods: Fracture Characteristics



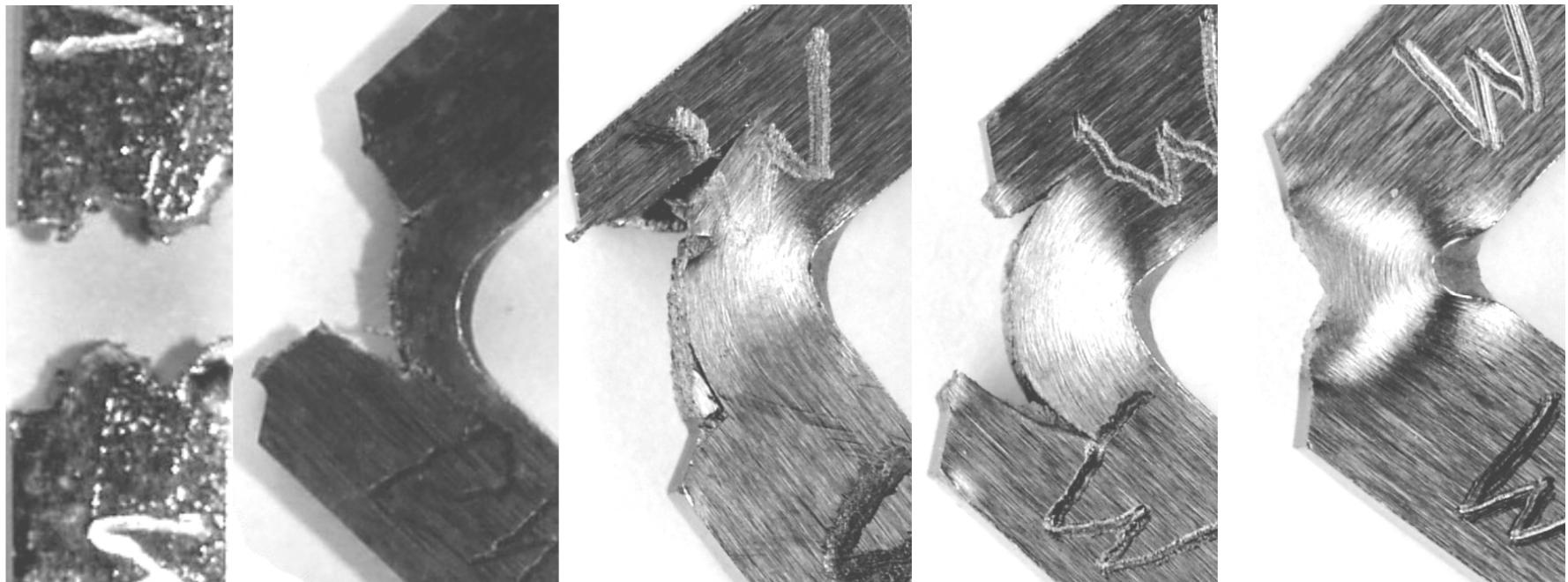
Rods: Fracture Characteristics



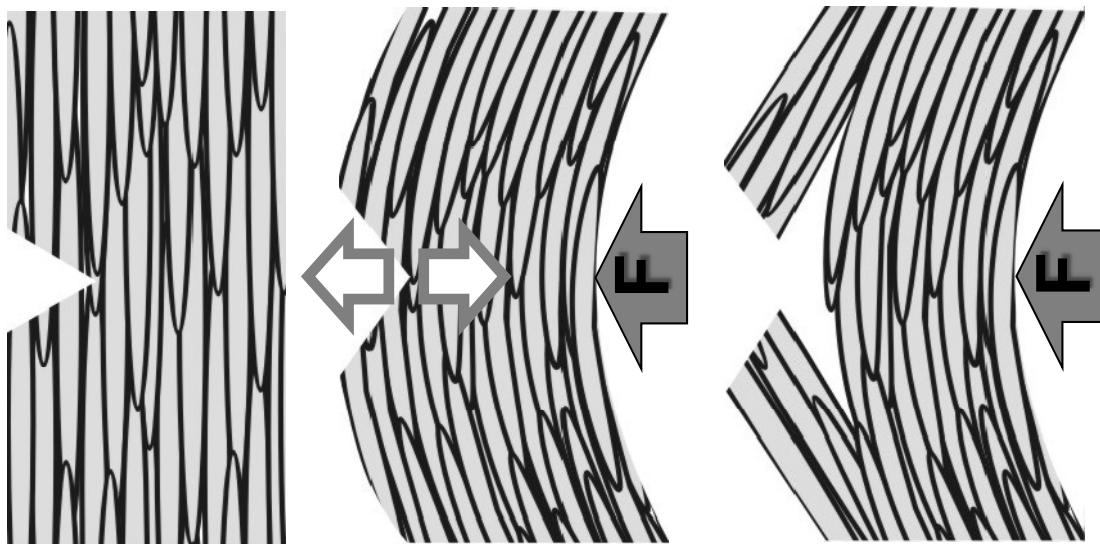
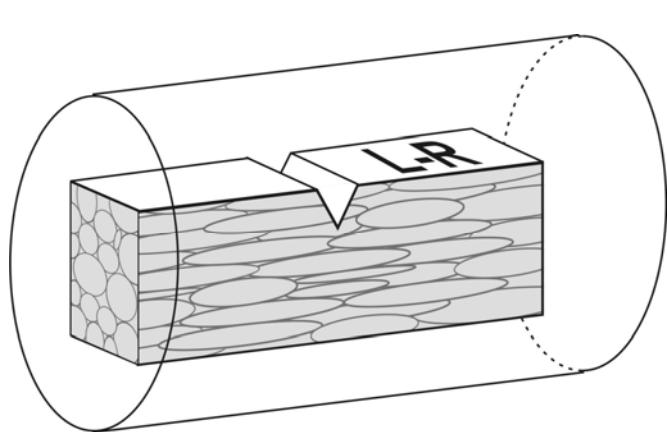
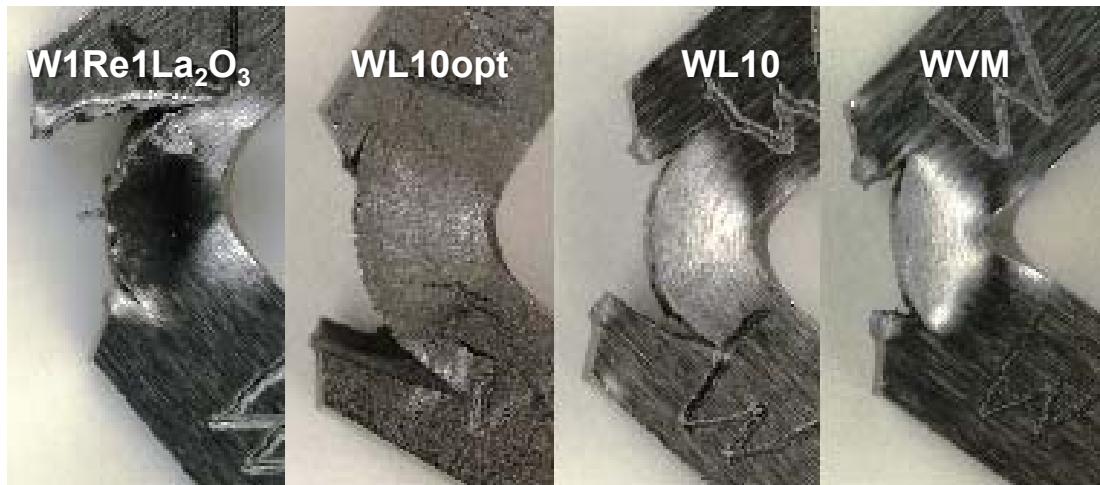
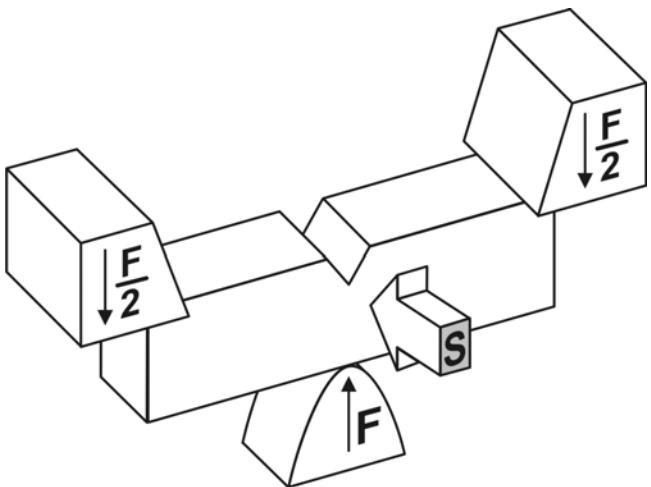
Transition of Fracture Modes



brittle → **delamination** → **ductile**

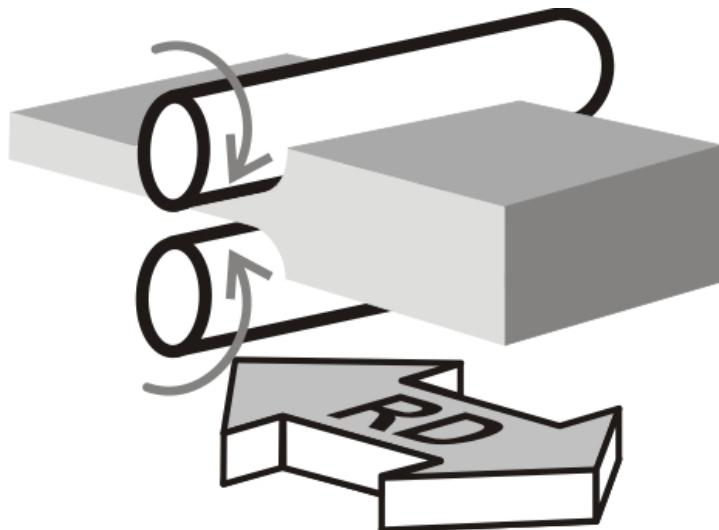


Delamination Fracture in Rods

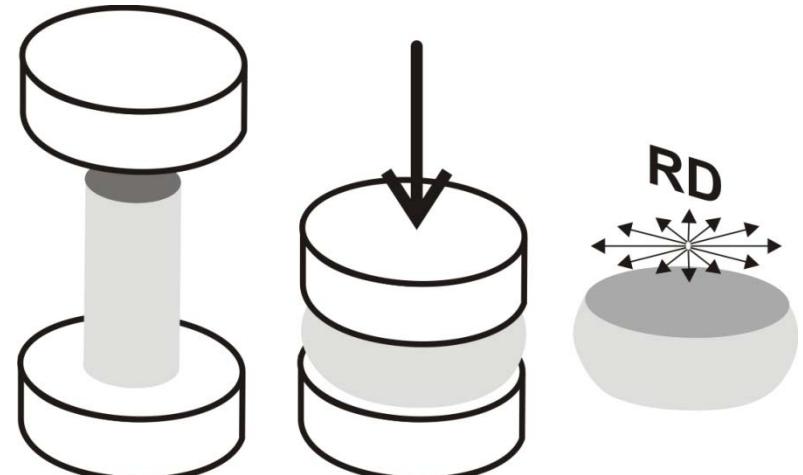


Fabrication of Half-finished Products

Rolling of Plates



Forging of Round Blanks



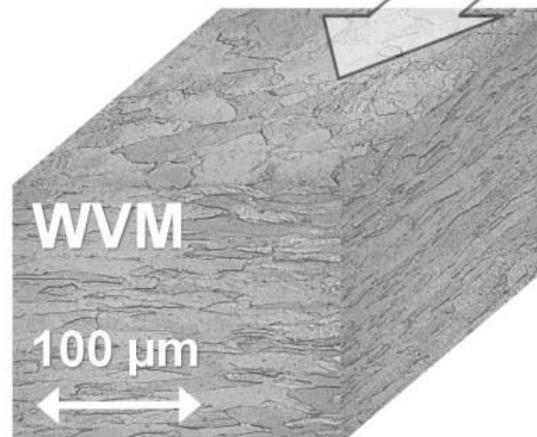
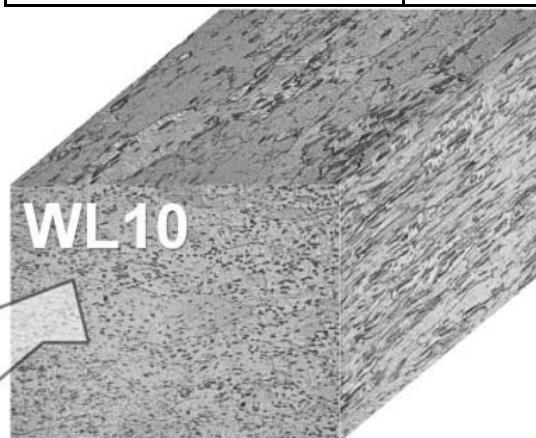
Microstructure Anisotropy

Plates: Metallography

thickness 3.6 mm 91%



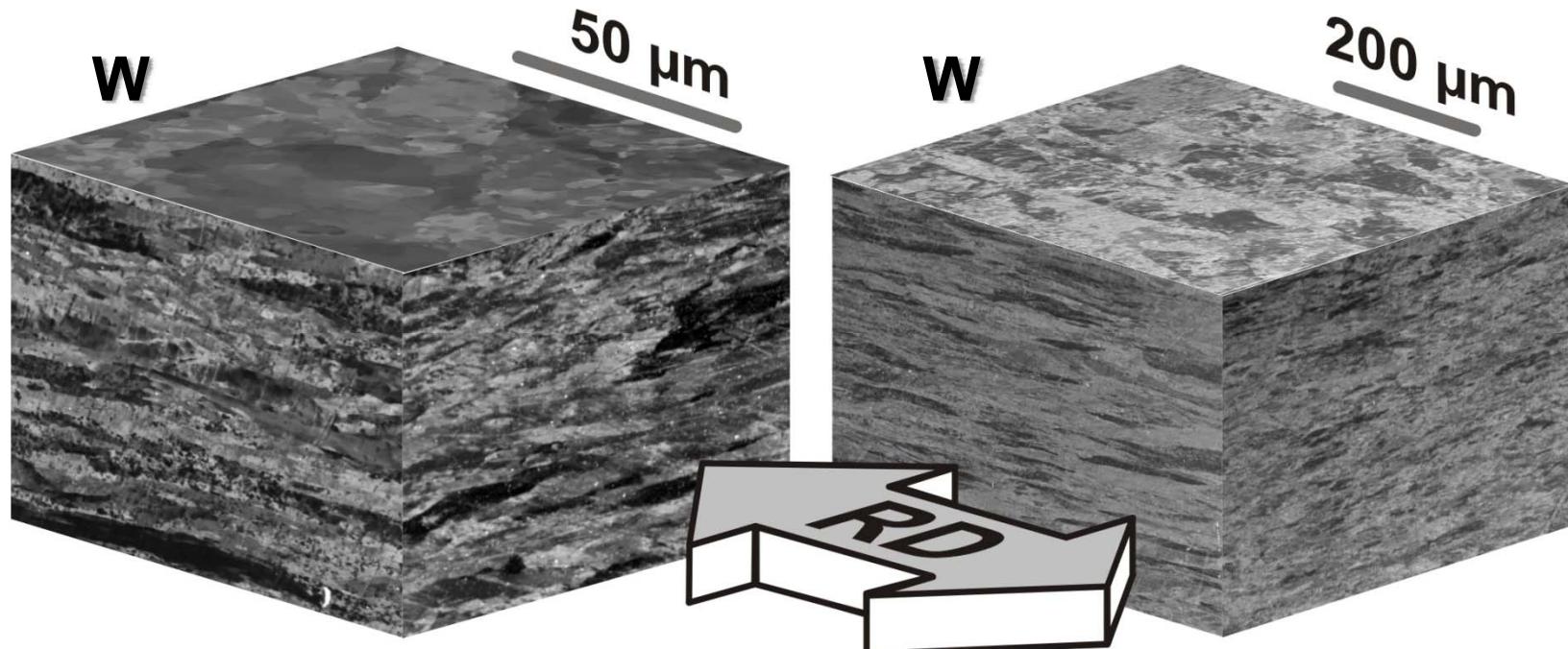
thickness 3.6 mm 91%



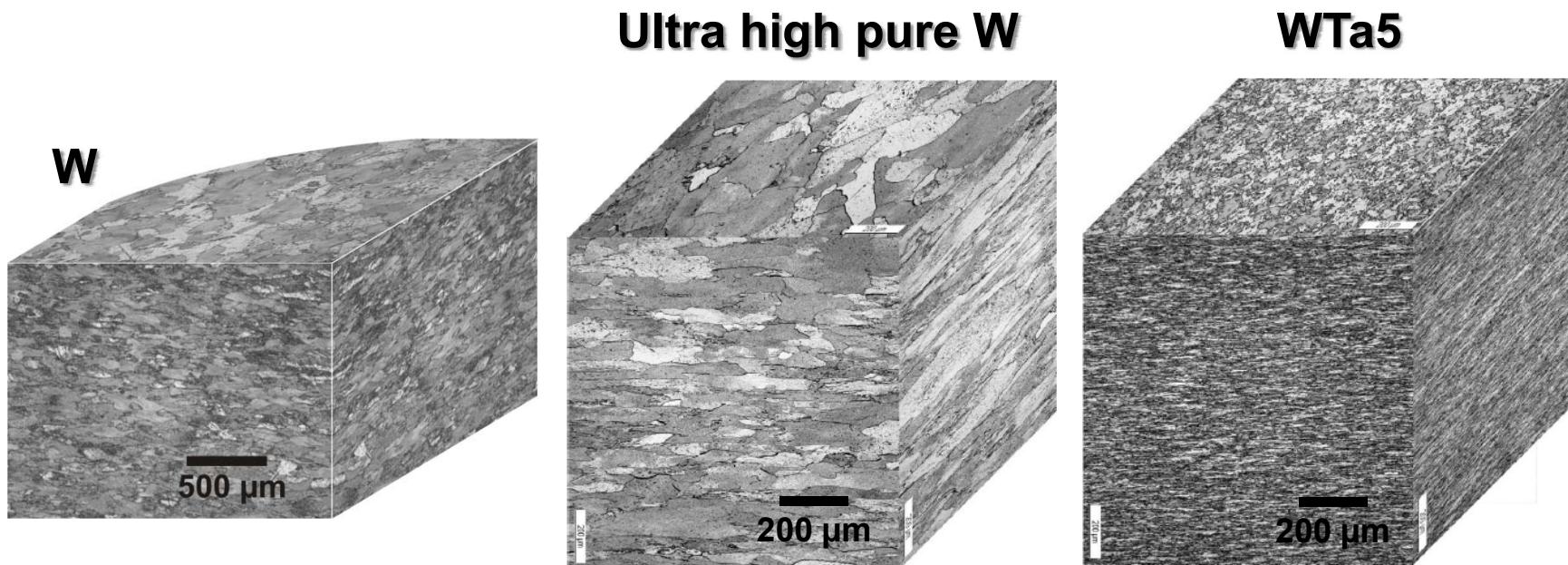
thickness 3.6 mm 91%

Microstructure Anisotropy

Plates: SEM / FIB channeling effect

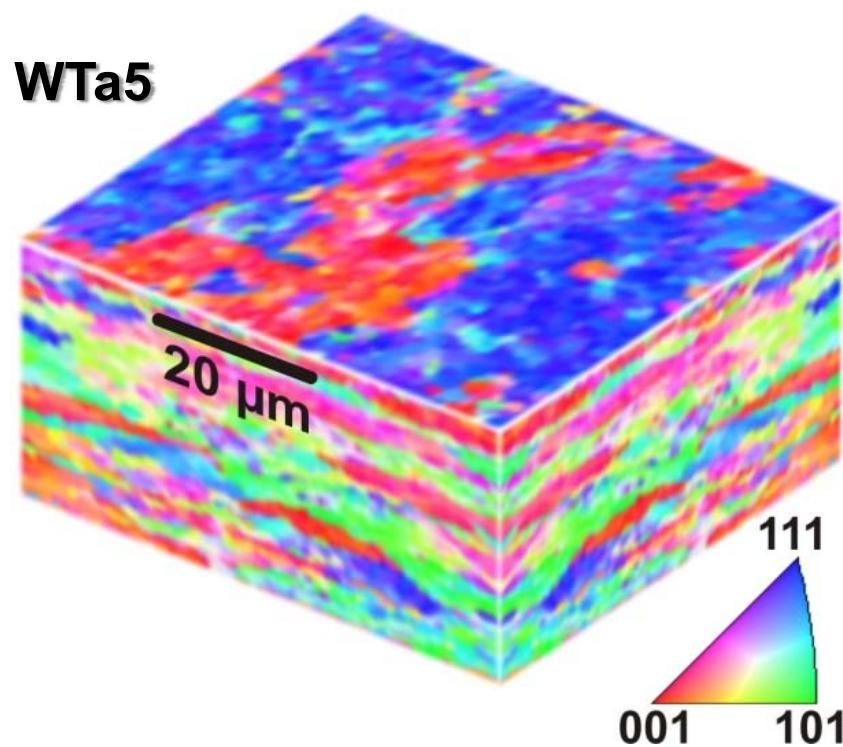


Round Blanks: Metallography



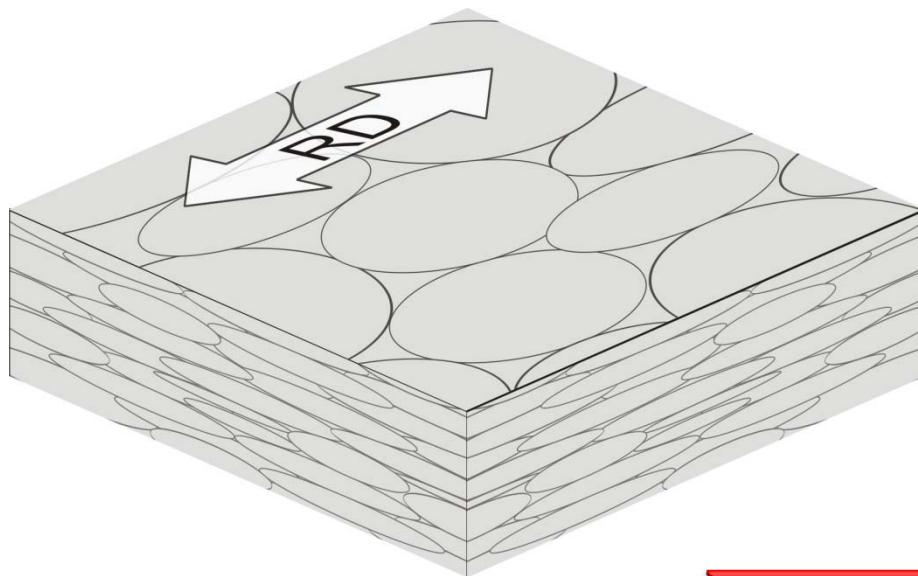
Microstructure Anisotropy

Round Blanks: EBSD

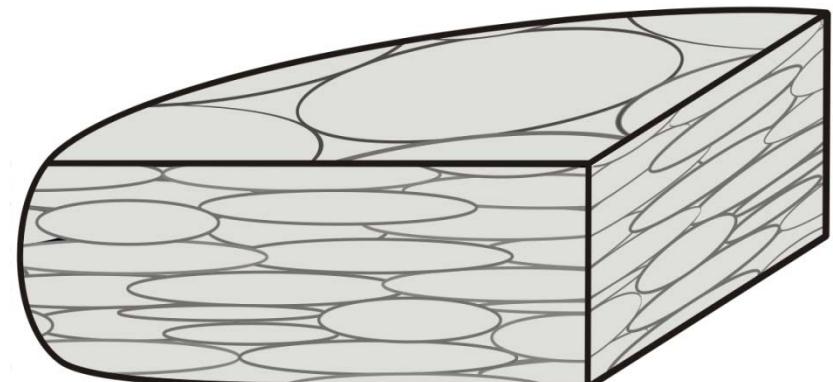


Microstructure Anisotropy

Plates



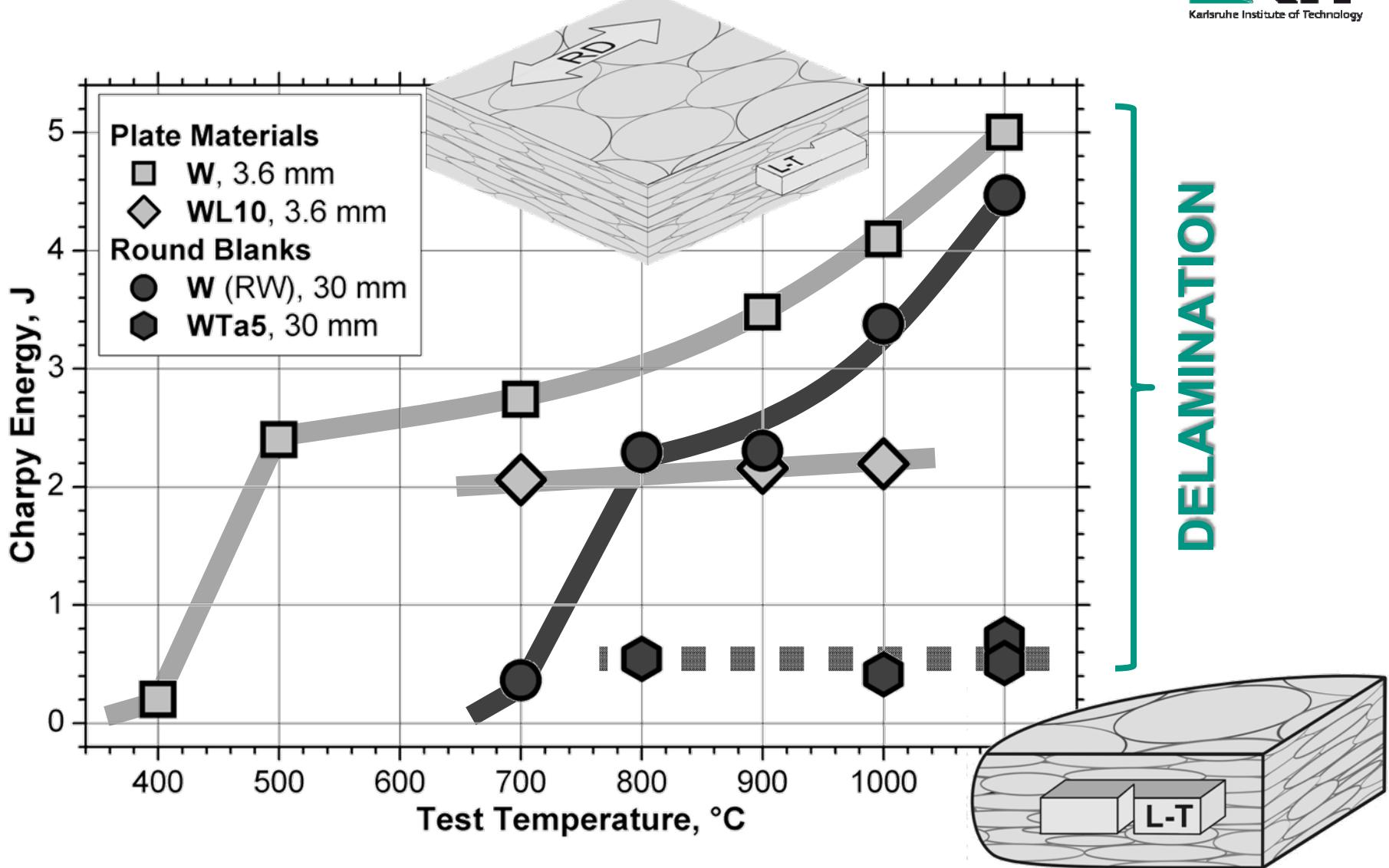
Round Blanks



Stack of „Pancakes“

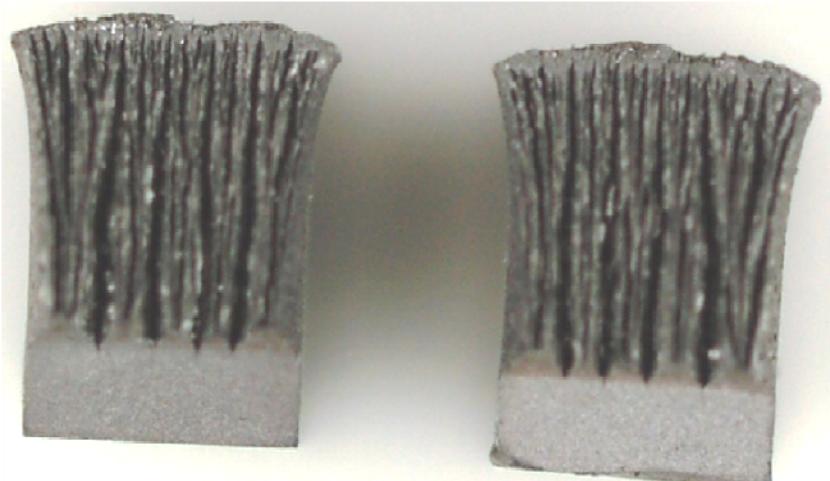


Charpy Tests, Plate Materials

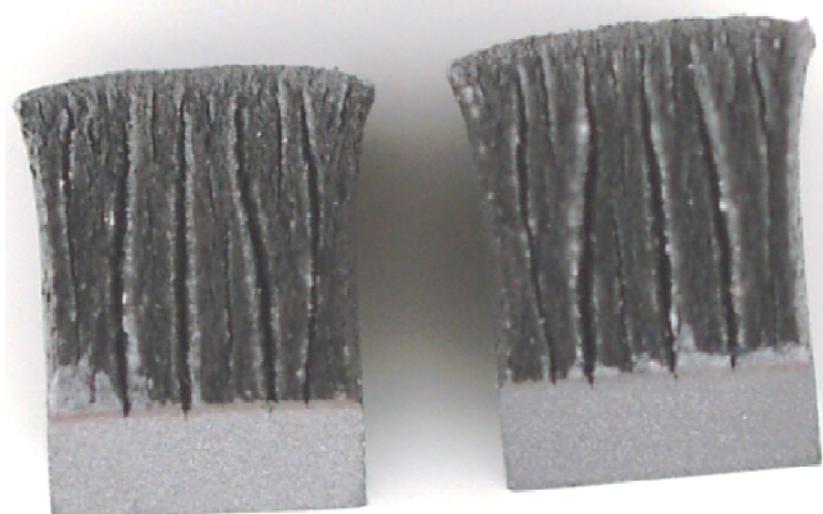


Fracture: W & WL10, plates

W

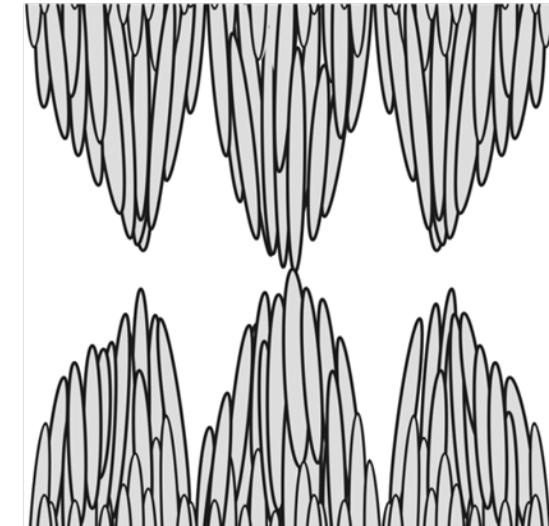
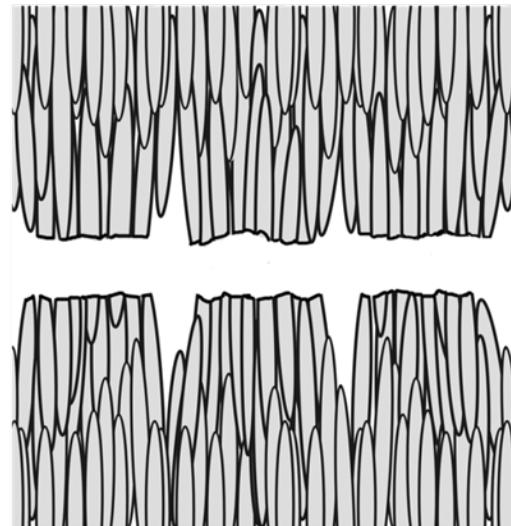
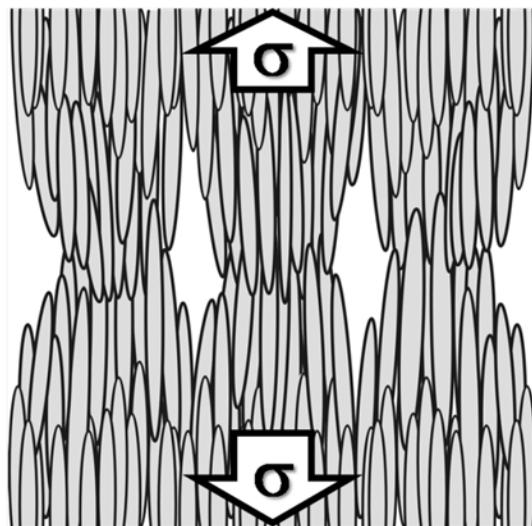
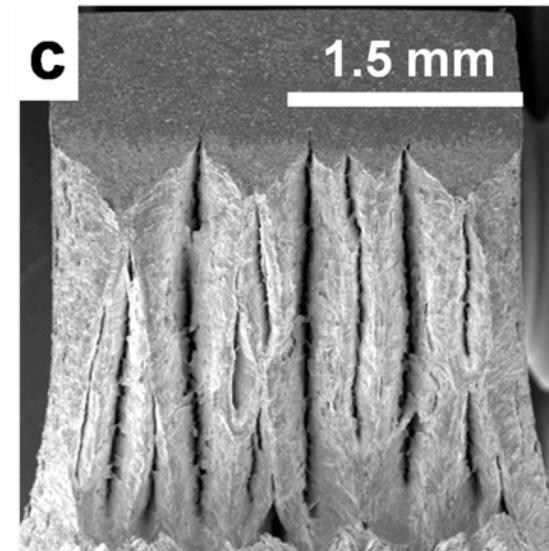
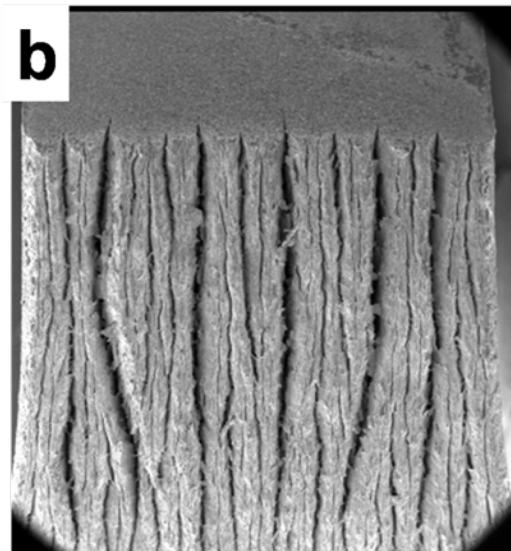
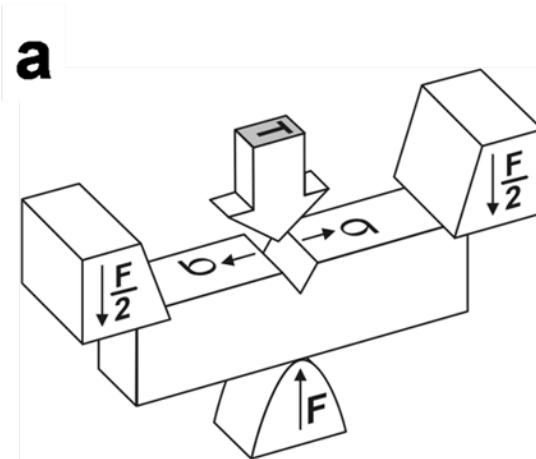


WL10



Tested at 1000 °C !!!

Delamination Fracture in Plates



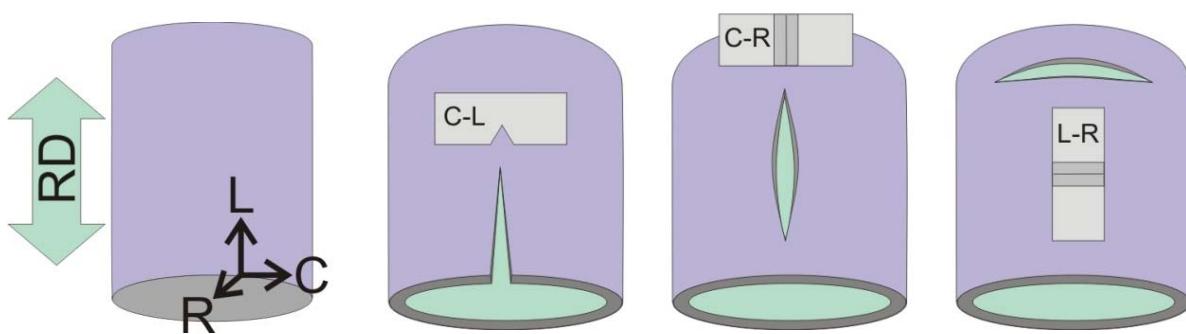
Important Conclusions for HHFCs

- Plates delaminate at all temperatures
- Higher deformation degree improves D-Delam.-TT
- Oxide particles (and K doping) promote delamination
- Microcracks (by EDM) promote delamination
- Notches, edges, grooves, etc. promote delamination

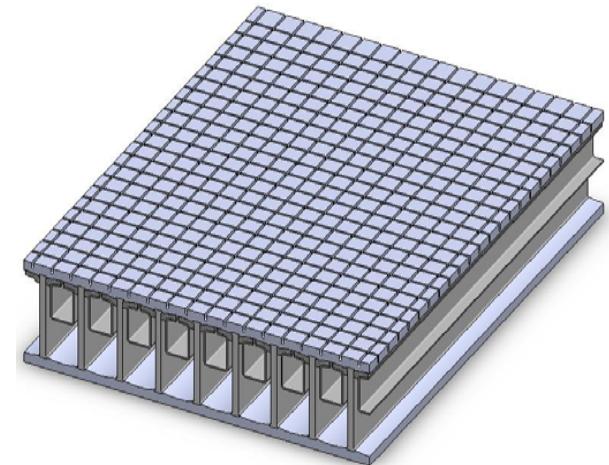
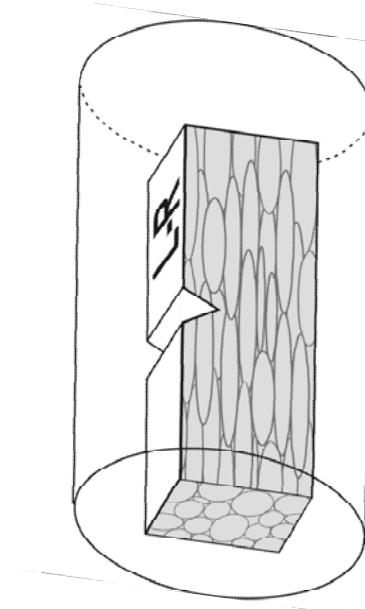
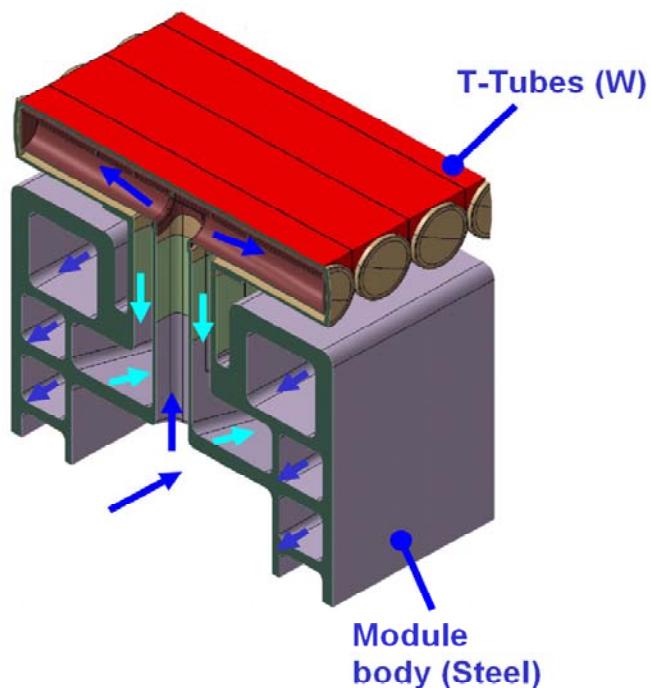
In other words:

- ➔ Use highly deformed W rod material
- ➔ Produce parts with flat surfaces, fabricated by milling, sawing, turning (avoid EDM!)

But how to fabricate divertor parts?



→ J. Reiser et al., FZK



Problem of Microstructure Orientation



Pipe Impact Test

→ B. Dafferner, P. Norajitra,
M. Rieth, 2010



**... and that's only one reason why
DEMO is so challenging!**



THANKS

for your interest