

Ex-vessel Fuel Coolant Interaction Experiment in the DISCO Facility

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- Experiment in the DISCO facility, similar to those made for Direct Containment Heating (DCH), but with **water in the pit**, that would give **data for the validation of the codes** in geometrical situation closer to the reactor ones than all other available data
- No triggered steam explosion, only premixing stage is investigated (but possibility of spontaneous explosion)

Relevance for SARNET2

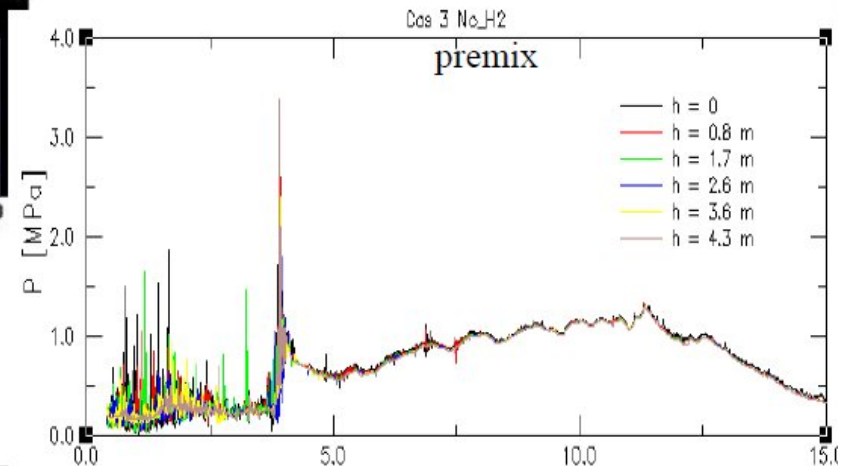
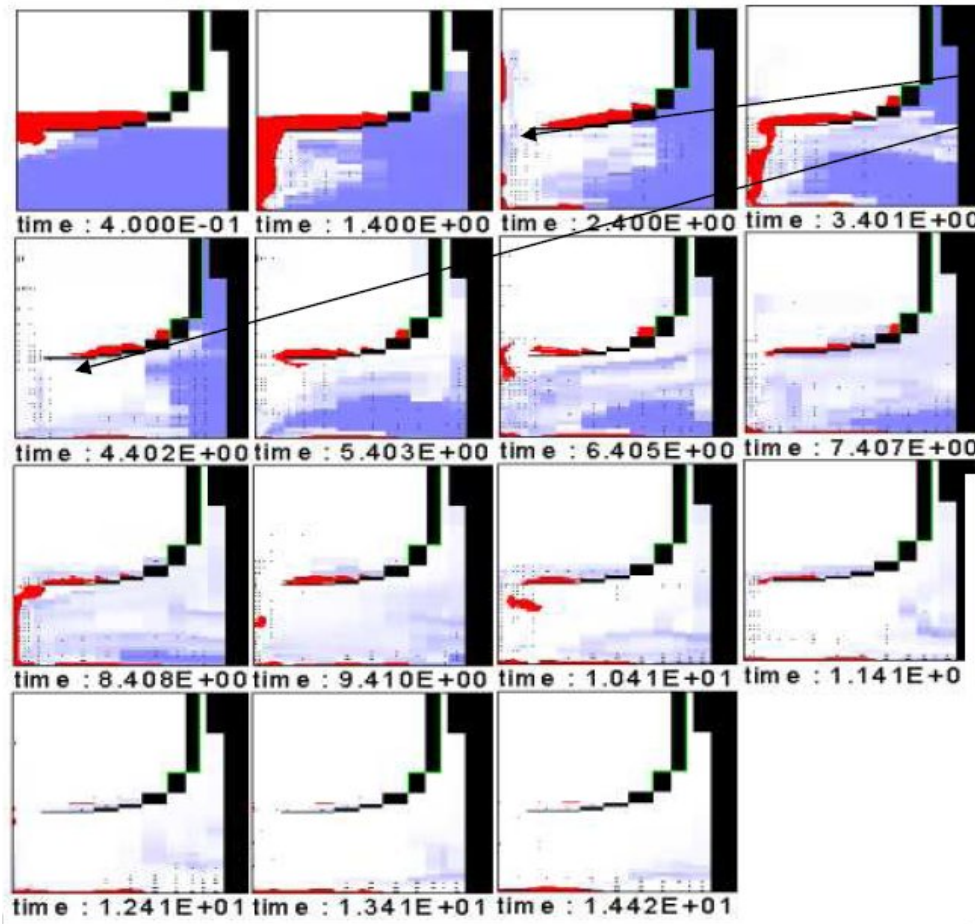
- Ex-vessel Fuel Coolant Interaction (WP 7.1) and debris formation (WP 5.3) are two high-priority issues of SARNET2. Despite the importance of these issues, only a few experimental data are available for the qualification of codes.

- Database for premixing modeling assessment for application of ex-vessel situation is very limited
 - Water subcooling (~50 K)
 - High temperature
 - High density
 - No way to assess the behavior with existing database
 - FARO L31 (ISPRA): 100 kg UO₂/ZrO₂ (gravity driven)
 - TROI-VISU (KAERI, SERENA): 15 kg UO₂/ZrO₂ (gravity driven)
- ***Behavior is not as expected from “classical” FCI experiments***
 - Jet fragmentation with small fragments compared to TROI or FARO, even at low melt vessel pressure
 - Due to water inertia and small flow area around vessel
 - No escape for pressure
 - Vapor film around the jet is unstable
- ***Purpose is to check the code evaluation of fragmentation in more “reactor-like” configuration***



Vessel pressure [b]	2
Breach diameter [m]	0.7
Sub-cooling [K]	50
Water height [m]	4
Corium Super-heat	200

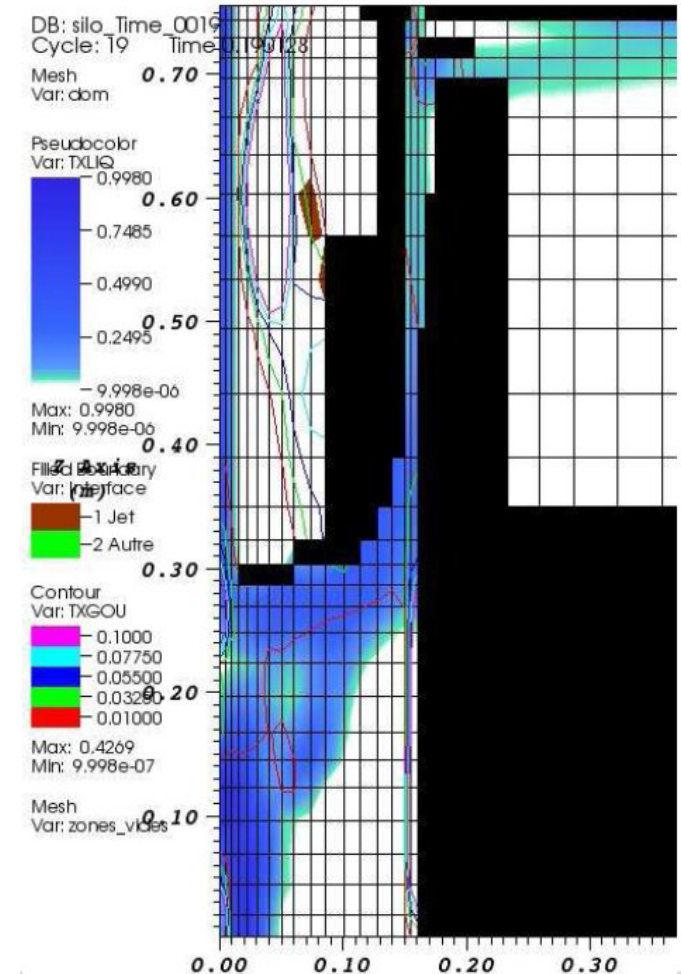
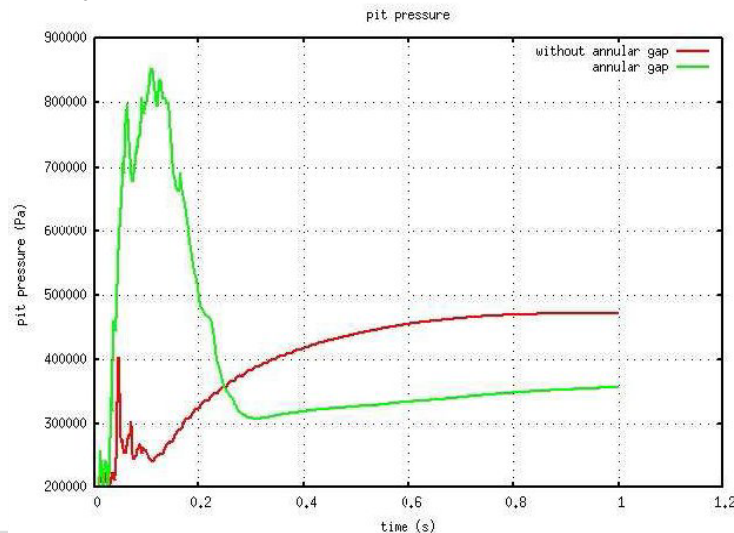
- 2 typical behaviors:
 - $P_{pit} > P_{vessel}$ then strong potential interaction
 - High tendency to sweep out water and large part of melt



- Investigating the fragmentation processes and subsequent phenomena occurring consecutively to the break of the vessel and melt ejection

- Information will be useful for several SARNET2 WPs:
 - Melt fragmentation processes for high velocity melt jets through a precise analysis of the size of the debris found (WP7.1, WP5.3)
 - Pressurization of the pit and containment during the mixing (WP7.1)
 - Debris bed characteristics important for coolability: shape, porosity, debris size distribution (WP5.3)
 - Melt and water dispersion out of the pit during the process: initial conditions for MCCI (WP6)
 - Oxidation of the iron to be compared with cases without water: impact of water on DCH (WP7.1)
 - Hydrogen production and potential impact of water for combustion (WP7.2)

- Calculations with rough mesh
- Strong interaction in most cases due to Pit pressure > Vessel pressure
- Water + melt flow back into the vessel
- Not possible to pour all the corium
- Weakest interaction for larger annular section
- But very fast dispersion of melt

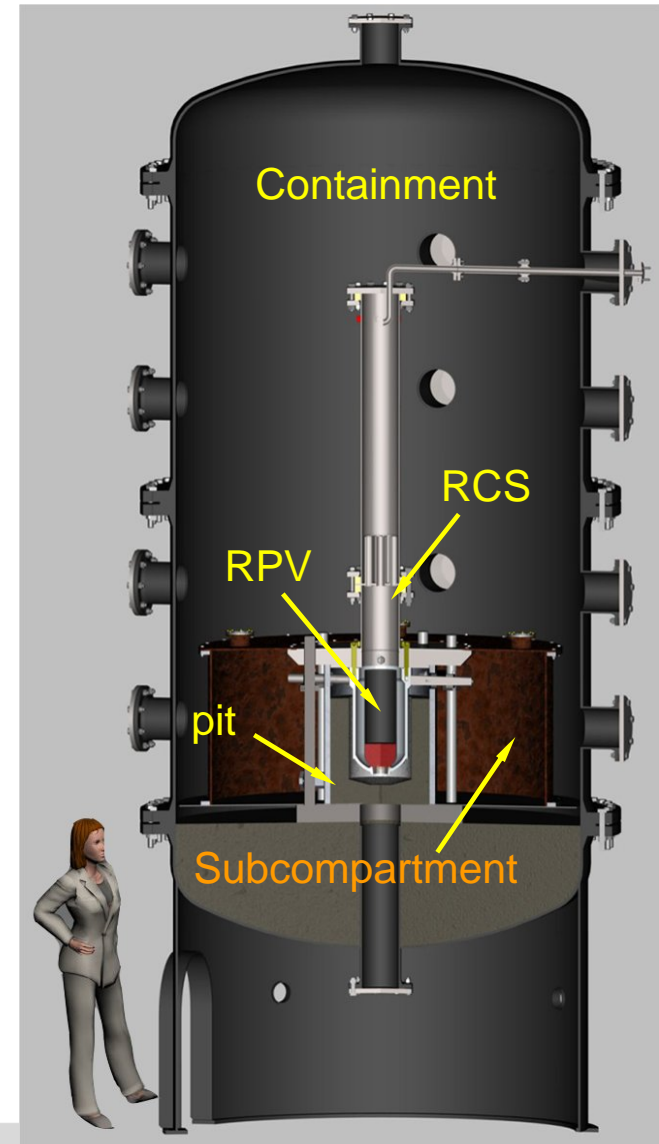


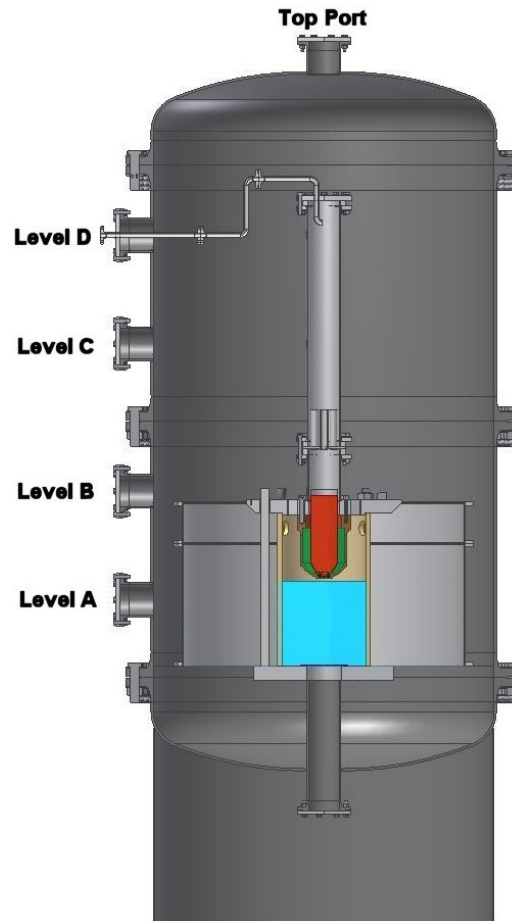
■ Tests with

- Scale 1:18 (EPR)
- Iron-alumina melt (2400 K)
- Steam (10-20 bar)
- Air-steam-hydrogen atmosphere
- Production and combustion of hydrogen

■ Measurements of

- Pressures (15)
- Gas temperatures (22)
- Hydrogen production and combustion (gas samples)
- Melt dispersal fractions
- Video cameras (4)

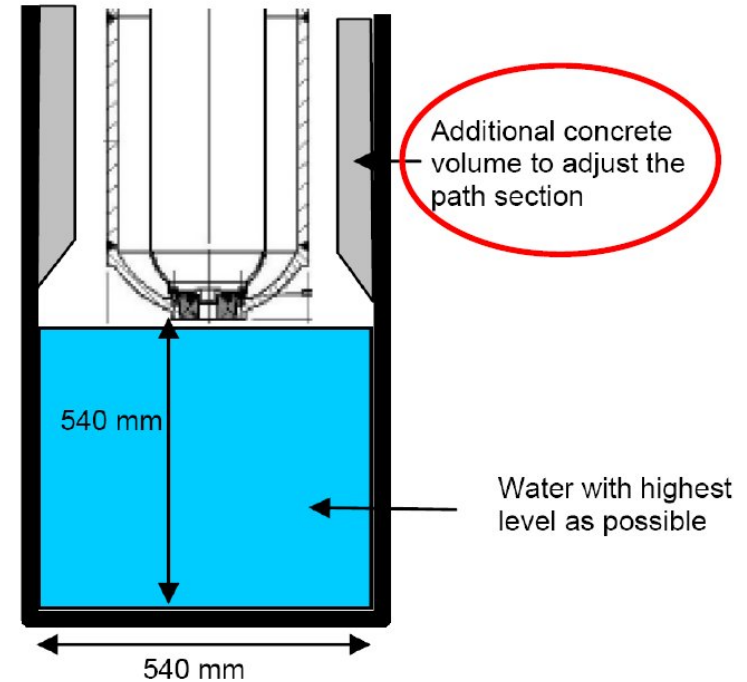


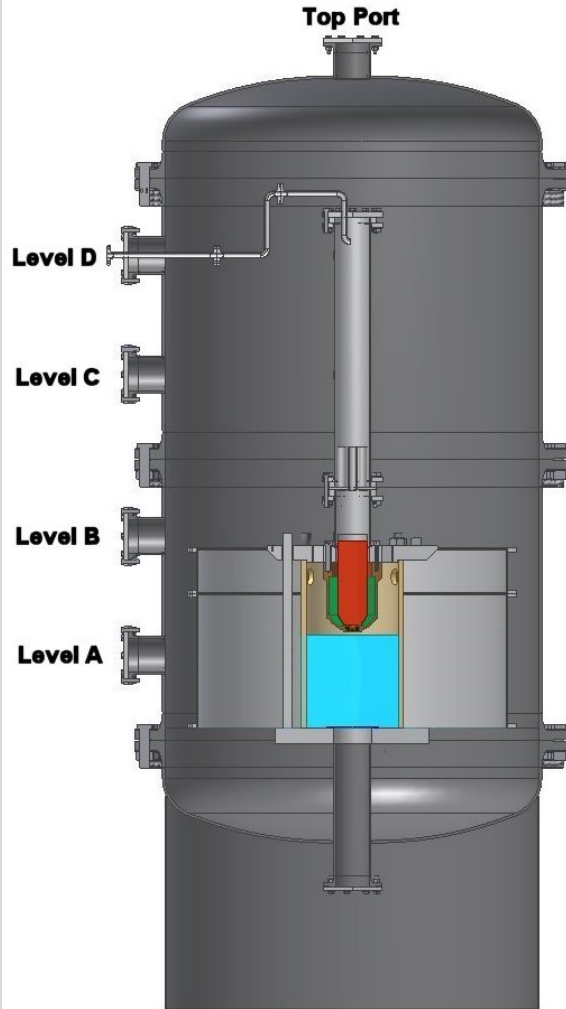


$$V_{\text{melt}} = 0.0026 \text{ m}^3$$

$$V_{\text{water}} = 0.125 \text{ m}^3$$

$$V_w/V_m = 48$$





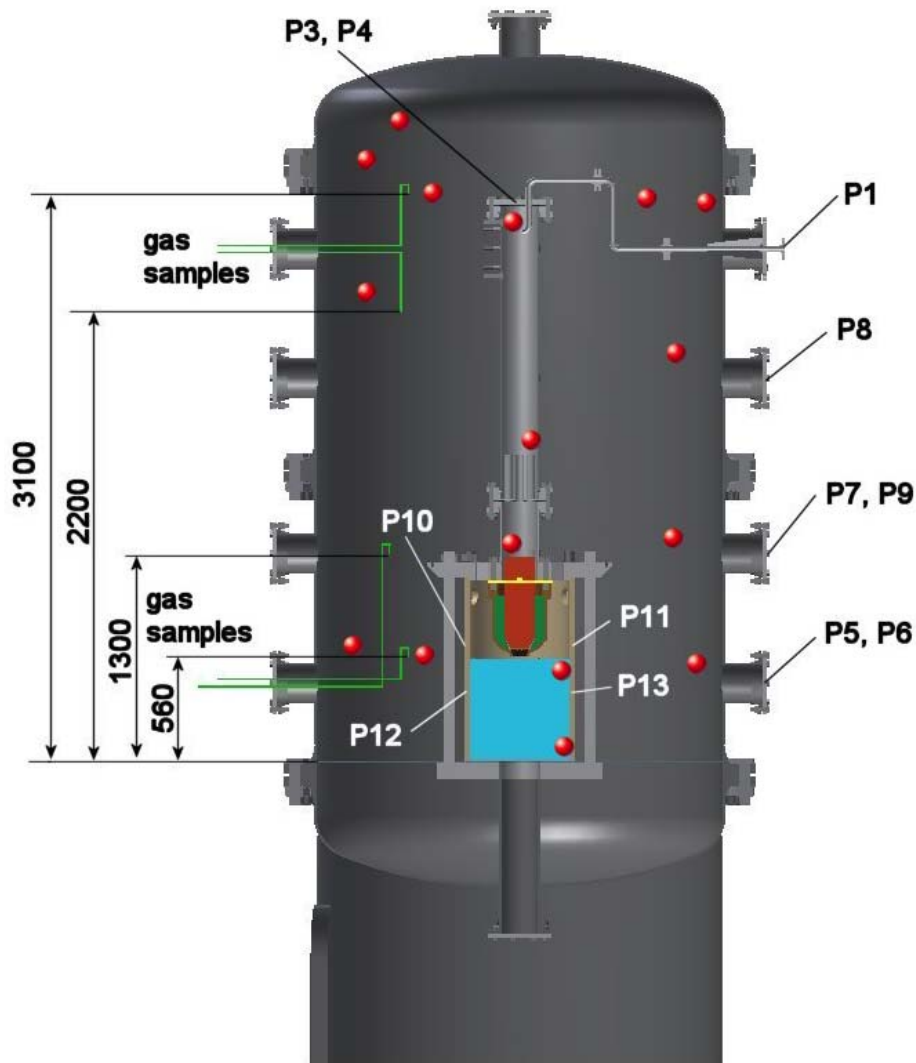
No specific reference to a particular reactor, so simplifications for code calculations and analysis

- Symmetric reactor pit, no access: 2D calculations
- Subcompartment without cover plates
- Reactor pit circumferential exits (8) without main cooling lines
- Open flow paths from pit to containment
- Height and diameter of the water pool in the cavity both as high as possible to limit scaling effects: 540 mm
- Distance between lower edge of the RPV and water level: 20 mm
- Temperature of the water: 85 °C

Geometry and initial conditions

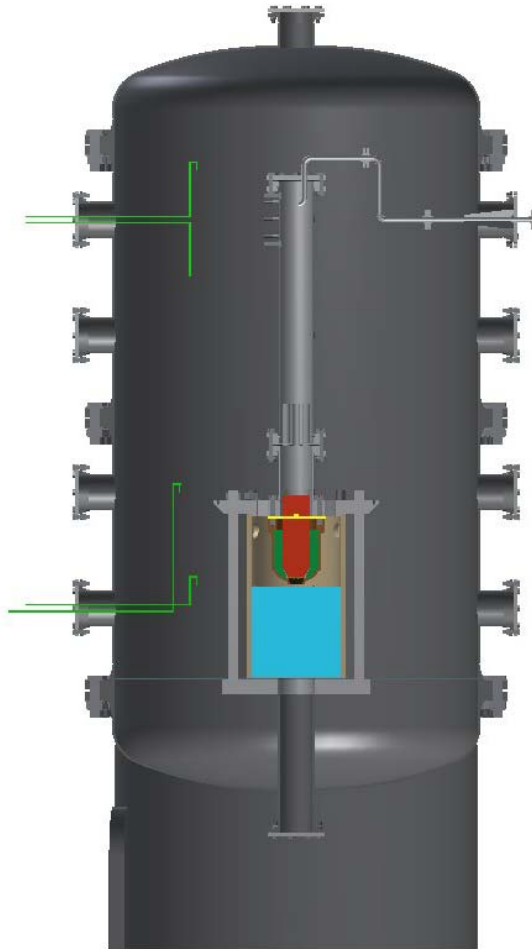
CON: Volume	m ³	13,88
CON: Height	m	4.5
CON: Diameter	m	2.17
Cavity: Volume	m ²	0.2034
Cavity: Height	m	0.984
Cavity: Diameter	m	0.540
Flow nozzles (8x cut out area)	m ²	0.0603
Flow area into con. (8 holes)	m ²	0.0688

CON: Pressure	MPa	0.2
CON: Temperature	°C	100
CON: Atmosphere	-	Air/Steam
RPV: Breach diameter	mm	30
RPV: Driving pressure	MPa	0.6
RPV: Amount of thermite	kg	10.64
Water pool	l / °C	125 / 85



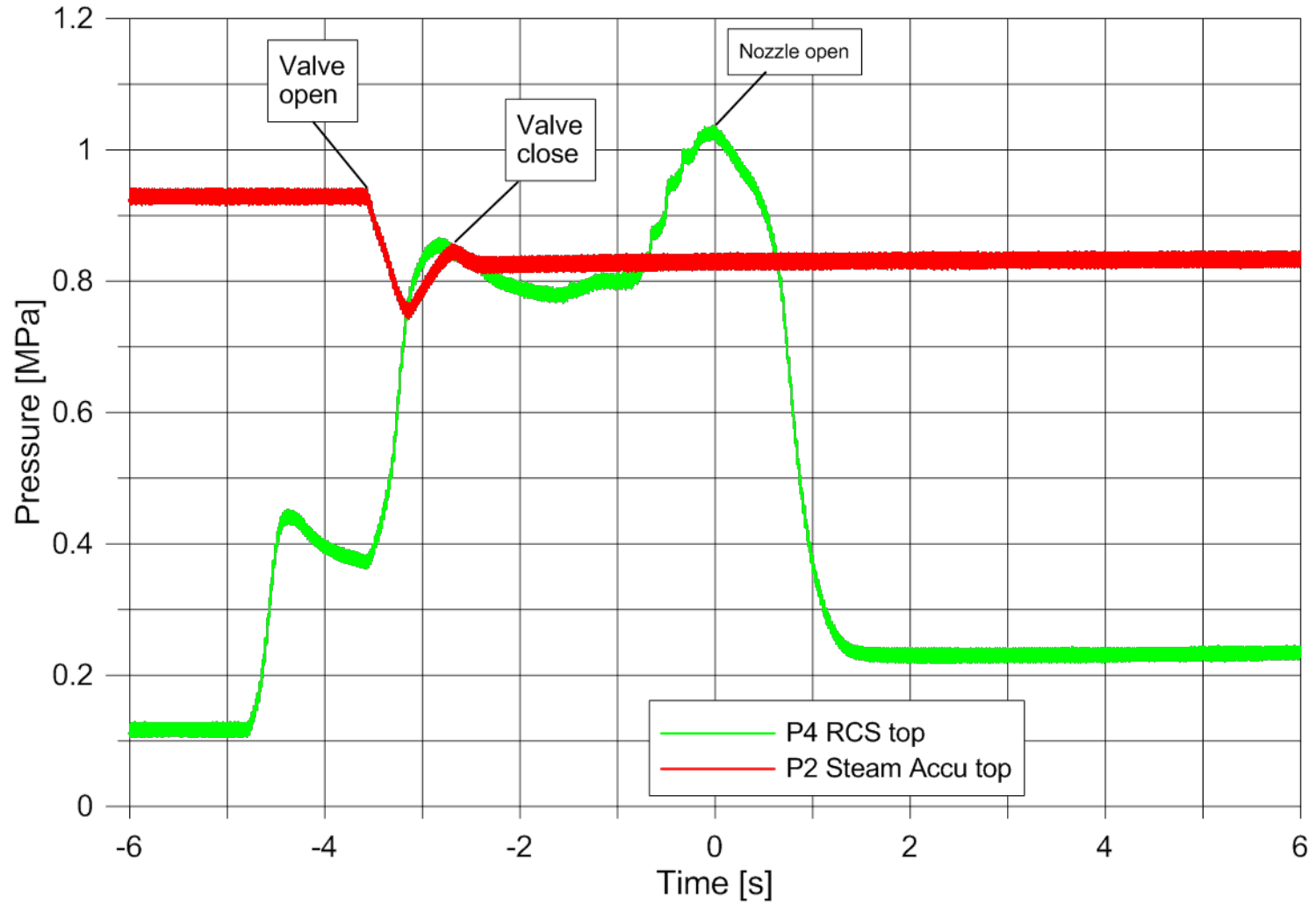
- 5 pressure transducers at reactor pit, sampling rate >2 kHz
- 3 transducers below water level, range: 1.7, 3.5, 30 MPa
- 2 transducers above water level, range: 3.5, 3.5 MPa
- Thermocouples in containment, subcompartment, RCS and RPV
- Pre and post test analysis of gas samples in containment
- Collecting of the melt debris and sieve analysis

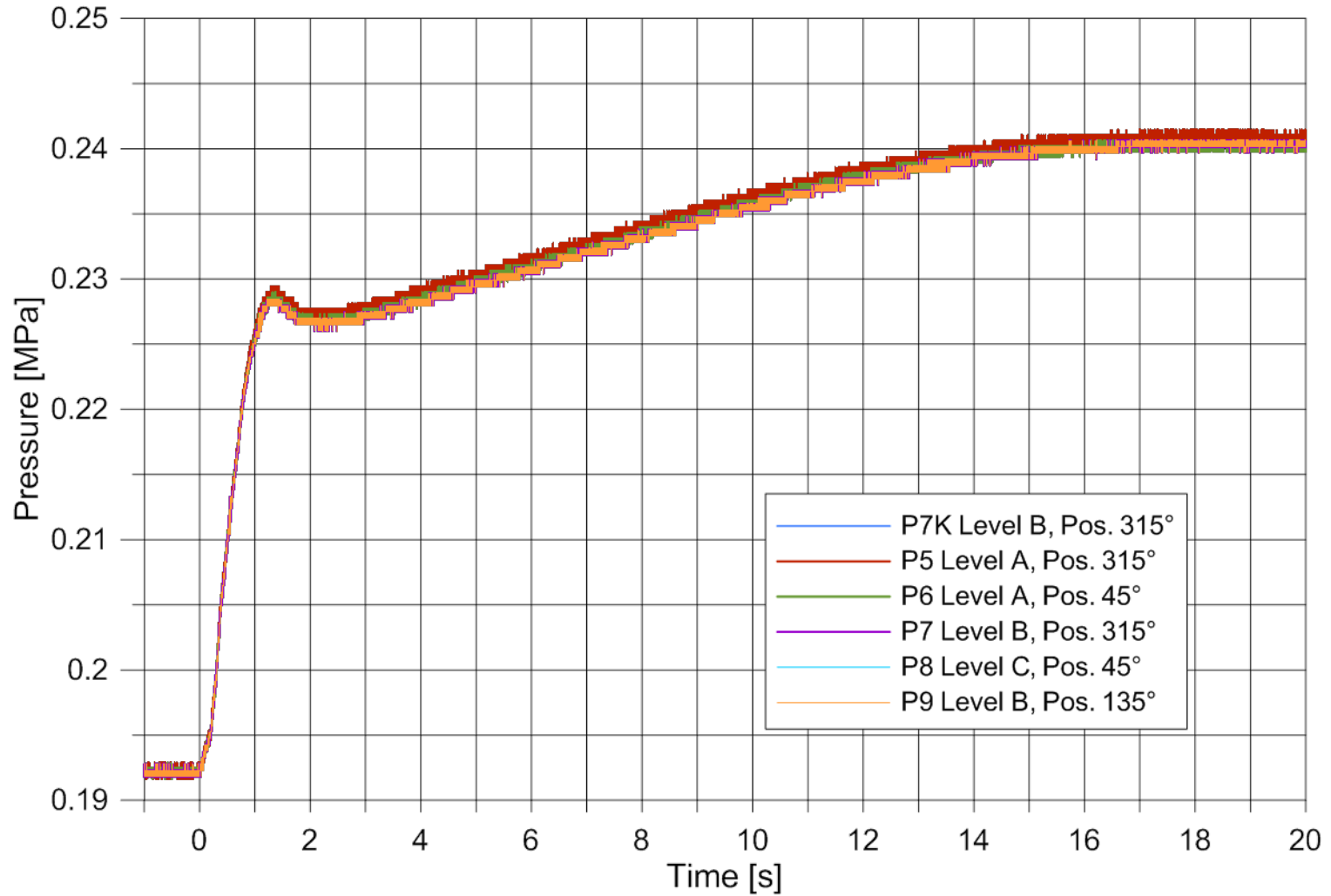
Test procedure

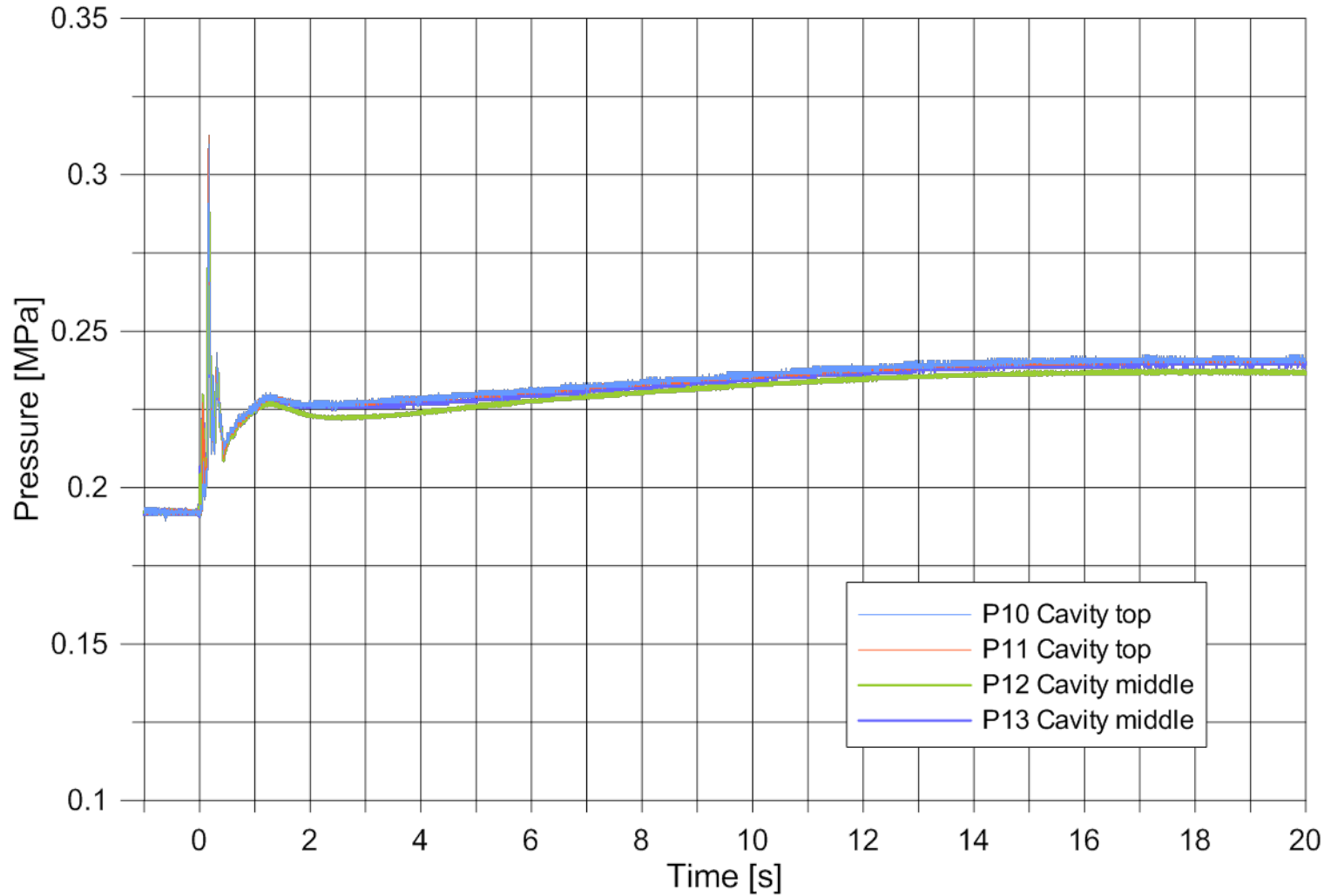


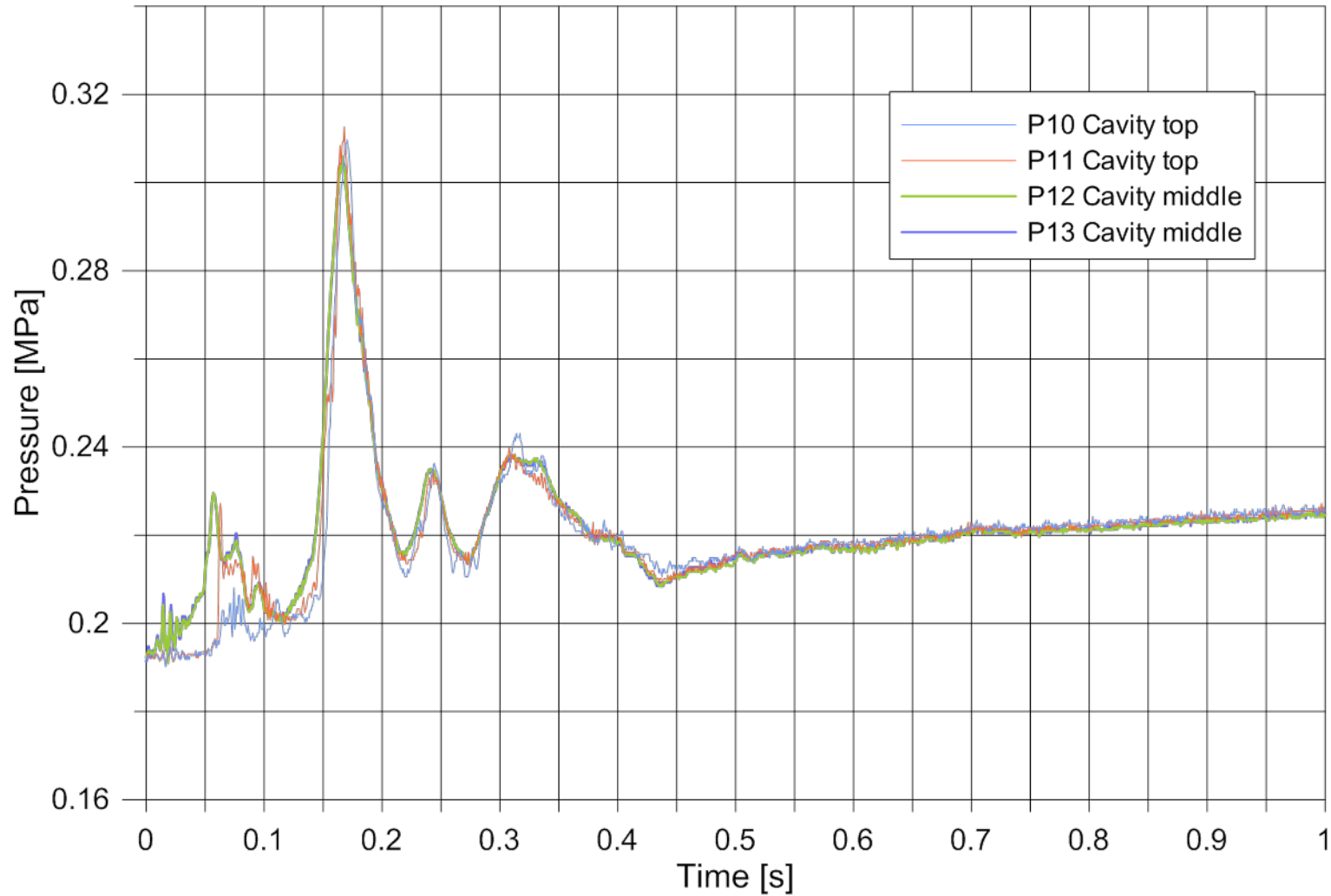
- Containment (steam, press, temp)
- Loading steam accumulator
- Water pool
- Gas sample
- Ignition (trigger: temp, press)
- Steam valve open (1 s)
- Melt plug (brass)
- Discharge of melt
 - increase temp, press
 - hydrogen burning
- Gas sample
- Collecting of particles

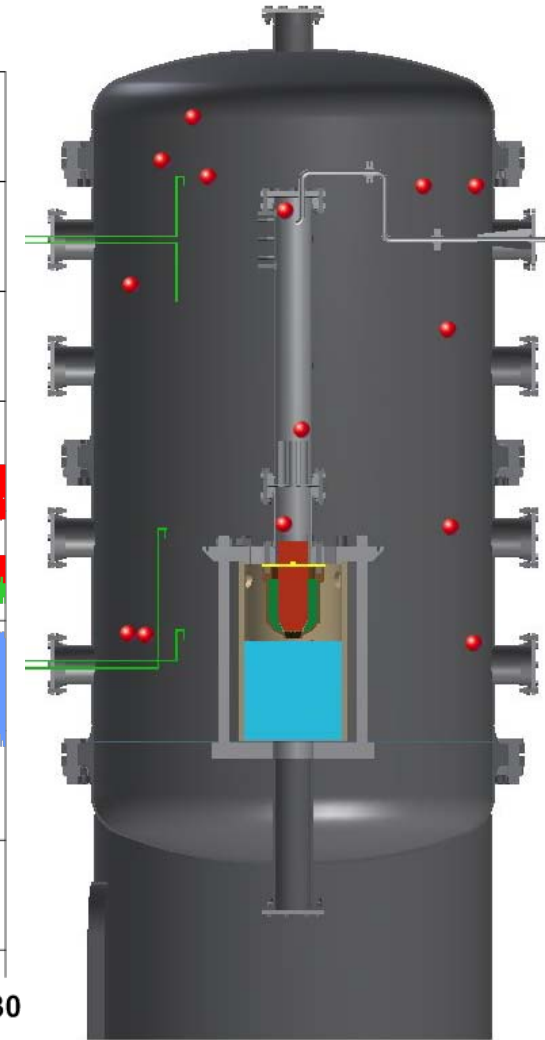
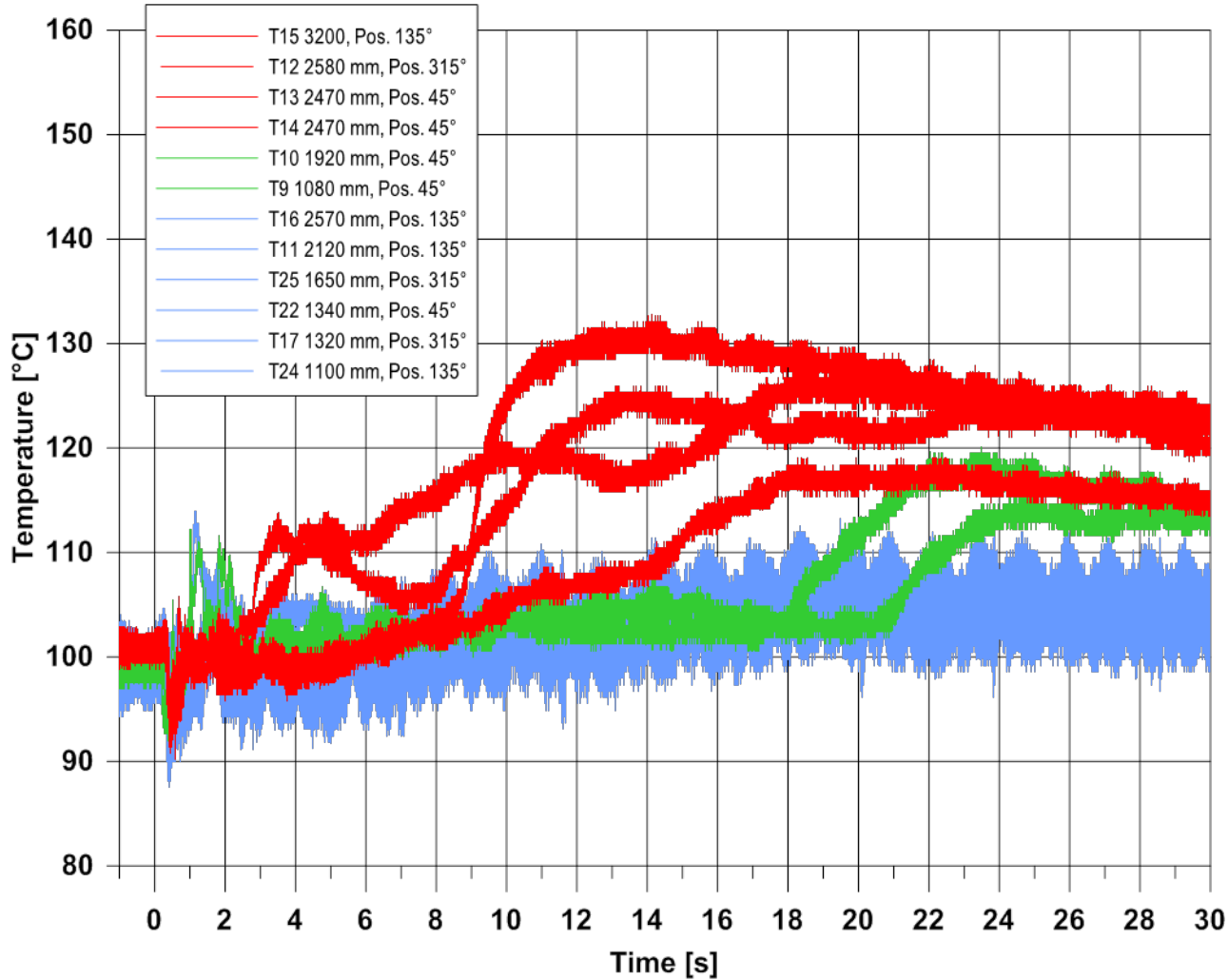
Pressures Steam Accumulator and RPV

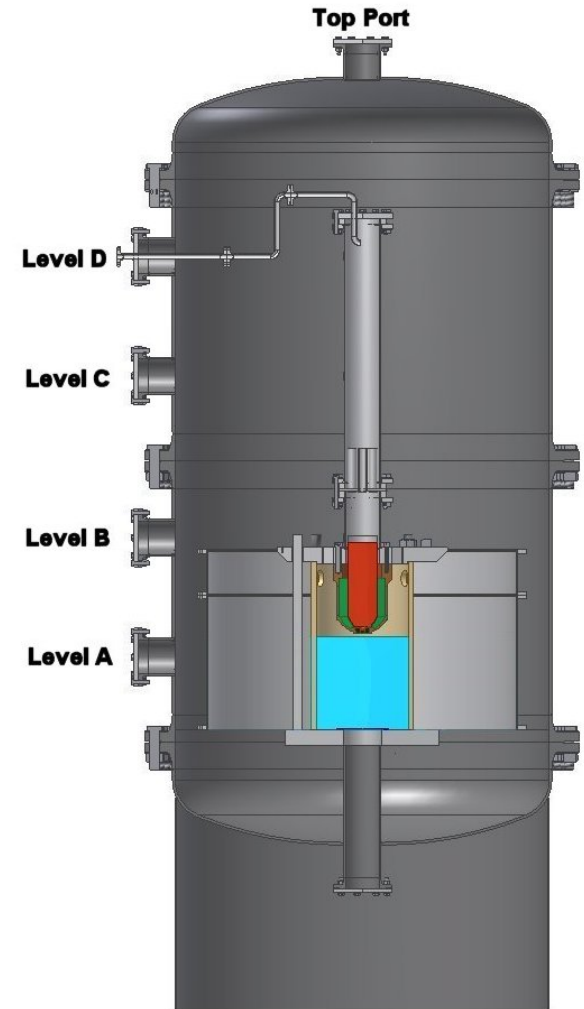
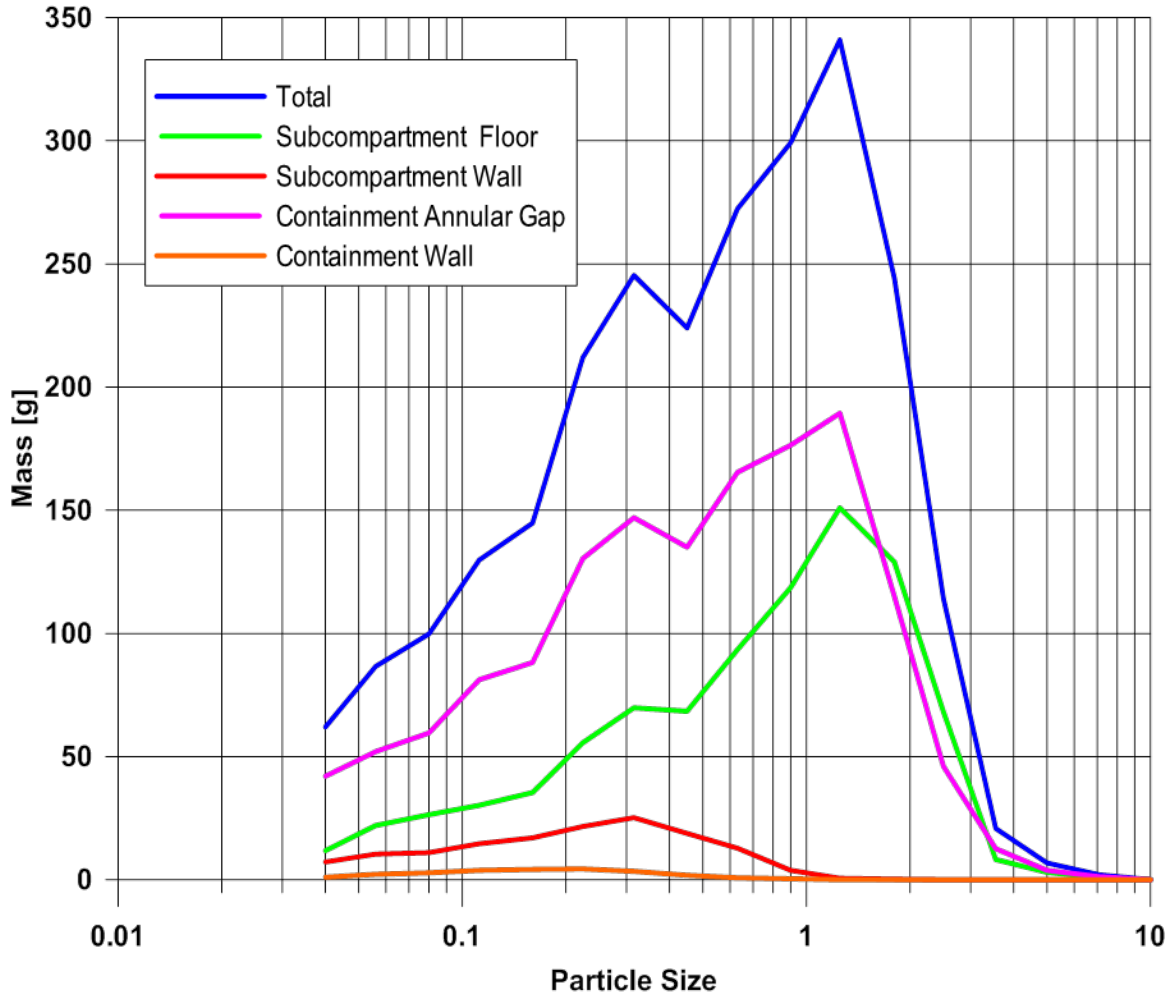




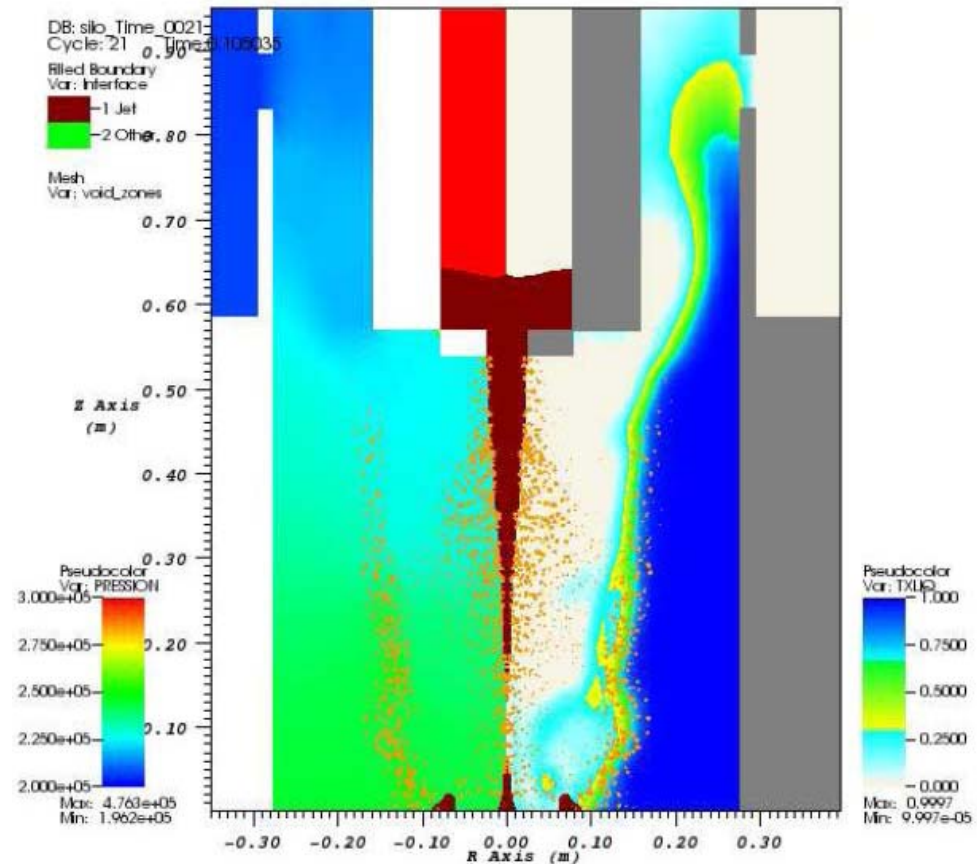








- Simplified vessel geometry but refined mesh
 - High sensitivity of jet fragmentation when water contacts the jet
 - Important work of analysis
 - Some 2D sloshing effect
 - 3D to be investigated
 - Generally pressure in the pit reaches vessel pressure
 - Strong interaction



- The experiment addresses SARP high priority issues
- No experiment is known with pressure driven melt ejection in reactor geometry at accident conditions
- Bridges the gap between DCH and ex-vessel FCI issues
- Data will be used for code qualification
- Analysis in the frame of SARNET2 WP7.1 and WP5.3 through post-test calculations
 - MC3D (IRSN, CEA, ...)
 - JEMI (IKE Stuttgart)