

Creep Strength Of Chromium-Containing Conventional And ODS Steels In Oxygen-Controlled Pb At 650°C

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Overview

- Creep-rupture tests in oxygen-controlled heavy liquid metal (Pb) in comparison to air
- Tested material:
 - Conventional f/m steels T91 and P92
 - F/m 9Cr-, ferritic 12Cr- and 14Cr-ODS steels
- Experimental conditions:
 - Environments: (i) oxygen-controlled Pb ($c_o=10^{-6}$ mass%)
 - (ii) air
 - Temperature: 650°C
 - Stress range: facilitating short- (~1 h) and long-term (~10,000 h) tests

Attractiveness of ODS:

- ✓ High-temperature strength and resistance to neutron irradiation.
- ✓ High oxidation resistance reached through Cr (9-14 mass%) and fine-grained structure with oxide particles.

Creep-rupture tests in oxygen-controlled heavy liquid metal (Pb)

Continuous control of oxygen concentration in Pb

Measurements:

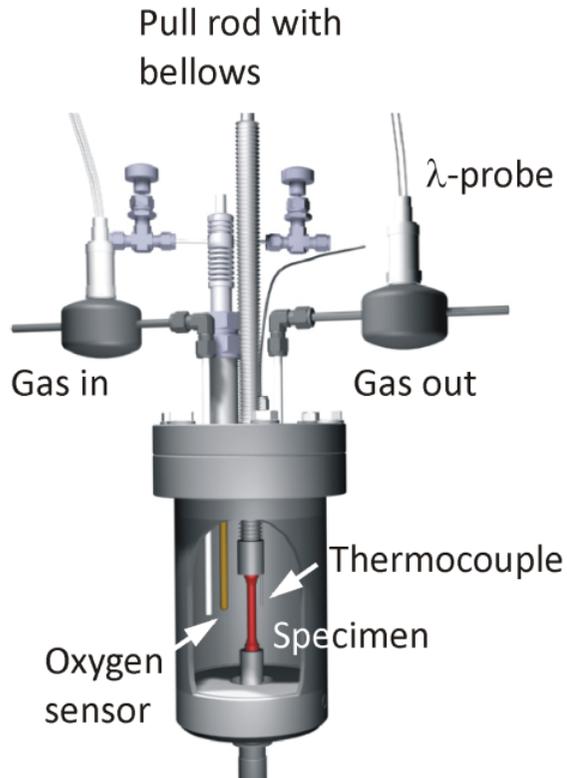
- Oxygen activity close to the specimen
- λ -sensors in gas -inlet and -outlet
- Temperature of Pb
- Gas flow (Ar, Ar/H₂ and synthetic air)

Conditions:

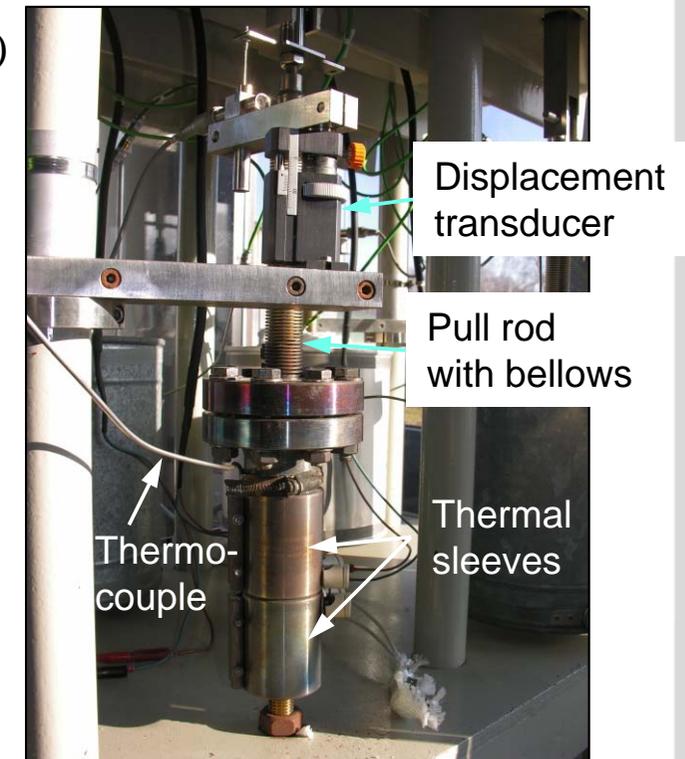
- ❑ stagnant Pb or LBE (900 ml)
- ❑ $T_{\max} = 650^{\circ}\text{C}$
- ❑ $c_o^{\max} = c_{HLM}^{\text{saturation}}$
- ❑ $c_o^{\min} = 10^{-8} - 10^{-9}$ mass %

CRISLA Facility:

- 5 independent capsules for HLM
- 3 independent capsules for air (gas)



CRISLA-capsule for HLM



CRISLA-capsule for gas

Tested materials

9Cr-ODS (plates)						
Fe	Cr	Mo	Mn	Ni	Y*	
bal	8.8	1.92	0.33	0.21	0.34	

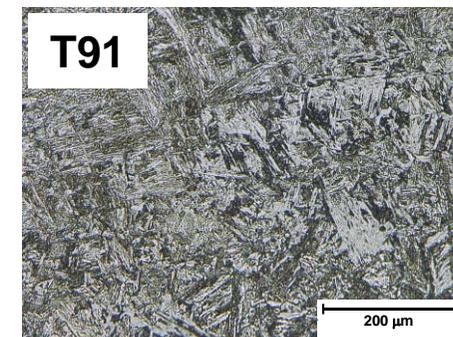
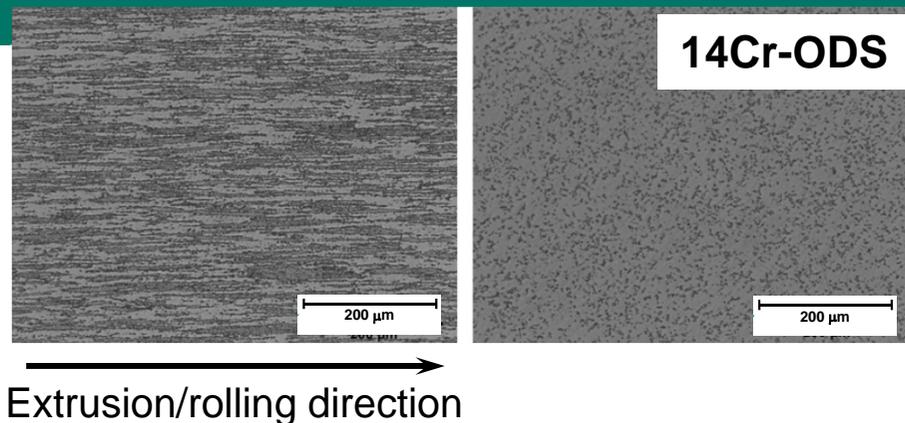
12Cr-ODS (plates)							
Fe	Cr	Mo	W	Ti	Mn	Ni	Y*
bal	12.2	<0.01	1.94	0.25	<0.01	<0.01	0.17

14Cr-ODS (bars)						
Fe	Cr	W	Ti	Mn	Y*	
bal	13.45	0.88	0.39	0.27	0.22	

* as Y₂O₃

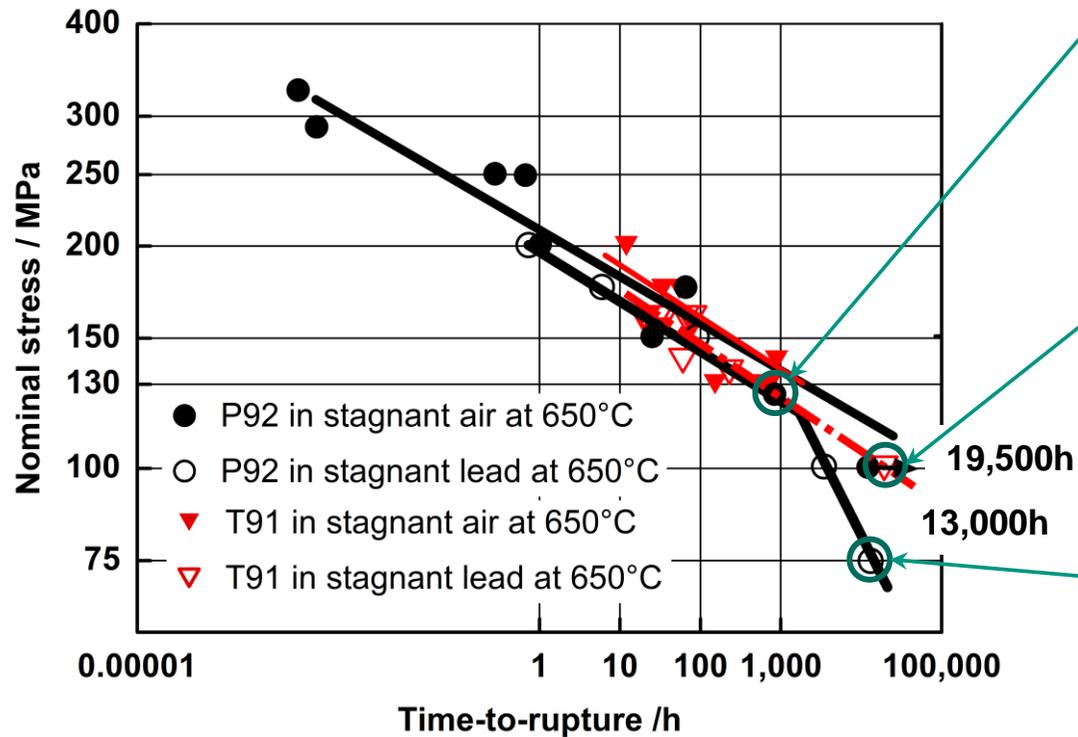
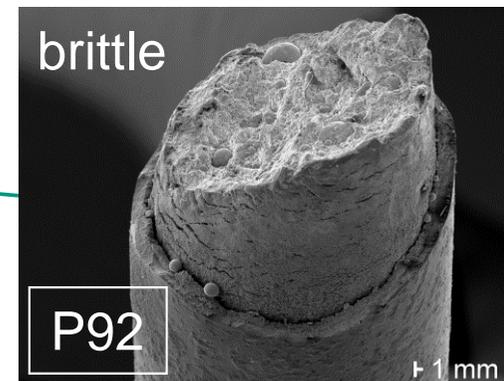
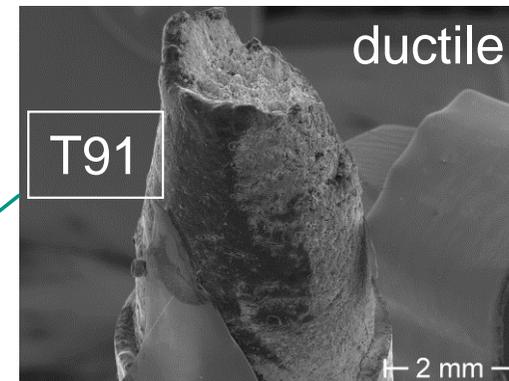
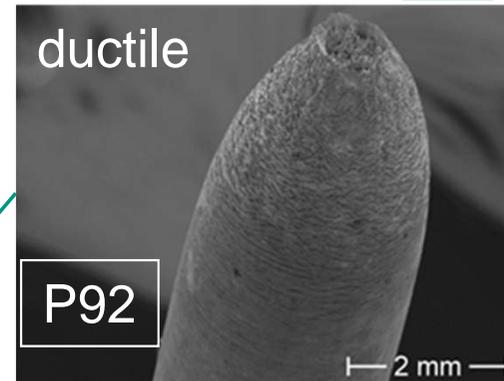
T91					
Fe	Cr	Mo	Mn	Si	V
bal	8.99	0.89	0.38	0.22	0.21

P92					
Fe	Cr	Mo	W	Mn	V
bal	8.99	0.49	1.75	0.43	0.2



Results for T91 and P92

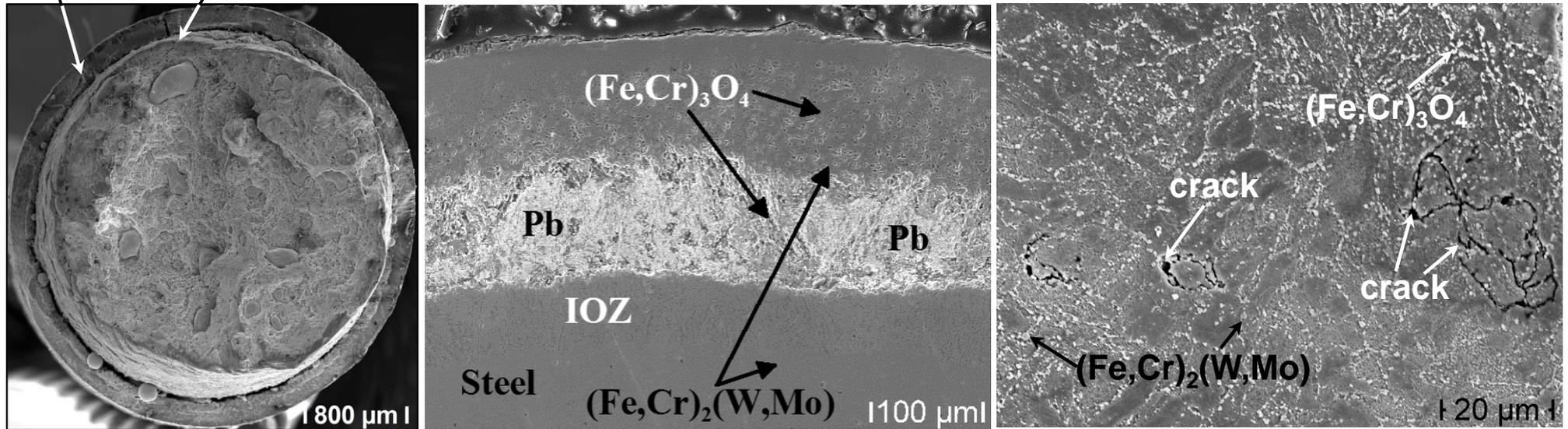
- ✓ Generally ductile behaviour.
- ✓ Insignificant difference between Pb and air.
- ✓ P92 shows brittle rupture mode at 75 MPa ($t_R=13,000h$).



Results for P92

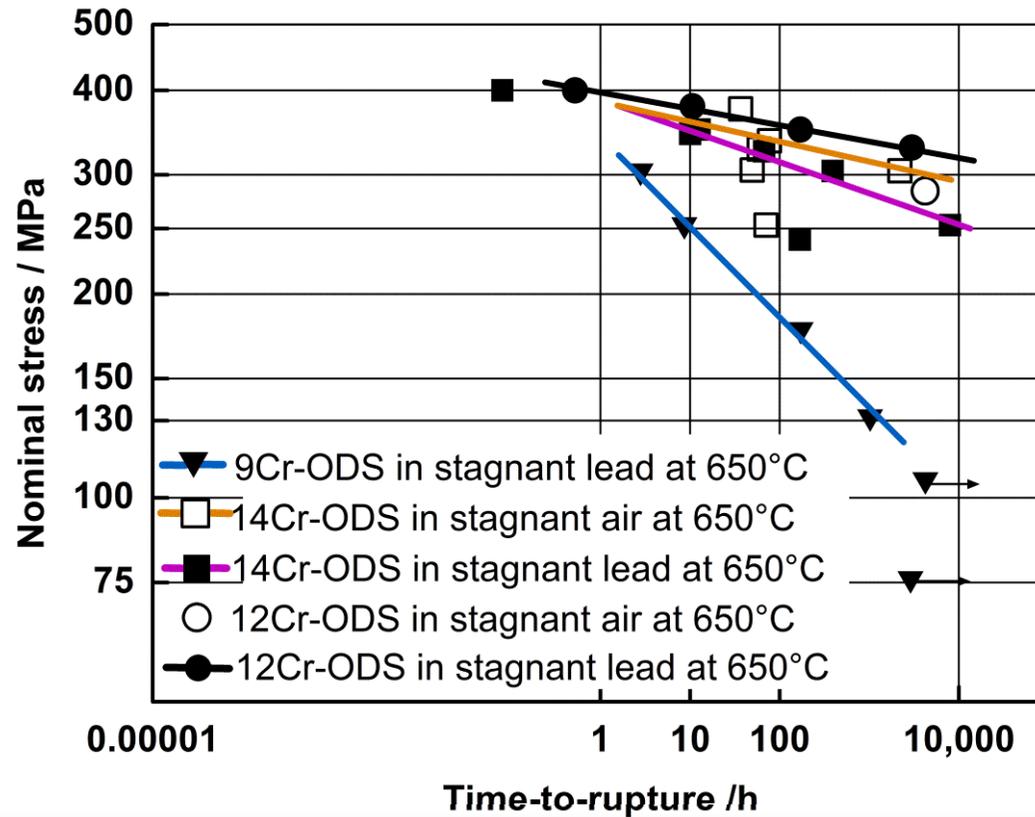
P92 at 75MPa and 13,090h

Oxide scale Failure origin



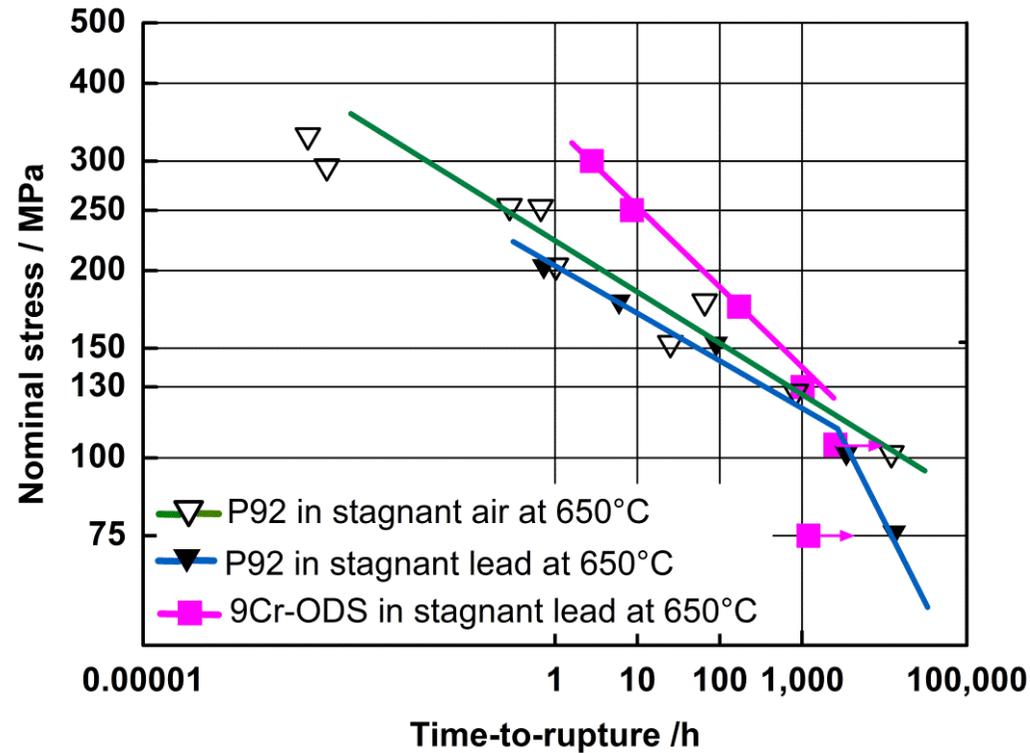
- ✓ Indications for LME: Failure origin at surface. Pb at oxide scale/steel interface.
- ✓ Indications for thermal aging: Increase in size and number of precipitates.
- ✓ Difficult to separate the influence of these two effects in the creep-rupture tests.

Creep strength of 9-14 Cr ODS steels in Pb and air at 650°C



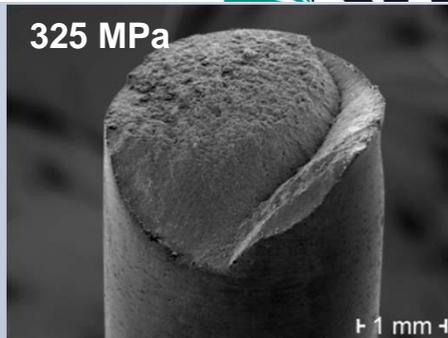
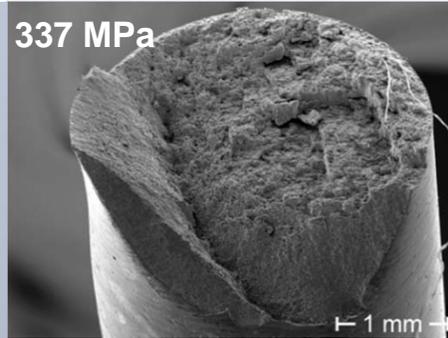
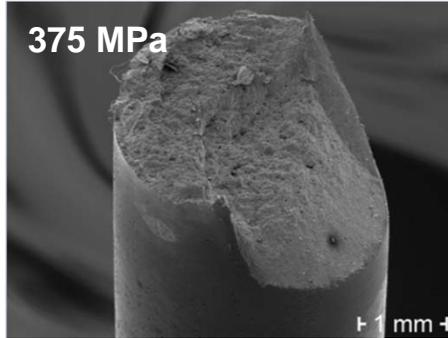
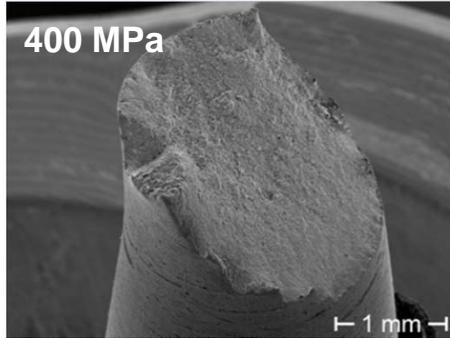
- ✓ 12Cr- and 14Cr-ODS: insignificant difference in strength in oxygen-controlled Pb and air at 650°C.
- ✓ The lower the stress, the bigger the difference in strength between 12/14Cr-ODS and 9Cr-ODS in Pb (and air).

Creep strength of 9Cr-ODS in comparison to conventional P92

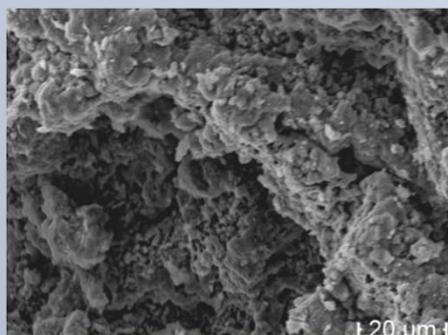
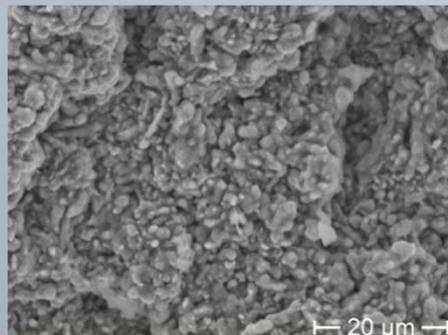
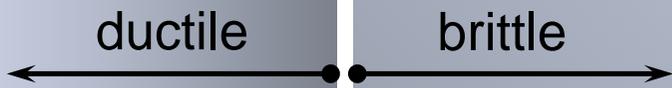


✓ The lower the stress, the smaller the difference in strength between 9Cr-ODS and P92 (T91) in Pb (and air).

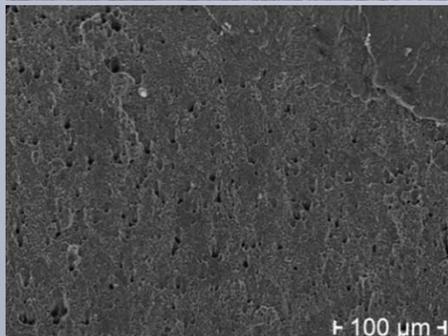
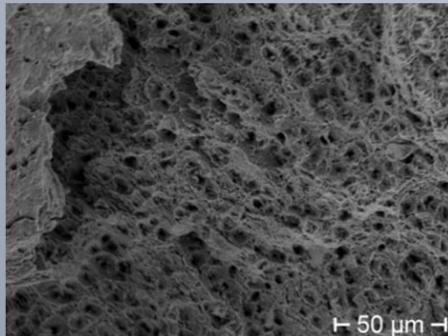
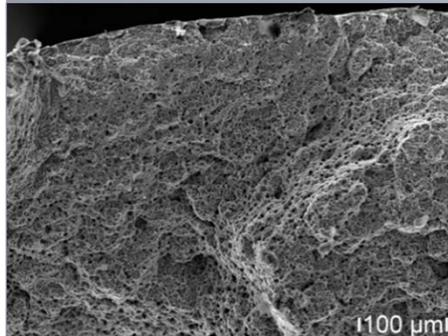
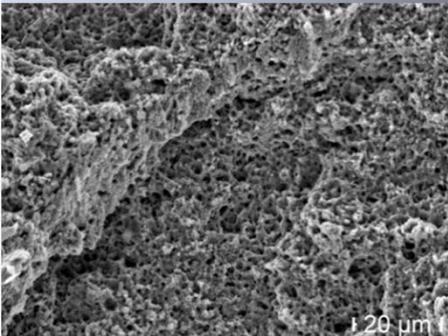
Fracture analysis of 14Cr-ODS



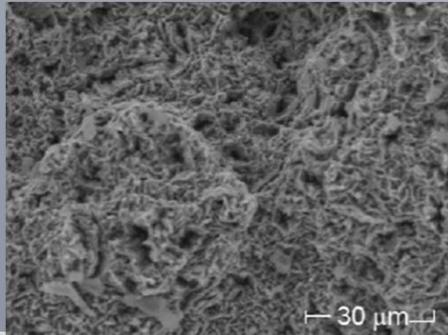
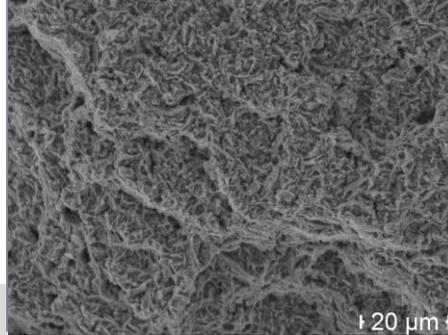
(i) Intergranular fracture (brittle)



(ii) Dimples (ductile)



(iii) Intermediate structure



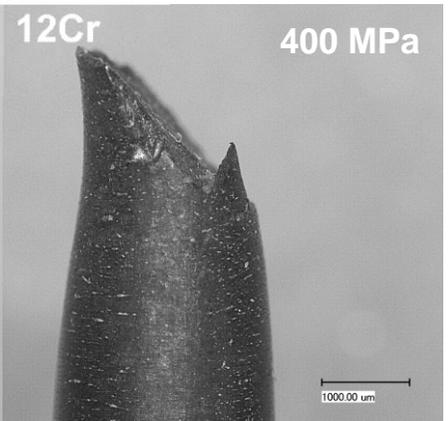
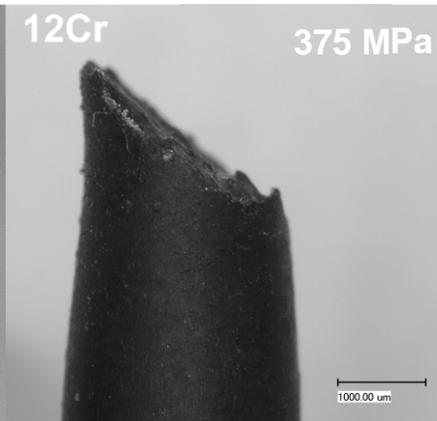
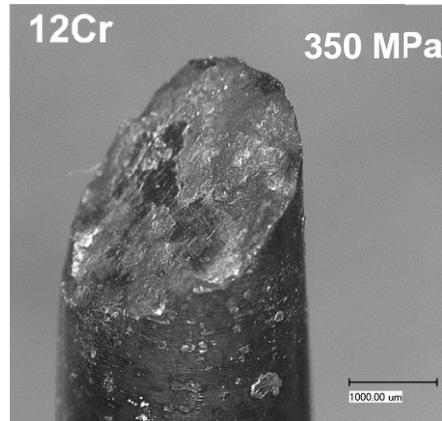
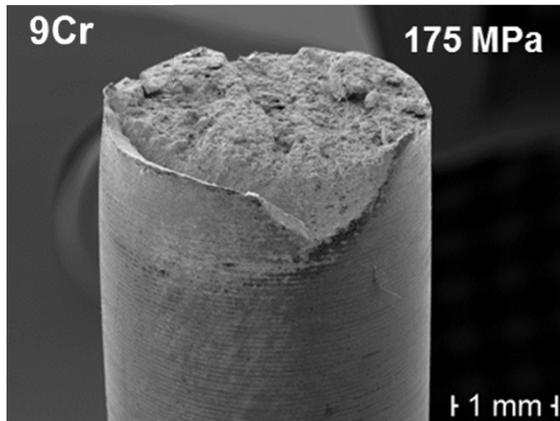
Z=62 %; $\epsilon_R=18$ %

Z=4 %; $\epsilon_R=7$ %

Z=5 %; $\epsilon_R=7$ %

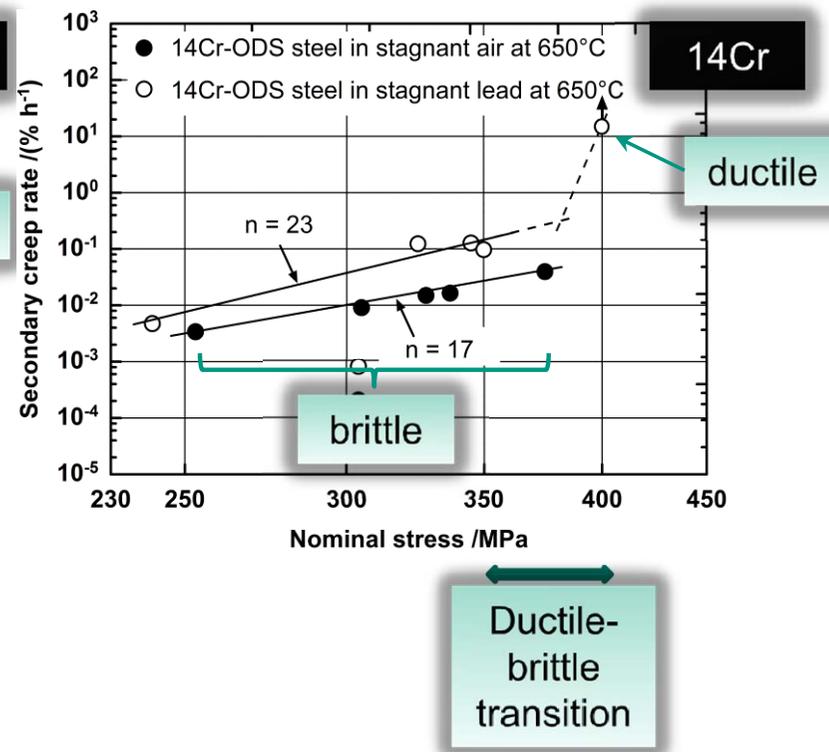
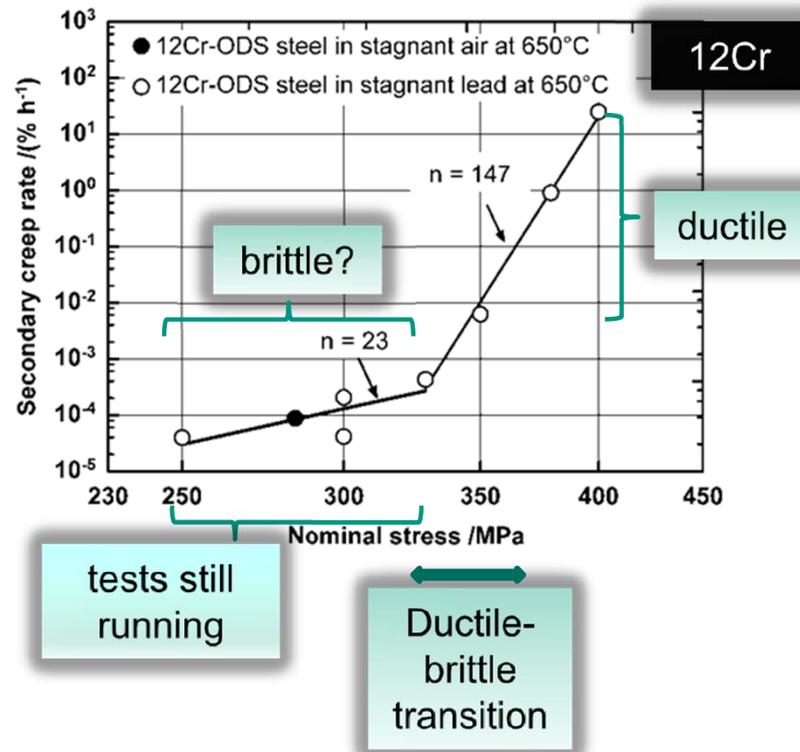
Z=6 %; $\epsilon_R=6$ %

Secondary creep vs. Fracture mode of ODS

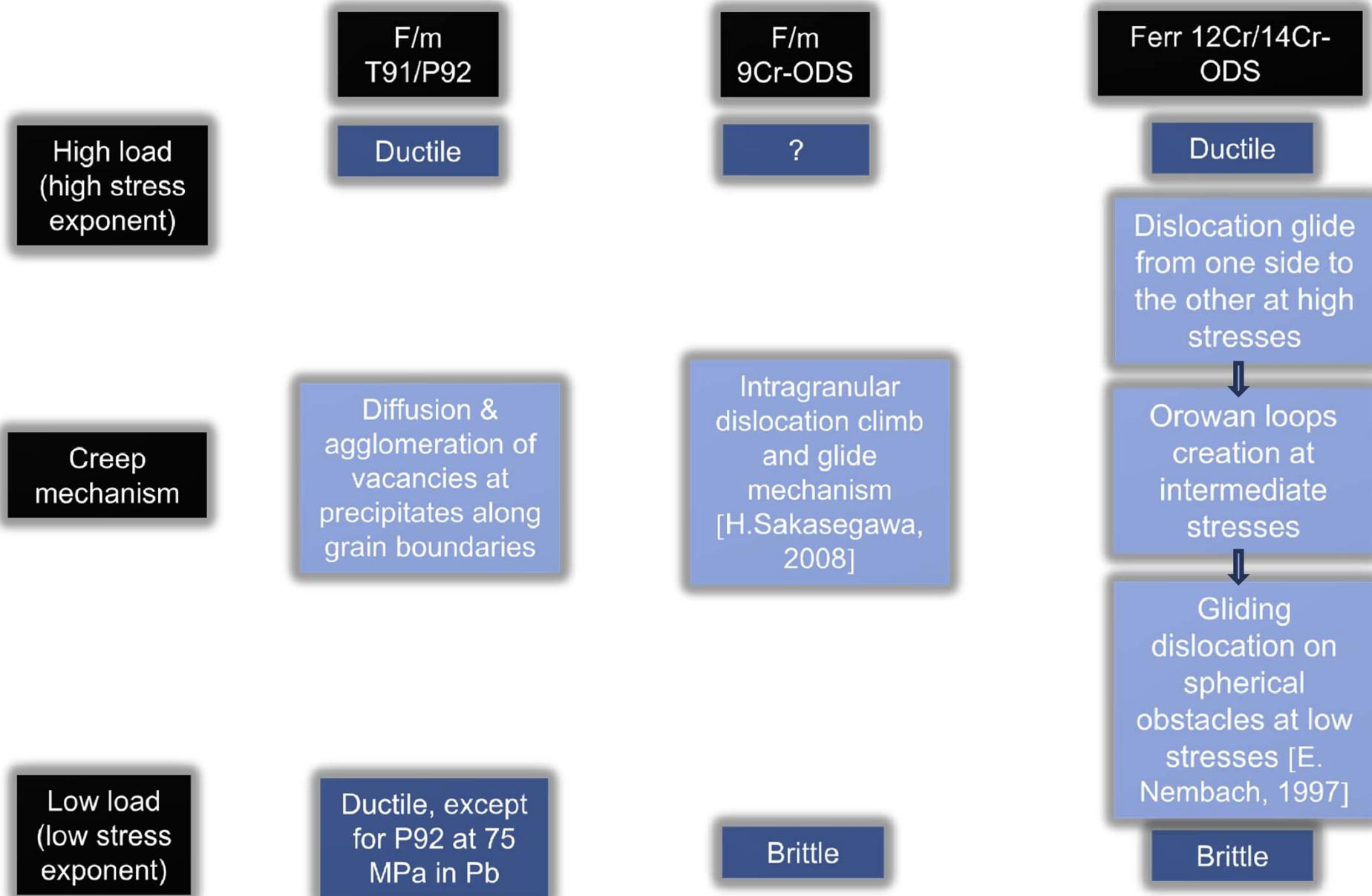


9Cr

brittle at ≤ 300 MPa



Summary: Creep and fracture



Conclusion

- ✓ Creep-rupture in static Pb ($650^{\circ}\text{C}/10^{-6}$ mass%) generally similar to tests in air.
- ✓ Change in rupture mode for f/m P92 at 75 MPa in Pb.
- ✓ Influence of Pb and thermal aging not yet possible to separate.
- ✓ 12-14Cr (ferritic) ODSs generally stronger than 9Cr-ODS (ferritic/martensitic).
- ✓ Brittle fracture at low load, ductile fracture at high load (<330/350 MPa)
- ✓ Influence of deformation rate (secondary creep)?

Acknowledgment

- ✓ Funding by the EURATOM 7th Framework Programme within the cross-cutting project GETMAT is gratefully acknowledged.