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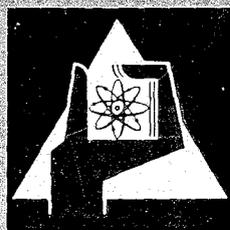
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A Pulse Shape Discrimination Circuit for Lithium-Drifted
Germanium Diodes

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A PULSE SHAPE DISCRIMINATION CIRCUIT FOR LITHIUM-DRIFTED GERMANIUM DIODES

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A pulse-shape discrimination circuit has been developed which is sensitive to a slow time-constant component in the charge carrier collection of lithium-drifted germanium detectors. Preamplifier output pulses containing such a component are rejected. By this method the spectrum shapes can be improved considerably. In

high-energy gamma-ray spectra the background under the peaks is reduced by a factor of up to 3. The resolution of the spectra is not affected. The attenuation of the peaks is certainly less than 10%.

1. Introduction

In neutron capture gamma-ray spectroscopy lithium-drifted germanium detectors are applied with the most promising results in the high-energy region above about 3 MeV, ref.¹). In this region the diodes are used as double-escape spectrometers. The double-escape peaks

are superimposed on a background which arises from Compton scattering, electron and bremsstrahlung escape. For making full use of the detector resolution and for detecting weak lines, a considerable reduction of the background is desirable. In this paper a circuit is described which discriminates against detector pulses with slow time-constant components. Such pulses obviously make an important contribution to the back-

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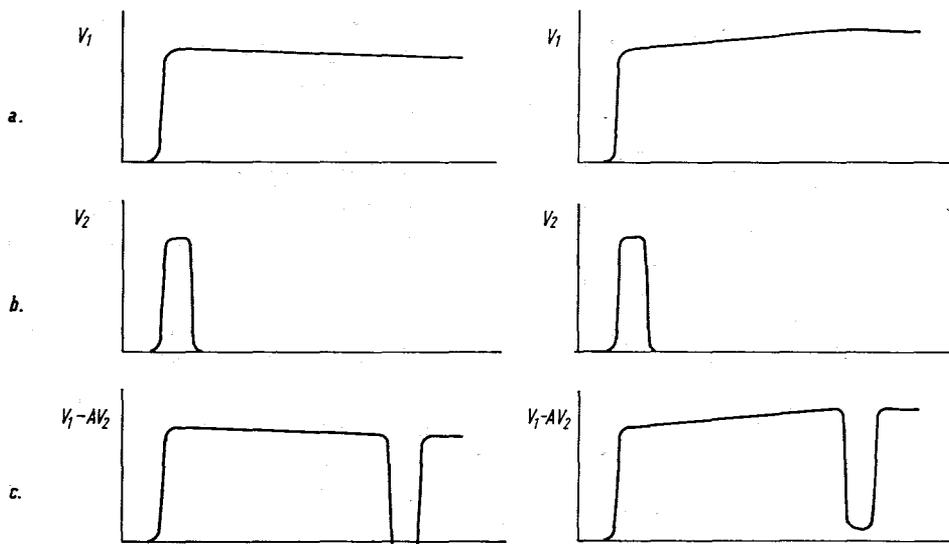


Fig. 1. Simplified pulse shapes for type I pulses on the left and type II pulses on the right.

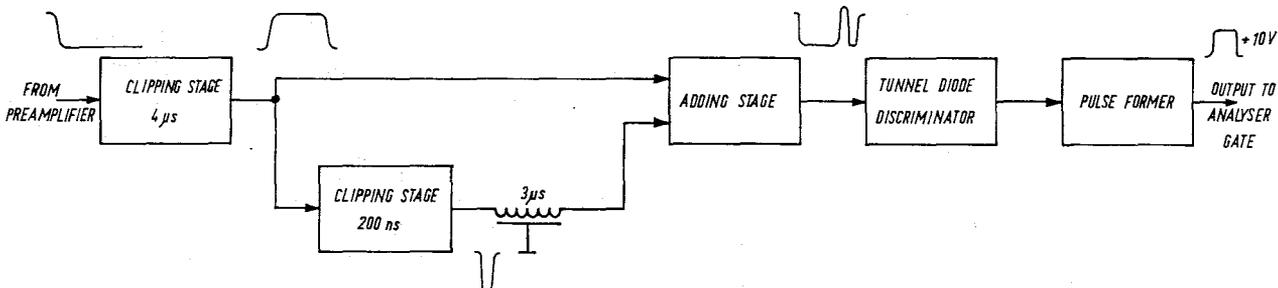


Fig. 2. Block diagram of the pulse-shape discriminator.

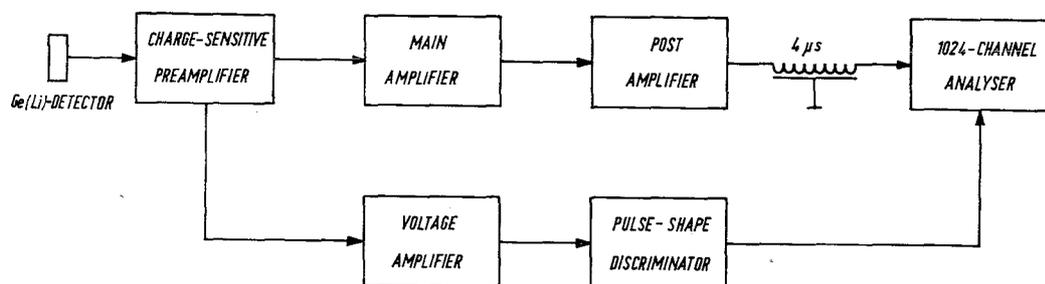


Fig. 4. Electronic arrangement for gamma-ray measurements.

sion time for charge carriers created in the undepleted region was measured to be about $3 \mu\text{s}$.

Thus the signals arising from particles not completely stopped within the intrinsic region have two components, a fast component of the order of nsec and a slow diffusion component of the order of μsec .

These pulses will be labelled type II pulses in contrast to the pulses due to particles completely stopped within the depletion region which are labelled type I pulses.

3. Principle of discrimination

Fig. 1 shows the shape of the two pulse types, on the left a type I pulse and on the right a type II pulse. By means of this figure the principle of pulse-shape discrimination can be easily explained. At the end of the fast-rising component there is not yet a marked influence of slow time-constants components. After some μsec , however, all diffusion components, if present, contribute to the pulse shape. By comparing the pulse heights after these time intervals, information can be obtained whether a diffusion component exists or not.

By clipping the input pulse, the pulse shape shown in fig. 1b is obtained. After amplifying this signal by a factor somewhat greater than one the signal is delayed and subtracted from the unshaped pulse (fig. 1c). Type I pulses are crossing the zero level, whereas for type II pulses there is no zero crossing. In a following low-threshold discriminator stage this zero crossing is used as a criterium, whether a type II pulse with diffusion component is produced.

4. Description of electronic design

The block diagram of the pulse-shape discriminator is shown in fig. 2. The input pulses coming from the preamplifier have a risetime of 50 ns and an exponential decay of $60 \mu\text{s}$. In the first clipping stage consisting of a short-circuited delay line and an inverting amplifier the pulses are limited to a width of $4 \mu\text{s}$ in order to avoid baseline shifts and pile-up effects. Then the shaped pulse is fed into two channels. In one channel the pulse is inverted and clipped again after the first rise

by a short-circuited delay line. The pulse width is now 200 ns. To the first approximation the shape is equal for both types of pulses as shown in fig. 1b. In the clipping stage the amplification factor can be adjusted. After a delay of $3 \mu\text{s}$ equal to the maximum diffusion time the signal is fed into an adding circuit and is added to the undelayed $4 \mu\text{s}$ pulse from the first clipping stage. For a type I pulse without diffusion component the signal crosses the zero level and produces a positive overshoot. This overshoot should be as small as possible for making the discrimination independent of the input pulse height over a wide range and for discriminating against small diffusion components. The lower limit for the positive overshoot, however, is set by the noise of the preamplifier which is in the order of some millivolts. For a type II pulse the signal remains below the zero level and thus does not trigger the following discriminator.

The required discriminator must have a very small threshold. We used a tunnel diode circuit⁵⁾ with a maximum sensitivity of 3 mV. The discriminator output pulses are fed into a pulse former which gives a ten volt pulse for gating the analyser.

The circuit diagram of the pulse-shape discrimination is shown in fig. 3.

5. Experimental results

The electronic arrangement for obtaining the gamma-ray spectra is given in fig. 4. The detector used for the measurements was a 2 mm deep diode with 2.8 cm^2 sensitive area. Fig. 5 shows two high-energy neutron capture gamma-ray spectra from natural strontium in the energy range from 6264 keV to 7527 keV. The upper spectrum was taken under normal conditions without discriminator whereas the lower spectrum was recorded by coincidence gating with the discriminator pulses. As can be seen, the background is reduced by a factor which increases with decreasing energy. At 7.5 MeV it is 2.3, at 6.2 MeV a value of 3.0 is observed. The attenuation of the double-escape peaks is less than 10%. In a 13 h run a fwhm of 9.1 keV at 7 MeV was

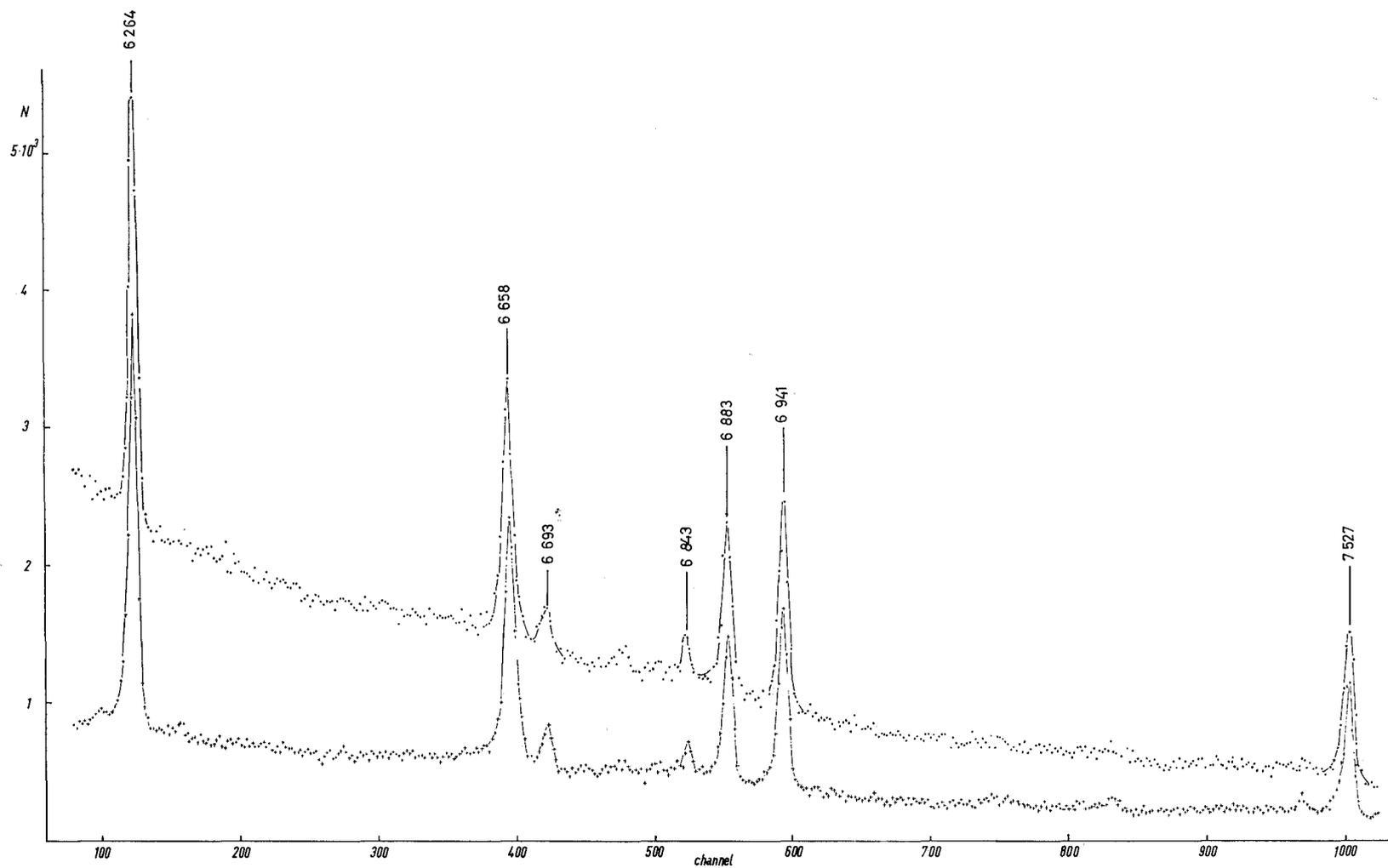


Fig. 5. Gamma-ray spectrum from thermal neutron capture in natural strontium. The lower curve was taken by coincidence gating with the discriminator pulses, the upper curve gives the ungated spectrum.

measured for both spectra. Thus the resolution is not affected by the pulse-shape discrimination. This is as expected from the circuit design. The resulting improvement of the spectra is particularly important when studying weak gamma-rays in the presence of intense lines.

For spectra of low-energy gamma-rays the reduction of the background by the pulse-shape discriminator is smaller than in the high-energy region. In the Compton distribution of ^{60}Co up to 25% of the pulses are rejected while the full-energy peaks remain unaffected. Since the improvement of the spectrum shape increases towards lower energy losses, the technique is particularly recommended when investigating low-energy gamma-rays in the presence of intense high-energy radiation. This is, for instance, always true of neutron capture spectroscopy.

The above measurements were also performed with a

2 cm³ diode. In this case the intrinsic region had a depth of 5 mm and the sensitive area was 4 cm². The results obtained were very similar to those observed with the small detector. Thus it is reasonable to assume that the pulse-shape discrimination method is very useful also for larger diodes, at least when the sensitive volume is in the region of a few cm². The same may be true for coaxially drifted diodes with an uncompensated core.

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