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Deformation of ⁵⁶Fe from 104 MeV *a*-Particle Scattering

von

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Abstract

Differential cross sections have been measured for the elastic and inelastic scattering of 104 MeV α -particles from ⁵⁶Fe. The angular distributions are analyzed in terms of coupled channels on the basis of a symmetric and asymmetric rotator model. The analyses use a semimicroscopic folding procedure /// and additionally in some cases the conventional extended optical model. Deformation parameters, rms-radii, multipole moments of nuclear matter, and transition probabilities have been extracted.

Untersuchung der Deformation von ⁵⁶Fe mit 104 MeV α-Teilchen Streuung

Zusammenfassung

Am Karlsruher Isochronzyklotron wurden differentielle Wirkungsquerschnitte der elastischen und inelastischen Streuung von 104 MeV α -Teilchen an ⁵⁶Fe gemessen. Die experimentellen Daten wurden durch "coupled-channel" Rechnungen auf der Basis eines symmetrischen und eines dreiachsial-asymmetrischen Rotationsmodells analysiert. Dabei wurde ein halbmikroskopisches Faltungsverfahren benutzt, das eine deformierte Nukleonendichteverteilung zugrunde legt. Es werden mittlere quadratische Radien und innere Multipolmomente der Nukleonenverteilung berechnet und Übergangswahrscheinlichkeiten angegeben.

1. Introduction

Level schemes and E2-properties of nuclei in the 1f-2p-shell indicate collective features intermediate between harmonic vibrations and rigid rotations (cf Lesser et al. 1972, Towsley et al. 1972, Parikh 1972, Chandra and Rustgi 1972, Rebel et al. 1972a, 1973a, 1973b). The magnitude of B(E2)-values and the static quadrupole moments Q_2^+ of the first excited 2⁺ states provide a sensitive measure for the deformation of the nuclear surface. According to the usual rotational model, the sign of ${\bf Q}_{2^+}$ distinguishes between prolate and oblate shape of the nucleus. Electromagnetic transition probabilities and static quadrupole moments have been measured by nuclear resonance fluorescence (Kelly and Beard 1961, Metzger 1961) and Coulomb excitation experiments (Andreyev et al. 1960, Lesser et al. 1972, Towsley et al. 1972), respectively. In particular the large quadrupole moment and the E2-properties of ⁵⁶Fe exhibit this nucleus to be a strongly deformed almost pure prolate rotator. The experimental B(E2; $0^+ \rightarrow 2^+$), B(E2; $2^+ \rightarrow 4^+$) and Q_{2^+} values correspond to intrinsic quadrupole moments Q_0 of 93 \pm 8 (Metzger 1961), 98 \pm 1, 99 \pm 20 and $+87 \pm$ 20 e fm² (Lesser et al. 1972), derived on the basis of a symmetric rotator. Assuming a triaxial asymmetric nucleus with an asymmetry angle γ = 20 $^{\rm O}$ the measured probabilities are also consistent with $Q_{0} = 102 \text{ e fm}^{2}$. Davydov and Chaban (1960) explained the level scheme of 56 Fe in the framework of an asymmetric rotator model with B-vibrations resulting in $\gamma = 17^{\circ}$ and a softness parameter $\mu = 0.61$. Recently, an analysis (Rebel et al. 1974) of the level scheme and B(E2)-values of ⁵⁶Fe was performed on the basis of the

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generalized collective model worked out by Gneuss and Greiner (cf Gneuss and Greiner 1971, Gneuss et al. 1969, 1970). The resulting collective energy surface representing the potential energy $V(\beta,\gamma)$ in an intrinsic frame and in terms of the usual shape parameters β and γ shows two minima in the range of the zero-point oscillation: one potential energy minimum for a prolate shape, the other representing an asymmetrically deformed shape.

In this paper, we report investigations of the collective behavior of 56 Fe which use the scattering of 104 MeV α -particles. First results of this experiment have been already published elsewhere (Gils et al. 1974a). The experiment aimed at specific information on the shape and intrinsic mass quadrupole moment of the ⁵⁶Fe nucleus. Because of the strong absorption in nuclear matter medium energy α -particle scattering is a surface reaction and therefore an excellent tool for the study of nuclear deformations. Previous studies of the elastic and inelastic α -particle scattering (Rebel et al. 1972a, 1973b) have shown that these experiments are not only sensitive to higher order deformations such as hexadecapole components in nuclear shape but also sensitive to the sign of the deformation parameters (Rebel 1972). This is due to the interference of single- and higher-order excitation processes which influence the observed distinct diffraction patterns of the differential cross sections and which allow discrimination between prolate and oblate nuclear shapes by a coupled channel analysis.

For 104 MeV α -particles the target-projectile interaction is mainly the nuclear interaction, which is conventionally parametrized as an optical potential. Though very successful in

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describing the scattering cross sections such a scattering model introduces an unavoidable model dependence into the extracted information. Furthermore, the relation between spatial size and deformation of the optical potential on the one side and of the nuclear matter density distribution on the other side is not quite clear and of complex nature. However, there is considerable evidence (Rebel 1974) that a simple procedure generating the real part of the optical potential by folding the projectilebound nucleon interaction over the nucleon distribution provides an adequate way to relate size and shape of the nucleus to the experimental cross sections, at least in the diffraction region. The results for the rms-radius $\langle r^2 \rangle^{1/2}$ and for the intrinsic quadrupole moment Q_0 quoted in this paper are extracted by such a folding model analysis of the experimental data.

2. Experimental procedure and results

The present (α, α') scattering experiments continue similar studies (Rebel et al. 1972a, 1973b) of the stable even Ni- and Ti-isotopes. The measurements used the scattering facilities at the 104 MeV α -particle beam of the Karlsruhe Isochronous Cyclotron. The target was a self supporting ⁵⁶Fe foil (99.5 % enrichement) of 2.1 [±] 0.1 mg/cm² thickness. In a first run the α -particle beam was not energy-analyzed in order to avoid background from slit scattering and to extend the measurements of the elastic and 2_1^+ inelastic cross sections on to very forward angles ($\approx 6^\circ$ lab). For a further independent run the α -particle beam was energyanalyzed to about 60 keV. The relatively large scattering chamber (130 cm diameter), a small beam spot (~1 mm width,~2 mm height) and a beam divergence of about $\pm 0.1^{\circ}$ enabled a good angular accuracy ($\Delta\theta(FWHM) \approx 0.25^{\circ}$) of the angular distributions. The absolute zero of the angular scale has been determined by measuring the sharp diffraction minima on both sides of the incident beam. Beam currents were varied from a few nA to the order of 200 nA. The scattered α -particles were detected by four telescopes of two 2 mm transmission mounted silicon surface barrier detectors. The four telescopes were rigidly mounted to the same movable arm, with a fixed angle of 1.5° between them.

The set-up of the electronics is shown in fig. 1. It consists of a conventional pre- and main-amplifying system for each detector branch. The biased amplifiers select and stretch a small energy interval between 0 and about 5 MeV excitation energy out of the whole α -particle spectrum. The router unit sets additional bits characterizing the origin of the converted pulse - to the on-line computer. The computer is programmed as a multichannel pulse height analyzer, and it stores the events in four 1K-memories one for each detector. The overall energy resolution was about 120-200 keV FWHM.

Particle identification was found not to be neccessary because the maximum energy loss of protons, deuterons, tritons and 3 He particles in 4 mm silicon is 26, 37, 43 and 93 MeV, respectively. So the (Z=1)-particles can only cause pulses in a region of the spectrum which is cut off by the biased amplifier. Due to the large difference in binding energies between 3 He and 4 He the maximum energy of 3 He particles produced is considerably lower than that of the elastically scattered α -particles.

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Accidental coincidences between two or more detectors which may cause a wrong pulse height in the ADC were found to be negligible at the beam currents used. Therefore, it was not neccessary to use a special set-up of the routing unit which could suppress such pile-up events but which is more difficult to handle and to adjust. The measurements at very forward scattering angles were carried out with one detector only. More details of the experimental arrangement and the data handling have been described in previous papers (Rebel et al. 1973b, 1972a,b).

As an example fig. 2 shows an energy spectrum of the outgoing α -particles. For forward angles there are also contamination peaks from ¹²C and ¹⁶O which walk out of the region of interest (up to about 2.7 MeV) beyond 25^O. In a detailed analysis of the energy spectra the continuous background was subtracted and the line shapes were fitted by an asymmetric Gaussian form thus separating in most cases the contribution of interfering contamination peaks. In fig. 2 the dashed line indicates the contributions of single peaks to the total spectrum.

The measured differential cross sections for the elastic and inelastic scattering to the first 2^+ and 4^+ states and to the second 2^+ -state are shown in fig. 3. The data were taken in 0.5° steps up to about $50^{\circ}(lab)$ where the oscillation pattern is clearly damped. The quoted error bars include the uncertainty due to finite angular acceptance which has been transformed into a cross section error. Especially in the region of the deep minima this "angular uncertainty" is dominating when compared to the statistical error which is smaller than 1 % for the elastic cross

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section at $\theta < 30^{\circ}$ even at the minima. From purely experimental considerations (foil thickness, detector solid angle, beam current) the absolute scale of the cross section is determined to within ca. 10 %. Finally we have normalized our data at most forward angles to the optical model results of elastic scattering as optical model calculations show very little variation in magnitude at small angles for any reasonable description of the elastic scattering cross section.

3. Elastic Scattering Analysis

The conventional optical model analysis of the elastic scattering using the standard Saxon-Woods-form (with volume absorption) for the nuclear potential

$$U(r_{\alpha}) = -V_{0}(1 + e^{X_{v}})^{-1} - i W_{0}(1 + e^{X_{w}})^{-1}$$

$$x_{v,w} = (r_{\alpha} - r_{v,w} \cdot A^{1/3})/a_{v,w}$$
(3.1)

and a Coulomb potential from a uniformly charged sphere with $R_c = 1.3 \cdot A^{1/3}$ results in

$$J_{R} = \frac{V_{o}\pi}{A} \int_{0}^{\infty} f(r_{\alpha}) r_{\alpha}^{2} dr = \left| \frac{4}{3} V_{o} \overline{W} R_{v}^{3} \left[1 + \left(\frac{\pi a_{v}}{R_{v}} \right)^{2} \right] / 4A \right| = 318.6 \text{ MeV } \text{fm}^{3}$$

based on the parameter set given in tab. 1.

As known from previous studies such a parameter set seems to be favored for higher α -particle energies. In the present analysis we did not look very systematically for alternative parameter families. In general, studies of the ambiguities require data of a larger angular range exceeding the diffraction region. This was out of the scope of our present investigation. A more microscopic description of the elastic α -particle-nucleus scattering starts with the intuitive expression

$$U_{R}(\vec{r}_{\alpha}) = \int \rho_{m}(\vec{r}) V_{eff}(\vec{r}_{\alpha} - \vec{r}) d^{3}r \qquad (3.2)$$

for the real central interaction potential, where $\rho_{\rm m}(\vec{r})$ is the nucleon (centers) density distribution and $V_{\rm eff}(\vec{r}_{\alpha}-\vec{r})$ an adequate effective α -particle-bound nucleon interaction. We use the Gaussian interaction proposed by Bernstein (1969) (cf Bernstein and Seidler 1971, 1972)

$$V_{eff} = \lambda_R V_o \exp(-|\vec{r}_{\alpha} - \vec{r}|^2/\mu^2)$$
 (3.3)

with $V_o = 37$ MeV and $\mu = 2.0$ fm. The parameter λ_R takes into account the "renormalization" due to the presence of the other bound nucleons. Its value is determined phenomenologically thus absorbing some uncertainties. Preceding investigations (Bernstein and Seidler 1971, Lerner et al. 1972) on α -particle scattering from 40 Ca yielded $\lambda_R = 0.92 \pm 0.1$ for α -particles of $E_{lab} = 104$ MeV. We repeated such studies of λ_R on the basis of our own data for seven (N=Z)- nuclei (Gils and Rebel 1974b) resulting in a value $\lambda_R = 0.86 \pm 0.06$. However, as discussed by Gils and Rebel (1974b) it seems reasonable to us finally to fit λ_R simultanously with size and shape parameters for every individual nucleus. For our analysis the nucleon density distribution is assumed to have a Fermi form

$$\rho_{\rm m} = \rho_{\rm o} \left[1 + \exp((\mathbf{r} - c_{\rm m})/a_{\rm m}) \right]^{-1}$$
 (3.4)

and to be identical for neutrons and protons $(\rho_m \equiv \rho_p \equiv \rho_n)$. The folded potential U_R (eq. 3.2) replaces the real part of the standard optical potential (eq. 3.1); in most cases the imaginary potential representation of eq. 3.1 remains unchanged (procedure A). In order to get a feeling of the influence of this representation we used alternatively Bernstein's representation (procedure B)

$$U_{I}(r_{\alpha}) = (\lambda_{I}/\lambda_{R}) U_{R}(r_{\alpha})$$
(3.5)

The results are compiled in tab. 1 and displayed in fig. 4. In the first run, the matter parameters c_m and a_m were fixed to corresponding values of the charge distribution. Elton and Swift (1964) investigated the charge density distribution of 56 Fe by electron scattering. Assumming a two-parameter Fermi shape (eq.3.4) they obtained

$$\langle r^2 \rangle_{ch}^{1/2} = 3.75 \text{ fm} \text{ c}_{ch} = 4.00 \text{ fm} \text{ a}_{ch} = 0.57 \text{ fm}$$

These values c_{ch} and a_{ch} can be related to the corresponding parameters of a Fermi shaped nucleon (= proton) density distribution in the following way: The rms-radius $\langle r^2 \rangle_{ch}^{1/2}$ of the charge distribution is converted to the rms-radius of the proton (centers) distribution $\langle r^2 \rangle_{p}^{1/2}$ via the relation

$$\langle r^{2} \rangle_{ch} = \langle r^{2} \rangle_{p} + \langle r^{2} \rangle_{s.p.}$$
 (3.6)

where $\langle r^2 \rangle_{s.p.}^{1/2} = 0.8$ fm is the rms-radius of the charge distribution of a single proton. The difference in rms-radiis of the charge distribution and of the distribution of the protons'centers now can be ascribed to a change in the diffuseness value $a_{ch}^+ a_m$ setting $c_m = c_{ch}$, or to a change of $c_{ch}^+ c_m$ fixing $a_{ch}^- = a_m$, alternatively. Using $a_m^- = a_{ch}^- = 0.57$ fm the values extracted from electron scattering correspond to

$$c_m = 3.85 \text{ fm}$$
 and $\langle r^2 \rangle_m^{1/2} = 3.66 \text{ fm}$

With that fixed values the parameters W_o , r_w and a_w were varied to find a minimum in χ^2 per degree of freedom.

In the second step we did not restrict us to matter values given but we allowed both c_m and a_m (and finally λ_R , too) to vary thus determining these parameters independent from other measurements. Detailed studies showed (Gils et al. 1974a, 1974b) that the differential cross sections are not sensitive to the particular choice of c_m and a_m , provided that the combination reproduces the correct value of the rms-radius.

The folding model analysis of elastic scattering results in

 $c_m = 3.84 \pm 0.06 \text{ fm}$ $a_m = 0.57 \pm 0.01 \text{ fm}$

$$\langle r^2 \rangle_m^{1/2} = 3.64 \pm 0.06 \text{ fm}$$

The value of the rms-radius $\langle r^2 \rangle_m^{1/2}$ of the nucleon distribution corresponds to $\langle r^2 \rangle_{n m}^{1/2} = 3.73 \stackrel{t}{=} 0.06$ fm for the nucleon ar matter distribution which is the quantity comparable to the charge distribution.

4. Inelastic Scattering

The macroscopic approach to the description of inelastic scattering is based on the assumption that the interaction potential follows the deformation of the nuclear surface. In the traditional "extended optical model" the interaction potential is represented by a deformed complex potential the size and shape of which is parametrized by introducing an expansion in spherical harmonics for the radius parameter ($r_{v,w}$ in expression (3.1)). Since we are mainly interested in the deformation of the nuclear surface rather than of the optical potential, we applied the folding concept to the inelastic scattering analysis, too. For this purpose we introduced into the relation (3.2) a deformed nucleon density distribution with an angular dependent nuclear radius. The nucleon density distribution was assumed to have Fermi shape and the Gaussian form of the effective interaction (eq. 3.3) with the parameter values $\lambda_{\rm R}$, $V_{\rm O}$ and μ given in sect. 3 was used. For the imaginary part of the optical potential we chose the macroscopic Saxon-Woods form enabling the geometry and depth to be independent of the real potential. The deformation of the imaginary potential was fixed to the values resulting from the calculation using the extended optical potential described above.

The calculation of the differential cross sections for the various states was performed by a coupled channel method. It takes explicitely into account the higher order excitation processes due to the strong coupling among the states. Coulomb excitation is considered by a potential which is deformed corresponding to the nuclear one. The numerical calculations were carried out with a modified version (Schweimer and Raynal 1973) of the code ECIS which includes the fitting procedure.

4.1. Symmetric Rotational Model

The axially symmetric rotator model was applied to the scattering from the 0^+ (ground state), 2_1^+ and 4_1^+ states at 0., 0.847 and 2.09 MeV excitation energy. The half-way radius R of the complex potential (Saxon-Woods form) or of the nucleon density distribution is parametrized in the body fixed system by

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$$R(\mathbf{A}') = R_{0}(1 + B_{2} Y_{20} (\mathbf{A}') + B_{4} Y_{40} (\mathbf{A}'))$$
(4.1)

The differential cross sections were simultaneously fitted in a $0^+-2^+_1-4^+$ coupling scheme, starting from the results obtained in the elastic scattering analysis. The result is shown in fig. 5, the final parameter values are quoted in table 2. The results indicate prolate deformation of the 56 Fe nucleus with a very small hexadecapole contribution. As exspected the folding model requires smaller values for the size and shape parameters c, a and β_2 . A more detailed study on prolate-oblate effects and on the dependence of the deformation parameters β_2 , β_4 from adopted size parameters c, a is given in ref. (Gils et al.1974a). From tab. 2 we extract the rms-radius $\langle r^2 \rangle_m^{1/2}$ and the intrinsic quadrupole (\mathbb{Q}_{20}) and hexadecapole (\mathbb{Q}_{40}) moments calculated for the real potential and the nucleon density distribution.

 $\langle r^2 \rangle_{Pot}^{1/2} = 4.81^{\pm} 0.05 \text{ fm } Q_{20}^{Pot} = +116^{\pm}5 \text{ e } \text{fm}^2 \quad Q_{40}^{Pot} = +570^{\pm}50 \text{ e } \text{fm}^4$ $\langle r^2 \rangle_m^{m} = 3.70^{\pm} 0.04 \text{ fm } Q_{20}^{m} = +95^{\pm}4 \text{ e } \text{fm}^2 \quad Q_{40}^{m} = +450^{\pm}40 \text{ e } \text{fm}^4$

In order to compare these results with charge rms-radii and multipole moments we again convert the values to values of a nucleon matter distribution according to eq. (3.6). Now the difference in rms-radii can be ascribed to a change of c_m , a_m or of the deformation parameters β_1 . For simplicity and consistency we assume the deformation and diffuseness to be unchanged and change only the half-way radius. Thus we obtain

 $\langle r^2 \rangle_{nm}^{1/2} = 3.78 \pm 0.04 \text{ fm} \quad Q_{20}^{nm} = \pm 100 \pm 4 \text{ e fm}^2 \quad Q_{40}^{nm} = \pm 500 \pm 40 \text{ e fm}^4$

4.2. Asymmetric Rotational Model

Suggested by results of the generalized collective model (Rebel et al. 1974), we analyzed the scattering from the 0^+ , 2_1^+ , 4_1^+ and 2_2^+ states in the framework of a triaxial deformed rotator with pure quadrupole deformation (Davydov and Filippov 1958). The radius parameter R of the interaction potential or of the nucleon density distribution, respectively, is characterized in the intrinsic frame by

$$R(\mathbf{A}', \mathbf{\phi}') = R_{0} \{1 + \sum_{\mu \doteq 0, \pm 2}^{a} 2\mu Y_{2\mu}(\mathbf{A}', \mathbf{\phi}')\}$$
(4.2)

Usually one describes the deviation from axial symmetry by the asymmetry angle γ and a deformation parameter ß which corresponds to the quadrupole deformation β_2 in the limit of vanishing asymmetry. The relations between these parameters are

$$a_{20} = \beta \cos \gamma; a_{22} = a_{2-2} = \frac{1}{\sqrt{2}} \beta \sin \gamma = a_{20} \frac{1}{\sqrt{2}} \tan \gamma$$
 (4.3)

In this model the collective wave functions for the n-th state

$$|IM;n\rangle = \sum_{K=even} A_K^{(n)} \phi_{MK}^{I}(\vec{s})$$

are superpositions of states of different K quantum numbers. The mixing amplitudes $A_{\rm K}^{(n)}$ are functions of the asymmetry angle γ . Thus the deviation from axial symmetry enters the scattering both via the ratio a_{22}/a_{20} and via the amplitudes $A_{\rm K}^{(n)}$. As e.g. shown in ref. (Rebel et al. 1973a) the asymmetry angle γ and the energy scale factor (containing a mass parameter and the deformation parameter β) can be determined by fitting the level spectrum. A fit to the states 2_1^+ , 2_2^+ , 3^+ , and 4_1^+ with equal weight on each state resulted in $\gamma = 19, 6^{\circ}$. The experimental and calculated excitation energies and the mixing amplitudes for various different γ -values are given in tab. 3.

Recently, Abecasis and Hernández (1972) worked out an asymmetric rotator model with a variable moment of inertia. We varied the asymmetry angle γ and the softness parameter ρ of this model to fit the energy level positions. The fit resulted in nearly the same asymmetry angle ($\gamma = 19.0^{\circ}$) as in the rigid Davydov-Filippov model. The parameter ρ has been found to be $\rho = 6 \cdot 10^{-3}$ indicating the softness of 56 Fe. This corroberates the information extracted from the collective energy surface reported in ref (Rebel et al. 1974).

Fig. 6 shows the measured and calculated angular distributions of the 0^+ , 2_1^+ , 4_1^+ and 2_2^+ states based on a coupled channel calculation including the folding procedure with parameter values given in line 2 of tab. 4. In some additional calculations, we tried to use various different γ -values between 10[°] and 28[°]. In the lower left hand part of fig. 6 the χ^2 -values of these runs are plotted. The minimum is at $\gamma = 19^{\circ}$. Potential parameters and the deformation B were fixed during the scan. A 6-parameter fit at $\gamma = 10^{\circ}$ (tab. 4, line 3) shows that the χ^2 -value does not change significantly when varying the potential parameters. Looking on the partial χ^2 -values (tab. 5) concerning the different states, it is obvious that the minimum mainly arises from a better description of the 2^+_2 -state. The calculated angular distribution of the 2^+_2 state for $\gamma = 10^\circ$ (dashed line in fig. 6) indicates the sensitivity to the γ -value. From the parameter values given in tab. 4 we quote the following results

$$\beta = 0.241 \qquad \gamma = 19^{\circ}$$

$$\langle r^{2} \rangle_{m}^{1/2} = 3.77^{\pm}0.06 \text{ fm} \qquad Q_{20}^{m} = 101^{\pm}2 \text{ e fm}^{2} \qquad Q_{22}^{m} = 20.2^{\pm}0.4 \text{ e fm}^{2}$$

$$\langle r^{2} \rangle_{nm}^{1/2} = 3.85^{\pm}0.06 \text{ fm} \qquad Q_{20}^{nm} = 106^{\pm}2 \text{ e fm}^{2} \qquad Q_{22}^{nm} = 21.2^{\pm}0.4 \text{ e fm}^{2}$$

5. Summary

Completing recent studies of the collective behavior of even f-p-shell nuclei (Rebel et al. 1972, 1973b) we have experimentally investigated the scattering of 104 MeV α -particles from ⁵⁶Fe. The measured differential cross sections have been analyzed in terms of coupled channels on the basis of a symmetric and a triaxial rotator model. We mainly were interested in the deformation of the nuclear matter density distribution and tried to extract from the data intrinsic multipole moments and values of the transition probabilities for ⁵⁶Fe. The traditional way describing inelastic scattering on the basis of a macroscopic, phenomenologically deformed optical potential provides information on the deformation of the interaction potential which is affected by the finite size of the projectile. Indeed, the values of the deformation parameters obtained in the framework of the usual extended optical model are different e.g. for α -particle and proton scattering. The deformation parameters of the interaction potential reflect only roughly the deformation of the density distribution of the target nucleus. Therefore, we used for our analysis a semimicroscopic folding model which relates the differential cross sections in a more direct way to size and shape of target nucleus. The folding model generates the interaction potential by averaging an effective α -bound nucleon interaction over a deformed distribution of the target nucleons. Such an interaction is used in the coupled channel analysis fitting the measured cross sections

by adjusting the size and shape parameters of the nucleon distribution. This procedure has been successfully applied in several preceding investigations. The following details of the procedure used in the present paper should be remarked:

- (i) Contrary to other authors (Lerner et al. 1972, Bernstein and Seidler 1971, 1972) we find it reasonable to determine the phenomenological parameter λ_R for every invidual target nucleus separately, as λ_R may also reflect some structure effects.
- (ii) Exchange effects which sometimes are discussed (Bimbot et al. 1973) have not been explicitely included in the present analysis. Preliminary calculations showed that they are of minor importance for the diffraction region of the angular distribution and may be already absorbed by the phenomenological adjustment of the effective α-nucleon interaction.
- (iii) Converting our results of the nucleon distribution to the nuclear matter distribution which is comparable to the charge distribution we use for the rms-radius of a single neutron $\langle r^2 \rangle_{s.n.}^m$ the proton value $\langle r^2 \rangle_{s.p.}^m = 0.64$ and ascribe the difference between nucleon and nuclear matter distribution to the half way radius of the underlying functional form of the distribution. In this way rms-radii and intrinsic multipole moments are calculated by numerical integration over the deformed distribution.

We quote as final results:

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A) Analysis of the ground-state band: Symmetric Rotator Model

- $Q_{20} = + 100 \pm 4 \text{ e fm}^2 \qquad Q_{40} = 500 \pm 40 \text{ e fm}^4$ $Q_{2_1^+} = -28.5 \pm 1.1 \text{ e fm}^2$ $B(E2; 0^+ + 2^+) = 990 \pm 80 \text{ e}^2 \text{ fm}^4$ $B(E4; 0^+ + 4^+) = (4.4 \pm 0.4) \cdot 10^4 \text{ e}^2 \text{ fm}^8$
- B) Analysis including the second 2⁺-state: Asymmetric Rotator Model *)

 $B = 0.241 \quad B_{eff} = 0.216 \quad \gamma = 19^{\circ}$ $Q_{20} = +106 \stackrel{\pm}{=} 2 e fm^{2} \qquad Q_{22} = 21.2 e fm^{2}$ $Q_{0} = +101 \stackrel{\pm}{=} 2 e fm^{2}$ $Q_{21} = -28.9 \stackrel{\pm}{=} 0.6 e fm^{2} \qquad Q_{22} = -Q_{21} \stackrel{\pm}{=}$ $B(E2; 0^{+} + 2^{+}) = 1010 \stackrel{\pm}{=} 40 e^{2} fm^{4}$

It is conspicuous that the asymmetric rotator model analysis which reveals a triaxial deformation of $\gamma \approx 20^{\circ}$ has little effect to the values of quadrupole moment $Q_{2\frac{1}{1}}$ extracted by the symmetric rotator model analysis of the ground band.

In tab. 6 the results are compared with other experimental results.

The values extracted from helion and α -particle scattering in the framework of a deformed optical potential underestimate moments and transition probabilities compared to proton scattering and electromagnetic findings, even when - by the recipe of Bernstein (1969) - the deformation parameters are "renormalized".

^{*)} Beff, Qo, and Q2⁺ are defined according to Davydov and Filippov (1958)

The value of the asymmetry angle γ which we obtain from our analysis is in good agreement with the results of analyses of the level spectrum of 56 Fe. (Davydov and Chaban 1960, Davydov and Filippov 1958, Abecasis and Hernández 1972). A recent investigation of the collective energy surface of 56 Fe results in effective γ -values for the various states ranging from about 19° to 21° .

However, it should be remarked that there are significant deviations of the experimental $2\frac{1}{2}^{+}$ -differential cross section from a pure collective description. This has been also found in a recent investigation on the basis of a more generalized collective model (Rebel et al. 1974). We ascribe the deviation to an unknown admixture to the $2\frac{1}{2}^{+}$ -amplitude which is neglected by the collective model. Though spurious such an amplitude influences the cross section very sensitively.

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| V _o [MeV] | r _v [fm] | a _v [fm] | W _o [MeV] | r _w [fm] | a _w [fm] | <r<sup>2>^{1/2} Pot [fm]</r<sup> | χ^2/F | | , | |
|----------------------|--|---------------------|----------------------|---------------------|---------------------|---|-------------------|---|----------|--|
| 114(1) | 1.31(1) | 0.71(1) | 21.4(4) | 1.58(1) | 0.61(2) | 4.69(6) | 5.5 | macroscopic optical potential 6 parameters varied | | |
| λ _R | c _m A ^{-1/3} [fm] | a _m [fm] | W _o [MeV] | r _w [fm] | a _w [fm] | <r<sup>2>^{1/2}_m [fm]</r<sup> | χ ² /F | real para- meters varied | comments | |
| 0.86 | 1.01 | 0.57 | 26(1) | 1.54(1) | 0.60(2) | 3.66 | 16.0 | _ | proc. A | |
| 0.86 | 1.037(5) | 0.54(1) | 26(1) | 1.56(2) | 0.57(1) | 3.67(3) | 15.6 | c _m , a _m | Α | |
| 0.92 | 1.02(2) | 0.55(2) | 24(1) | 1.60(1) | 0.54(2) | 3.65(6) | 10.3 | c _m , a _m | Α | |
| 0.900(4) | 1.00(1) | 0.57(2) | 22.1(8) | 1.60(1) | 0.55(2) | 3.64(6) | 9.0 | $\lambda_{\rm R}^{\rm m}$, $c_{\rm m}^{\rm m}$, $a_{\rm m}^{\rm m}$ | A | |
| | | | λ _I | | | | | | | |
| 0.86 | 1.09(1) | 0.47(2) | 0.494(5) | - | - | 3.67(4) | 16.3 | c _m , a _m | В | |
| 0.90 | 1.06(1) | 0.48(2) | 0.514(6) | - | - | 3.61(4) | 16.4 | c _m , a _m | В | |

Tab. 1: Results of the elastic scattering analysis. Procedure A of the folding model uses a macroscopic imaginary potential the three parameters of which are all varied. The numbers in brackets are the standard errors in the last digit of the quoted values. The procedure of determination of the errors is given in ref. (Rebel et al. 1972b).

| V _o [MeV] | $r_v [fm]$ | a _v [fm] | W _o [MeV] | r _w [fm] | a _w [fm] | ^B 2 | ßų | <r<sup>2>^{1/2} [fm]</r<sup> | χ ² /F | | |
|----------------------|--|---------------------|----------------------|---------------------|---------------------|----------------|----------------|---|-------------------|--|-----------------|
| 108(2) | 1.348(8) | 0.71(1) | 21.7(7) | 1.61(1) | 0.50(1) | 0.178(2) | 0.009(4) | 4.81(5) | 14.4 | extended poter | optical tial |
| λ _R | c _m A ^{-1/3} [fm] | a _m [fm] | W _o [MeV] | r _w [fm] | a _w [fm] | ⁸ 2 | ₿ _Ц | <r<sup>2>^{1/2} m [fm]</r<sup> | χ ² /F | real para- meters varied | comments |
| 0.86 | 1.01 | 0.57 | 18.3(6) | 1.60(1) | 0.58(2) | 0.256(3) | 0.02(1) | 3.71 | 24.0 | | proc.A |
| 0.86 | 1.23(2) | 0.32(4) | 28(3) | 1.59(1) | 0.47(2) | 0.208(5) | 0.011(6) | 3.88(4) | 18.4 | ° _m ,a _m | А |
| 0.92 | 1.06(2) | 0.51(2) | 18.5(9) | 1.63(1) | 0.52(1) | 0.239(4) | 0.019(8) | 3.71(4) | 15.5 | c _m ,a _m | А |
| 0.950(8) | 1.04(2) | 0.53(2) | 18(1) | 1.65(1) | 0.49(1) | 0.238(5) | 0.026(9) | 3.70(4) | 14.3 | λ _R ,c _m ,a _m | Α |
| | | | λ _I | | | | | | | | |
| 0.95 | 1.09(1) | 0.43(2) | 0.454(4) | - | - | 0.237(4) | 0.036(7) | 3.65(4) | 19.0 | c _m ,a _m | В |

Tab. 2: Results of the symmetric rotator coupled channel analysis $(0^+ - 2^+_1 - 4^+ - \text{coupling})$. In all cases the deformation parameters and the imaginary potential parameters were varied. The numbers in brackets indicate the standard errors in the last digit.

| I | E_n^{exp} [MeV] | E_n^{th} [MeV] | A _o (n) | A ₂ ⁽ⁿ⁾ | A ₄ (n) | |
|-----------------------|-------------------|------------------|--------------------|-------------------------------|--------------------|-------------------------------------|
| 2 <mark>+</mark> 1 | 0.847 | 0.690 | 0.9968 | 0.0797 | | $\gamma = 19.6^{\circ}$ obtained by |
| 2 <mark>*</mark> | 2.66 | 2.70 | -0.0797 | 0.9968 | | fitting the energy levels |
| 3 † | 3.45 | 3.39 | 0.0 | 1.0 | | |
| 4 + 1 | 2.09 | 2.17 | 0.9612 | 0.2758 | 0.0083 | |
| 2 <mark>1</mark> | | 0.641 | 0.9993 | 0.0377 | | $\gamma = 16^{\circ}$ fixed |
| 2 <mark>*</mark> | | 3.84 | -0.0377 | 0.9993 | | |
| 3 * | | 4.48 | 0.0 | 1.0 | | |
| 4 ⁺ 1 | | 2.09 | 0.9899 | 0.1418 | 0.0020 | |
| 2 <mark>1</mark> | | 0.762 | 0.9821 | 0.1885 | | $\gamma = 24^{\circ}$ fixed |
| 2 <mark>*</mark> | | 1.97 | -0.1885 | 0.9821 | | |
| 3 * | | 2.73 | 0.0 | 1.0 | | |
| 4 + 1 | | 2.21 | 0.8758 | 0.4816 | 0.0331 | |

Tab. 3: Different sets of mixing amplitudes resulting from the asymmetric rotator description of the ⁵⁶Fe level spectrum

| V _o [MeV] | r _w [fm] | a _w [fm] | W _o [MeV] | r _w [fm] | a _w [fm] | ^a 20 | Ŷ | <pr2>1/2 [fm] Pot</pr2> | χ ² /F | | |
|----------------------|---|---------------------|----------------------------------|---------------------|---------------------|-------------------|-------------------------|---|-------------------|--|--|
| 107(2) | 1.357(8) | 0.70(1) | 22(1) | 1.61(1) | 0.51(2) | 0.176(2) | 19.6 | 4.82 | 17.2 | extended op 7 parameter | tical model s varied |
| λ _R | c _m A ^{1/3} [fm] | a _m [fm] | W _o [MeV] | r _w [fm] | a _w [fm] | ^a 20 | Y | <r<sup>2>^{1/2} [fm]</r<sup> | χ ² /F | real para- meters varied | comments |
| 0.93(3) 0.96(1) | 1.16(1) 1.09(1) | 0.38(2) 0.48(3) | 28(3) 18(2) ^A I | 1.56(2) 1.66(2) | 0.52(2) 0.47(2) | 0.227(5) 0.227 | 19.6 10 ⁰ | 3.77(6) 3.73(6) | 20.6 25.9 | λ _R ,c _m ,a _m λ _R ,c _m ,a _m | p roc. A A a ₂₀ fixed |
| 0.93 | 1.10(1) | 0.43(2) | 0.449(9) | - | - | 0.225(4) | 19.6 | 3.69(6) | 21.2 | c _m , a _m | В |

Tab. 4: Triaxial rotator analysis $(0^+ 2_1^+ - 4^+ - 2_2^+ - \text{coupling})$. In all cases the imaginary potential parameters were varied. The numbers in brackets indicate the standard errors in the last digit.

| Ŷ | χ^2/F (total) | χ^2/F (0 ⁺) | $\chi^2/F(2_1^+)$ | $\chi^2/F (4_1^+)$ | $\chi^2/F(2_2^+)$ |
|------|--------------------|------------------------------|-------------------|--------------------|-------------------|
| 10 | 28.2 | 19.3 | 25.5 | 7.3 | 79.9 |
| 14 | 23.0 | 19.7 | 24.2 | 7.1 | 47.9 |
| 17 | 20.5 | 18.2 | 24.7 | 5.5 | 35.5 |
| 18 | 20.2 | 18.0 | 24.9 | 5.4 | 33.9 |
| 19 | 20.1 | 17.8 | 25.2 | 5.2 | 33.4 |
| 19.6 | 20.2 | 17.7 | 25.4 | 5.2 | 33.6 |
| 21 | 20.4 | 17.4 | 25.7 | 4.9 | 35.5 |
| 24 | 22.3 | 16.8 | 26.2 | 4.3 | 48.3 |
| 28 | 28.3 | 16.2 | 27.2 | 3.8 | 88.0 |
| | | | | | |

Tab. 5: Total and partial χ^2 -values per degree of freedom for different asymmetry angles γ . In all cases the potential parameters were fixed to the values of tab. 4, line 2 and the parameter ß was set to $\beta = 0.241$.

| Method | Reference | [₿] 2 | $Q_{20} [e fm^2]$ | Q_{21}^{+} [e fm ²] | $B(E2) \uparrow [e^{2} fm^{4}]$ | B(E2)↑/B(E2) s.p. |
|---------------------------------------|--------------------------------|------------------------|-------------------------------------|-----------------------------------|---------------------------------|-------------------------|
| Electromagnetic (average) | Stelson and Grodzins (1965) | 0.23 | (95) | (27) | 900 - 100 | 14.1 - 1.6 |
| Electromagnetic (reorientation) | Lesser et al. 1972 | | (+87 <mark>+</mark> 20) | -24.9-5.8 | 970 ± 20 | 15.2 ± 0.3 |
| p,p (average) | Peterson 1969 | | (102) | (29) | 1030 [±] 300 | 16.2 [±] 4.7 |
| p,p'; DWBA | Main 1971 | 0.20 [±] 0.02 | (90) | (26) | 810 ± 100 | 12.7 <mark>+</mark> 1.6 |
| 3 He; α (average) | Peterson 1969 | | (84) | (24) | 700 ± 70 | 11.0 [±] 1.1 |
| ³ He, ³ He'; CC | Marchese et al.1973 | 0.21 | (79) | (23) | 623 ^{*)} | 9.8 |
| a,a'; DWBA | Bernstein 1969 | | (89 ± 6) | (26+2) | 792 [±] 121 | 12.4 [±] 1.9 |
| a,a'; CC, Folding, SR | present experiment | 0.238 | +100 ⁺ 4 | (-28.5 ⁺ 1.2) | (990 [±] 80) | 15.6 [±] 1.3 |
| a,a'; CC, Folding, ASR | present experiment | ß = 0.241 | Q ₀ =+101 [±] 2 | (-28.9±0.6) | (1010 [±] 40) | 15.9 ± 0.6 |

Tab. 6: Comparison of deformation parameters, quadrupole moments and transition probabilities of 56 Fe obtained by different experimental methods. Values in brackets are deduced from B(E2)-values given by the relations $Q_{20} = \sqrt{\frac{16\pi}{5}} B(E2) + and Q_{2} + = -\frac{2}{7} Q_{20}$. In the case of the asymmetric rotator analysis (ASR) the parameters ß and Q_0 are comparable to B_2 and Q_{20}

*)Calculated from β_2 and R_v by the method given by Bernstein (1969).

Figure Captions

- Fig. 1: Set-up of the electronics. The numbers correspond to the producers' type identifications of the NIM-modules used (BA: Canberra; all the others: Ortec).
- Fig. 2: Energy spectrum of the outgoing α -particles from ${}^{56}\text{Fe}(\alpha, \alpha'){}^{56}\text{Fe}$. The dashed line indicates the contribution of a single peak to the whole spectrum. The states at -2.96, -3.125 and -3.37 MeV are only analyzed for background considerations.
- Fig. 3: Experimental differential cross sections: 56 Fe(α, α') 56 Fe. The theoretical curve represents the result of the conventional optical model analysis of elastic scattering. This paper is not engaged in the angular distribution of the 3 state shown.
- Fig. 4: Folding model analysis of elastic scattering. In the inserted χ^2 -contour plot over the $c_m a_m$ -plane the correlation between these two parameters is demonstrated. The full line shows the corresponding values of c_m and a_m for $\chi^2 = 1.5 \cdot \chi^2_{min}$. The dashed straight lines mark constant rms-radii and the bend dashed line follows the valley of minimal χ^2/F for given a_m shown in the second inserted graph.
- Fig. 5: Symmetric rotator model analysis of inelastic scattering using the folding procedure. The parameters of the interaction potentials are given in tab. 2 (line5).
- Fig. 6: Triaxial rotator model analysis of inelastic scattering using the folding procedure. The dashed $2\frac{1}{2}^{+}$ angular distribution corresponds to $\gamma = 10^{\circ}$. Interaction potential parameters are given in tab. 4 (line2). The inserted graph shows the curve of the χ^2 -values per degree of freedom over the asymmetry angle γ .

F-1



Zykl. 30,10.74

Fig. 1









Fig. 3



Fig. 4



Fig. 5



Fig. 6

•

Appendix

Experimental cross sections: The quoted errors of the experimental cross sections include the error arising from the finite angular acceptance which is converted into a cross section error.

This paper is not engaged in the cross sections of the -3 state given.

- A2 -

SCATTERING OF 104 NEV ALPHAPARTICLES DN 56 FE

Q = 0.0 NEV I = 0+ ECH = 97.064 NEV K = 4.1647/FERMI ETA = 1.60628

| LA THE TA DEGREE | BORATORY DA SIGMA MB/SR | TA DSIGHA ¥ | RUTHERFORD SIGMA/SR | THETA DEGREE | CH DATA SIGHA MB/SR | D SIGMA · HB / SR |
|------------------------------|--|--------------------------|--|------------------------------|--|--|
| 6.00 7.00 8.00 8.50 | 1.812E 04 4.410E 03 2.501E 03 2.877E 03 | 7.6 4.3 3.1 1.5 | 4.211E-01 1.897E-01 1.834E-01 2.688E-01 | 6.44 7.51 8.58 9.12 | 1.574E 04 3.832E 03 2.174E 03 2.501E 03 | 1.191E 03 1.664E 02 6.784E 01 3.661E 01 |
| 8.65 9.00 | 2.741E 03 3.071E 03 | 1.7 1.2 | 2.746E-01 3.605E-01 | 9.28 9.66 | 2.383E 03 2.670E 03 | 3,977E 01 3,195E 01 |
| 9.15 9.50 | 2.968E 03 2.895E 03 | 0,5 3.1 | 3.722E-01 4.217E-01 | 9.82 10.19 | 2.581E 03 2.518E 03 | 1.325E 01 7.833E 01 |
| 9.65 10.00 | 2.886E 03 2.445E 03 | 1.2 | 4.475E-01 4.370E-01 | 10.35 10.73 | 2.510E 03 2.127E 03 | 3.016E 01 8.899E 01 |
| 10.15 10.50 | 2.625E 03 1.934E 03 | 3.7 0.7 | 4•979E-01 4•200E-01 | 10,89 11,27 | 2.284E 03 1.683E 03 | 0.526E 01 1.106E 01 |
| 10.65 11.00 | 1.907E 03 1.316E 03 | 7.2 8.9 | 4.382E-01 3.440E-01 | 11.43 11.80 | 1.659E 03 1.145E 03 | 1.196E 02 1.015E 02 |
| 11.15 11.50 | 1.251E 03 7.329E 02 | 9.2 10.8 | 3•452E-C1 2•287E-01 | 11.96 12.34 | 1.089E 03 6.380E 02 | 1.000E 02 6.899E 01 |
| 11.65 | 7.578E 02 3.367E 02 | 11.9 13.5 | 2.491E-01 1.245E-01 | 12.50 | 6.597E 02 2.932E 02 | 7.820E 01 3.967E 01 |
| 12.15 | 3.532E 02 1.090E 02 | 18.6 | 1•372E-01 4•743E-02 | 13.03 | 3.076E 02 9.494E 01 | 5.734E 01 1.449E 01 |
| 13.00 | 2. 586E 01 | 25.3 | 1.316E-02 | 13.94 | 2.253E 01 | 5.697E 00 |
| 13.50 | 5.852E 01 | 23.0 | 3+460E-02 | 14.48 | 5.100E 01 | 1.174E 01 |
| 14.00 | 1.259E 02 | 14.2 | 8.603E-02 1.052E-01 | 15.02 | 1.097E 02 | 1.560E 01 |
| 14.50 | 2.154E 02 2.494E 02 | 7.2 | 1.692E-01 2.041E-01 | 15.55 | 1.878E 02 2.175E 02 | 1.346E 01 |
| 15.00 | 2.926E 02 3.086E 02 | 2.1 | 2.631E-01 2.687E-01 | 16.09 | 2.552E 02 2.692E 02 | 5.252E 00 6.505E 00 |
| 15.50 15.65 | 3.222E 02 3.208E 02 | 1.2 | 3.301E-01 3.414E-01 | 16.62 16.78 | 2.811E 02 2.799E 02 | 3.315E 00 5.388E 00 |
| 16.00 16.15 | 3.040E 02 2.487E 02 | 4.5 4.6 | 3.533E-01 2.999E-01 | 17.16 17.32 | 2.653E 02 2.171E 02 | 1.191E 01 1.007E 01 |
| 16.50 16.65 | 2.360E 02 2.063E J2 | 5.0 5.3 | 3.099E-01 2.808E-01 | 17.69 17.85 | 2.061E 02 1.801E 02 | 1.032E 01 9.553E 00 |
| 17.00 17.15 | 1.771E 02 1.413E 02 | 8.2 | 2.619E-01 2.163E-01 | 18.23 18.39 | 1.547E 02 1.234E 02 | 1.263E 01 8.004E 00 |
| 17.50 | 1.049E 02 7.821E 01 | 1.2 | 1.740E-01 1.342E-01 | 18.76 | 9.166E 01 6.835E 01 | 1.089E 00 6.749E 00 |
| 18.00 | 3.144F 01 | 13.4 | 9.435E-02 6.028E-02 | 19.30 | 4.446E 01 2.749E 01 | 5.977E 00 3.699E 00 |
| 18.50 | 9.113E 00 | 32.8 | 3.4025-02 1.9465-02 | 19.83 | 7.970E 00 | 2.616E 00 |
| 19.15 | 5.672E 01 | 12.0 | 1.345E-02 | 20.53 | 4.962E 00 | 5.934E-01 |
| 19.65 | 1.568E 01 | 18.9 | 4.118E-02 8.010E-02 | 21.06 | 1.372E 01 | 2,588E 00 |
| 20.15 | 3.443E 01 4.862E 01 | 6.2 4.4 | 9.989E-02 1.510E-01 | 21.60 | 3.015E 01 4.259E 01 | 1.872E 00 |
| 20.65 | 5,262E 01 5,904E 01 | 3,9 | 1.682E-01 2.017E-01 | 22.13 | 4.610E 01 5.174E 01 | 1.799E 00 1.670E 00 |
| 21.15 21.50 | 6.231E 01 6.829E 01 | 1.6 0.9 | 2.190E-01 2.561E-01 | 22.67 23.04 | 5.461E 01 5.987E 01 | 8.644E-01 5.170E-01 |
| 21.65 22.00 | 6.844E 01 6.672E 01 | 1.2 3.0 | 2.638E-01 2.740E-01 | 23.20 23.57 | 6.001E 01 5.852E 01 | 7.026E-01 1.750E 00 |
| 22.15 22.50 | 5.819E 01 5.706E 01 | 3,3 4,2 | 2.454E-01 2.560E-01 | 23.73 24.11 | 5.104E 01 5.007E 01 | 1.673E 00 2.099E 00 |
| 22.65 23.00 | 5.014E 01 4.532E 01 | 4.4 | 2•310E-01 2•218E-01 | 24.27 | 4.400E 01 3.979E 01 | 1.943E 00 2.771E 00 |
| 23.15 | 3.723E 01 2.968E 01 | 4.3 | 1.869E-01 1.581E-01 | 24.80 | 3.269E 01 2.607E 01 | 1.407E 00 1.853E 00 |
| 23.65 | 1. 92 6E 01 | 7.9 | 1.115E-01 | 25.71 | 1.693E 01 | 1. 344E 00 |
| 24.15 | 1. 173E 01 | 13.0 | 7.365E-02 6.5025-02 | 25.87 | 1.031E 01 | 1,336E 00 |
| 25.00 | 7.771E 00 | 2.2 | 5.283E-02 5.247E-02 | 26.78 | 6.836E 00 | 1.519E-01 2.208E-01 |
| 25.50 | 7.957E 01 8.315E 00 | 7.5 | 5•848E-02 6•253E-02 | 27.31 27.47 | 7.003E 00 7.320E 00 | 5.240E-01 3.055E-01 |
| 26.00 | 1.081E 01 1.143E 01 | 5.6 | 8.575E-02 9.274E-02 | 27.84 28.00 | 9.520E 00 1.007E 01 | 5.338E-01 3.998E-01 |
| 26.65 27.15 | 1.394E 01 1.694E 01 | 3.3 2.3 | 1.218E-01 1.593E-01 | 28.53 29.07 | 1.228E 01 1.494E 01 | 4.095E-01 3.451E-01 |
| 27.65 28.15 | 1.845E 01 1.721E 01 | 1.6 | 1.864E-01 1.865E-01 | 29.60 30.13 | L.628E 01 1.519E 01 | 2.588E-01 3.123E-01 |
| 28.65 29.15 | 1.555F 01 1.329E 01 | 2.3 | 1.805E-01 1.651E-01 | 30.66 31.20 | 1.374E 01 1.175E 01 | 3.214E-01 3.349E-01 |
| 29.65 | 1.096E CL 8.337E 00 | 3.4 | 1.455E-01 1.182E-01 | 31.73 | 9.693E 00 7.378E 00 | 3.326E-01 5.032E-01 |
| 31.15 | 4.889E 00 | 4.8 | 8.880E-02 7.872E-02 | 33.32 | 4.332E 00 | 2.064E-01 |
| 31.65 | 3. 585E DO | 5.5 | 6 • 142E-02 | 33.85 | 3.178E 00 | 1.763E-01 |
| 32.65 | 3.630E 00 3.673E 00 | 2.1 2.3 | 7.020E-02 7.291E-02 | 34.92 35.15 | 3.223E 00 3.262E 00 | 6.706E-02 7.587E-02 |
| 33.15 33.65 | 3.902E 00 4.016E 00 | 3.4 3.4 | 8.005E-02 8.733E-02 | 35.45 35.98 | 3.466E 00 3.570E 00 | 1.166E-01 1.229E-01 |
| 34.15 34.37 | 4.172E 00 4.484E 00 | 2.5 3.1 | 9.607E-02 1.059E-01 | 36.51 36.74 | 3.711E 00 3.990E 00 | 9.448E-02 1.241E-01 |
| 34.65 35.15 | 4.198E 00 3.778E 00 | 3.5 4.0 | 1.023E-01 9.730E-02 | 37.04 37.57 | 3.737E 00 3.366E 00 | 1 • 2 9 2 E - 01 1 • 3 5 2 E - 01 |
| 35.65 35.87 | 3.229E 00 2.885E 00 | 3.2 5.1 | 8 • 78 3E-02 8 • 0 37 E-02 | 38.10 38.33 | 2.879E 00 2.573E 00 | 9.236E-02 1.318E-01 |
| 36.15 | 2.696E 00 2.206E 00 | 5.2 6.0 | 7.740 E-02 6.678 E-02 | 38.63 39.16 | 2.405E 00 1.970E 00 | 1.257E-01 1.172E-01 |
| 37+15 | 1. 42 7E 00 | 4. 2 6. 4 | 5+442E+C2 4+793E+02 | 40.22 | 1.524E 00 | 8.192E-02 |
| 38.65 | 1.150E 00 | 3.5 | 4.273E-02 | 41.27 | 1.030E 00 | 3.635E-02 |
| 39.65 | 1. 32 3C 00 1. 16 8E 00 | 5.4 | 5.423E-02 5.023E-02 | 42.33 42.86 | 1.187E 00 1.048E 00 | 6+464E-02 3+482E=02 |
| 40.65 41.15 | 1.523E 6.1 1.594E 30 | 5.3 4.9 | 6.868E-02 7.533E-02 | 43.39 | 1.368E 00 1.433E 00 | 7. 22'7E - 92 6. 958E - 92 |
| 41.65 | 1.198E 00 1.283E 00 | 3.2 5.3 | 5.929E-02 6.646E-02 | 44.44 44.97 | 1.078E 00 1.156E 00 | 3.484E-02 6.124E-02 |
| 42.65 43.15 | 1.377E 00 1.028E 00 | 5.5 3.7 | 7.461E-02 5.823E-02 | 45.50 46.92 | 1.241E 00 9.274E-01 | 6.769E-02 3.436E-02 |
| 44.15 44.65 | 1.003E 00 8.272E-01 | 6.4 4.4 | 6.199E-02 5.336E-02 | 47.08 47.60 | 9.064E-01 7.482E-01 | 5.826E-02 3.278E-02 |
| 45.15 46.15 | 7.685E-01 7.167E-01 | 6.2 4.8 | 5.172E-02 5.240E-02 | 48.13 49.18 | 6.957E-01 6.500E-01 | 4.294E-02 3.112E-02 |
| 46.65 | 9.248L-01 1.021L 00 | 5.3 | 1.043E-02 8.095E-02 5.7475.00 | 49.70 | 8.395E-01 9.277E-01 | 4.880F-02 4.916E-02 |
| 48.15 | 9.152E-01 | 5.7 | 7.853E-02 | 51.28 | 8.331E-01 | 0.4018 - 02 4.740E - 02 5.1005-02 |
| 50 • 15 50 • 45 | 7. 743E-01 | 7.7 | 7.0740E-02 7.079E-02 | 53,37 53,00 | 7.075E-01 | 5. 461E-02 |
| 52.15 55.15 | 4.608E-01 3.820E-01 | 13.1 | 5.330E-02 5.436E-02 | 55.47 | 4.227E-01 3.525E-01 | 5.538E-02 3.324E-02 |
| 56,65 58,15 | 4.434E-01 3.425E-01 | 8.4 9.3 | 6.965E-02 5.920E-02 | 60.16 61.72 | 4.105E-01 3.181E-01 | 3.447E-02 2.964E-02 |

SCATTERING OF 104 NEV ALPHAPARTICLES ON 56 FE

| | | Q = -0.847 | MEV | | 1 = | 2+ |
|-----|---|--------------------|-------|-------------|-----|---------------|
| EC₽ | - | 96.218 P EV | κ = - | 4.1465/FERM | I | ETA = 1.61333 |
| | | | | | | |

| | LABORATORY DATA Theta Sigma Dsigma Degree Mb/Sr 7 | CM DATA Theta Signa Degree Mb/Sr Mb/Sr |
|---|--|---|
| | 6.00 2.120E 02 37.1 7.00 1.520E 02 6.1 | 6.44 1.841E 02 6.831E 01 7.51 1.320E 02 8.089E 00 |
| | 8.00 6.319E 01 12.2 8.50 2.873E 01 12.6 8.65 3.544E 01 11.8 | 8.59 5.490E 01 6.676E 00 9.12 2.496E 01 3.146E 00 9.28 3.080E 01 3.637E 00 |
| | 9.00 1.255E 01 8.2 9.15 1.466E 01 17.0 | 9.66 1.091E 01 8.899E-01 9.82 1.274E 01 2.166E 00 |
| | 9.50 8.711E 00 21.4 9.65 1.074E 01 3.5 | 10.20 7.572E 00 1.618E 00 10.36 9.336E 00 3.276E-01 10.73 1.562E 01 3.1465 00 |
| • | 10.15 1.722E 01 8.4 10.50 3.596E 01 11.8 | 10.89 1.497E 01 1.260E 00 11.27 3.127E 01 3.705E 00 |
| | 10.65 2.475E 01 9.0 11.00 5.717E 01 5.2 | 11.43 2.152E 01 1.943E 00 11.80 4.973E 01 2.591E 00 |
| | 11.15 3.915E 01 8.7 11.50 7.185E 01 1.3 11.55 5.949E 01 5.5 | 11.97 3.408E 01 2.970E 00 12.34 6.251E 01 7.842E-01 12.50 5.089E 01 2.782E 00 |
| | 12.00 7.532E 01 0.9 12.15 7.072E 01 1.7 | 12.08 6.555E 01 5.904E-01 13.04 6.155E 01 1.030E 00 |
| | 12.50 7.318E 01 3.9 12.65 6.780E 01 1.9 | 13.41 6.370E 01 2.490E 00 13.57 5.902E 01 1.147E 00 |
| | 13.00 5.911E 01 6.5 13.15 5.870E 01 5.0 13.50 4.002E 01 6.4 | 13495 5.1476 01 3.3486 00 14.11 5.1126 01 2.5756 00 14.48 3.4866 01 2.2346 00 |
| | 13.65 3.876E 01 9.6 14.00 2.727E 01 9.9 | 14.65 3.376E 01 3.236E 00 15.02 2.376E 01 2.347E 00 |
| | 14.15 2.196E 01 12.7 14.50 1.382E 01 16.6 14.65 1.114E 01 30.1 | 15.18 1.912E 01 2.434E 00 15.56 1.204E 01 2.4004E 00 15.72 9.709E 00 2.922E 00 |
| | 15.00 7.446E 00 13.6 15.15 4.766E 00 16.4 | 16.09 6.491E 00 8.822E-01 16.25 4.155E 00 6.832E-01 |
| | 15.50 2.456E 00 21.9 15.65 3.750E 00 17.0 | 16.63 2.142E 00 4.686E-01 16.79 3.271E 00 5.546E-01 |
| | 16.00 5.101E 00 16.9 16.15 1.089E 01 6.8 16.50 9.366E 00 13.9 | 17.16 4.450E 00 7.536E-01 17.32 9.501E 00 6.433E-01 17.70 8.173E 00 1.338E 00 |
| | 16.65 1.073E 01 6.8 17.00 1.582E 01 7.4 | 17.86 9.365E 00 6.414E-01 18.23 1.381E 01 1.018E 00 |
| | 17.15 1.729E 01 4.3 17.50 2.153E 01 2.5 17.65 2.117E 01 2.5 | 18.39 1.510E 01 6.431E-01 18.77 1.880E 01 4.631E-01 18.93 1.860E 01 4.631E-01 |
| | 18.00 2.377E 01 1.3 18.15 2.311E 01 1.8 | 19-30 2-077E 01 2-633E-01 19-46 2-019E 01 3-641E-01 |
| | 18.50 2.408E 01 3.7 18.65 2.235E 01 1.9 | 19.84 2.105E 01 7.800E-01 20.00 1.954E 01 3.623E-01 |
| | 19.00 1.979E 01 2.6 19.15 1.578E 01 3.8 19.50 1.743E 01 5.6 | 20.37 1.730E 01 4.539E-01 20.53 1.730E 01 6.654E-01 20.91 1.525E 01 8.546E-01 |
| | 19.65 1.545E 01 6.1 20.00 1.266E 01 7.8 | 21.07 1.352E 01 8.245E-01 21.44 1.108E 01 8.642E-01 |
| | 20.15 1.043E 01 6.1 20.50 7.840E 00 8.8 | 21.60 9.128E 00 5.534E-01 21.98 6.863E 00 6.032E-01 |
| | 20.65 6.5022 00 7.7 21.00 4.500E 00 4.9 21.15 3.712E 00 6.6 | $22 \cdot 14$ $5 \cdot 5935$ 00 $4 \cdot 3935 - 01$ $22 \cdot 51$ $3 \cdot 941E$ 00 $1 \cdot 926E - 01$ $27 \cdot 67$ $3 \cdot 251E$ 00 $2 \cdot 132E - 01$ |
| | 21.50 3.608E 00 3.2 21.65 3.024E 00 4.1 | 23.05 3.161E 00 1.008E-01 23.21 2.650E 00 1.083E-01 |
| | 22+00 3+628E 00 9+6 22+15 3+784E 00 6+3 22-50 5-268E 00 5+4 | 23.58 3.180E 00 3.048E-01 23.74 3.318E 00 2.076E-01 24.11 4.620E 00 2.076E-01 |
| | 22.65 4.956E 00 6.0 23.00 6.806E 00 3.0 | 24.65 5.972E 00 1.780E-01 |
| | 23.15 6.659E 00 4.3 23.50 7.443E 00 5.3 | 24.81 5.844E 00 2.499E-01 25.18 6.534E 00 3.473E-01 |
| | 24.00 9.241E 00 2.0 24.15 9.252E 00 2.2 | 25.72 8.117E 00 1.631E-01 25.88 8.127E 00 1.794E-01 |
| | 24.50 9.371E 00 7.2 24.65 9.353E 00 1.6 | 26.25 8.235E 00 5.890E-01 26.41 8.220E 00 1.339E-01 |
| | 25.00 9.049E 00 3.8 25.15 8.359E 00 3.0 25.50 7.569E 00 4.6 | 26.78 7.956E 00 3.054E-01 26.94 7.351E 00 2.187E-01 27.32 6.658E 00 3.062E-01 |
| | 25.65 7.136E 00 3.7 26.00 6.040E 00 5.6 | 27.48 6.279E 00 2.330E-01 27.85 5.316E 00 3.000E-01 |
| | 26.15 5.489E 00 4.8 26.65 3.587E 00 5.5 27.15 2.569E 00 5.7 | 28.01 4.832E 00 2.339E-01 28.54 3.512E 00 1.925E-01 29.07 2.412E 00 1.925E-01 |
| | 27.65 2.301E 00 5.0 28.15 2.022E 00 5.1 | $29 \cdot 61$ $2 \cdot 617E$ 00 $1 \cdot 241E \cdot 01$ $29 \cdot 61$ $2 \cdot 629E$ 00 $1 \cdot 619E - 01$ $30 \cdot 14$ $1 \cdot 784E$ 00 $9 \cdot 114E - 02$ |
| | 28.65 2.354E 00 4.2 29.15 2.825E 00 3.7 | 30.67 2,078E 00 8.778E 02 31.20 2.496E 00 9.161E-02 |
| | 29.65 3.3082 00 2.8 30.15 3.8092 00 3.1 30.65 3.7875 00 3.8 | 31.74 2.924E 00 8.184E-02 32.27 3.369E 00 1.034E-01 32.80 3.352E 00 1.260E-01 |
| | 31.15 3.718E 00 2.5 31.37 3.350E 00 4.1 | 33.33 3.293E 00 8.210E-02 33.57 2.968E 00 1.212E-01 |
| | 31.65 3.788E 00 4.6 32.15 2.724E 00 7.0 32.65 2.263E 00 3.9 | 33.86 3.357E 00 1.547E-01 34.39 2.416E 00 1.700E-01 34.93 2.00E 00 7.881E-02 |
| | 32.87 2.127E 00 4.3 33.15 1.624E 00 5.6 | 35.16 1.888E 00 8.169E 02 35.46 1.442E 00 8.022E-02 |
| | 33.65 1.761E 00 5.1 34.15 1.318E 00 3.5 | 35.99 1.565E 00 8.047E-02 36.52 1.172E 00 4.074E-02 |
| | 34.57 1.330E 00 3.8 34.65 1.360E 00 7.2 35.15 1.278E 00 4.3 | 30.75 1.1835 00 4.450E-02 37.05 1.210E 00 8.751E-02 37.58 1.138E 00 4.883E-02 |
| | 35.65 1.388E 00 3.2 35.87 1.376E 00 4.0 | 38.11 1.237E 00 3.914E-02 38.34 1.227E 00 4.912E-02 |
| | 36.15 1.657E 00 4.7 36.65 1.667E 00 4.9 37.15 1.685E 00 3.0 | 38.64 1.478E 00 6.981E-02 39.17 1.488E 00 7.266E-02 39.70 1.505E 00 4.468E-02 |
| | 37.65 1.622E 00 5.1 38.15 1.570E 00 5.1 | 40.23 1.450E 00 7.29E 02 40.76 1.404E 00 7.205E 02 |
| | 38.65 1.329E 00 3.4 39.15 1.344E 00 5.5 39.65 1.050E 00 5.5 | 41.28 1.190E 00 4.074E-02 41.81 1.204E 00 6.665E-02 |
| | 40.15 5.716E-01 6.1 40.65 1.062E 00 10.5 | 42.84 3.40 9.537E-01 3.138E-02 43.40 9.537E-01 9.968E-02 |
| | 41.15 1.015E 00 6.0 41.65 8.359E-01 3.7 | 43.93 9.122E-01 5.431E-02 44.45 7.519E-01 2.802E-02 |
| | 42.15 1.158E 00 5.6 42.65 1.092E 00 6.3 43.15 8.967E-01 3.6 | 44.98 1.042E 00 5.869E-02 45.51 9.839E-01 6.155E-02 46.03 8.086E-01 2.913F-02 |
| | 44.15 1.024E 00 5.9 44.65 8.734E-01 4.2 | 47.09 9.250E-01 5.481E-02 47.61 7.897E-01 3.325E-02 |
| | 45•15 8•667E-01 6•0 46•15 7•330E-01 4•4 66•65 8•039E-01 4•3 | 48.14 7.843E-01 4.674E-02 49.19 6.645E-01 2.905E-02 69.72 7.285E-01 4.55E-02 |
| | 47.15 7.786E-01 6.1 47.65 6.674E-01 8.7 | 50.24 7.071E-01 4.329E-02 50.77 6.067E-01 5.297E-02 |
| | 48.15 6.821E-01 6.6 49.15 5.710E-01 9.9 | 51.29 6.207E-01 4.076E-02 52.34 5.205E-01 5.169E-02 |
| | 50.65 5.755E-01 11.3 52.15 3.418E-01 15.4 | 53•39 3•5492−01 4•611E−02 53•91 5•262E−01 5•921E−02 55•48 3•134E−01 4•838E−02 |
| | 52.65 3.870E-01 8.2 54.15 1.654E-01 12.8 | 56.00 3.552E-01 2.922E-02 57.57 1.523E-01 1.945E-02 |
| | 55.15 3.736E-01 9.0 56.65 2.937E-01 10.3 58.15 3.337E-01 0.5 | 58.61 3.447E-01 3.110E-02 60.17 2.718E-01 2.808E-02 61.73 2.925-01 2.805E-02 |
| | 50+15 5+225E-01 9+5 63+15 1+187E+01 14+4 64+65 8+609E-02 17+5 | 61.73 2.5792T=01 2.6829E=02 66.91 1.114E=01 1.604E=02 68.46 8.109E=02 1.419E=02 |
| | 66.15 6.716E-02 19.0 | 70.01 6.348E-02 1.206E-02 |

- A4 -

SCATTERING OF 104 MEV ALPHAPARTICLES ON 56 FE

Q = -2.085 MEV I = 4+

ECM = 94.979 MEV K = 4.1198/FERMI ETA = 1.62381

| LA | BORATORY DA | TA | ТИЕТА | | DSTGMA |
|-----------------|----------------------------|--------------|----------------|------------------------|------------------------|
| DEGREE | MB/SR | 8310HA 8 | DEGREE | MB/SR | MB / SR |
| 12.15 | 8.811E-01 7.182E-01 | 11.4 | 13.04 | 7.662E-01 | 8.757E=02 |
| 13.15 | 8.691E-01 | 9.3 | 14.12 | 7.562E-01 | 7.030E-02 |
| 13.65 14.15 | 6.362E-01 7.940E-01 | 9°2 11°2 | 14.65 15.19 | 5.537E-01 6.912E-01 | 5°06/E-05 7°948E-05 |
| 14.65 | 1.029E 00 | 9.4 13.5 | 15.72 | 8.961E-01 | 8.409E-02 |
| 16.15 | 1.085E 00 | 12.9 | 17.33 | 9.458E-01 | 1.219E-01 |
| 16,65 17,15 | 1.097E 00 2.726E-01 | 12.8 21.0 | 17.87 | 9.566E-01 2.378E-01 | 1.229E=01 4.999E=02 |
| 17.65 | 2.186E-01 | 14.9 | 18.94 | 1.908E-01 | 2.842E-02 |
| 19,65 | 3.981E-01 | 12.5 | 21.08 | 3.480E-01 | 4.336E-02 |
| 20.15 | 4.808E-01 6.430E-01 | 8.3 | 21.61 22.15 | 4°204E-01 2°622E-01 | 4.213E-02 4.665E-02 |
| 21.15 21.65 | 6.065E-01 5.154E-01 | 9°1 | 22°68 23°22 | 5。308E-01 4。513E-01 | 4。841E-02 4。543E-02 |
| 22.15 | 4.549E-01 | 11.3 | 23.75 | 3.985E-01 | 4.487E=02 |
| 23,15 | 2.617E-01 | 13.7 | 24.82 | 2.834E-01 2.295E-01 | 3.1348-02 |
| 23,65 24,15 | 2.659E-01 2.826E-01 | 11.9 10.4 | 25°35 25°89 | 2°333E-01 2°481E-01 | 2°771E-05 2°242 |
| 24.65 | 2.751E-01 | 8.2 | 26.42 | 2.416E-01 | 1.974E-02 |
| 25.65 | 3. 715E-01 | 10.3 | 27.49 | 3. 266E-01 | 3.379E-02 |
| 26.15 26.65 | 4.324E-01 4.582E-01 | 11.5 9.3 | 28°02 52°52 | 3.804E-01 4.033E-01 | 4₀367E-02 3₀765E-02 |
| 27.15 | 4.765E-01 | 7.0 | 29.09 | 4.196E-01 | 2.921E-02 |
| 28,15 | 4. 304 E-01 3. 971 E-01 | 9.0 | 30.15 | 3.501E-01 | 3.143E-02 |
| 28.65 29.15 | 3.727E-01 3.147E-01 | 8.3 7.9 | 30°69 31°22 | 3°288E-01 2°778E-01 | 2°719E-05 2°501E-05 |
| 29.65 | 2.688E-01 | 8.3 | 31.75 | 2.374E-01 | 1.979E-02 |
| 30. 15 | 2.273E-01 | 15.5 | 32.81 | 2.010E-01 | 3.111E-02 |
| 31.15 31.37 | 2.358E-01 2.196E-01 | 13.1 9.0 | 33°35 33°58 | 2。087E-01 1。944E-01 | 2.110E-02 1.752E-02 |
| 31.65 | 2.844E-01 | 13.8 | 33.88 | 2.518E-01 | 3.473E-02 |
| 32.65 | 2.619E-01 | 8.5 | 34.94 | 2. 322E-01 | 1.981E-02 |
| 32.87 33.15 | 2.597E-01 3.351E-01 | 7.3 13.7 | 35°17 35°47 | 2。303E-01 2。973E-01 | 1.680E-02 3.182E-02 |
| 33.65 | 3.596E-01 | 11.3 | 36.00 36.53 | 3.193E-01 | 3.614E-02 |
| 34.37 | 2.194E-01 | 9.5 | 36.77 | 1.950E-01 | 1.849E-02 |
| 34.65 35.15 | 2.474E-01 2.199E-01 | 13.3 13.5 | 37°06 37°59 | 2.200E-01 1.957E-01 | 2.936E-02 2.641E-02 |
| 35,65 35,87 | 1.519E-01 | 10.1 | 38°12 38°36 | 1.353E-01 | 1.370E-02 |
| 36.15 | 1.123E-01 | 18.6 | 38,65 | 1.001E-01 | 1.8586-02 |
| 36.65 37.15 | 2.072E-01 1.309E-01 | 13.8 11.6 | 39°18 39°11 | 1.848E-01 1.168E-01 | 2.549E-02 1.359E-02 |
| 37.65 38.15 | 9.357E-02 | 20.6 17.8 | 40°24 40°24 | 8。357E-02 1。048E-01 | 1.720E-02 |
| 38.65 | 1.267E-01 | 10.6 | 41.30 | 1.133E-01 | 1.197E-02 |
| 39.15 39.65 | 1.991E-01 | 14.0 | 42.36 | 1. 342E-01 | 2.499E-02 |
| 40°15 40° 65 | 1.199E-01 1.564E-01 | 10.4 15.8 | 42°83 43°41 | 1.075E-01 1.404E-01 | 1.122E-02 2.219E-02 |
| 41.15 | 1.457E-01 | 15.7 | 43.94 | 1.309E-01 | 2.055E-02 |
| 42.15 | 1.114E-01 | 18.1 | 45.00 | 1.002E-01 | 1.809E-02 |
| 42.65 43.15 | 1.168E-01 8.493E-01 | 18.3 1.2 | 45°53 46°05 | 1.052E-01 7.654E-01 | 1₀924E∞02 9₀283E-03 |
| 44.15 | 1.079E-01 | 18.3 | 47.11 | 9.741E-02 | 1.780E-02 |
| 45,15 | 9.411E-02 | 17.7 | 48.16 | 8.511E-02 | 1.507E-02 |
| 46.15 46.65 | 6.163E-02 9.055E-02 | 15°5 18°8 | 49°21 49°24 | 5°584E-02 8°212E-02 | 8.633E-03 1.544E-02 |
| 47.15 | 1.023E-01 | 17.0 | 50.26 50.79 | 9.286E-02 | 1.578E-02 |
| 48.15 | 1.354E-02 | 46.4 | 51.31 | 1.231E-02 | 5.716E-03 |
| 49。15 50。15 | 4.327E-02 1.610E-01 | 35.7 13.5 | 52,36 53,41 | 3。942E-02 1。470E-01 | 1.449E-02 1.991E-02 |
| 50.65 | 7.643E-02 | 30°7 | 53,93 | 6.984E-02 | 2.143E-02 |
| 52.15 | 3. 748E-02 | 45.1 | 55,50 | 3.435E-02 | 1.550E-02 |
| 52°65 54°15 | 8.389E-02 1.735E-02 | 17.6 39.0 | 56°05 21°52 | 7。696E-02 1。597E-02 | 1.355E-02 6.230E-03 |
| 55.15 | 1.029E-01 | 16.9 | 58.63 | 9.489E-02 | 1.599E-02 |
| 58,15 | 5.179E-02 | 23.6 | 61.75 | 4.806E-02 | 1.134E-02 |
| 63.15 64.65 | 1.172E-02 3.600E-02 | 45°2 26°9 | 66°94 68°48 | 1.100E-02 3.390E-02 | 4。967E-03 9。115E-03 |
| 66.15 | 7.950E-03 | 59.7 | 70.03 | 7.512E-03 | 4.487E-03 |

SCATTERING OF 104 MEV ALPHAPARTICLES ON 56 FE

Q = -2.658 MEV I = 2+

ECM = 94.406 MEV K = 4.1073/FERMI ETA = 1.62873

| LA | BORATORY DA | ТА | | CM DATA | |
|-----------------|------------------------|--------------|-----------------------------|------------------|-------------------|
| τηε τα | SIGMA | DSIGMA | THETA | SIGMA | DSIGMA |
| DEGREE | MB/SR | æ | DEGREE | MB/SR | MB/SR |
| 8.65 | 4.779E 00 | 10.7 | 9.29 | 4.148E 00 | 4.434E-01 |
| 9.15 | 2.397E 00 | 13.5 | 9.83 | 2.081E 00 | 2.806E-01 |
| 9.65 | 1.822E 00 | 5.3 | 10.36 | 1.582E 00 | 9.993E-02 |
| 10.15 | 2.560E 00 | 7.0 | 10.90 | 2.223E 00 | 1.562E-01 |
| 10.65 | 2.936E 00 | 6.8 | 11.44 | 2.550E 00 | 1.736E-01 |
| 11.15 | 3.885E 00 | 6.8 | 11,97 | 3.375E 00 | 2.306E-01 |
| 11.65 | 4.992E 00 | 4.4 | 12.51 | 4.338E 00 | 1.907E-01 |
| 12.15 | 5.516E 00 | 3.8 | 13.05 | 4°795E 00 | 1.809E-01 |
| 12.65 | 4.729E 00 | 4.9 | 13.58 | 4º112E 00 | 2.034E-01 |
| 13.15 | 3.675E 00 | 7.0 | 14.12 | 3.196E 00 | 2.247E-01 |
| 13.65 | 2 . 744E 00 | 9.5 | . 14.65 | 2°387E 00 | 2º258E-01 |
| 14.15 | 1.590E 00 | 12.3 | 15.19 | 1.384E 00 | 1.703E-01 |
| 14.65 | 1.163E 00 | 12.1 | 15.73 | 1.012E 00 | 1.221E-01 |
| 15,15 | 5.603E-01 | 19.5 | 16.26 | 4.879E-01 | 9.500E-02 |
| 15.65 | 5.433E-01 | 17.1 | 16.80 | 4.733E-01 | 8.106E-02 |
| 16.15 | 1.338E 00 | 6.9 | 17.33 | 1.166E 00 | 8.059E-02 |
| 16.65 | 5.802E-01 | 16.0 | 17.87 | 5.058E-01 | 8.109E-02 |
| 17.15 | 1.289E 00 | 99 | 18.41 | 1.124E 00 | 1.114E-01 |
| 17.65 | 1.577E 00 | 89 | 18.94 | 1.376E 00 | 1.221E-01 |
| 18.15 | 2.389E 00 | 4.9 | 19.48 | 2.085E 00 | 1.027E-01 |
| 18.65 | 2.077E 00 | 4.7 | 20.01 | 1.813E 00 | 8.470E-02 |
| 19.15 | 1.904E 00 | 6.0 | 20.55 | L. 663E 00 | 1.005E-01 |
| 19.65 | 1.499E 00 | | 21.08 | 1.310E 00 | 1.007E-01 |
| 20.15 | 1.021E 00 | 904 | 21.02 | 8.925E-01 | 8.350E=02 |
| 200 65 | | 1100 | 22013 | | 6 11 (E= 92 |
| 21012 | 5.002 E-01 | 1001 | 22007 | $5_{0} 520 = 01$ | |
| 22012 | | | 23012 | | 4 e 9 3 4 E = U 2 |
| 22000 | 5.544 5-01 | 1001 | 24027 | 40 41 3 C - VI | 4 4442E-02 |
| 23015 | 5 0085-01 | 700 | 24002 | 4.6715-01 | 2-070E=02 |
| 2/15 | 7 2485-01 | 5.5 | 25,89 | 4.360E=01 | 2.5175-02 |
| 24015 | 6.871 E-01 | 5.3 | 25007 | 6.032E-01 | 3.789E=02 |
| 25,15 | 4. 721 E-01 | 7.1 | 26.96 | 4.147E-01 | 2.930F=02 |
| 25.65 | 5. 345E-01 | 5.2 | 27,49 | 4.697E-01 | 2.465F= 02 |
| 26,15 | 4. 022 E-01 | 7.6 | 28.03 | 3-537E-01 | 2.695E-02 |
| 26.65 | 3.386E-01 | 9.4 | 28,56 | 20979E-01 | 2.799F=02 |
| 27.15 | 2.607E-01 | 10.6 | 29.09 | 2.295E-01 | 2.442E-02 |
| 27.65 | 1.652E-01 | 13.3 | 29.63 | 1.455E-01 | 1.940E-02 |
| 28.15 | 9.484E-02 | 16.2 | 30.16 | 8.359E-02 | 1.355E-02 |
| 28.65 | 1.756E-01 | 10.6 | 30.69 | 1.549E-01 | 1.635E-02 |
| 29.15 | 1.366E-01 | 12.6 | 31.22 | 1.205E-01 | 1.519E-02 |
| 29.65 | 2.407E-01 | 9 • 8 | 31.76 | 2.125E-01 | 2.078E-02 |
| 31.15 | 2.628E-01 | 8.6 | 33,35 | 2.325E-01 | 2.009E-02 |
| 31.37 | 2.666E-01 | 8.02 | 33.59 | 2°326-01 | 1.929E-02 |
| 32.65 | 2.472E-01 | 8.9 | 34.95 | 26191E-01 | 1,955E-02 |
| 32.87 | 2.220E-01 | 9.1 | 35.18 | 1.968E-01 | 1.792E-02 |
| 34.15 | 1.099E-01 | 13.1 | 36.54 | 9.762E-02 | 1.276E-02 |
| 34.37 | 1.229E-01 | 12.4 | 36 . 77 | 1.092E-01 | 1.359E-02 |
| 35.65 | 1.379E-01 | 11.8 | 38.13 | 1.228E-01 | 1.446E-02 |
| 35.87 | 1.166E-01 | 13.1 | 38.36 | 1.038E-01 | 1.359E-02 |
| 37.15 | 1.385E-01 | 11.9 | 39.72 | 1.236E-01 | 1.468E-02 |
| 38.65 | 9.702E-02 | 13.8 | 41.31 | 8.676E-02 | 1.200E-02 |
| 40.15 | 6.802E-02 | 16.6 | 42.89 | 6.097E-02 | L.013E-02 |
| 41.65 | 6.3/5E-02 | 14.1 | 44 . 48 | 5.729E-02 | 8.066E-03 |
| 43015 | 50264E-02 | 1703 | 40.06 | 407435-02 | 90136E=03 |
| 44000 | 0. U20E-U2 | 1103 | 41.04 | 20442E-UZ | 704U4E-U3 |
| 4001) /7/5 | 3000UE - 02 | 1004 | 47022 50 00 | 30 30 5E=02 | 20427E=03 |
| 4/000 40:15 | 20 771 E-UZ | 4LeU 34 0 | 50°80 Estation | 201112-02 | 10114E=UZ |
| 77017 50 45 | 40204EPUZ / 5695-02 | 20.07 | 2 Co 3 C | Je UD95912 | 16377E*VZ |
| 50 00 50 1 E | 100000002 2 7040-00 | 2761 477 | フラ ₀ 74 ビビ ビリ | TO 11 35 UZ | 1 507E-M2 |
| 77073 | J0 1200-02 | 1077 | 22021 | Je Jr 4 C | 107615-42 |

SCATTERING OF 104 MEV ALPHAPARTICLES DN 56 FE

Q = -4.505 MEV I = 3-

ECM = 92.559 MEV K = 4.0669/FERMI ETA = 1.64491

| LA | BORATORY DA | ТА | | CM DATA | |
|---------------|------------------------|------------------------|----------------|-------------------|-----------|
| THETA | SIGMA | DSIGMA | THETA | S I GM A | DS I GMA |
| DEGREE | MB/SR | 2 | DEGREE | MB/SR | MB/SR |
| | | | | | |
| 8.65 | 3.949E 01 | 18.5 | 9.30 | 3.423E 01 | 6.319E 00 |
| 9.15 | 3.132E 01 | 11.4 | 9 <u>•</u> 83 | 2.715E 01 | 3.104E 00 |
| 9 ° 65 | 3.710E 01 | 5.1 | 10.37 | 3°212E 01 | 1.648E 00 |
| 10.15 | 2°201E 01 | 2.5 | 10.91 | 1.914E 01 | 4.753E-01 |
| 10.65 | 1.315E 01 | 11.2 | 11.44 | 1.141E 01 | 1.276E 00 |
| 11.15 | 7.698E 00 | 8 . 0 | 11.98 | 6°679E 00 | 5.373E-01 |
| 11.65 | 5.863E 00 | 4.02 | 12.52 | 5.089E 00 | 2.150E-01 |
| 12.15 | 5.822E 00 | 4.7 | 13.05 | 5°024E 00 | 2.373E-01 |
| 12.65 | 7.615E 00 | 6.9 | 13.59 | 6.613E 00 | 4.552E-01 |
| 13.15 | 1.074E 01 | 5.6 | 14.13 | 9.329E 00 | 5.264E-01 |
| 13.65 | 1.298E 01 | 3.3 | 14.66 | 1.128E 01 | 3.672E-01 |
| 14,15 | 1.337E 01 | 3.0 | 15.20 | 1.162E 01 | 3.451E-01 |
| 14.65 | 1.516F 01 | 2.2 | 15.74 | 1,318E 01 | 2.939E-01 |
| 15,15 | 1.395F 01 | 3,9 | 16.27 | 1, 21 3E 01 | 4.715E-01 |
| 15-65 | 1.211E 01 | 4.9 | 16.81 | 1-054E 01 | 5.137E-01 |
| 16.15 | 8.799E NO | 6.9 | 17.35 | 7.658E 00 | 5,265E=01 |
| 16.65 | 6.690E 00 | 7.6 | 17.88 | 5.824E 00 | 4.410F-01 |
| 17 15 | A 9375 00 | 87 | 18.42 | 4.2136 00 | 3.6545-01 |
| 17 45 | 4.057E 00 | 0 / | | 2 420E 00 | 2 2725-01 |
| | | 704 | | 204395 00 | 20212E-01 |
| 10.15 | 20492E UU | 404 | 17047 | 201700 00 | 90022ETU2 |
| 18.02 | 2.608E 00 | 408 | 20.02 | 2.214E 00 | |
| 19.15 | 3.341E 00 | 5.8 | 20.56 | 2.914E 00 | 1.6805-01 |
| 19.65 | 4.012E 00 | 5.01 | 21.10 | 3.501E 00 | 1.785E-01 |
| 20.15 | 4.964E 00 | 3.8 | 21.63 | 4.334E 00 | 1.666E-01 |
| 20°65 | 5.359E 00 | 3.0 | 22.17 | 4.681E 00 | 1.401E-01 |
| 21.15 | 5.024E 00 | 3.2 | . 22.70 | 4.390E 00 | 1.392E-01 |
| 21,65 | 5.000E 00 | 4.8 | 23.24 | 4.371E 0 0 | 2.109E-01 |
| 22.15 | 3.174E 00 | 8.6 | 23.77 | 2°746E 00 | 2.379E-01 |
| 22.65 | 2.588E 00 | 6.7 | 24.31 | 2.265E 00 | 1.510E-01 |
| 23.15 | 1.871E 00 | 5.8 | 24.84 | 1.638E 00 | 9.420E-02 |
| 23.65 | 2.108E 00 | 3.0 | 25 . 37 | 1.846E 00 | 5.544E-02 |
| 24.15 | 1.655E 00 | 5.4 | 25.91 | 1.450E 00 | 7.800E-02 |
| 24.65 | 1.402E 00 | 3.6 | 26.44 | 1.229E 00 | 4.398E-02 |
| 25.15 | 1.615E 00 | 4.3 | 26.98 | 1.417E 00 | 6.060E-02 |
| 25.65 | 1.799E 00 | 3.0 | 27.51 | 1.579E 00 | 4.744E-02 |
| 26.15 | 1.825E 00 | 3.0 | 28,04 | 1.603E 00 | 4.882E-02 |
| 26.65 | 2.038E 00 | 3.8 | 28,58 | 1,791E 00 | 6.799E-02 |
| 27,15 | 2.156F 00 | 2.9 | 29,11 | 1.896F 00 | 5.480E-02 |
| 27.65 | 2.012E 00 | 4.2 | 29.64 | 1.770E 00 | 7.352E=02 |
| 28.15 | 1.577E ()) | 7.8 | 30-18 | 1.388E 00 | 1.084E=01 |
| 28.65 | 9. 508Em01 | 10-5 | 30-71 | 8-3755-01 | 8.765E-02 |
| 2015 | 6 762E-01 | 5 3 | 31 24 | 5.9425 - 01 | 3,1325=02 |
| 20 65 | 0 0245-01 | / O | 21.78 | 9. 664E-01 | 4.261E=02 |
| 27000 | 7 9255-01 | 407 | 22 27 | 6 014E=01 | 3.7530=02 |
| 21 27 | 7 2005-01 | Je 1 | 33 61 | 6 520E=01 | 3.2435=02 |
| 27021 | | 260 | 24 07 | | 3 5515-02 |
| 32000 | | 401 | 24071 | | 30331E=UZ |
| 32001 | 8.717E-01 | 4.0 | 55°20 | 10/21E-01 | 201125-02 |
| 34, 15 | 7.807E-01 | 409 | 36.56 | 6.927E-01 | 3.415E-02 |
| 34.37 | 7.722E-01 | 5.0 | 36.80 | 6.854E-01 | 3.435E-02 |
| 35.65 | 5.552E-01 | 6.0 | 38.15 | 4.937E-01 | 2.986E-02 |
| 35,87 | 5.408E-01 | 6.1 | 38.39 | 4.811E-01 | 2.927E-02 |
| 37.15 | 3.996E-01 | 7.02 | 39.75 | 3.561E-01 | 2.561E-02 |
| 38.65 | 3.627E-01 | 7.1 | 41.33 | 3.240E-01 | 2.300E-02 |
| 40.15 | 3.012E-01 | 7.9 | 42.92 | 2.697E-01 | 2.136E-02 |
| 41.65 | 2.735E-01 | 8.1 | 44.51 | 2.455E-01 | 2.000E-02 |
| 43.15 | 2.111E-01 | 9.9 | 46.09 | 1.900E-01 | 1.884E-02 |
| 46.15 | 1.843E-01 | 8.7 | 49 ° 25 | 1.668E-01 | 1.448E-02 |
| 47.65 | 2.331E-01 | 14.8 | 50.83 | 2.115E-01 | 3.122E-02 |
| 49.15 | 1.885 E-0 1 | 17.2 | 52:40 | 1.716E-01 | 2.950E-02 |
| 50° 65 | 1.444E-01 | 22.7 | 53 ° 97 | 1.318E-01 | 2.986E-02 |
| 52.15 | 1.480E-01 | 23.2 | 55.54 | 1.355E-01 | 3.141E-02 |
| | | | | | |