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Model Code System for
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Intermediate Energies**

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**Institut für Reaktorsicherheit
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Abstract

The DISCA code has been originated to obtain reaction cross-sections, energy and angular particle distributions in nuclear reactions induced by incident nucleons and alpha-particles at intermediate energies.

The code implements the advanced intranuclear cascade evaporation model considering the nucleon-cluster interactions. The nuclear model is based on the realistic approximation of the Woods-Saxon nucleon density distribution. The modeling of intranuclear interactions takes into account along with the Pauli principle the number of essential features of nucleon-nucleon and nucleon-cluster interactions resulting from the quantum mechanical consideration of these effects. The model discussed can be applied to the calculation of excitation functions and total and differential nuclear reaction cross-sections over the entire energy range of precompound exciton models application and at the higher energies of incident particles.

DISCA – Code System zur Berechnung von Partikelverteilungen und Wirkungsquerschnitten für Kernreaktionen bei mittleren Energien basierend auf einem fortgeschrittenen intranuklearen Kaskaden Verdampfungsmodell mit vorgeformten Clustern

Zusammenfassung

Der DISCA Code ist entwickelt worden für die Berechnung von Wirkungsquerschnitten und Energie- und Winkelverteilungen von Kernreaktionen mit Nukleonen und Alpha-Teilchen mittlerer Energie.

Der Code implementiert das weiterentwickelte intranukleare Kaskaden Verdampfungsmodell, das die Nukleon-Cluster Wechselwirkung berücksichtigt. Das Kernmodell basiert auf der realistischen Annäherung der Woods-Saxon Nukleonen Dichteverteilung. Die Modellierung der intranuklearen Wechselwirkungen berücksichtigt neben dem Pauli Prinzip eine Reihe wesentlicher Eigenschaften der Nukleon-Nukleon und Nukleon-Cluster Wechselwirkungen, die aus der quantenmechanischen Betrachtung resultieren.

Das diskutierte Modell kann angewendet werden für die Berechnung von Anregungsfunktionen und totalen und differentiellen Wirkungsquerschnitten über den gesamten Energiebereich, für den das Precompound Excitonen Modell gültig ist und für einfallende Teilchen mit höheren Energien.

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The DISCA code has been elaborated to study nucleon and α -particle interactions with nuclei at intermediate energies.

The code calculates energy and angular distributions of particles emitted in nuclear reactions, residual nuclei yields, recoil spectra, total nonelastic cross-section for nuclear reactions induced by nucleons and α -particles. The code implements the advanced intranuclear cascade evaporation model with consideration of the nucleon-cluster interactions.

1. History of the code development

The creation of the DISCA code was initiated in 1987. The brief history of the code is described below.

DISCA: creation of general algorithm of the code refers to the works [1,2]. The code has been used for gas production and displacement cross-section calculations for stainless steel components irradiated with neutrons and protons at the energy up to 150 MeV [3] and for the creation of the BISERM-1 data library [4-7]

DISCA-2 or DISCA-S: the code algorithm, the routines for n - n interactions and particle evaporation simulation have been improved. The code has been used for the calculations of radioactive nuclide production cross-sections [8,9] and the cross-section evaluation for the BISERM-2 library [10,11].

DISCA-3: the code algorithm has been completely rewritten, the simulation of the α -particle knock-out and pick-up processes was included in the code [12]

DISCA-3D: the code was extended to describe the deuteron interactions with nuclei [13], the interactions with light nuclei and to perform simple calculations for thick targets.

DISCA-C/05 is the current version of the code realized in April, 2005. The parameters of the model were optimized. The code was used for helium production cross-section calculation for tungsten and tantalum isotopes [14].

2. Description of the model

2.1 Model of the nucleus

In the calculations the nucleus is broken up into concentric regions (zones) with uniform density. The number of zones is defined by the code parameter KZONESC (Sect.7). The position of nuclear zones is defined according to the Woods-Saxon expression

$$\rho(r) = \frac{\rho_0}{1 + \exp[(r - c)/a_d]}, \quad (1)$$

where $c=1.07 A^{1/3}$ fm, $a_d=0.545$ fm, $\rho_0 = 0.17$ fm⁻³.

The momentum distribution for nucleons for each zone is defined according to the Fermi gas model. Fermi momentum and energy are

$$p_{ni}^F = (3\pi^2 \mathbf{h}^3 \rho_{ni})^{1/3} \quad (2)$$

$$T_{ni}^F = (p_{ni}^F)^2 / 2m \quad (3)$$

where index “n” relates to nucleon, and ρ_i is the nucleon density in i-th zone.

It is supposed that besides of nucleons the nucleus consists of preformed clusters: tritons, ³He nuclei and α -particles. The maximum kinetic energy of the clusters (Fermi energy) and their potentials are defined by

$$T_{\alpha i}^F = 4T_{ni}^F, \quad T_{ti}^F = T_{hi}^F = 3T_{ni}^F, \quad (4)$$

$$U_{\alpha i} = T_{ni}^F + B_{\alpha}, \quad U_{ti} = T_{ti}^F + B_t, \quad U_{hi} = T_{hi}^F + B_h, \quad (5)$$

where $T_{\alpha i}^F, T_{ti}^F, T_{hi}^F$ are Fermi energy for α -particles, tritons and ³He, correspondingly, B_{xi} is the separation energy calculated using table of experimental nuclide masses, U_{xi} is the potential for considered type of the particles.

The value of U_{xi} in Eq(4),(5) is in agreement with the real part of optical potential obtained in Refs.[15,16] from data for α -particle elastic scattering on nuclei.

According to Ref.[17] the momentum distributions for tritons, ${}^3\text{He}$ and α -particles are taken as

$$N_{\alpha}(\mathbf{p}_{\alpha})d\mathbf{p}_{\alpha} \propto p^8 dp d\Omega, \quad (6)$$

$$N_t(\mathbf{p}_t)d\mathbf{p}_t = N_h(\mathbf{p}_h)d\mathbf{p}_h \propto p^6 dp d\Omega \quad (7)$$

2.2 Definition of the point of intranuclear interaction and partner characteristics

The method proposed to define the point of the interaction and partner characteristics is discussed in Refs.[12,13]. Let us consider a particle moving with kinetic energy T inside the nucleus. Probability of interaction per unit length is equal to

$$Q(\mathbf{r}) = \sum_x \rho_x(\mathbf{r}) \sigma_x^{\text{eff}}(T), \quad (8)$$

where the summing is performed over all particles inside the nucleus, ρ_x is the density of particles of type “x”, σ_x^{eff} is the effective cross-section for interaction of the considered particle and a particle of the x-type.

The cross-section σ_x^{eff} is defined as follows

$$\sigma_x^{\text{eff}}(T) = (1/v) \int v_{\text{rel}} \sigma_x(\mathbf{p}, \mathbf{p}_x) N_x(\mathbf{p}_x) d\mathbf{p}_x, \quad (9)$$

where v is the absolute value of the velocity and \mathbf{p} is the momentum of the considered particle corresponding to the energy T , v_{rel} is the relative velocity for two particles in the coordinate system with the motionless x-particle, $\sigma_x(\mathbf{p}, \mathbf{p}_x)$ is the interaction cross-section, which depends on the absolute value and direction of momentums of colliding particles.

The numerical calculation of Q value, Eq.(8) is noticeable simplified taking into account that the effective cross-section value σ_x^{eff} calculated using Eq.(9) at different T values is close to the value of the cross-section for interaction of the considered particle with a motionless partner (particle of x-type) $\sigma_x^{\text{eff}}(T) \cong \sigma_x(T) = \sigma_x(\mathbf{p}, \mathbf{p}_x = 0)$.

Fig.1 shows the ratio $\sigma_x^{\text{eff}}(T) = (1/v) \int v_{\text{rel}} \sigma_x(\mathbf{p}, \mathbf{p}_x) N_x(\mathbf{p}_x) d\mathbf{p}_x / \sigma_x(T)$ calculated for nucleon-nucleon and nucleon- α interactions at different nucleon kinetic energy T .

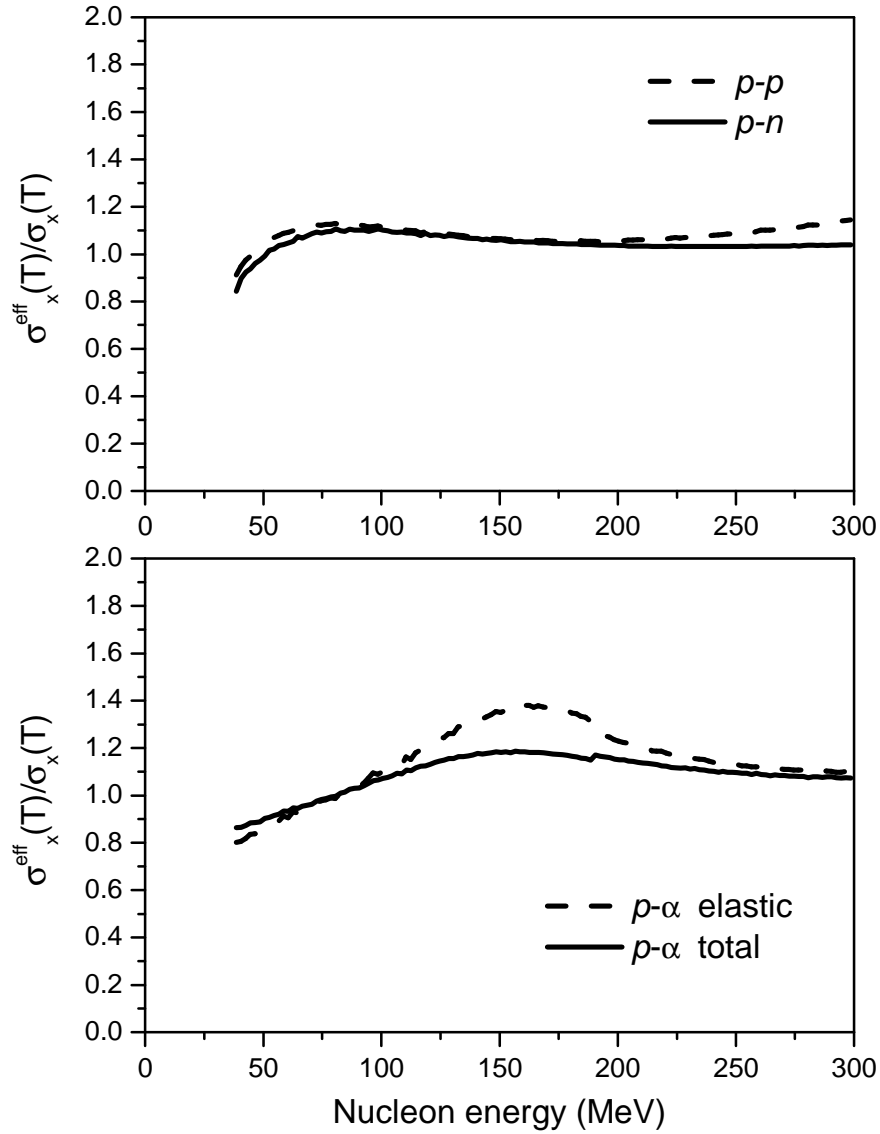


Fig.1 The ratio of the effective cross-section for nucleon-nucleon and nucleon- α interactions inside a nucleus and the cross-section corresponding to the motionless partner.

Data shown in Fig.1 correspond to the central nuclear zone with the biggest value of T_n^F , where the difference between $\sigma_x^{\text{eff}}(T)$ and $\sigma_x(T)$ is maximal. One can see that the ratio of cross-sections is close to unity. Therefore, the probability of interaction of the considered particle with the particles of the nucleus can be calculated using the following approximation

$$Q(\mathbf{r}) = \sum_x \rho_x(\mathbf{r}) \sigma_x(T) \quad (10)$$

The particle range (L) in nuclear matter is defined by

$$\int_0^L Q(\mathbf{r}) dl = -\ln \xi, \quad (11)$$

where ξ is the random number from the interval [0,1].

For a nucleus with constant density zones Eq.(11) is written as

$$\sum Q_i(\mathbf{r}_i) \Delta l_i = -\ln \xi, \quad (12)$$

where Q_i is the probability of particle interaction with nuclear matter in the i-th zone, Δl_i is the length of the trajectory part in the i-th zone.

The point of the interaction is defined using Eq.(12) as follows.

The random number ξ is sampled in the interval [0,1]. For the considered particle with momentum \mathbf{p} , located in the point with the radius-vector \mathbf{r} , the distance for the nearest zone boundary Δl is calculated according to the momentum direction. The value of the sum, Eq.(12) is increased by the $Q(\mathbf{r}) \Delta l$ value. If the resulting value $\sum Q_i(\mathbf{r}_i) \Delta l_i$ is much larger than $-\ln \xi$, than the particle is shifted by a distance corresponding to the rigorous equality of Eq.(12). In this case, the particle coordinates correspond to the point of interaction with an intranuclear cluster or nucleon. If $\sum Q_i(\mathbf{r}_i) \Delta l_i < -\ln \xi$, the particle crosses the zone boundary. According to its new momentum direction, a new distance for the zone boundary is calculated, the sum, Eq.(12) is increased by the new $Q(\mathbf{r}) \Delta l$ value again etc, until an equality Eq.(12) is fulfilled.

After the definition of the point of interaction, the type of partner and its momentum are obtained by the Monte Carlo method. Note that the partner characteristics are defined only once, in contrast with the repeated random choice of the partner type and momentum, as used in Refs.[5,6].

The partner type is defined according to the relation between the items in Eq.(10) for the calculation of the probability Q . The interaction of the considered particle with nucleons, α -, t- and ${}^3\text{He}$ -clusters is taken into account. The partner momentum is defined according to the distribution $(v_{\text{rel}}/v)\sigma_x(\mathbf{p}, \mathbf{p}_x)N_x(\mathbf{p}_x)d\mathbf{p}_x$.

The efficiency of the algorithm for momentum definition is based on the following property of the distribution

$$\int (v_{\text{rel}}/v)\sigma_x(\mathbf{p}, \mathbf{p}_x)N_x(\mathbf{p}_x)d\Omega_x \cong \sigma_x(\mathbf{p}, \mathbf{p}_x = 0) \int N_x(\mathbf{p}_x)d\Omega_x, \quad (13)$$

According to Eq.(13) the result of integration does not depend from the absolute value of \mathbf{p}_x and the value p_x can be independently chosen at random based on the $N_x(p_x)$ distribution. To obtain the momentum direction the following expression is used

$$\int (v_{\text{rel}}/v)\sigma_x(\mathbf{p}, \mathbf{p}_x) d\Omega_x = \xi \sigma_x(T), \quad (14)$$

where ξ is the random number, T is the kinetic energy of primary (considered) particle corresponding to the momentum \mathbf{p} , and the absolute value p_x is defined according to the $N_x(p_x)$ distribution.

2.3 Probability of intranuclear interaction

For a proton moving inside the nucleus with kinetic energy T , the probability of interaction with nuclear matter is

$$Q_i = \rho_i [\varphi_n \sigma^{\text{pn}}(T) + \varphi_p \sigma^{\text{pp}}(T) + \varphi_\alpha \sigma^{\text{p}\alpha}(T) + \sigma_{\text{p-u}}^{\text{pt}}(T)], \quad (15)$$

where ρ_i is the nucleon density for the i -th zone, σ^{pn} and σ^{pp} are cross-sections for interactions with intranuclear neutron and proton, correspondingly, $\sigma^{\text{p}\alpha}$ is the cross-

section for interaction with a “preformed” α -cluster, σ_{p-u}^{pt} is the cross-section for the “pick-up” processes combining the proton and a “preformed” triton to form of the α -particle, φ_n , φ_p , φ_α are relative numbers of neutrons, protons and α -clusters in the nucleus, correspondingly.

Typical values of φ_α obtained from the analysis of experimental α -particle spectra are from 0.05 to 0.1. Values of φ_n and φ_p depend from the total number of nucleons in nuclei and φ_α value.

A similar equation describes the neutron moving inside the nucleus.

For excited α -particle, the elastic scattering and break-up processes at the interactions with intranuclear nucleons are considered. For calculating the nucleon-nucleon interaction cross-sections, the following approximation formulas from Ref.[18] are used

$$\sigma^{pn}(T) = \begin{cases} -5057.4/T^2 + 9069.2/T + 6.9466, & T \leq 40 \text{ MeV} \\ 239380.0/T^2 + 1802.0/T + 27.147, & 40 < T \leq 400 \text{ MeV} \\ 34.5, & 400 < T \leq 800 \text{ MeV} \end{cases} \quad (16)$$

$$\sigma^{pp}(T) = \begin{cases} -1174.8/T^2 + 3088.5/T + 5.3107, & T \leq 40 \text{ MeV} \\ 93074.0/T^2 - 11.148/T + 22.429, & 40 < T \leq 310 \text{ MeV} \\ 887.37/T + 0.05337T + 3.5475, & 310 < T \leq 800 \text{ MeV} \end{cases} \quad (17)$$

where the cross-sections are given in millibarns.

For calculating nucleon- α interaction cross-sections, the approximation formulas obtained in Ref.[12] are used. These were obtained on the basis of experimental and evaluated data from Refs.[19,20] at energies above 14 MeV and the BROND-2 data for low energies. The total and elastic scattering cross-sections for nucleon- α interaction are calculated as follows

$$\sigma^{\text{p}\alpha}(\text{T}) = \begin{cases} 6754.8\text{T}^2 - 1608.5\text{T} + 778.94, & \text{T} \leq 1.125 \text{ MeV} \\ 7467.2/\text{T}^{1.6089} - 51.109\text{T} + 1773.7, & 1.125 < \text{T} \leq 20 \text{ MeV} \\ 5230.0/\text{T}^{0.43473} + 1.2270\text{T} - 658.81, & 20 < \text{T} \leq 190 \text{ MeV} \\ 3425.3/\text{T} + 0.073484\text{T} + 74.410, & 190 < \text{T} \leq 1000 \text{ MeV} \end{cases} \quad (18)$$

$$\sigma_{\text{el}}^{\text{p}\alpha}(\text{T}) = \begin{cases} 6754.8\text{T}^2 - 1608.5\text{T} + 778.94, & \text{T} \leq 1.125 \text{ MeV} \\ 7466.4/\text{T}^{1.6338} - 53.939\text{T} + 1815.2, & 1.125 < \text{T} \leq 20 \text{ MeV} \\ 10182.0/\text{T}^{0.76746} + 0.68190\text{T} - 282.56, & 20 < \text{T} \leq 190 \text{ MeV} \\ 4833.8/\text{T} + 0.036414\text{T} - 2.9546, & 190 < \text{T} \leq 1000 \text{ MeV} \end{cases} \quad (19)$$

where $\sigma^{\text{p}\alpha}$ is the total cross-section and $\sigma_{\text{el}}^{\text{p}\alpha}$ is the elastic scattering cross-section in millibarns.

The energy dependence of the pick-up cross-section $\sigma_{\text{p-u}}^{\text{pt}}(\text{T})$ is defined according to the form-factor $F_{1,3}$ calculated in Ref.[21] corresponding to formation of the α -particle from three nucleons with energy below the Fermi energy and one nucleon with energy above the Fermi energy. The cross-section is

$$\sigma_{\text{p-u}}^{\text{pt}}(\text{T}) = \zeta \left[-1,011 \times 10^{-6} \varepsilon^3 + 1,748 \times 10^{-4} \varepsilon^2 - 1,128 \times 10^{-2} \varepsilon + 0,275742 \right] / (R \rho_i), \quad (20)$$

where $\varepsilon = \text{T} - \text{T}_{\text{ni}}^{\text{F}}$ ($\varepsilon < 67 \text{ MeV}$), $R = 1.25 \text{ A}^{1/3}$, ζ is the fitting parameter, which typical value is equal to 14.

To obtain the momentum of the particles after interactions, the angular distribution for nucleon-nucleon scattering is parameterized as

$$\sigma(\theta) = A(\text{T}) + B(\text{T}) \cos^n \theta, \quad (21)$$

where the coefficients $A(\text{T})$ and $B(\text{T})$ and the “n” values are defined in Ref.[22].

The angular distributions for elastic nucleon- α scattering are calculated according to Ref.[23] as

$$\sigma(\theta) = C(\theta) \exp\left(-k(\theta)\sqrt{\text{T}}\right), \quad (22)$$

where θ is the angle in CM system and $C(\theta)$ and $k(\theta)$ are parameters, which do not depend on the primary nucleon energy.

The values of $C(\theta)$ and $k(\theta)$ tabulated in Ref.[32] are approximated by polynomials

$$C(\theta) = 1.4447 \times 10^{-6} \theta^3 + 1.0774 \times 10^{-4} \theta^2 - 8.87098 \times 10^{-2} \theta + 6.7415 \quad (23)$$

and

$$\begin{aligned} k(\theta) &= 4.0 \times 10^{-3} \theta, & \text{if } \theta < 30^\circ \\ k(\theta) &= -1.4519 \times 10^{-10} \theta^5 + 6.6868 \times 10^{-8} \theta^4 - 1.0539 \times 10^{-5} \theta^3 + \\ &\quad + 6.1054 \times 10^{-4} \theta^2 - 3.8739 \times 10^{-3} \theta - 7.7636 \times 10^{-2}, & \text{if } 30^\circ \leq \theta \leq 165^\circ \\ k(\theta) &= 0.36889, & \text{if } \theta > 165^\circ \end{aligned} \quad (24)$$

where angle θ is given in degrees.

2.4 Pauli principle and limitation on orbital particle momenta

In the simulation of intranuclear interactions, the Pauli principle is taken into account as well for nucleon-nucleon as for nucleon- α collisions. The check provides that the kinetic energy of interacting particles is never below the Fermi energy. Also, the restriction on the orbital momenta of nucleons discussed in Ref.[24] is considered.

Finite nuclear sizes impose restrictions on the orbital momenta of the interacting nucleons. According to Ref.[25], the orbital momenta l of nucleons colliding within a square potential well should not exceed the product of asymptotic nucleon momentum and nucleus radius: $l \leq p_a R$, where p_a is the linear momentum the nucleon would have outside the nucleus and R is the nucleus radius. This restriction on l results from the fact that the nucleus has no states below the centrifugal barrier [25]. For a nuclear model with the multi-region density, the restriction on the orbital momenta of nucleons colliding in the i -th zone has the following form [24,25]

$$l \leq p_{i+1} R_i, \quad (25)$$

where l is the angular momentum of the nucleon with momentum p_i in the i -th zone, p_{i+1} is the momentum the nucleon would have in the $i+1$ -th zone (the regions are

numbered beginning from the nucleus center), and R_i is the radius of the i -th zone in which the two nucleons collide. The relationship between p_i and p_{i+1} is derived from the following relation between corresponding values of the nucleon kinetic energy T_i and T_{i+1}

$$T_{i+1} = T_i - T_i^F + T_{i+1}^F, \quad (26)$$

where T_i^F is the Fermi energy in the i -th zone. If the i -zone has the maximum radius, then $T_{i+1}^F = -B_b$, where B_b is the binding energy of the nucleon or α -particle in the nucleus.

Restriction, Eq.(25) on orbital momenta leads to a reduced total number of intranuclear interactions and to an increased emission of high energy particles from the nucleus. The calculations show [24] that use of Eq.(25) along with the Pauli principle results in a much better reproduction of the experimental data for low and intermediate primary particle energies.

Fig.2 illustrates how the restriction on orbital momenta used in modeling nucleon-nucleon interactions affects the accuracy of the calculation of double-differential cross-sections. The calculated spectrum for 19 MeV neutrons produced by irradiation of ^{93}Nb with 26 MeV neutrons is shown in Fig.2. The calculations were performed with and without checking of Eq.(25) for intranuclear interactions. In both calculations the effects of the refraction and reflection of the nucleon momentum at the boundary of nuclear regions were taken into account. The total reaction cross-section was normalized to the same value of the cross-section, obtained by the optical model. Fig.2 shows that a more accurate description of intranuclear processes leads to a better agreement between the calculations and experimental data [26].

2.5 Distortion of particle trajectory inside the nucleus

When the nucleon moves in a non-uniform nuclear potential well its path is distorted and the distortion is simulated by describing the refraction and reflection of the nucleon momentum at the boundary of nuclear regions.

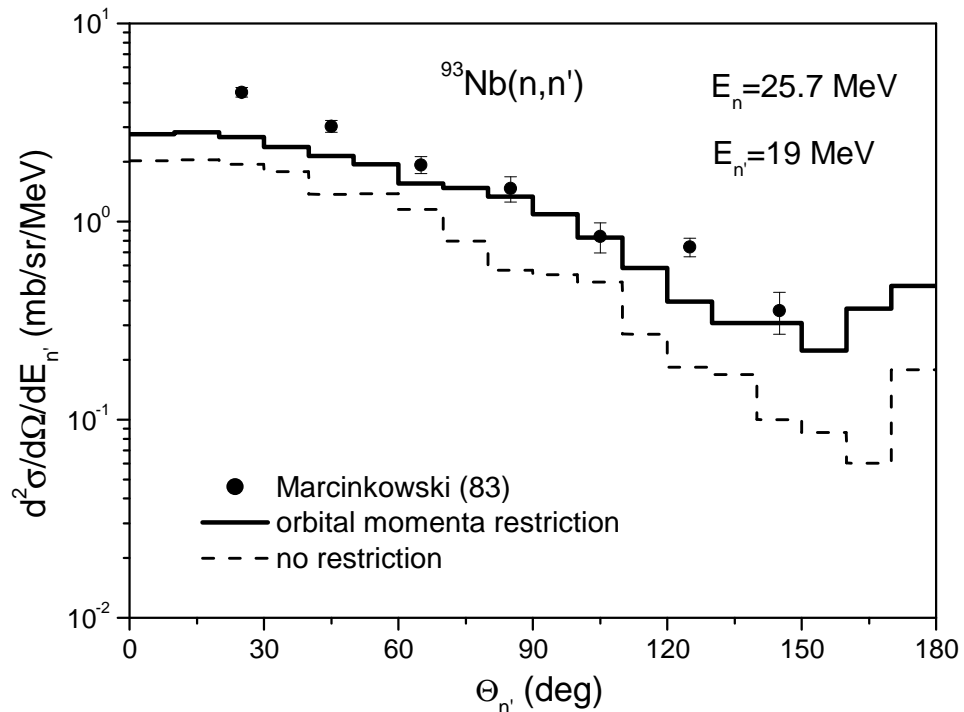


Fig.2 Double-differential cross-section for 19 MeV neutrons emitted in the reaction $^{93}\text{Nb}(n,n')$ induced by 25.7 MeV neutrons. Calculations are carried with the checking of Eq.(25) for nucleon-nucleon interactions (solid line) and without the checking (dashed line). The refraction and reflection of the nucleon momentum at the nuclear zone boundaries are taken into account. Experimental data are taken from Ref.[26].

The problem of describing refraction and reflection processes has been discussed long before [22,27]. In Ref.[27] it was shown that these effects when included in the model algorithm deteriorate the level of agreement between calculated and

experimental data. The neglecting of refraction and reflection is the default (recommended) option for calculations using the Bertini and ISABEL codes from MCNPX package [28]. However, it was proved [22] that the classical interpretation of refraction and reflection effects was quite justified and cannot be used as a basis for disregarding these effects.

A solution of the problem was given in Ref.[25] where it was pointed out that the calculations in Ref.[27] did not take into account the effect associated with the restriction on orbital momenta of interacting nucleons, Eq.(25). As shown in Ref.[25] and confirmed by the DISCA calculations, taking into account refraction and reflection and meeting condition Eq.(25) the agreement between calculations and experimental data in the intermediate energy range is noticeably improved.

The effects of refraction and reflection of particle momentum on the boundary of two nuclear zones is considered in all DISCA simulations.

2.6 Cut-off energy

The cutoff energy T_{cut} is a parameter of the intranuclear cascade model and presents the minimal energy of the fast particle emitted from the nucleus [22]. When the kinetic energy T of a particle residing in the potential well meets the condition

$$T^F < T < T^F + B + T_{\text{cut}}, \quad (27)$$

where B is a binding energy, it is generally accepted, that the particle is absorbed by the nucleus and its further movement is not observed.

From the calculations performed [24] it follows that the best results are obtained if the cut-off energy for neutrons and protons is assumed to be equal to zero, and penetration through the Coulomb barrier for protons is simulated.

In modeling the cascade process for protons approaching the nucleus with energies less than the Coulomb potential, the tunnel effect is considered in the

following way. The probability of penetrating through the Coulomb barrier is as follows [24]

$$D = \exp\left(-2 \frac{R}{\mathbf{D}(V_p)} \left[(V_p / \varepsilon)^{1/2} \arccos(\varepsilon / V_p)^{1/2} - (1 - \varepsilon / V_p)^{1/2} \right]\right), \quad (28)$$

where ε is the energy of proton outside the nucleus, V_p is the Coulomb potential, $\mathbf{D}(V_p)$ is the de Broglie wave length of the proton at the energy V_p equal to $4.5 \cdot V_p^{-1/2}$ fm.

By generating a random number and using Eq.(28) for the proton with the energy $0 < \varepsilon < V_p$ one can find whether the proton is absorbed or emitted from the nucleus. If the under-barrier effect is taken into consideration the smooth dependence of the proton nonequilibrium spectrum on the energy of the outgoing particle is described (Fig.3). In the pre-equilibrium exciton model similar energy dependence for the calculated spectrum is observed when calculating the inverse reaction cross-section for protons via the optical model describing the proton absorption and scattering in a realistic potential well.

2.7 Particle evaporation

The description of the particle evaporation by the intranuclear cascade evaporation model is linked to the problem of developing an efficient algorithm to simulate this process by the Monte Carlo method. The efficiency of the algorithm ensuring the speed of the computer code often implies that the particle evaporation widths are calculated through analytical formulas rather than by means of numerical integration. Old versions of the DISCA code preceding DISCA-3 used the analytical expression for calculating of the particle emission probability. New versions starting from DISCA-3 implement the method described in Ref.[29] (“single width integration”).

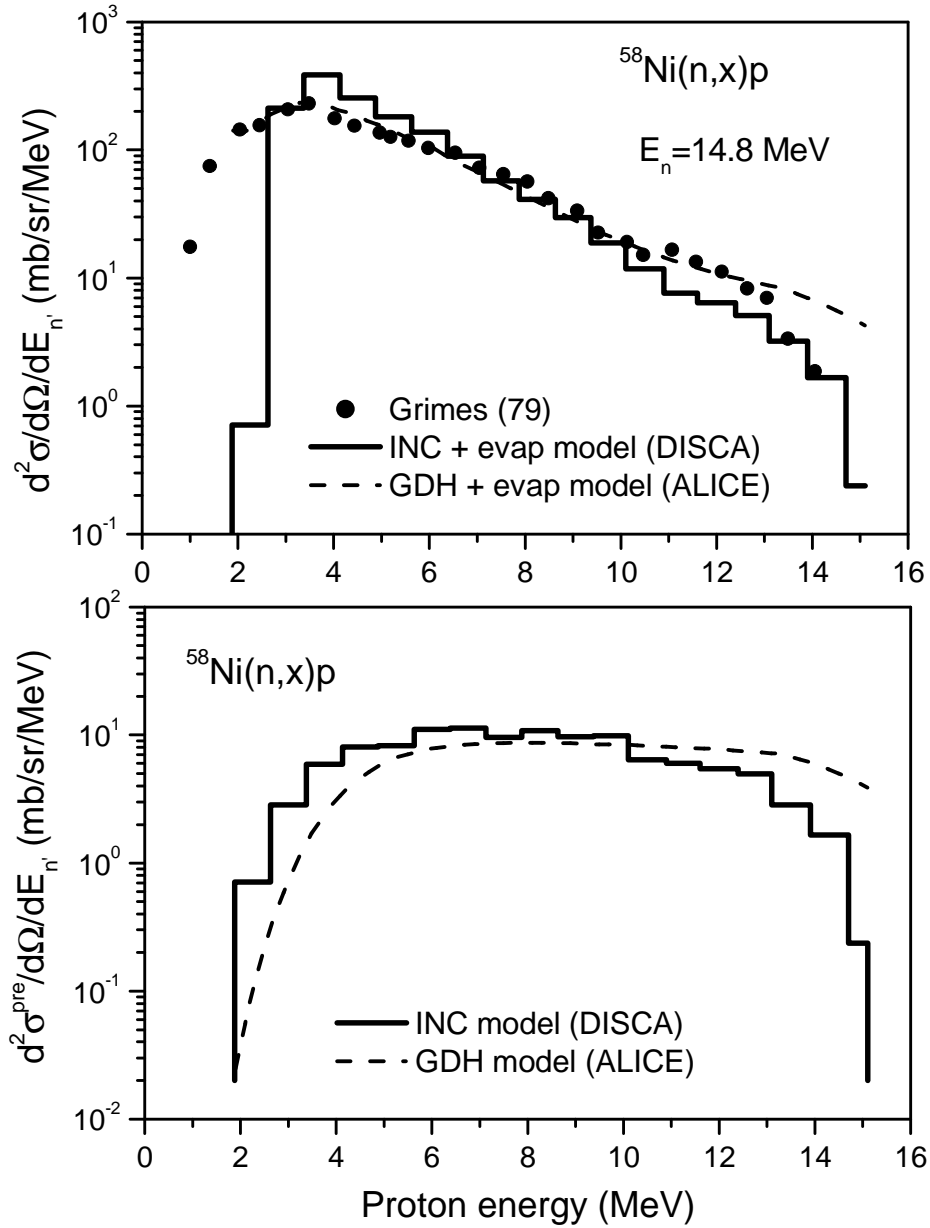


Fig.3 Proton energy distribution for the $^{58}\text{Ni}(n,x)p$ reaction induced by 14.8 MeV neutrons calculated using the intranuclear cascade evaporation model by the DISCA code (histogram) and using the geometry dependent hybrid exciton and evaporation model [28,29] by the ALICE (dashed line). Upper figure shows the sum of the non-equilibrium and evaporation spectrum, bottom figure shows the calculated non-equilibrium spectrum. Experimental data (circle) are taken from Ref.[30].

The probability of evaporation of the x-type particle from the excited nucleus is obtained by the Weisskopf formula

$$W_x \propto \int (2S_x + 1) \mu_x \varepsilon_x \sigma_{\text{inv}}(\varepsilon_x) \rho(U) d\varepsilon_x, \quad (29)$$

where S_x , μ_x , ε_x are the particle spin, reduced mass and kinetic energy, correspondingly, σ_{inv} is the inverse reaction cross-section, $\rho(U)$ is the level density for the residual nucleus with the excitation energy U .

Instead of the crude approximation for $\rho(U)$ used in several codes [31] $\rho(U) = C \exp(2\sqrt{aU})$, where C is a constant, and “a” is the level density parameter, the nuclear level density is calculated according to the Fermi gas model

$$\rho(U) = (1/12)\pi^{1/2} a^{-1/4} U^{-5/4} \exp(2\sqrt{aU}) \quad (30)$$

at the high excitation energy U and by the “constant temperature” model at low energy of excitation. The inverse reaction cross-sections are calculated using phenomenological formulas from Ref.[32], which approximate the results of optical model calculations. Evaporation is considered for neutrons, protons, deuterons, tritons, ^3He nuclei and α -particles.

2.8 Binding energies

The particle binding energies are calculated using the experimental masses of nuclei. If experimental data are absent, the formula of Myers, Swiatecki, Lysekil [29] is used to obtain the particle separation energy for residual nuclei (Z,N) with $Z - Z_C \leq 9$ and $N - N_C \leq 22$, where Z_C and N_C are numbers of protons and neutrons in initial compound nucleus. The algorithm of the calculation is taken from Ref.[29]. The binding energies for other nuclei are calculated using the Cameron formula [22]. The calculations for tritons and ^3He are always performed according to Cameron [22].

2.9 Total nonelastic interaction cross-section

The cross-section of nonelastic interaction of the primary particle with a nucleus (σ_{non}) is calculated internally by the code or estimated using the data for nucleons from Ref.[33] and for α -particles from Ref.[19] or calculated by approximating formulas [32].

The input variable INFS0 (Sect.7) defines what type of the nonelastic cross-section is used for the total normalization of the calculated residual nuclei yields and particle distributions.

The total cross-section of the interaction of an incident nucleon with a nucleus is calculated by the code as $\sigma_{\text{tot}} = \pi(R_{\text{max}} + \mathbf{D})^2$, where R_{max} is the radius of the outmost nuclear zone, \mathbf{D} is the wavelength of the incident nucleon. The nonelastic reaction cross-section σ_{non} is defined as $\sigma_{\text{non}} = \sigma_{\text{tot}}(N/N_{\text{tot}})$, where N is the number of events resulting to nucleus excitation and N_{tot} is the total number of events.

Fig.4 shows the σ_{non} cross-section calculated using the DISCA code and obtained by the optical model with different set of the optical potentials. As can be seen from Fig.4 the calculations by the DISCA code are in agreement with the σ_{non} values obtained using the optical model.

2.10 Simulation of atomic displacements in materials

The DISCA code calculates the displacement cross-section for nonelastic interactions of incident particles with nuclei. The cross-section is calculated by the formula

$$\sigma_d(E_p) = \sum_i \int_{E_d}^{T_i^{\text{max}}} \frac{d\sigma(E_p, Z_T, A_T, Z_i, A_i)}{dT_i} v(T_i, Z_T, A_T, Z_i, A_i) dT_i, \quad (31)$$

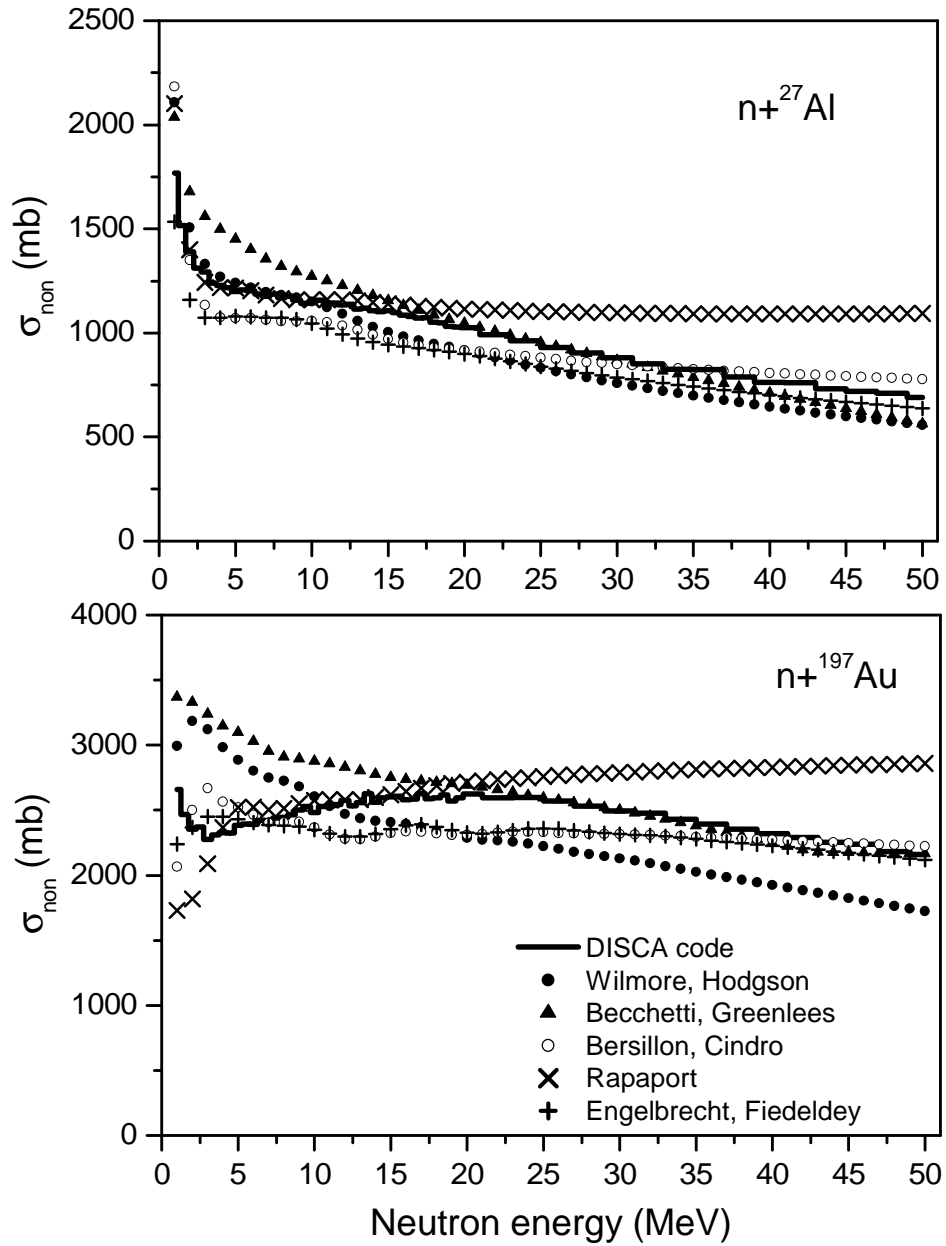


Fig.4 Total nonelastic interaction cross-section for ^{27}Al and ^{197}Au irradiated with neutrons, calculated by the DISCA code (histogram) and using the optical model [34] with potentials: Wilmore-Hodgson (dark circle), Becchetti-Greenlees (triangle), Bersillon-Cindro (open circle), Rapaport (cross), Engelbrecht-Fiedeldey (plus).

where E_p is the incident proton energy, $d\sigma/dT_i$ is the cross-section of energy transfer to recoil atom, Z_i and A_i are the atomic number and the mass number of the recoil atom, correspondingly, Z_T and A_T are the same for the target material, $v(T_i)$ is the number of Frenkel pairs produced by PKA with the kinetic energy T_i , T_i^{\max} is the maximal energy of the PKA spectrum, E_d is effective threshold displacement energy, the summing is for all recoil atoms produced in the irradiation.

The number of defects produced by the PKA in material $v(T)$ is calculated according to the NRT approach [35] with the value of “k” parameter defined according to Robinson [36]

$$v(T) = \eta \frac{0.8}{2E_d} T_{\text{dam}}(T), \quad (32)$$

$$T_{\text{dam}}(T) = \frac{T}{1 + k \left(3.4008 \varepsilon^{1/6} + 0.40244 \varepsilon^{3/4} + \varepsilon \right)}, \quad (33)$$

$$k = \frac{32}{3\pi} \left(\frac{m_e}{M_T} \right)^{1/2} \frac{(A_i + A_T)^{3/2} Z_i^{2/3} Z_T^{1/2}}{A_i^{3/2} (Z_i^{2/3} + Z_T^{2/3})^{3/4}}, \quad (34)$$

$$\varepsilon = [A_T T / (A_i + A_T)] [a / (Z_i Z_T e^2)], \quad (35)$$

$$a = a_0 (9\pi^2 / 128)^{1/3} (Z_i^{2/3} + Z_T^{2/3})^{-1/2}, \quad (36)$$

where η is the defect production efficiency [37], m_e is the mass of an electron, M_T is the mass of the target atom, a_0 is the Bohr radius, “e” is the electron charge; the kinetic energy T of the recoil atom is taken in keV.

In the DISCA calculations the η value is taken equal to unity. Subroutine DEFINE_ED contains the data for the effective threshold displacement energy E_d used for the σ_d computation.

3. Energy range of the model applicability

3.1 Low energy limit

As follows from the comparison of the DISCA calculations and experimental data the discussed intranuclear cascade evaporation model can be used for the calculation of total and differential cross-sections of nuclear reactions over the entire energy range in which pre-equilibrium exciton models are applicable, i.e. at energies above several mega electron-volts [24]. The applicability of the model at relatively low energies is due to the fact that the model algorithm takes into account the factors discussed above in Sect. 2.3 and 2.4.

The agreement between cross-sections calculated using the intranuclear cascade model discussed and those obtained by the hybrid exciton model [28,29] testifies to similarity of both approaches as noted in Ref.[38]. Both models are semi-classical and regard the dynamics of the non-equilibrium process as a series of quasi-free nucleon-nucleon interactions. The comparison of results of calculations with experimental data proves that the approximation of the intranuclear cascade model in which nucleons are assumed to follow quasi-classical paths is “not less reasonable” as the assumption of the hybrid exciton model concerning equal probabilities of configurations with a certain number of excitons and a transition from “n” to “n+2” exciton state as a result of interaction of the “leading” particle with the nucleons. The roughness of both approaches appears to be quite comparable.

The formal applicability criterion of the model applicability is the smallness of the incident particle wavelength compared to its free path length Λ within the nucleus [24]

$$\frac{\mathbf{D}}{\Lambda} = \frac{W}{E} \left(\frac{1+V}{E} \right)^{-1/2} \ll 1, \quad (37)$$

where V and W are, respectively, the real and imaginary parts of the optical potential regarded as a square well, and E is the primary particle energy.

Taking into account the typical relation between the values of W and V values [24], condition Eq.(37) is actually met at energies above several mega electron-volts.

3.2 High energy limit

At present time, the model discussed does not suppose the nonelastic nucleon-nucleon interactions. For this reason the current version of the DISCA code is used for the simulations at the projectile energy up to 600-800 MeV.

4. Peculiarities of simulation of the non-equilibrium α -particle emission from nuclei

The calculations show that the knock-out of preformed α -particle resulting from elastic nucleon- α interaction plays the secondary role in the forming of the non-equilibrium α -particle emission distribution at medium energies of the α -spectrum. The energy distribution of α -particles calculated using the knock-out model ($\zeta=0$ in Eq.(15),(20)) has a “hole” at the medium part of the spectrum, which is characteristic also of the calculations using the pre-equilibrium exciton model. Fig.5 shows the difference between experimental data [39] and the α -particle spectrum calculated by the pre-equilibrium exciton model [40] and intranuclear cascade model taking into account the knock-out of α -particles by the fast nucleons and neglecting the pick-up process.

In spite of the secondary role of the knock-out process in the non-equilibrium α -particle emission, the elastic nucleon interaction with preformed α -clusters has a noticeable effect on the nucleon emission at large emission angles. Fig.6 shows the double differential cross-section for protons emitted from the $^{90}\text{Zr}(p,p')$ reaction induced by 80 MeV protons. The calculations are performed with and without consideration of the α -particle knock-out in nuclear reaction. The pick up of the ^3He

or triton cluster forming α -particle was not considered in both cases ($\zeta=0$). It can be seen from Fig.6 that the agreement with experimental data [41] is substantially improved with the consideration of the processes of the interaction of nucleons with α -clusters of the nucleus.

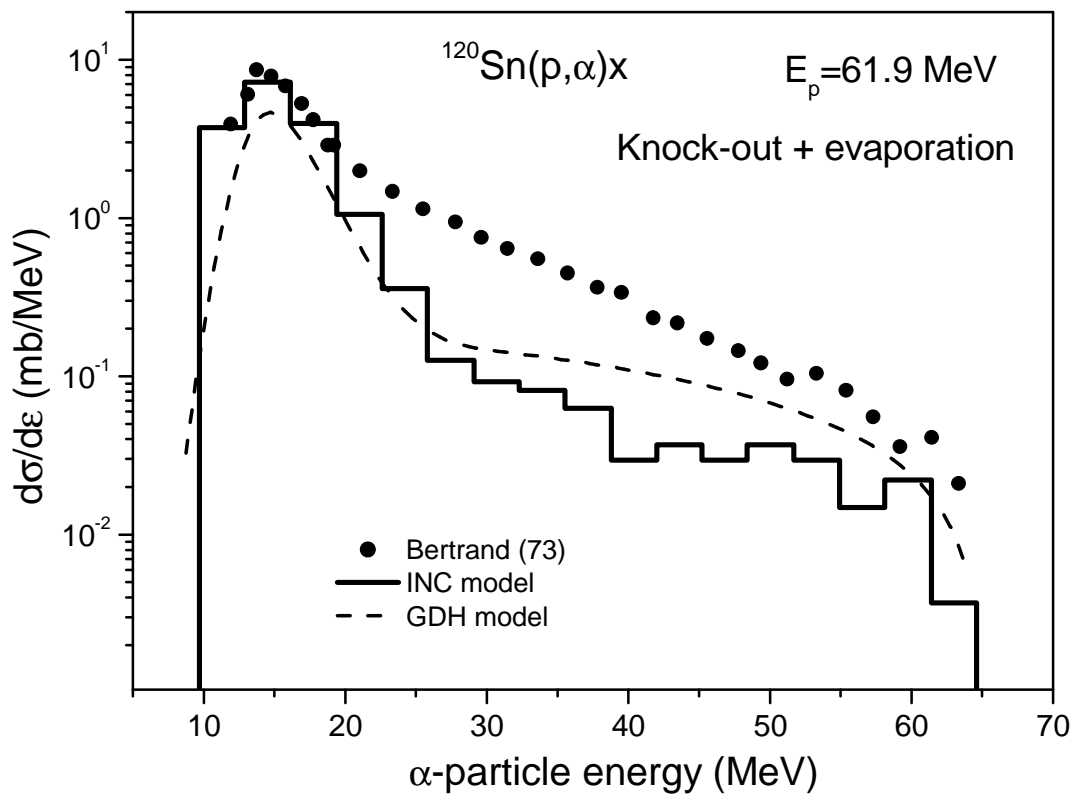


Fig.5 Contribution of the knock-out process and the evaporation in the energy distribution of α -particles emitted from the $^{120}\text{Sn}(p,\alpha)x$ reaction induced by 61.9 MeV protons. Calculations are performed using the DISCA code (histogram) and the modified ALICE code [40] (dashed line). Experimental data are from Ref.[39].

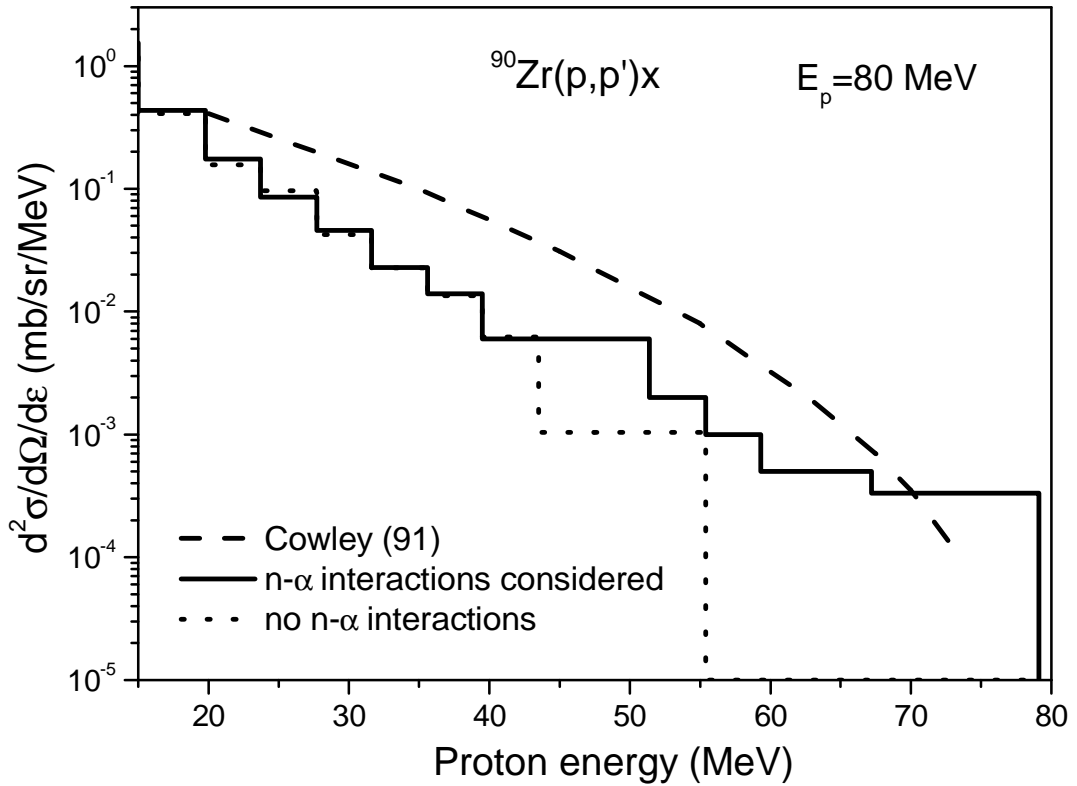


Fig.6 Double differential cross-section for protons emitted from the $^{90}\text{Zr}(p,p')x$ reaction induced by 80 MeV protons. Calculations are performed using the DISCA code with (solid histogram) and without (dashed histogram) consideration of the elastic nucleon- α interactions. Experimental data (dashed line) are from Ref.[41].

The experimental α -particle spectra from nucleon induced reaction at energies up to hundreds MeV are correctly described considering three basic mechanisms of the α -particle emission in nuclear reactions: the knock-out, pick-up and evaporation. Fig.7 shows the contribution of the different processes in the $^{209}\text{Bi}(p,\alpha)x$ reaction induced by 90 MeV protons.

Next figure (Fig.8) shows the role of the nuclear regions with low density on the forming of the non-equilibrium α -particle spectrum. The calculations are performed assuming that the α -particles are formed only in the nuclear region with the density lower than $0.1 \cdot \rho_0$, where ρ_0 is the density of nucleons in the center of nucleus, and considering the α -particle formation in total nuclear volume. Fig.8 show that the calculated α -particle spectrum is formed mainly from intranuclear interactions in nuclear region with low density $\rho \leq 0.1 \cdot \rho_0$.

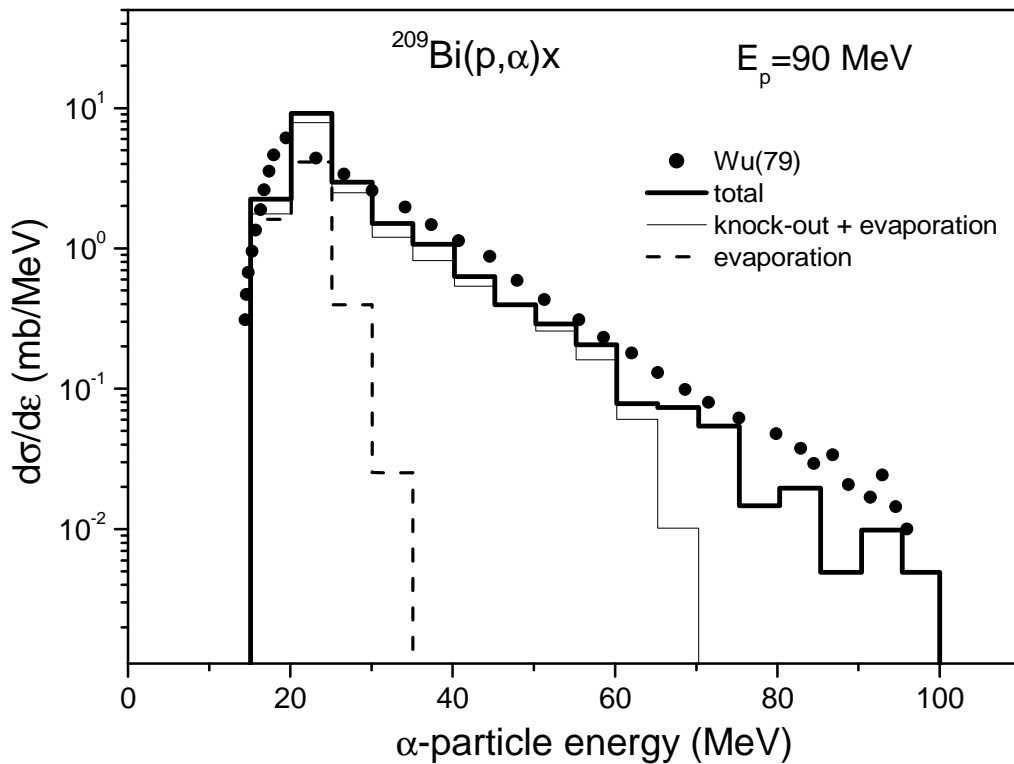


Fig.7 Contribution of the different processes in the of α -particle emission from the $^{209}\text{Bi}(p,\alpha)x$ reaction induced by 90 MeV protons. Calculations are performed using the DISCA code (histograms). Experimental data are from Ref.[42].

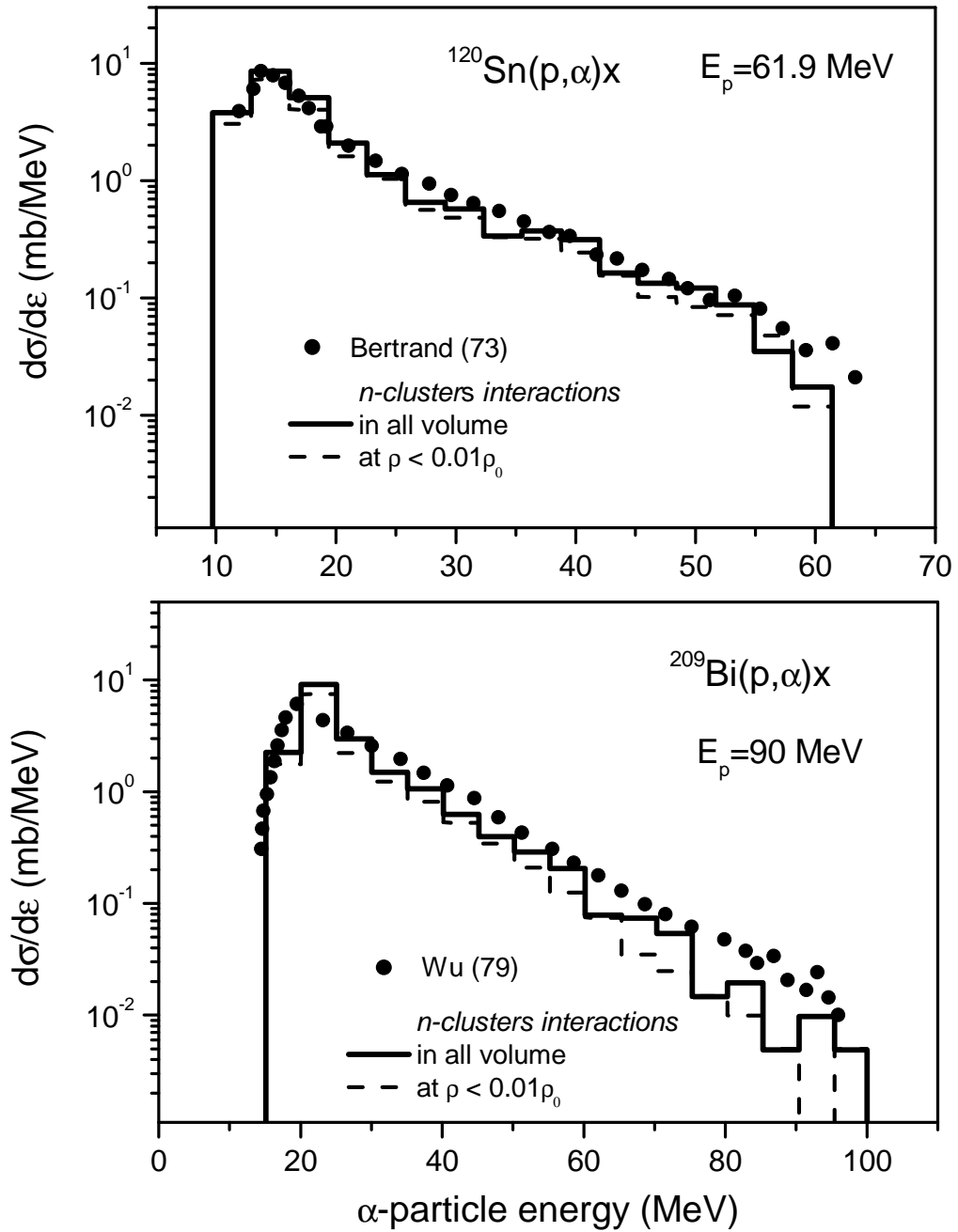


Fig.8 The α -particle emission spectrum calculated taking into account nucleon and preformed clusters (t , ^3He , α) interactions in all nuclear volume (solid histogram) and in the region with low density (dashed histogram). Experimental data are from Refs.[39,42].

Fig.9 shows an influence of the cluster momentum distribution on the calculated value of the α -particle emission spectrum for medium nuclei. Calculations were performed using Eq.(4)-(7) and simple approximations for the cluster momentum distributions and Fermi energies

$$N_x(\mathbf{p}_x) d\mathbf{p}_x \propto p^2 dp d\Omega, \quad (37)$$

and

$$T_{\alpha i}^F = T_{t i}^F = T_{^3\text{He}}^F = T_{n i}^F, \quad (38)$$

where symbol “x” refers to the α -particle, triton, ^3He and nucleon.

It is seen from Fig.9 that the use of the approximation equations Eq.(37),(38) instead of Eq.(4)-(7) results at the proton energy 62 MeV to the simple redefinition of the ζ value, Eq.(20). For 500 MeV protons the simulation of the cluster momentum distribution according to Eq.(37),(38) distorts high energy part of the calculated α -spectrum.

5. Examples of DISCA calculations

The applicability of the model for calculations at low projectile energies is illustrated by the data in Fig.10-12. The examples of calculated energy and angular α -particle distributions are shown in Fig.13-16.

Fig.17,18 demonstrate an importance of the consideration of the non-equilibrium α -particle emission to describe excitation functions of $(p,xnypz\alpha)$ reactions. Fig.19 shows the non-equilibrium component of the α -particle production cross-section for ^{197}Au . For the comparison the results obtained by the ALICE/ASH code is also shown. It is seen that despite of the difference of the models the knock-out contribution and the total non-equilibrium α -production cross-sections are close.

Many other examples of the DISCA code application can be found in Refs.[1-14, 24, 31, 38, 45-48].

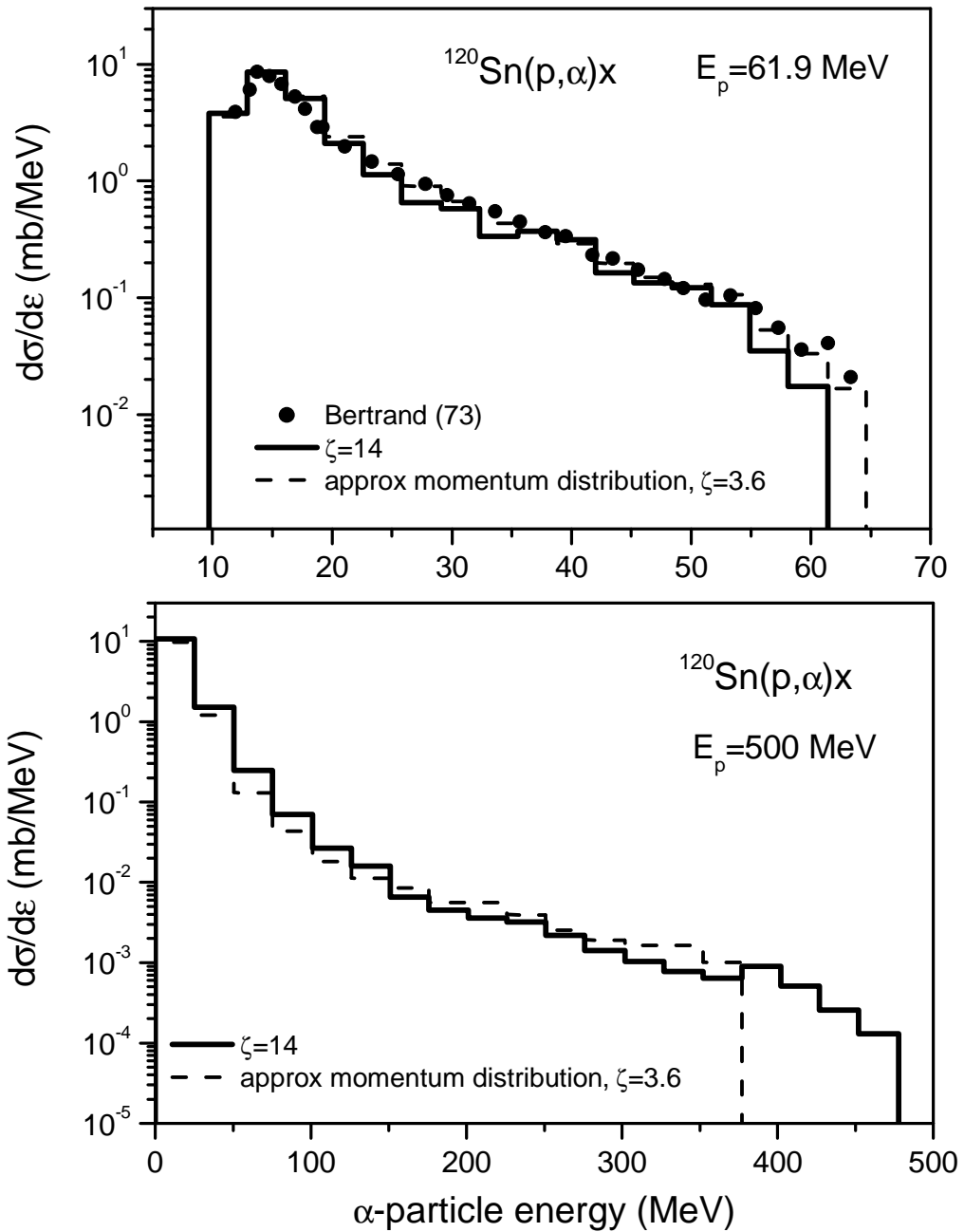


Fig.9 The α -particle emission spectrum calculated using Eq.(4)-(7) (solid histogram) and approximation expressions Eq.(37),(38) (dashed histogram) at different value of the ζ value. Experimental data are from Ref.[39].

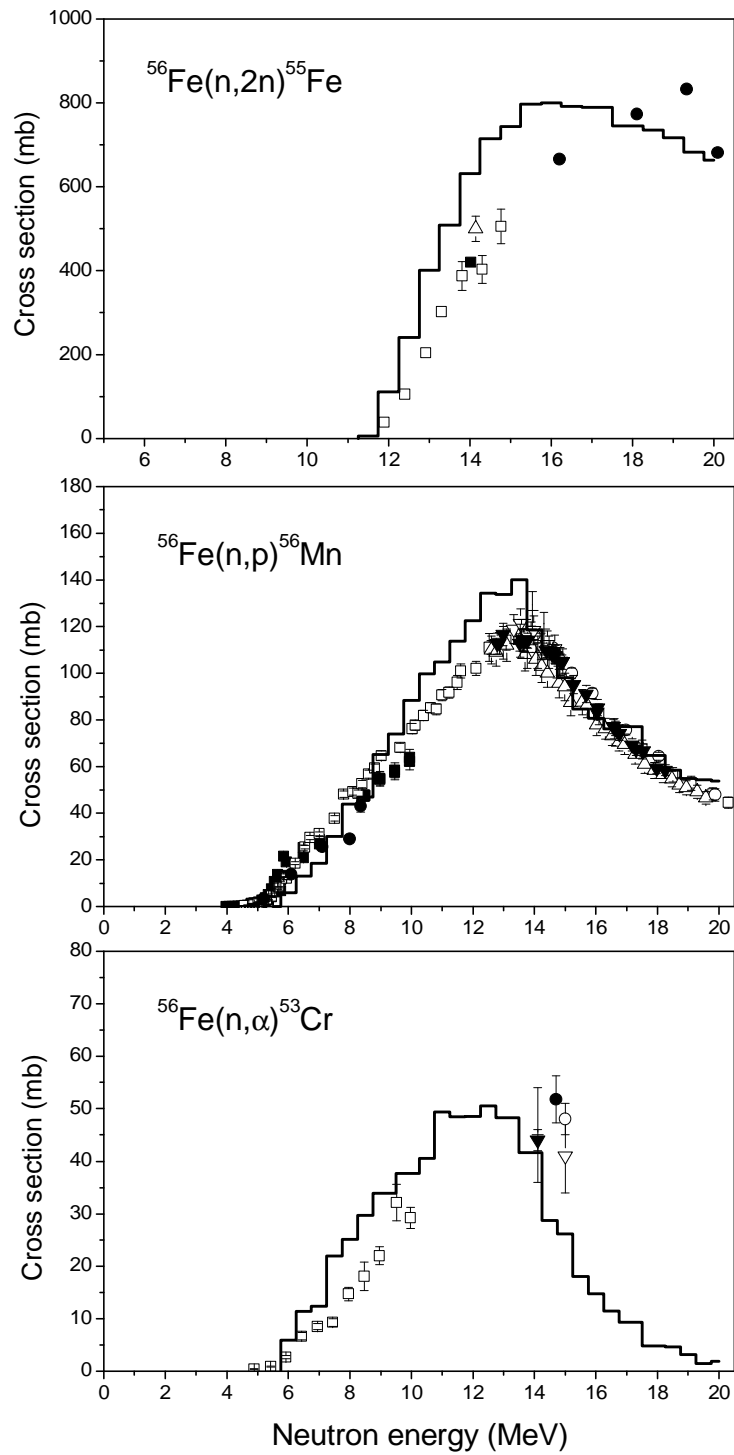


Fig.10 Neutron induced reaction cross-section for ^{56}Fe calculated using the DISCA code (histogram) at primary energies below 20 MeV. Experimental data are from EXFOR.

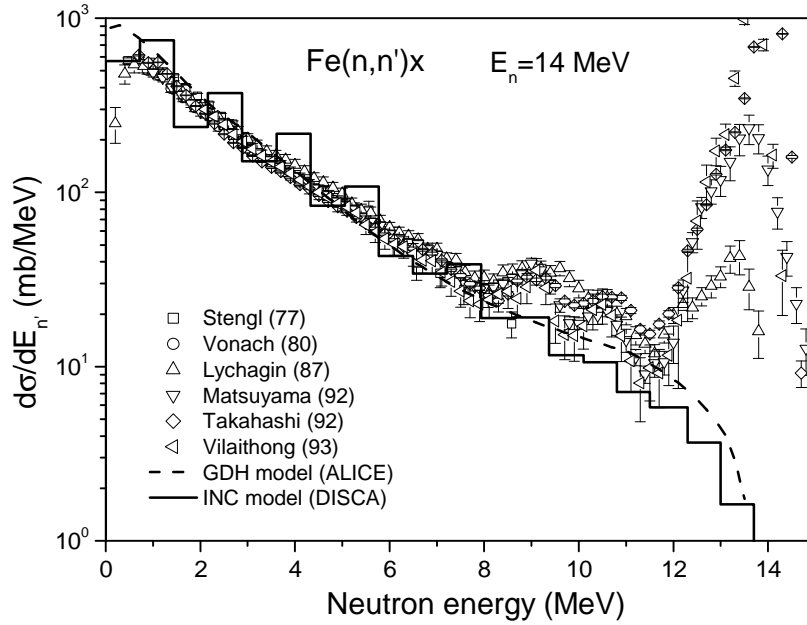


Fig.11 Neutron emission spectrum for the $\text{Fe}(n,n')x$ reaction induced by 14 MeV neutrons calculated by the intranuclear cascade evaporation model using the DISCA code (histogram) and by the GDH model using the ALICE code [29] (dashed line). Experimental data are from EXFOR.

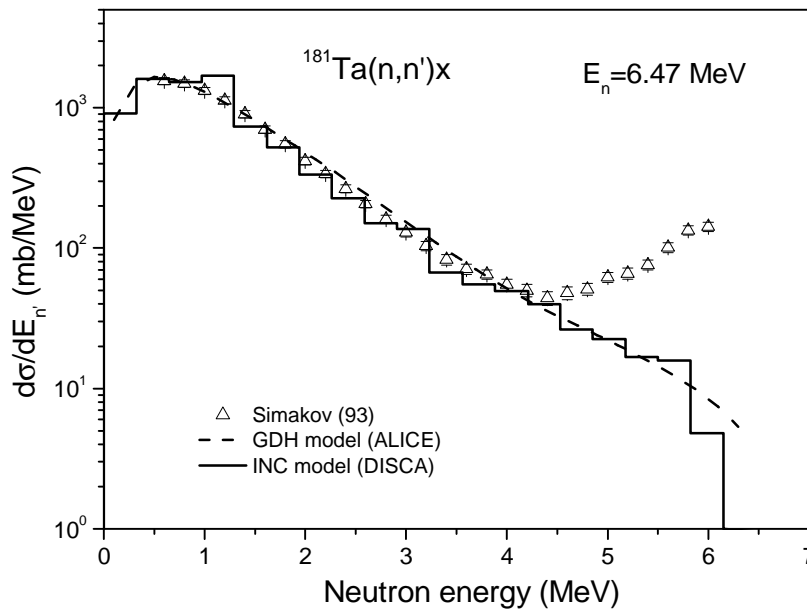


Fig.12 Neutron emission spectrum for the $^{181}\text{Ta}(n,n')x$ reaction induced by 6.47 MeV neutrons calculated using the DISCA code (histogram) and the ALICE code [29] (dashed line). Experimental data are from EXFOR.

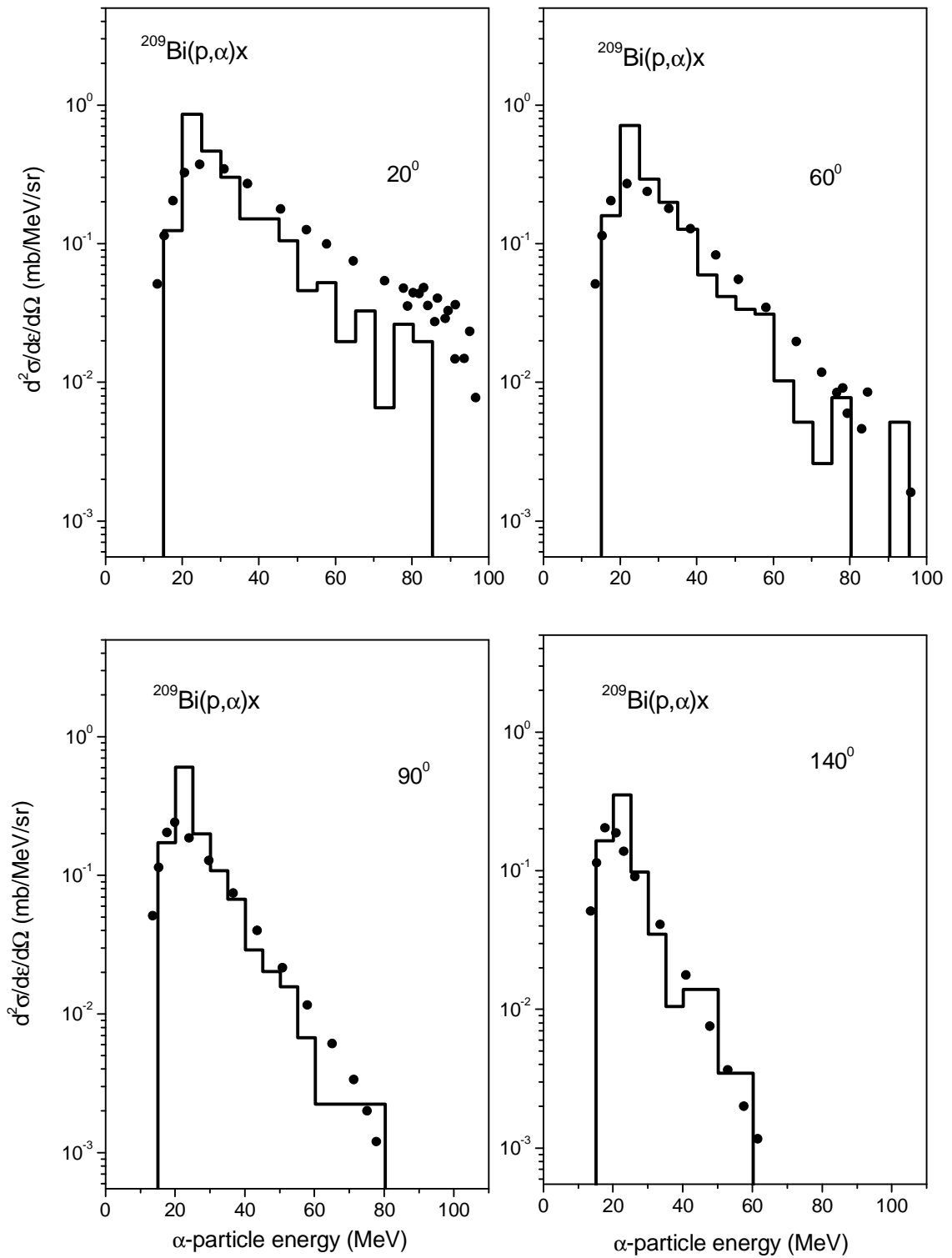


Fig.13 Calculated double differential cross-section for α -particles emitted from ^{209}Bi irradiated with 90 MeV protons. Experimental data (circle) are from Ref.[42].

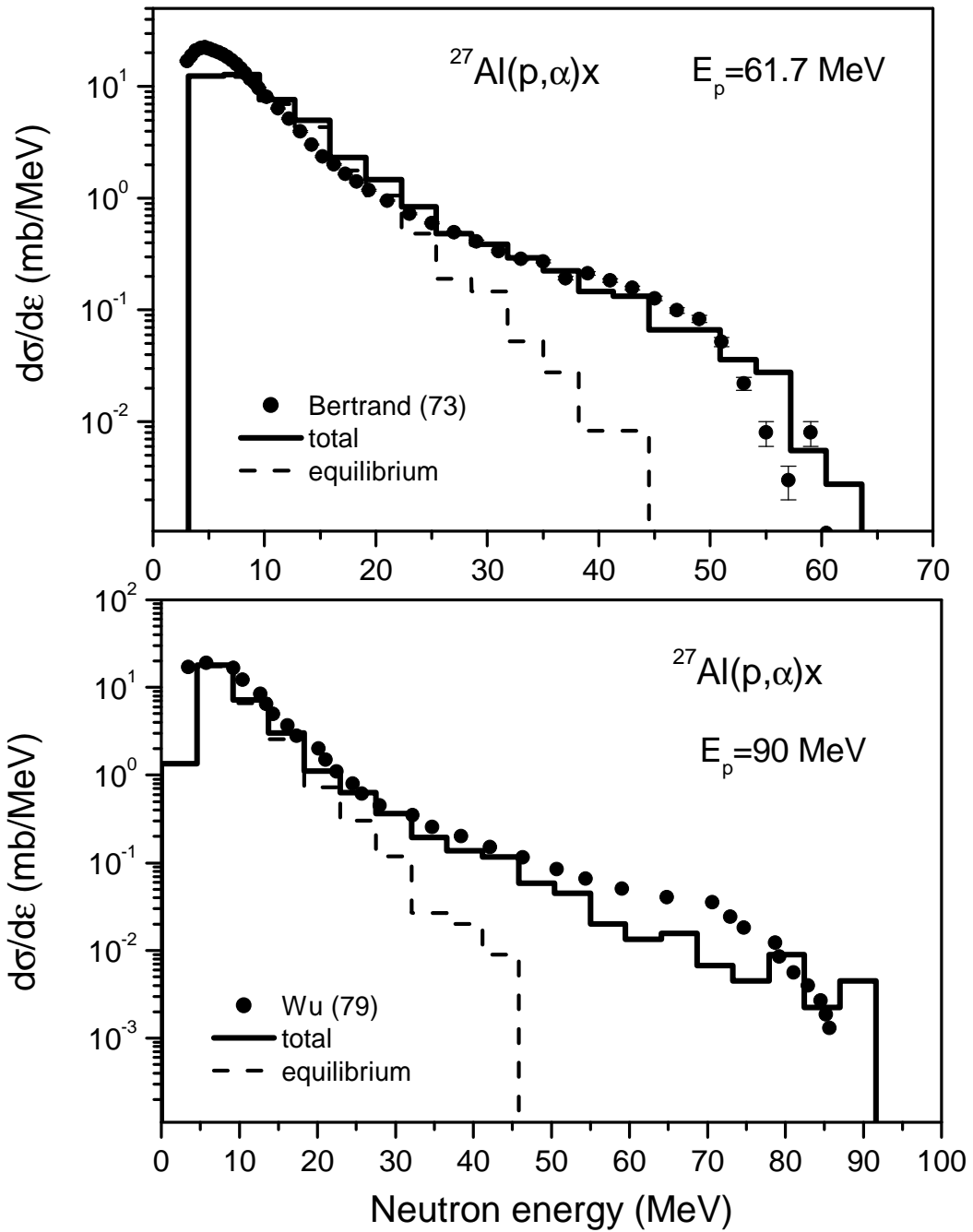


Fig.14 Energy distribution of α -particles from the $^{27}\text{Al}(p,\alpha)x$ reaction induced by 61.7 and 90 MeV protons calculated using the DISCA code. Experimental data are from Refs.[39,42].

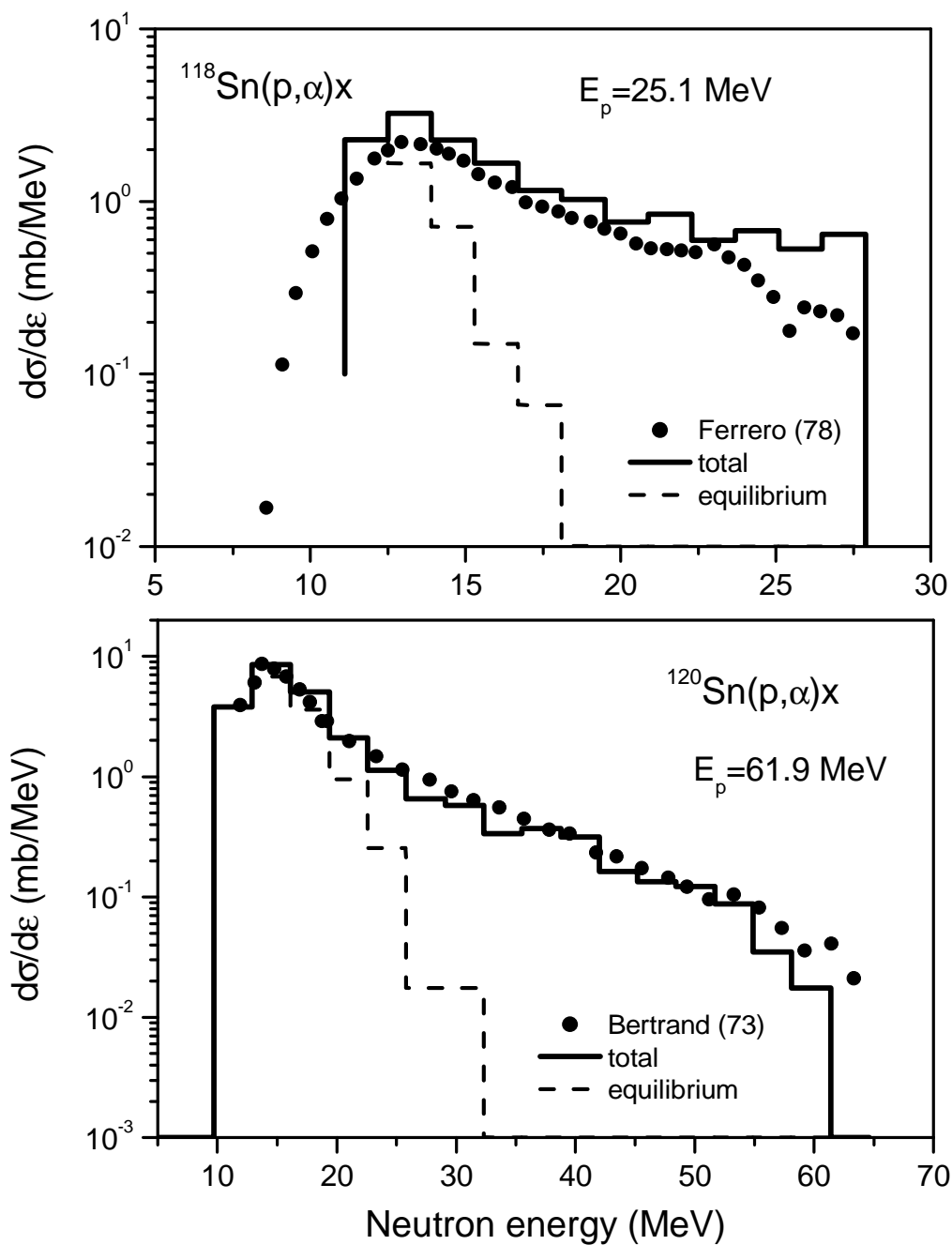


Fig.15 Energy distribution of α -particles from the $^{118}\text{Sn}(p,\alpha)x$ reaction induced by 25.1 MeV protons and from the $^{120}\text{Sn}(p,\alpha)x$ reaction induced by 61.9 MeV protons calculated using the DISCA code. Experimental data are from Refs.[39,43].

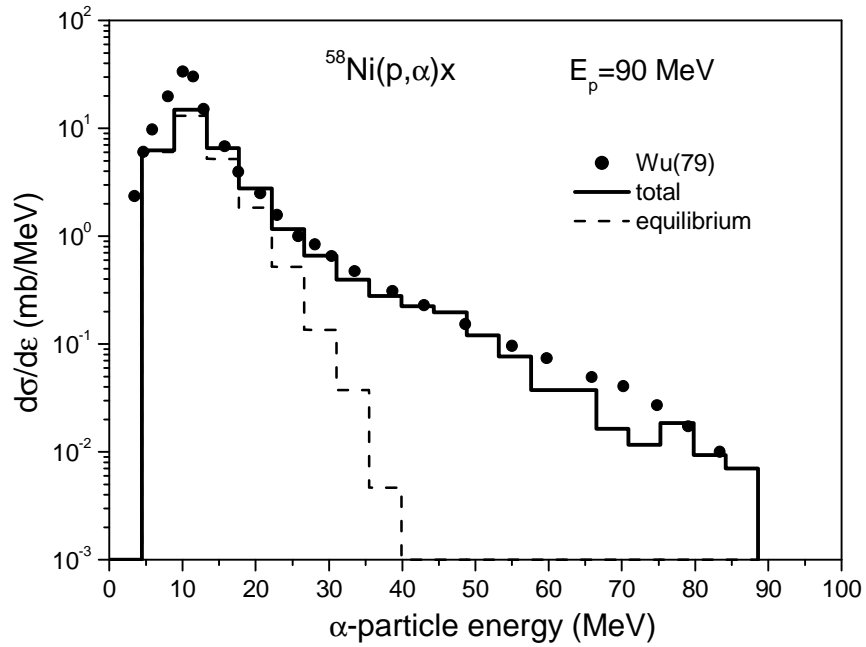


Fig.16 Energy distribution of α -particles from the $^{58}\text{Ni}(p,\alpha)x$ reaction induced by 90 MeV protons calculated using the DISCA code. Experimental data are from Ref.[42].

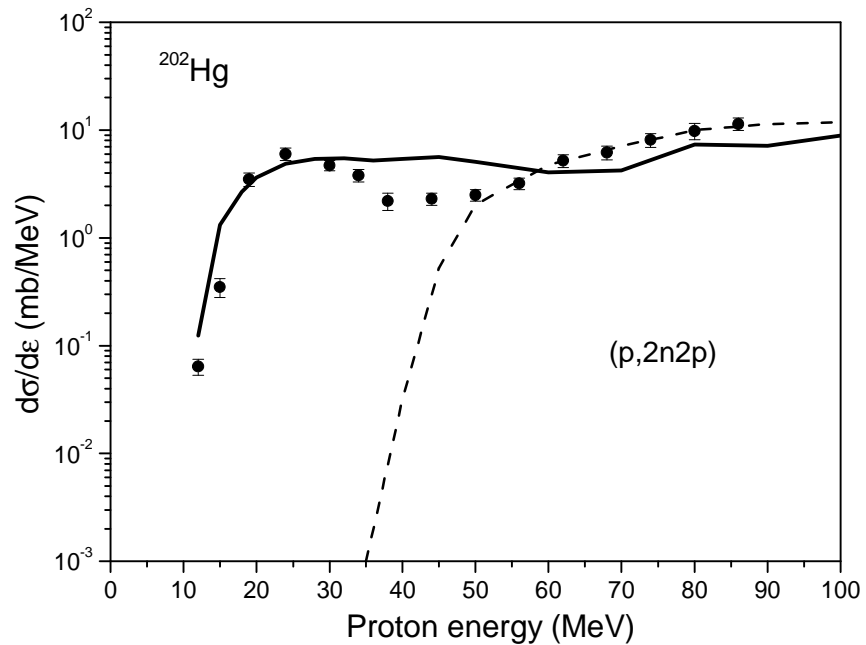


Fig.17 Excitation function of the $(p,2n2p)$ reaction for ^{202}Hg calculated using the DISCA code with (solid line) and without (dashed line) consideration of nucleon-cluster interactions. Experimental data are from Ref.[44].

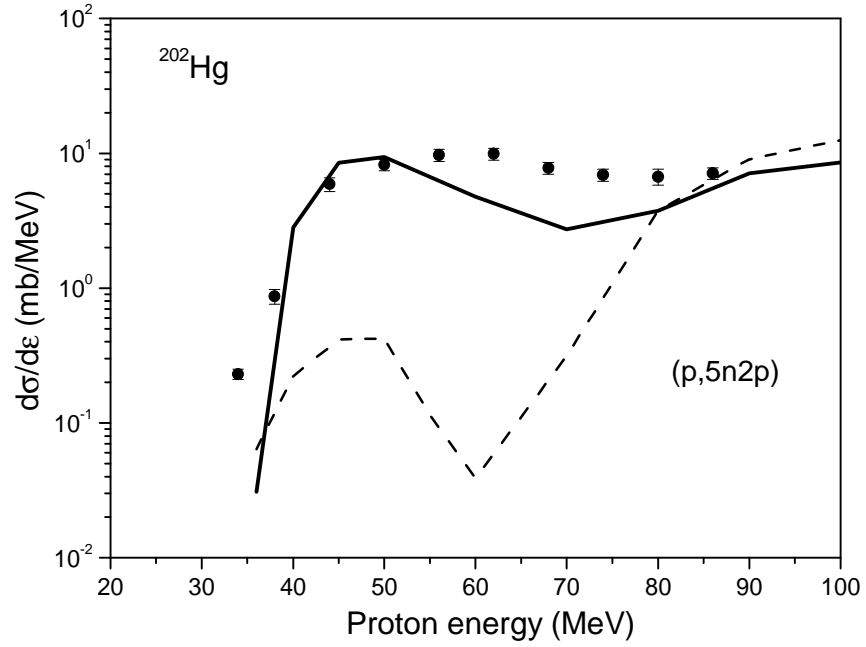


Fig.18 Excitation function of the (p,5n2p) reaction for ^{202}Hg calculated using the DISCA code with (solid line) and without (dashed line) consideration of nucleon-cluster interactions. Experimental data are from Ref.[44].

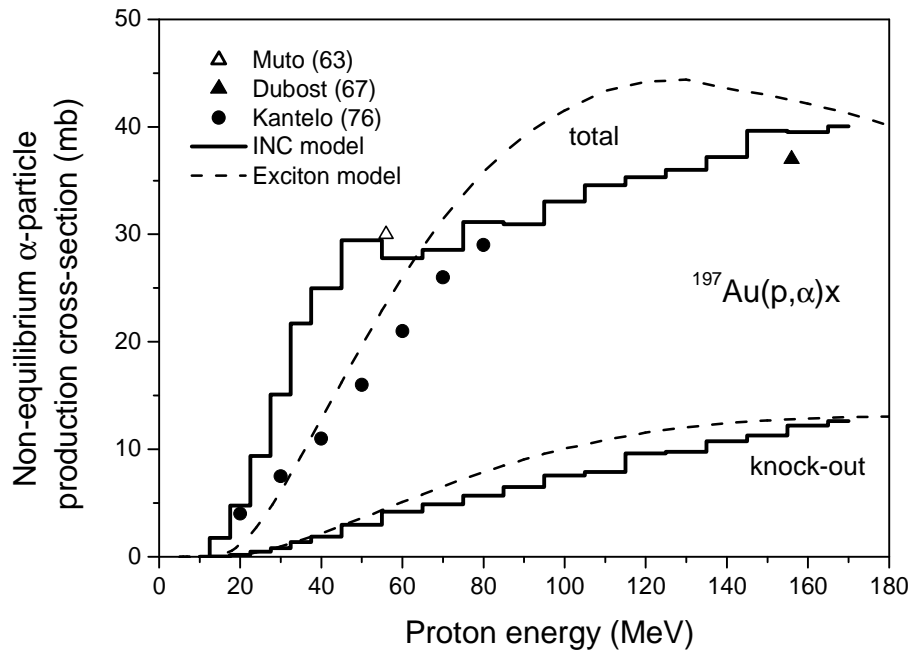


Fig.19 Production cross-section for non-equilibrium α -particles calculated using the DISCA code ($\phi_\alpha=0.06$, $\zeta=14$) (solid line) and the ALICE/ASH code (dashed line). The parameters of the pre-equilibrium exciton model from the ALICE/ASH code were obtained from the analysis [14] of available experimental α -particle emission spectra. Experimental data are from Refs.[44,51,52].

6. Computer compatibility

The DISCA code is written in FORTRAN. The code uses a random number generator, which can be different for different FORTRAN compilers. The current version of the code uses the GNU FORTRAN built-in random number generator RAND. To substitute it by the other one it is necessary to check the FUNCTION RANDOM in the code.

7. Input data file

The structure of the input data reflects historical stages in the DISCA code development. New features were introduced in the code keeping the possibility to use the same input structure for old and new versions of the code. In particular, it simplifies the comparison of the calculations performed using the DISCA-C code and DISCA-S code, which implement different models for intranuclear interactions. The description of the input is given below.

Card 1. Name of output files NAMRD: “NAMRD.XXX”. Format is (A8).

Card 2. The title of the task described in 72 characters including blank spaces.

Card 3. Parameters INFBIG, INFS0, INFSCR, INFDOS, INF DEN, INFSEP

Parameter INFBIG defines the size of printed information about details of the calculation. The value is from 0 to 3. Recommended: INFBIG = 0 or 1.

INFS0 defines the type of the cross-section for nonelastic interactions (σ_{non}) used for overall normalization of the results obtained. INFS0 = 1: the σ_{non} value is calculated using the Barashenkov data Ref.[33]; INFS0 = 2: the nonelastic cross-

section is calculated internally by the DISCA code; INFS0 = 3: the σ_{non} value is taken from the input file (*Card 10*); INFS0 = 4: the nonelastic cross-section is evaluated by the analytical expressions from Ref.[49] obtained using the results of optical model calculations. INFS0=4 is valid for nucleon incident energy up to 50 MeV. For incident α -particles INFS0 is set to 1. Recommended: INFS0 = 1.

INFSCR is the screen printing option for each Monte Carlo event proceeded. INFSCR = 1: yes, = 0: no.

INFDOS is not used in the present version of the code.

INFDEN defines the calculation of the non-equilibrium component of the triton and ^3He production cross-section according to the “nuclear bond breakdown” model from Ref.[50]. INFDEN=10: the calculations performed; INFDEN=0: no. Recommended: INFDOS = 10.

INFSEP is the option for the separate printing of the cross-sections calculated for a number of reactions (in addition to NAMRD.LIB file). INFSEP = 0 : no printing; INFSEP = 1: print cross-sections for reactions identified by the number of neutrons, protons and α -particles escaped. In this case the next lines of the input file must contain the number of particles. For example, for reactions (n,2n), (n,np2 α), (n,4n2p) three lines must be supplied: 2 0 0; 1 1 2; -4 2 0, and the minus sign for the last line means the end of the reaction list. INFSEP = 2 is as =1, but reactions are identified by Z and A for residual nucleus. For example, for reactions producing ^{55}Fe and ^{54}Mn nuclei two lines must be added: 26. 55.; -25. 54. No more than cross-sections for 100 reactions are printed separately. Full information about the cross-sections obtained is written in the NAMRD.LIB file (Sect.8). If the INFSEP parameter is increased by 10, the file NAMRD.ALP will be created (see below). Recommended value of INFSEP is 10, 11 or 12.

Cards group 4 (exact number depends from the number of reactions introduced according to the *INFSEP* parameter). Cards contain angles and energies of secondary particles for printing double differential cross-sections.

Nine emission angles in degrees are read for each secondary particle by Format (1X,9F6.1) for the calculation of the double differential cross-section $d^2\sigma d\Omega^{-1}d\epsilon^{-1}$ ($\text{mb}\cdot\text{MeV}^{-1}\cdot\text{sr}^{-1}$), which depends from the particle emission energy. Five energy intervals (MeV) are read by Format (1X, 5(F6.1,1X,F5.1)) for the double differential cross-section ($\text{mb}\cdot\text{MeV}^{-1}\cdot\text{sr}^{-1}$) calculation, which depends from the particle emission angle. The first symbol in each line (“N”, “P” or “A”) identifies the outgoing particle.

Data are presented for various outgoing particles in arbitrary order. Some particle types can be omitted. Note, that angles and energies introduced relate to the laboratory coordinate system. The double differential cross-sections are calculated for selected angles \pm DCEN, where the value of DCEN is defined in subroutine INIDAT.

Card 5. Parameters FIALPH, XPARDE, FICAP, MZONA, KZONESC

FIALPH is the relative number of α -clusters in the nucleus. It is the φ_α parameter from Eq.(15). The typical FIALPH value is from 0.05 to 0.1.

XPARDE defines the value of the level density parameter for equilibrium states: $a = A/\text{XPARDE}$, where A is the atomic mass number. The typical XPARDE value is from 7 to 10.

FICAP defines the probability of the triton and ^3He cluster pick-up, which results to the α -particle formation. It is the ζ parameter from Eq.(20). The typical value is about 14.

MZONA defines the number of the nuclear zone, beginning with which the nucleon-clusters interactions are considered. The nuclear zones are counted from the center of the nucleus. The MZONA value depends from the value of the KZONESC parameter. The typical value is from 1 to 5 for the division of nucleus on ten concentric regions (KZONESC=0).

KZONESC defines the number of nuclear zones with constant density in the nucleus approximating Wood-Saxon density distribution. KZONESC = 0 or 1: the nucleus is subdivided on 10 zones. The division of the Wood-Saxon density distribution is defined by the A1(i) array values in the subroutine INIDAT. The most remote zone corresponds to the nuclear density 0.01 of the density at the center of the nucleus. KZONESC = 2: the nucleus is subdivided on 33 zones. The division is defined by the A2(i) array in the subroutine INIDAT. The most remote zone corresponds to the nuclear density 10^{-5} of the density at the center. Recommended: KZONESC=0.

Card 6. The number of Monte Carlo events, KHIST. The KHIST value corresponds to elastic and nonelastic interactions of the incident particle with the nucleus.

Card 7. Values MPARIN, Z, AN

MPARIN defines the type of the projectile. MPARIN = 1: incident particle is neutron; = 2: proton; = 3: α -particle.

Z and AN are atomic number and atomic mass number of the target nucleus.

Card 8. The kinetic energy of projectile, T0 in MeV

Card 9. The use of this and next cards relates to old input structure of the code. New energy on this *Card* will continue the calculations. If no real value is found on the *Card*, the input value is interpreted as IDOPCS value from the old input of the DISCA code. IDOPCS defines the reading of the nonelastic cross-section used for overall normalization of the results of calculations (see below).

Card 10. The card is used in the case if no incident particle energy is found on the *Card 9*.

The *Card* allows to read the nonelastic reaction cross-section CSABS (barn) used for overall normalization of the results.

Card 11. Parameter ICONT. The card is used in the case if no incident particle energy is found on the *Card 9*.

ICONT defines if the calculations continue for new incident energy and new IDOPCS value. Recommended: omit *Card 10* and *Card 11*.

Example of the INPUT file

Table 1 shows an example of the DISCA code input. The task consists in the simulation of the $p+^{27}\text{Al}$ interaction at two proton incident energies equal to 62 and 90 MeV.

The nucleus is subdivided on ten concentric nuclear zones. The relative number of α -clusters, ϕ_α is equal to 0.05, the pick-up coefficient ζ is equal to 14. The simulation of the nucleon-cluster interactions is performed starting from fifth nuclear zone. The production cross-section for ^{22}Na , ^{24}Na and ^{26}Al is printed separately. Total number of Monte Carlo events for each incident energy is equal 200,000. The output file name is DISCAL27.

The energy and angular distribution will be printed for secondary neutrons, protons and α -particles. The double differential cross-section for neutrons escaped is calculated at 30° , 60° , 120° etc angles and for the outgoing energy intervals: from 17.5 to 22.5 MeV, from 37.5 to 42.5 MeV, from 57.5 to 62.5 MeV etc.

Table 1

```
DISCAL27
  Proton induced reaction for Al-27
0 1 1 0 10 12
 11 22
 11 24
-13 26
N 30.0 60.0 120.0 150.0 145.0 155.0 160.0 170.0 175.0
 17.5- 22.5 37.5- 42.5 57.5- 62.5 77.5- 82.5 95.0-105.0
P 20.0 30.0 45.0 60.0 75.0 90.0 105.0 120.0 140.0
 17.5- 22.5 37.5- 42.5 57.5- 62.5 77.5- 82.5 95.0-105.0
A 20.0 30.0 45.0 60.0 75.0 90.0 105.0 120.0 140.0
 55.0- 65.0 80.0- 90.0 100.0-120.0 110.0-140.0 200.0-300.0
0.05 9.0 14.0 5 1
200000
2 13. 27.
62.
90.
```

8. Output data files

The results of calculations are written in several output files. The name of files is defined by the character input variable NAMRD (Sect. 7). The brief description of output files is given below.

NAMRD.FUL contains detail information about calculations performed.

Printed:

- calculation options;
- cross-sections for reactions selected by the input parameter INFSEP;
- cross-sections for nonelastic interactions (barn) used for the particle production and displacement cross-section normalization;
- displacement cross-section (barn);
- neutron, proton, α -particle, deuteron, triton and ^3He production cross-sections (barn);
- energy and angular distributions of emitted particles in tables and in graphs. Units are mb/MeV for particle spectra and mb/MeV/sr for double differential cross-sections. Data are in the laboratory coordinate system.
- recoil spectrum (mb/MeV)

NAMRD.SHO contains information about the nonelastic cross-section, displacement cross-section and the particle production cross-sections.

NAMRD.LIB contains calculated cross-sections for all open reaction channels.

Printed: Z and A of the target nucleus, the energy of the projectile, the type of the projectile, the cross-section of nonelastic interactions (mb) used for the normalization of cross-sections printed, the origin of the nonelastic cross-

section (single character), number of chemical elements in the file (in brackets), the name of the code, number of Monte Carlo events corresponding to the nonelastic interactions, Z of the residual nucleus, number of isotopes (in brackets), A of the residuals, the production cross-sections (mb).

NAMRD.MLT contains information about particles emitted on the cascade and evaporation stages of the reaction.

Printed: details of the α -particle, triton and ^3He production, average energy of the excitation of residual nuclei formed after the cascade stage (MeV), multiplicity of neutrons, protons and α -particles emitted during the cascade and equilibrium stage of the reaction (dimensionless).

NAMRD.NNN, **NAMRD.PPP** and **NAMRD.AAA** contain neutron, proton and α -particle energy and angular distributions, respectively. The energy of ejectile is given in MeV. Spectra are given in mb/MeV and double-differential cross-sections are in mb/MeV/sr.

Printed: First column: the outgoing particle energy; second column: the non-equilibrium spectrum; third column: the evaporation spectrum; fourth: the total spectrum; columns 5-13: double differential cross-sections depending from the outgoing particle energy given in the first column; column 14: the angle of the particle emitted (degrees); columns 15-19: double differential cross-sections depending from the emission angle of the outgoing particle printed in 14 column. Energies and angles are given in the laboratory coordinate system.

NAMRD.ALP includes calculated non-equilibrium and total production cross-sections for α -particles (mb). Cross-sections are normalized on the

nonelastic cross-section printed in NAMRD.FUL and NAMRD.SHO files.

9. Publications relating to the DISCA code

The DISCA code has been used for

- the residual nuclei yields calculation in Refs.[9,12,24,31,46,47]
- the calculation of the energy and angular distribution of secondary particles in nuclear reactions in Refs.[12,24,38]
- simulation of deuteron interaction with nuclei in Ref.[13]
- the damage cross-section calculation in Refs.[1-5,7,10-12,45,48]
- the helium and tritium production calculation in Refs.[3,4,6-8,10-12,14,45].

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The text of the DISCA code

```
* * * * *
*
*                                     Version: 2005
*
* DISCA-C/05
*
* Intranuclear cascade evaporation model with clusters
*
* * * * *
* CHARACTER NAMRD*8, IDPA*1, NAMPAR(3)*1, C80*80
* REAL*8 INFGEN
* COMMON/DATINI/RA,T0,W0 /NPROL/NPROL/KHIST/KHIST
* COMMON/CSABS/CSABS,FIALP2 /INFGEN/INFGEN(9) /IWRI/IWRI
* COMMON/EOUT/SPE(19,5,3),PI(19),EOUT1(5,3),EOUT2(5,3),MSPE
* COMMON/SPEFUL/ANGLIM(9,2,3),ANGSUM(21,9,3),ANGCEN(9,3),DCEN,MANG
* COMMON/TEMP2/BONNE /XPARAM/XPARAM,FIALPH /NREJ/REFR,NREJ
* COMMON/INIQBO/Z,CKA,CKB,RPA,RPB,RALA,RALB
* COMMON/EVA/PARALP,PARPRO /INFDIS/INFDIS,INFOUP(3)
* COMMON/MAIIPR/IPR /AN/AN /INF/INFBIG,INFS0
* COMMON/IDOPCS/IDOPCS /MPARIN/MPARIN /MAX/MAXNEU,MAXPRO
* COMMON/INF001/INFKAL /INF002/INFDOS
* COMMON/INF003/INFDEN /INF004/KHIST0 /INFBON/IBOND
* COMMON/INF005/INFDM /INFSEP/KSEP(100,4),INFSEP,JSEPM
* COMMON/LIB91/WINLIB(100,250),INFLIB
* COMMON/K1996/K1996 /FICAP/FICAP,MZONA
* DATA NAMPAR/1HN,1HP,1HA/
C
C Input data file
C
C      Open(5,file='disca.dat')
C
C INPUT CARD 1
C*****
C-----
C
C NAMRD: Name of output files Namrd.XXX
C-----
C
C      Read(5,111)Namrd
111      Format(a8)
C
C      CALL OPEN_OUTPUT_FILES(NAMRD)
C
C
C Define general options for calculations
C
```

```

CALL OPTIONS(IPR,BONNE,IWRI,INFKAL)
C
C INPUT CARD 2
C*****
C-----
C
C INFGEN(): Text from 72 symbols will be printed in output file
C-----
C
C READ(5,1900)(INFGEN(I),I=1,9)
C
C
C INPUT CARD 3
C*****
C-----
C
C INFBIG : defines the bulk of the printed results of
C calculation
C = 0 : most appropriate information will printed; the
C arrays of COMMON Block MASOUT are not used in
C counting of events
C = 1 : additional information about options and parameters
C of calculation
C = 2 : printing of the lumped cross-sections and displa-
C cement cross-sections for reactions (1988)
C = 3 : the same as =2, but detail information for
C reactions (1988)
C Recommended: INFBIG=0
C
C INFS0 : defines the type of nonelastic cross-section
C used for normalization of the cross-sections
C and particle spectra obtained
C = 1 : data taken from Barashenkov, JINR, R2-89-770,
C 1989 (Subr BARASH)
C = 2 : nonelastic cross-section is calculated by the code
C using the INC model
C = 3 : data taken from input file (unit=5) is used
C = 4 : nonelastic cross-section is calculated according
C to Chatterjee A. et al, IAEA,INDC(IND)- 27/GJ, 1980
C Valid only for incident particle energies below
C 50 MeV. For primary alpha-particles INFS0 is turned
C to 1.
C Recommended: INFS0=1
C
C INFSCR : screen printing option for each Monte Carlo event
C proceeded, = 1 yes, = 0 no.
C Recommended: INSCR=1
C
C INFDOS : defines the Coulomb potential calculations for inve-
C rse reaction cross-sections (not used since 1996)
C = 0 : Coulomb potential is taken according to M.Blann
C = 1 : Coulomb potential is calculated according to
C V.M.Bychkov et al, 1982
C Recommended: INFDOS=0
C
C INFDEN : level density parameter calculation
C = 0 : a=A/XPARDE, ( XPARDE defined below )
C = 1-4: not used since 1996
C If INFDEN increased by 10, the non-equilibrium component of the triton,
C and He-3 production cross-section is calculated according to the

```

```

C "nuclear bond breakdown" model of F.P.Denisov, V.N. Mekhedov,
C "Nuclear Reactions at High Energies", Atomizdat, Moscow 1972, p.112
C Recommended: INFDOS=10
C
C   INFSEP      : option for printing of cross-sections for separate
C                 reactions
C   = 0         : no printing
C   = 1         : print cross-sections for reactions identified by
C                 the number of neutrons, protons and alphas escaped.
C                 For example for reactions (n,6np2a),(n,2n10p) one
C                 should insert two lines with
C                 6 1 2
C                 -2 10 0
C                 (minus means the end of reaction list ( < 100 )
more than 100)
C   = 2         : as =1, but reaction is identified by Z and A for
C                 residual nucleus. For example, for reactions
C                 resulting to nuclides 26. 55. and 25. 54. one should
C                 insert
C                 26. 55.
C                 -25. 54.
C If INFSEP increased by 10, the alpha particle production cross-section
C and its non-equilibrium component will printed in file NAMRD.ALP
C Recommended: INFSEP=10, 11 or 12
C
C-----
C           READ(5,*) INFBIG,INFS0,INFSCR,INFDOS,INFDEN,INFSEP
C
C           INFLIB=0
C           IF(INFSEP.GE.10) INFLIB=1
C           IF(INFSEP.GE.10) INFSEP=INFSEP-10
C           IF(INFSEP.EQ.1) CALL INSEP
C           IF(INFSEP.EQ.2) CALL INSEP2
C           INFDM=0
C           IF(INFDEN.GE.10)INFDM=1
C           IF(INFDEN.GE.10)INFDEN=INFDEN-10
C
C INPUT CARD GROUP 4 (or depends from number of reactions by INFSEP)
C*****
C-----
C
C Read angles and energies to store characteristics of secondary particles
C
C   The double differential cross-sections are calculated for selected
C   angles +/- DCEN (DCEN defined in Subr INIDAT) and selected energy ranges.
C   The first symbol in each line identifies an outgoing particle. Use
C   N,P and/or A only.
C   Nine angles (degrees) are read for each secondary particle by format
C   (1X,9F6.1) for the double differential cross-section  $d^2S/d\Omega dE$  calcula-
C   tion depending from particle emission energy (mb/MeV/sr) and five energy
C   intervals (MeV) by format (1X, 5(F6.1,1X,F5.1)) for the double differen-
C   tial cross-section calculation depending from emission angle (mb/MeV/sr)
C Example
CN   5.0  20.0  40.0  60.0  80.0 100.0 120.0 140.0 160.0
C   40.0- 50.0  80.0- 90.0 100.0-120.0 110.0-140.0 200.0-300.0
CP   5.0  20.0  40.0  60.0  80.0 100.0 120.0 140.0 160.0
C   40.0- 50.0  80.0- 90.0 100.0-120.0 110.0-140.0 200.0-300.0
C
C Note. Angles and energies relate to LCS system. Data can be introduced

```


C for different particles in arbitrary order. Any particle types can be
C omitted.

C-----
C

```
      INFDIS   =0
      INFOUP(1)=0
      INFOUP(2)=0
      INFOUP(3)=0
          MANG=9
          MSPE=5
2900  READ(5,3001)IDPA
3001  FORMAT(A1)
      DO 3100 MP=1,3
      IF(IDPA.EQ.NAMPAR(MP) ) GOTO 3300
3100  CONTINUE
      GOTO 4500
3300  BACKSPACE 5
      INFOUP(MP)=1
      READ(5,5000)(ANGCEN(ICEN,MP),ICEN=1,9)
5000  FORMAT(1X,9F6.1)
      READ(5,5001)(EOUT1(LL,MP),EOUT2(LL,MP),LL=1,5)
5001  FORMAT(1X, 5(F6.1,1X,F5.1) )
      GOTO 2900
4500  BACKSPACE 5
      IF(INFOUP(1).EQ.1.OR.INFOUP(2).EQ.1.OR.INFOUP(3).EQ.1)INFDIS=1
      IF(INFDIS.EQ.0)PRINT 3200
```

C

C

C INPUT CARD 5

C*****

C-----
C

```
C      FIALPH      : the relative number of alpha-clusters in nucleus.
C                  Typical FIALPH values are from 0.05 to 0.1
C
C      XPARDE      : defines level density parameter for equilibrium
C                  states, a = A/XPARDE. (XPARDE =8...10)
C
C      FICAP       : defines the pick-up probability for t ar He-3
C                  cluster resulting to alpha-particle formation.
C                  FICAP is about 14.
C
C      MZONA       : number of nuclear zone, beginning with which the
C                  non-equilibrium effects with alpha clusters are
C                  considered. The zones are counted from center of
C                  the nucleus. (MZONA depends from KZONESC value)
C                  Typical value is 1...5 for ten nuclear zones
C                  (KZONESC=0)
C
C      KZONESC     : defines number of zones with constant density in
C                  the nucleus approximating Wood-Saxon density distri-
C                  bution
C      = 0 or 1   : 10 zones. The division of the density distribution
C                  is defined by A1( ) array in Subr INIDAT. The most
C                  remote zone corresponds to the nuclear density 0.01
C                  of the density at the center.
C      = 2       : 33 zones. The division is defined by A2( ) array
C                  in Subr INIDAT. The most remote zone corresponds to
C                  the nuclear density 1.E-05 of the density at the
```

```

C                center.
C Recommended: KZONESC=0
C
C-----
C                READ(5,*)FIALPH,XPARDE,FICAP,MZONA,KZONESC
C
C                XPARAM=1./XPARDE
C
C                FI=FIALPH
C
C
C IBOND defines the method of the particle binding energy calculation
C   = 3 : the separation energy for neutrons, protons, deuterons
C         and alpha-particles is calculated using the table of
C         experimental masses and MSL-formula (M.Blann, Report
C         LLL(USA), UCID19614(1982)) for nuclei with
C         Z - Z(compound) < 9 and N - N(COMPOUND) < 22. For other
C         cases the Cameron formula is used.
C   = 2 : use the Cameron formula
C   = 1 : not used since 1993
C If IBOND < 0 : test printing for selected ABS(IBOND) option
C
C                IBOND=3
C                IBONDS=IABS(IBOND)
C
C PARALP and PARPRO are normalization coefficients for "old"
C Dostrovsky et al formulas for inverse cross-sections
C (See also Barashenkov, Toneev, "Interaction...",1972, p.413)
C                PARALP=1.
C                PARPRO=1.
C
C
C INPUT CARD 6
C*****
C-----
C                KHIST : the number of Monte Carlo events
C
C-----
C                READ(5,*)KHIST
C
C                KHIST0=KHIST
C
C
C INPUT CARD 7
C*****
C-----
C                MPARIN defines projectile
C   = 1 : incident particle is neutron
C   = 2 : proton
C   = 3 : alpha-particle
C
C                Z and AN are atomic number and atomic mass number for target
C                nucleus
C
C-----
C                READ(5,*)MPARIN,Z,AN
C
C                IF(MPARIN.eq.3) INFS0=1

```



```

C      CSABS is the nonelastic reaction cross-section (barn)
C      (only for IDOPCS=1)
C-----
          READ(5,*)CSABS
C
1818  continue
C
C
C
C INPUT CARD 9B (Old DISCA format. Read comment to CARD 9)
C*****
C-----
C
C      ICONT defines the continuation of the calculations for new incident
C      energy and new IDOPCS value
C
C          = 1   : new energy
C          = 0   : end of calculations
C
C-----
          READ(5,*)ICONT
C
1819  IF(INFLIB.EQ.1)  CALL ZERLIB
      PRINT 1987,T0,BONNE,KHIST,XPARAM
      IF(IBONDS.LT.1.OR.IBONDS.GT.3)GOTO 97
      IF(INFBIG.GT.1.AND.INFS0.EQ.0)INFS0=1
      IF(INFS0.EQ.3.AND.IDOPCS.EQ.0)INFS0=1
      IF(INFKAL.NE.1.OR.T0.LE.60.)GOTO 100
      IF(IWRI.NE.0)WRITE(IWRI,1830)T0
      WRITE(IPR,1830)T0
      PRINT 1830,T0
      STOP
97          IF(IWRI.NE.0)WRITE(IWRI,1840)IBOND
          WRITE(IPR,1840)IBOND
          PRINT 1840,IBOND
          STOP
100  GOTO(101,102,103),IBONDS
101          MAXNEU=13
          MAXPRO=9
          STOP
102          CALL PRECAM
          GOTO 104
103          CALL PRECAM
          CALL PRELYM
104  CONTINUE
          CALL ZERO1
          CALL INIDAT(KZONESC)
          CALL MASDAT
          CALL DENS
          IIII=-1
          KHIST=KHIST0
          DO 10 I=1,KHIST
              Istor=I
              IF(INFSCR.NE.1)GOTO 6
              ICC=I/500
              IF(ICC.NE.IIII)PRINT 2000,I
              IF(ICC.NE.IIII)IIII=ICC
C
C Label 10 is for normal end of MC history, Label 8 means too many reflec-

```

C tions (more than REFR), Label 40 means the dimension of arrays is not
 C sufficient to proceed KHIST events

C

```

6 CALL MODEL(IXX)
  GOTO(8,10,40),IXX
8 NREJ=NREJ+1
10 CONTINUE
20 CALL OUTPUT
* PRINT *, 'K1996 = ', K1996
  IF(ICONT.EQ.1)GOTO 1811
  STOP
40 KHIST=ISTOR
  GOTO 20

```

C

```

1830 FORMAT(1X,'Old Kalbach,Mann parametrization is not valid for '
  +' T0 =',G12.5)
1840 FORMAT(1X,'Incorrect IBOND number ',I6)
1987 FORMAT(1X,' T0=',F7.1,' BONNE=',F5.3,' KHIST=',I6/1X,' XPARAM=',
  +F7.3)
1900 FORMAT(9A8)
2000 FORMAT(1X,'***** EVENT ',I6)
3200 FORMAT(1X,60('*'))/1X,10X,'Characteritics of secondary particl',
  +'es are not stored'/1X,60('*'))
  END
*****
* SUBROUTINE A1B1B2 *
*****
SUBROUTINE A1B1B2
COMMON/FIGA1B/T1(16),BA1(16),BB1(16),BB2(9),BB3(8)
COMMON/ACTA1B/TREST /A1BNPD/S(4),PAR1 /AUXIL/ICOU1,ICOU2
  ICOU1=ICOU1+1
  I=1
10 I=I+1
  IF(I.LE.16)GOTO 12
  I=16
  ICOU2=ICOU2+1
  GOTO 20
12 IF(TREST-T1(I))20,20,10
20 IF(I-9)40,40,30
30 BBB=BB3(I-8)
  AAA=BB3(I-9)
  PAR1=0.14285714
  GOTO 50
40 BBB=BB2(I)
  AAA=BB2(I-1)
  PAR1=0.2
50 D2=T1(I)
  D1=T1(I-1)
  DT=D2-D1
  A1=TREST*(BA1(I)-BA1(I-1))/DT+(D2*BA1(I-1)-D1*BA1(I))/DT
  B1=TREST*(BB1(I)-BB1(I-1))/DT+(D2*BB1(I-1)-D1*BB1(I))/DT
  BB=TREST*(BBB-AAA)/DT+(D2*AAA-D1*BBB)/DT
  SUM=2.*A1+0.25*B1+PAR1*BB
  S(1)=A1/SUM
  S(2)=S(1)+0.25*B1/SUM
  S(3)=S(2)+S(1)
  S(4)=S(3)+PAR1*BB/SUM
  RETURN
  END

```

```

*****
*                               SUBROUTINE ACTIN                               *
*****
      SUBROUTINE ACTIN(IKS)
      COMMON/FIGA1B/T1(16),BA1(16),BB1(16),BB2(9),BB3(8)
      COMMON/K/K /JACT/JACT
      COMMON/PARTIC/WP,PX,PY,PZ,P,T,E,X,Y,Z,R,JIN,M
      COMMON/NDIM/NPAR /PARTNR/PPX,PPY,PPZ,PP,MX
      COMMON/TYPACT/L,L7 /ACTA1B/TREST
      COMMON/ACTSCI/PINX1,PINY1,PINZ1,WPX,RK3,RK4,GAMMA,SK2,VC2,VCX,
      *VCY,VCZ,MPX
      COMMON/URAND1/IYG
      IF(L.NE.6) GOTO 1
      CALL PICKUP(IKS)
      RETURN
1  MPX=MX
      WPX=WM(MX)
      WPX2=WPX*WPX
      EP=SQRT(PP*PP+WPX2)
      E1=E+EP
      VCX=(PX+PPX)/E1
      VCY=(PY+PPY)/E1
      VCZ=(PZ+PPZ)/E1
      SK1=PX*VCX+PY*VCY+PZ*VCZ
      VC2=VCX*VCX+VCY*VCY+VCZ*VCZ
      GAMMA=1./SQRT(1.-VC2)
      EE=((GAMMA-1.)*SK1/VC2)-E*GAMMA
      PINX=PX+EE*VCX
      PINY=PY+EE*VCY
      PINZ=PZ+EE*VCZ
      EIN=GAMMA*(E-SK1)
      TREST=(E*EP-PX*PPX-PY*PPY-PZ*PPZ)/WPX-WP
      CALL ANGLE(QSIN,QCOS,FISIN,FICOS)
      IF(ABS(PINZ)-1.E-06)10,20,20
10  BX=0.
      BY=0.
      BZ=400.
      GOTO 30
20  BX=400.
      BY=400.
      BZ=-400.*(PINX+PINY)/PINZ
30  B=SQRT(BX*BX+BY*BY+BZ*BZ)
      PO2=PINX*PINX+PINY*PINY+PINZ*PINZ
      EPIN=SQRT(PO2+WPX2)
      RK0=QSIN/B
      RK1=RK0*FICOS*SQRT(PO2)
      RK2=RK0*FISIN
      PINX1=RK1*BX+RK2*(PINY*BZ-PINZ*BY)+QCOS*PINX
      PINY1=RK1*BY+RK2*(PINZ*BX-PINX*BZ)+QCOS*PINY
      PINZ1=RK1*BZ+RK2*(PINX*BY-PINY*BX)+QCOS*PINZ
      SK2=PINX1*VCX+PINY1*VCY+PINZ1*VCZ
      RK3=GAMMA*EIN
      RK4=GAMMA*EPIN
      TB1=RK3+GAMMA*SK2-WP
      TP1=RK4-GAMMA*SK2-WPX
      CALL PAULI(TB1,TP1,IKS)
      RETURN
      END
*****

```

```

*                               FUNCTION ANGKAL                               *
*****
      FUNCTION ANGKAL(QCOS,E1)
C QCOS is cos required
      DIMENSION P(30)
C P(1) value corresp to polynomial P(0)
      LMAX=9
      CALL LEGEN(QCOS,P)
C M=1 --- BKAL(0,E1)=1 ,P(1) -polynomial of (0) = 1
      S=1.
      DO 10 M=2,LMAX
10    S=S+BKAL((M-1),E1)*P(M)
      ANGKAL=S
      RETURN
      END
*****
*                               SUBROUTINE ANGLE                               *
*****
      SUBROUTINE ANGLE(QSIN,QCOS,FISIN,FICOS)
      COMMON/FIGALB/T1(16),BA1(16),BB1(16),BB2(9),BB3(8)
      COMMON/TYPACT/L,L7
      COMMON/ACTALB/TREST
      COMMON/URAND1/IYG
      GOTO(10,20,30,40,40),L
10    CALL NPDRAW(QCOS,FI)
      QSIN=SQRT(ABS(1.-QCOS*QCOS))
      FISIN=SIN(FI)
      FICOS=COS(FI)
      RETURN
20    CALL PPDRAW(QCOS,FI)
      QSIN=SQRT(ABS(1.-QCOS*QCOS))
      FISIN=SIN(FI)
      FICOS=COS(FI)
      RETURN
* N-A interaction
30    T = TREST
      CALL NADRAW(T,QCOS,FI)
      QSIN=SQRT(ABS(1.-QCOS*QCOS))
      FISIN=SIN(FI)
      FICOS=COS(FI)
      RETURN
* A-N interaction
40    T = TREST/4.
      CALL NADRAW(T,QCOS,FI)
      QSIN=SQRT(ABS(1.-QCOS*QCOS))
      FISIN=SIN(FI)
      FICOS=COS(FI)
      RETURN
      END
*****
*                               SUBROUTINE AUXANG                               *
*****
      SUBROUTINE AUXANG
C Angular distributions acording to Kalbach, Mann phenomenology
      COMMON/INTTR1/PWX,PWY,PWZ,TW,NPREN,NPREP,NPREA
      COMMON/MAIIPR/IPR /URAND1/IYG
      R=1.
      EKAL=TW
      RMAX=ANGKAL(R,EKAL)

```

```

      DO 100 I=1,100
C   Argument  QCOS=2.*X-1.
      C1=2.*RANDOM(0)-1.
C   Function
      C2=RMAX*RANDOM(0)
      RF=ANGKAL(C1,EKAL)
      IF(RF.GE.C2) GOTO 200
100  CONTINUE
      WRITE(IPR,150)RMAX,RF,C1,C2
150  FORMAT(1X,'Error: COS can not be obtained in Subr AUXANG'/
* 1X,'RMAX=',G12.5,' RF=',G12.5/' C1=',G12.5,' C2=',G12.5)
      STOP
200  QCOS=C1
      QSIN=SQRT(1.-QCOS*QCOS)
      FI=6.283*RANDOM(0)
      P=SQRT(TW*(TW+938.92635))
      PWZ=P*QCOS
      PWX=P*QSIN*COS(FI)
      PWY=P*QSIN*SIN(FI)
      RETURN
      END
*****
*           SUBROUTINE BARASH                               *
*****
      SUBROUTINE BARASH(TEST,MPAR9,A9,T9,CSNON)
*
* Evaluated nonelastic cross-sections (mb)
* Data taken from Barashenkov,JINR, R2-89-770,1989
* MPAR=1 : neutron incident; = 2 : proton
* IF TEST .ne. 0 : test printing
* A : Atomic mass number of target nucleus
* CSP(ENERGY,ATOMIC MASS) : proton cross-sections
* CSN(ENERGY,ATOMIC MASS) : neutron cross-sections
*
      DIMENSION CSP(46,12),CSN(46,12),ENERGY(46)
      DIMENSION CSPAL(46),CSPSI(46),CSPCA(46),CSPFE(46),CSPCU(46),
1      CSPMO(46),CSPCD(46),CSPSN(46),CSPW(46),CSPPB(46),
2      CSPU(46),CSPNA(46)
      DIMENSION CSNAL(46),CSNSI(46),CSNCA(46),CSNFE(46),CSNCU(46),
3      CSNMO(46),CSNCD(46),CSNSN(46),CSNW(46),CSNPB(46),
4      CSNU(46),CSNNA(46)
      DIMENSION RIDENT(12)
      DIMENSION AELEM(12)
      DIMENSION PPN(6),PPP(6)
      EQUIVALENCE (CSP(1),CSPNA(1)
+), (CSP(47),CSPAL(1)),(CSP(93),CSPSI(1)),(CSP(139),CSPCA(1)
+), (CSP(185),CSPFE(1)),(CSP(231),CSPCU(1)),(CSP(277),CSPMO(1)
+), (CSP(323),CSPCD(1)),(CSP(369),CSPSN(1)),(CSP(415),CSPW(1)
+), (CSP(461),CSPPB(1)),(CSP(507),CSPU(1))
      EQUIVALENCE (CSN(1),CSNNA(1)
+), (CSN(47),CSNAL(1)),(CSN(93),CSNSI(1)),(CSN(139),CSNCA(1)
+), (CSN(185),CSNFE(1)),(CSN(231),CSNCU(1)),(CSN(277),CSNMO(1)
+), (CSN(323),CSNCD(1)),(CSN(369),CSNSN(1)),(CSN(415),CSNW(1)
+), (CSN(461),CSNPB(1)),(CSN(507),CSNU(1))
C PROTON INDUCED REACTION
      DATA AELEM/ 23., 27., 28., 40., 55.9, 63.6, 96., 112.6, 118.8,
#      183.9, 207.3, 238./
      DATA ENERGY/14., 15., 16., 17., 18., 19., 20., 22.,
$      25., 27., 30., 33., 35., 37., 40., 45.,

```


\$ 50., 55., 60., 65., 70., 80., 90., 100., 120.,
 \$ 140., 150., 160., 180., 200., 250., 300., 350., 400.,
 \$ 500., 600., 700., 800., 900., 1000., 1500., 2000., 3000.,
 \$ 5000., 7000., 10000./
 DATA RIDENT/'NA', 'AL', 'SI', 'CA', 'FE', 'CU', 'MO',
 + 'CD', 'SN', 'W', 'PB', 'U'/
 DATA CSPNA/600., 617., 638.5, 660., 665., 670., 675., 680.,
 \$ 680., 670.,
 \$ 650., 605., 575., 565., 550., 525., 490., 470.,
 \$ 450., 435., 420., 385., 367., 360., 350., 350.,
 \$ 350., 345., 347., 350., 350., 350., 356., 364.,
 \$ 384., 392., 400., 408., 410., 420., 408., 412.,
 \$ 420., 411., 409., 407./
 DATA CSNNA/960., 930., 910., 890., 867.3, 844.67, 822.,
 \$ 790., 750., 725.,
 \$ 686., 646.4, 620., 612., 600., 575., 540., 518.5,
 \$ 497., 473.5, 450., 414., 390., 380., 372., 364.,
 \$ 360., 355., 354., 350., 350., 350., 356., 364.,
 \$ 384., 392., 400., 408., 410., 420., 408., 412.,
 \$ 420., 411., 409., 407./
 DATA CSPAL/650., 682., 690., 715., 726.67, 738.33,
 \$ 750., 762., 750., 740.,
 \$ 720., 681., 655., 640., 617., 575., 540., 505.,
 \$ 470., 462.5, 455., 432., 420.,
 \$ 408., 400., 403., 403., 408., 406., 404., 400.,
 \$ 402., 404., 408., 424., 438., 448., 450., 454.,
 \$ 456., 472., 480., 466., 456., 452., 448./
 DATA CSNAL/1000., 990., 975., 950., 935., 920.,
 \$ 905., 875., 825., 800.,
 \$ 762., 718.8, 690., 674.8, 652., 610., 570., 532.5,
 \$ 495., 487.5, 480., 456., 444.,
 \$ 432., 420., 420., 420., 420., 410., 410., 400.,
 \$ 402., 404., 408., 424., 438., 448., 450., 454.,
 \$ 456., 472., 480., 466., 456., 452., 448./
 DATA CSPSI/670., 700., 725., 750., 760., 770.,
 \$ 780., 780., 770., 757.,
 \$ 735., 708., 690., 668., 635., 585., 570., 530.,
 \$ 490., 482.5,
 \$ 475., 460., 446., 431., 423., 425., 425.,
 \$ 425., 425., 422., 422., 412., 416., 422., 440.,
 \$ 460., 472., 476., 479., 480., 492., 496., 488.,
 \$ 472., 472., 464./
 DATA CSNSI/1060., 1035., 1015., 990., 971.67, 953.33,
 \$ 935., 900., 860., 830.,
 \$ 790., 751., 725., 701., 665., 630., 600., 560.,
 \$ 520., 512.,
 \$ 504., 486., 470., 456., 444., 432., 432.,
 \$ 432., 418., 418., 415., 412., 416., 422., 440.,
 \$ 460., 472., 476., 479., 480., 492., 496., 488.,
 \$ 472., 472., 464./
 DATA CSPCA/770., 800., 823., 850., 866.67, 883.3,
 \$ 900., 925., 935., 920., 895.,
 \$ 859., 835., 821., 800., 750., 715., 678., 640., 622.5,
 \$ 605., 590., 588., 573.,
 \$ 555., 543., 540., 540., 540., 535., 530., 530., 540.,
 \$ 550., 570., 595., 610., 615., 620., 622., 629., 630.,
 \$ 620., 612., 607., 592./
 DATA CSNCA/1240., 1225., 1200., 1180., 1161.67, 1143.3,
 \$ 1125., 1090., 1045., 1020., 980.,

\$ 947., 925., 907., 880., 825., 770., 725., 680., 660.,
 \$ 640., 620., 615., 600.,
 \$ 580., 565., 560., 560., 560., 550., 535., 530., 540.,
 \$ 550., 570., 595., 610., 615., 620., 622., 629., 630.,
 \$ 620., 612., 607., 592./
 DATA CSPFE/900., 960.,1015.,1070.,1076.67,1083.3,
 \$ 1090.,1115.,1120.,1115.,1080.,
 \$ 1045.,1025.,1000., 960., 900., 885., 865., 790., 777.5,
 \$ 765.,
 \$ 740., 720., 700., 697., 697., 697., 697., 695., 690.,
 \$ 688., 690., 712., 705., 735., 750., 765., 775., 780.,
 \$ 795., 810., 813., 810., 784., 757., 743./
 DATA CSNFE/1440.,1433.,1411.5,1390.,1368.3, 1346.67,
 \$ 1325.,1280.,1260.,1215.,1180.,
 \$ 1140.,1110.,1080.,1040., 990., 955., 920., 885.,860.,
 \$ 835.,
 \$ 800., 780., 765., 750., 725., 720., 720., 710., 700.,
 \$ 700., 700., 712., 705., 735., 750., 765., 775., 780.,
 \$ 795., 810., 813., 810., 784., 757., 743./
 DATA CSPCU/935.,1000.,1030.,1060.,1103.3,1146.67,
 \$ 1190.,1220.,1250.,1240.,1210.,
 \$ 1150.,1130.,1115.,1050., 985., 950., 890., 870., 845.,
 \$ 820.,
 \$ 800., 785., 780., 770., 750., 745., 740., 735., 735.,
 \$ 745., 760., 762., 770., 795., 810., 825., 830., 840.,
 \$ 848., 870., 870., 868., 840., 825., 810./
 DATA CSNCU/1540.,1535.,1517.5,1500.,1481.67,1463.3,
 \$ 1445.,1407.,1380.,1330.,1300.,
 \$ 1285.,1270.,1240.,1190.,1090.,1010., 940., 920., 890.,
 \$ 860.,
 \$ 835., 820., 810., 800., 780., 775., 770., 760., 760.,
 \$ 758., 765., 765., 770., 795., 810., 825., 830., 840.,
 \$ 848., 870., 870., 868., 840., 825., 810./
 DATA CSPMO/1025.,1080.,1135.,1190.,1253.3,1316.67,
 \$ 1380.,1440.,1495.,1475.,1420.,
 \$ 1350.,
 \$ 1310.,1300.,1290.,1250.,1200.,1170.,1130.,1112.5,
 \$ 1095.,1060.,
 \$ 1040.,1022.,1020.,1016.,1016.,1016.,1016.,1012.,1005.,
 \$ 1005.,1005.,1010.,1060.,1085.,1100.,1110.,1120.,1127.,
 \$ 1150.,1160.,1140.,1100.,1085.,1080./
 DATA CSNMO/1790.,1775.,1757.5,1740.,1720.,1700.,
 \$ 1680.,1640.,1580.,1550.,1510.,
 \$ 1460.,
 \$ 1440.,1418.,1380.,1330.,1280.,1240.,1200.,1177.5,
 \$ 1155.,1140.,
 \$ 1110.,1110.,1080.,1065.,1050.,1050.,1025.,1020.,1015.,
 \$ 1020.,1022.,1026.,1060.,1085.,1100.,1110.,1120.,1127.,
 \$ 1150.,1160.,1140.,1100.,1085.,1080./
 DATA CSPCD/1020., 1100., 1162.5,1225.,1290.,1365.,1440.,1520.,
 \$ 1575.,1560.,1518.,1460.,1420.,1412.,1400.,1365.,1340.,
 \$ 1300.,1280.,1260.,1200.,1190.,1160.,6*1125., 3*1120.,
 \$ 1118.,1146.,1180.,1220.,1240.,1250.,1260.,1265.,1270.,
 \$ 1275.,1250.,2*1222.,1220./
 DATA CSNCD/1920.,1910.,1895.,1880.,1860.,1850.,1840.,1800.,1760.,
 \$ 1720.,1675.,1630.,1600.,1568.,1520.,1465.,1420.,1390.,
 \$ 1340.,1310.,1280.,1275.,1235.,1225.,1200.,3*1170.,
 \$ 1165.,1145.,1140.,1140.,1135.,1160.,1180.,
 \$ 1220.,1240.,1250.,1260.,1265.,1270.,

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$          1275.,1250.,2*1222.,1220./
DATA CSPSN/1020.,1080.,1175.,1270.,1335.,1400.,1465.,1505.,1610.,
$          1610.,1550.,1535.,1500.,1476.,1440.,1407.,1370.,1340.,
$          1300.,1285.,1260.,1230.,1215.,1200.,1180.,1170.,1170.,
$          1165.,1165.,
$          1170.,1165.,1165.,1183.,1195.,1240.,1270.,1285.,
$          1300.,1300.,1310.,1320.,1320.,1290.,3*1240./
DATA CSNSN/1945.,1940.,1922.5,1905.,1890.,1875.,1860.,1830.,1780.
$          ,1755.,1717.,1680.,1645.,1615.,1570.,1500.,1455.,1410.,
$          1370.,1340.,
$          1320.,1290.,1285.,1260.,1240.,1235.,1212.,1200.,
$          2*1200.,2*1190.,1200.,1210.,1240.,1270.,1285.,1300.,
$          1300.,1310.,1320.,1320.,1290.,3*1240./
DATA CSPW / 950.,1020.,1130.,1240.,1400.,1480.,1560.,1670.,1760.,
$          1830.,1850.,1855.,1870.,1858.,1840.,1800.,1770.,1740.,
$          1715.,1680.,1670.,1650.,1620.,1610.,6*1600.,1595.,
$          1585.,1595.,1615.,1640.,1700.,1720.,1730.,1740.,1750.,
$          1780.,1780.,1750.,1740.,1735.,1710./
DATA CSNW /2440.,2400.,2385.,2370.,2350.,2330.,2310.,2270.,2220.,
$          2195.,2150.,2100.,2070.,2046.,2010.,1945.,1900.,1850.,
$          1820.,1780.,1760.,1730.,1720.,1680.,1680.,1660.,1660.,
$          1650.,1650.,1640.,1640.,1612.,1615.,1625.,1640.,
$          1700.,1720.,1730.,1740.,1750.,
$          1780.,1780.,1750.,1740.,1735.,1710./
DATA CSPPB/ 900.,1060.,1130.,1200.,1310.,1420.,1515.,1620.,1750.,
$          1800.,1915.,1984.,2030.,2002.,1960.,1940.,1910.,1860.,
$          1840.,1810.,1780.,1770.,1760.,1740.,1720.,1725.,1740.,
$          1740.,1730.,1720.,1700.,1710.,1720.,1730.,1740.,1815.,
$          1835.,1860.,1890.,1895.,1920.,1920.,1890.,1850.,1835.,
$          1830./
DATA CSNPB/2580.,2550.,2527.5,2505.,2483.5,2462.,2460.,2435.,2380.
$          ,2355.,2280.,2220.,2180.,2176.,2170.,2130.,2080.,2035.,
$          1980.,1960.,1940.,1900.,1870.,1840.,1800.,1800.,1800.,
$          1780.,1760.,1760.,1740.,1730.,1725.,1740.,
$          1785.,1815.,1835.,1860.,1890.,
$          1895.,1920.,1920.,1890.,1850.,1835.,1830./
DATA CSPU / 800., 900.,1000.,1100.,1200.,1300.,1410.,1510.,1680.,
$          1800.,2000.,2120.,2200.,2152.,2080.,2060.,2025.,2100.,
$          2030.,2030.,2030.,2000.,3*1960.,1940.,1925.,1920.,
$          1905.,1890.,1860.,1880.,1910.,1930.,1945.,1985.,2010.,
$          2040.,2070.,2080.,2090.,2095.,2080.,2063.,2060.,2050./
DATA CSNU /2820.,2770.,2735.,2700.,2680.,2660.,2645.,2620.,2580.,
$          2550.,2515.,2476.,2450.,2426.,2390.,2320.,2260.,2225.,
$          2200.,2170.,2140.,2080.,2060.,2040.,2000.,1980.,1965.,
$          1960.,1930.,1920.,1890.,1905.,1920.,1945.,1970.,
$          1985.,2010.,
$          2040.,2070.,2080.,2090.,2095.,2080.,2063.,2060.,2050./
DATA PPN,PPP/6*1HN,6*1HP/
IF(TEST.NE.0.) GOTO 5000
  A=A9
  T0=T9
  MPARIN=MPAR9
  ISMALL = 0
C
  IF(A.GT.AELEM(12).OR.A.LE.0.) GOTO 10000
  IF(A.GE.AELEM(1) ) GOTO 44
  PRINT 3000
  ISMALL = 1
  A = AELEM(1)

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```

ASM = A9
44      IF(T0.LT.ENERGY(1) )                GOTO 20000
        IF(T0.GT.ENERGY(46)) PRINT 4000,ENERGY(46)
        IF(T0.GT.ENERGY(46)) T0 = ENERGY(46)
C
DO 50 I=1,12
IF(A.LE.AELEM(I)) GOTO 100
50      CONTINUE
        GOTO 10000
C
100     IA1=I-1
        IF(I.EQ.1)IA1=1
        IA2=I
C
DO 150 I=1,46
IF(T0.LE.ENERGY(I)) GOTO 200
150     CONTINUE
        GOTO 20000
C
200     IE1=I-1
        IF(I.EQ.1)IE1=1
        IE2=I
        IF(MPARIN.EQ.2)GOTO 201
        CS11=CSN(IE1,IA1)
        CS12=CSN(IE1,IA2)
        CS21=CSN(IE2,IA1)
        CS22=CSN(IE2,IA2)
        GOTO 202
201     CS11=CSP(IE1,IA1)
        CS12=CSP(IE1,IA2)
        CS21=CSP(IE2,IA1)
        CS22=CSP(IE2,IA2)
C
202     IF(IE1.EQ.IE2) CSMIN=CS11
        IF(IE1.EQ.IE2) CSMAX=CS12
        IF(IE1.EQ.IE2) GOTO 400
C
        E1=ENERGY(IE1)
        E2=ENERGY(IE2)
        CS1=CS11
        CS2=CS21
        RR=E2-E1
        AAA=(CS2-CS1)/RR
        BBB=(CS1*E2-E1*CS2)/RR
        CSMIN = AAA * T0 + BBB
C
        CS1=CS12
        CS2=CS22
        RR=E2-E1
        AAA=(CS2-CS1)/RR
        BBB=(CS1*E2-E1*CS2)/RR
        CSMAX = AAA * T0 + BBB
C
400     IF(IA1.EQ.IA2) CSNON=CSMIN
        IF(IA1.EQ.IA2) GOTO 555
        A1=AELEM(IA1)
        A2=AELEM(IA2)
        RR=A2-A1
        AAA=(CSMAX-CSMIN)/RR

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```

                BBB=(CSMIN*A2-A1*CSMAX)/RR
CSNON = AAA * A + BBB
555      IF(ISMALL.EQ.0) RETURN
        CSNON = CSNON * ( (ASM/A)**0.66666666 )
        RETURN

C
C TEST PRINTING
5000     PRINT 5010,(RIDENT(I),I=1,6)
5010     FORMAT(/1X,' E,MEV ',4X,6(8X,A2,7X))
        PRINT 5011,(AELEM(I),I=1,6)
5011     FORMAT(1X, 8X, 4X,6(6X,F6.2,5X))
        PRINT 5014,(PPN(II),PPP(II),II=1,6)
5014     FORMAT(1X, 8X, 4X,6(3X,A1,3X, 3X,A1,3X, 3X))
        PRINT 5012
5012     FORMAT(120('-'))
        DO 8000 II=1,46
8000     PRINT 5020,ENERGY(II),(CSN(II,JJ),CSP(II,JJ),JJ=1,6)
5020     FORMAT(1X,F8.1,4X,6(2F7.1,3H I ))
        PRINT 5015
5015     FORMAT(120('='))
        PRINT 5010,(RIDENT(I),I=7,12)
        PRINT 5011,(AELEM(I),I=7,12)
        PRINT 5014,(PPN(II),PPP(II),II=1,6)
        PRINT 5012
        DO 9000 II=1,46
9000     PRINT 5020,ENERGY(II),(CSN(II,JJ),CSP(II,JJ),JJ=7,12)
        STOP

C
10000    PRINT 1000,A
1000     FORMAT(1X,'SUBROUTINE BARASH: NO INFORMATION ABOUT A =',G12.5)
        STOP
20000    PRINT 2000,T0
        WRITE(1,2000)T0
        WRITE(8,2000)T0
        CSNON=0.
        RETURN
2000     FORMAT(1X,'SUBROUTINE BARASH: NO INFORMATION FOR ENERGY = ',
$ G12.5/ 1X,' CSNON =0. ')
3000     FORMAT(1X,'Attention !'/1X,' For low atomic numbers ',
$ ' SUBR BARASH gets approximated cross-sections'//)
4000     FORMAT(/1X,' Attention !'/1X,'BARASH: Cross-section is taken ',
$ ' at the energy = ',G14.7//)
        END

*****
*                SUBROUTINE BINDEN                *
*****
        SUBROUTINE BINDEN(ZEE,AMASS,NZ,NA,AP,AT,ZP,ZT,QVAL,M3,MP)
* taken from Blann code ALICE
        COMMON/LYM1/BE(11,24,4),SYMB(11,24),PAIR(11,24),SYMBP(11,24)
        DIMENSION EXCES(4),RES(4),ERR(4)
        DATA TAB/4H TAB/
        IZEE=ZEE+.1
        IMASS=AMASS+.1
        IAP=AP+.1
        IAT=AT+.1
        IZP=ZP+.1
        IZT=ZT+.1
        INP=IAP-IZP
        INT=IAT-IZT

```

```

      IRET=0
      N=IMASS-IZEE
      CALL MASS (IZP,INP,EXCES(1),ERR(1),IRET)
      CALL MASS (IZT,INT,EXCES(2),ERR(2),IRET)
      CALL MASS (IZEE,N,EXCES(3),ERR(3),IRET)
      IF(IRET.GT.0) GO TO 10
      IF(QVAL.NE.0.)GO TO 10
      QVAL=-EXCES(3)+EXCES(2)+EXCES(1)
cccc  WRITE(6,4)
      4  FORMAT(//,20X,'*****'//)
cccc  WRITE(6,5)QVAL
cccc  WRITE(6,4)
      5  FORMAT(20X,' QVAL USED (CALCULATED FROM MASS TABLE) = ',F5.1)
      10  IRET=0
          CALL MASS(0,1,EXCES(1),ERR(1),IRET)
          CALL MASS(1,0,EXCES(2),ERR(2),IRET)
          CALL MASS(2,2,EXCES(3),ERR(3),IRET)
          CALL MASS(1,1,EXCES(4),ERR(4),IRET)
          IF(IRET.GT.0) RETURN
cccc  WRITE(6,6)
      6  FORMAT(30X,'BINDING ENERGIES CALCULATED FROM MASS TABLE',
      1  ' WHERE POSSIBLE.')
cccc  IF(MP.EQ.0)WRITE(6,7)
      7  FORMAT(35X,'PAIRING REMOVED FROM MASSES IN TABLE')
cccc  IF (MP.EQ.0.AND.MC.EQ.1) WRITE(6,8)
      8  FORMAT (35X,'SHELL CORRECTION REMOVED FROM MASSES IN TABLE')
          DO 65 IZ=1,NZ
          DO 65 IA=1,NA
          IZZ=IZEE-IZ+1
          INN=IMASS-IZEE-IA+1
          IZZ1=IZZ-1
          INN1=INN-1
          INN2=INN-2
          IZZ2=IZZ-2
          IRET=0
          CALL MASS (IZZ,INN,XMASS,ERR(1),IRET)
          CALL MASS (IZZ,INN1,RES(1),ERR(1),IRET)
          IF(M3.GE.2)CALL MASS(IZZ1,INN,RES(2),ERR(2),IRET)
          IF(M3.GE.3)CALL MASS(IZZ2,INN2,RES(3),ERR(3),IRET)
          IF(M3.EQ.4)CALL MASS(IZZ1,INN1,RES(4),ERR(4),IRET)
          IF(IRET.GT.0) GO TO 65
          IF(MP.NE.0)GO TO 55
          XMASS=XMASS+PAIR(IZ,IA)
          RES(1)=RES(1)+PAIR(IZ,IA+1)
          RES(2)=RES(2)+PAIR(IZ+1,IA)
          RES(3)=RES(3)+PAIR(IZ+2,IA+2)
          RES(4)=RES(4)+PAIR(IZ+1,IA+1)
      55 DO 60 I=1,M3
      60  BE(IZ,IA,I)=-XMASS+EXCES(I)+RES(I)
          SYMB(IZ,IA)=TAB
      65  CONTINUE
          RETURN
      END
*****
*              FUNCTION BKAL(M,E1)              *
*****
      FUNCTION BKAL(M,E1)
      RM=FLOAT(M*(M+1))
      AL=0.036+0.0039*RM

```

```

BL=92.-90./SQRT(RM)
BKAL=FLOAT(2*M+1)/(1.+EXP(AL*(BL-E1)))
RETURN
END

```

```

*****
*                               BLOCK DATA                               *
*****

```

```

BLOCK DATA
COMMON/DATEVA/GP,GD,GT,GHE,GAL,GAMP,GAMD,GAMT,GAMHE,GAMAL,CP,CD,
*CT,CHE,CAL,VP,VD,VT,VHE,VAL,QN,QP,QD,QT,QHE,QAL
COMMON/FIGA1B/T1(16),BA1(16),BB1(16),BB2(9),BB3(8)
COMMON/DATCAM/CAMN(130),CAMP(130),MAXN,MAXP
COMMON/DOSTRO/RKPD(6),RKAD(6),CPD(6),CAD(6),ZD(6)
COMMON/DATREN/RL0N,RL1N,RM0N,RM1N,RN0N,RN1N,RN2N
COMMON/DATREP/POP,P1P,P2P,RL0P,RL1P,RM0P,RM1P,RN0P,RN1P,RN2P
COMMON/SHEL2/DWA(220)
COMMON/DATREA/POA,P1A,P2A,RL0A,RL1A,RM0A,RM1A,RN0A,RN1A,RN2A

```

C

```

DATA GAMP,GAMD,GAMT,GAMHE,GAMAL/2*1., 2*3., 2./
DATA T1/ 0., 40., 80., 120., 160., 200., 240.,
*280., 300., 320., 360., 400., 440., 480., 520., 560./
DATA BA1/1592., 12., 5.2, 3.3, 2.3, 2., 1.9, 1.8, 1.75,
* 1.7, 1.5, 1.4, 1.3, 1.2, 1.1, 1./
DATA BB1/ 0., 7., 8.1, 6.6, 3.9, 11*3.6/
DATA BB2/0., 7., 8.3, 9., 7.7, 6.5, 6.2, 6., 5.8071425/
DATA BB3/8.1299995, 7.8, 7.4, 7., 6.7, 6.4, 6.1, 5.8/

```

C

C

C

```

CAMN/CAMP : corrections for nuclei with neutrons/protons number
equal to array number
DATA CAMN/-8.4, -12.9, -8.0, -11.9, -9.2, -12.5, -10.8, -13.6,
* -11.2, -12.2,
* -12.81, -15.40, -13.07, -15.80, -13.81, -14.98,
* -12.63, -13.76, -11.37, -12.38, -9.23, -9.65, -7.64, -9.17,
* -8.05, -9.72, -8.87, -10.76, -8.64, -8.89, -6.60, -7.13,
* -4.77, -5.33, -3.06, -3.79, -1.72, -2.79, -0.93, -2.19,
* -0.52, -1.90, -0.45, -2.20, -1.22, -3.07, -2.42, -4.37,
* -3.94, -6.08, -4.49, -4.5, -3.14, -2.93, -1.04, -1.36, 0.69,
* 0.21, 2.11, 1.33,
* 3.29, 2.46, 4.30, 3.32, 4.79, 3.62, 4.97, 3.64,
* 4.63, 3.07, 4.06, 2.49, 3.30, 1.46, 2.06, 0.51, 0.74, -1.18,
* -1.26, -3.54, -3.97, -5.26, -4.18, -3.71, -2.10, -1.70, -0.08, -0.18,
* 0.94, 0.27, 1.13, 0.08, 0.91, 0.31, 0.49, -0.78, 0.08, -1.15,
* -0.23, -1.41, -0.42, -1.55, -0.55, -1.66, -0.66, -1.73, -0.75, -1.74,
* -0.78, -1.69, -0.78, -1.60, -0.75, -1.46, -0.67, -1.26, -0.51, -1.04,
* -0.53, -1.84, -2.42, -4.52, -4.76, -6.33, -6.76, -7.81, -5.80, -5.37,
* -3.63, -3.35/
DATA CAMP/ 20.8, 15.8, 21.0, 16.8, 19.8, 16.5, 18.8, 16.5,
* 18.5, 17.2,
* 18.26, 15.05, 16.01, 12.04, 13.27, 11.09,
* 12.17, 10.26, 11.04, 8.41, 9.79, 7.36, 8.15, 5.63, 5.88,
* 3.17, 3.32, 0.82, 1.83, 0.97, 2.33, 1.27, 2.92, 1.61,
* 2.91, 1.35, 2.40, 0.89, 1.74, 0.36, 0.95, -0.65, -0.04,
* -1.73, -0.96, -2.87, -2.05, -4.05, -3.40, -5.72, -3.75, -4.13,
* -2.42, -2.85, -1.01, -1.33, 0.54, -0.02, 1.74, 0.75,
* 2.24, 1.00, 1.98, 0.79, 1.54, 0.39, 1.08, 0.00, 0.78, -0.35, 0.58,
* -0.55, 0.59, -0.61, 0.59, -0.35, 0.32, -0.96, -0.52, -2.08, -2.46, -3.64,
* -1.55, -0.96, 0.97, 0.88, 2.37, 1.75, 2.72, 1.90, 2.55, 1.46, 1.93,
* 0.86, 1.17, 0.08, -0.39, -0.76, -0.39, -1.51, -1.17, -2.36, -1.95, -3.06,
* -2.62, -3.55, -2.95, -3.75, -3.07, -3.79, -3.06, -3.77, -3.05, -3.78, -3.12,

```

```

*-3.90,-3.35,-4.24,-3.86,-4.92,-5.06,-6.77,-7.41, 9.18,-10.16,
*-11.12,-9.76,-9.23,-7.96,-7.65/
C      1000. is simply "big" number
      DATA ZD/10., 20., 30., 50., 70., 1000./
      DATA RKPD/ 0.42, 0.58, 0.68, 0.77, 0.8, 0.8/
      DATA CPD/ 0.5, 0.28, 0.2, 0.15, 0.1, 0.1/
      DATA RKAD/ 0.68, 0.82, 0.91, 0.97, 0.98, 0.98/
      DATA CAD/ 3*0.1, 0.08, 0.06, 0.06/
C CHATTERJEE COMPILATION
C      NEUTRONS WILMORE
      DATA RL0N,RL1N,RM0N,RM1N,RN0N,RN1N,RN2N/
*31.05,-25.91,342.4,21.89,0.223,0.673,617.4/
C      PROTONS BECCHETTI
      DATA POP,P1P,P2P,RL0P,RL1P,RM0P,RM1P,RN0P,RN1P,RN2P/
*15.72,9.65,-449.0,0.00437,-16.58,244.7,0.503,273.1,-182.4,-1.872/
C      ALPHA-PARTICLES HUIZENGA
      DATA P0A,P1A,P2A,RL0A,RL1A,RM0A,RM1A,RN0A,RN1A,RN2A/
*10.95,-85.2,1146.,0.0643,-13.96,781.2,0.29,-304.7,-470.,-8.58/
      DATA DWA/22*0.0,
* -0.6, -0.7, -0.8, -0.9, -1.8, -2.0, -2.9, -2.4, -2.3, -1.6, -1.3,
* -1.0, -0.8, -0.4, -0.3, 0.1, 0.5, 0.8, 1.4, 2.0, 1.8, 1.5,
* 1.4, 1.3, 0.8, 0.3, -0.0, -0.8, -1.5, -1.6, -1.7, -1.8, -1.8,
* -1.8, -2.4, -2.0, -1.7, -1.6, -1.6, -1.3, -0.7, -0.6, -0.2, 0.0,
* 0.9, 0.8, 1.2, 1.5, 1.8, 2.0, 2.4, 1.8, 2.4, 2.0, 1.7,
* 2.4, 2.4, 1.8, 1.2, 0.4, -0.1, -0.3, 0.5, -0.9, -2.0, -1.7,
* -2.4, -2.4, -2.0, -1.6, -1.1, -0.7, -0.2, -0.2, -0.2, -0.1, 0.7,
* 1.2, 1.8, 0.1, 0.8, 1.1, 1.5, 1.6, 0.5, 0.7, 1.1, 1.2,
* 1.2, -0.0, 0.3, 0.2, 0.4, 0.3, 0.3, -0.7, -0.0, -1.1, -0.6,
* -0.7, -1.0, -1.6, -2.0, -1.7, -1.5, -2.2, -2.3, -3.1, -2.6, -3.2,
* -2.6, -3.3, -4.2, -2.4, -4.1, -3.8, -4.1, -3.7, -3.2, -2.9, -2.2,
* -2.4, -1.8, -0.6, -0.4, 0.1, 0.2, 0.3, -0.1, -0.5, -0.7, -1.1,
* -1.4, -1.7, -2.0, -2.1, -2.1, -2.3, -2.5, -2.2, -2.5, -2.7, -3.0,
* -3.2, -3.4, -3.1, -3.2, -3.4, -3.5, -3.3, -3.7, -3.1, -3.4, -3.5,
* -3.4, -3.2, -3.5, -3.2, -3.5, -3.7, -3.4, -3.4, -3.4, -3.2, -3.0,
* -2.9, -2.5, -2.8, -3.0, -3.3, -3.7, -4.3, -4.8, -5.4, -6.0, -6.8,
* -7.1, -8.1, -8.7, -9.2, -9.6,-10.5,-11.3,-12.2,-12.0,-12.7,-12.1,
*-11.2,-10.6,-10.0, -9.4, -8.8, -8.2, -7.6, -7.0, -6.4, -5.8, -5.2/
C RETURN
      END
*****
*                                BLOCK DATA C                                *
*****
      BLOCK DATA C
C Written by Barashenkov, Polanski
C      NUCLEUS-NUCLEUS CROSS-SECTION PARAMETERS
      COMMON/CX/CX(38)
      DATA CX/2.07,560.,0.8,0.426,
*          100.,-2.05,1.9,
*          200.,0.07,0.87,
*          20.,-1.55,2.1,
*          700.,-1.01,1.08,
*          400.,-0.59,0.94,
*          2.45,225.,-2.25,2.,
*          100.,-4.61,3.18,
*          185.,-3.,2.4,
*          185.,-3.,2.4,
*          185.,-4.77,3.18,
*          185.,-4.77,3.18/
      END

```



```

*****
*                               FUNCTION CAMERO                               *
*****
      FUNCTION CAMERO(RN,Z)
* Defect mass calculation. Barashenkov, Toneev "Interaction of particles
* and nuclei", 1972, Atomizdat (error on p.419 corrected)
      A=RN+Z
      A13=A*0.333333333
      A23=A13*A13
      A43=A23*A23
      Z43=Z**(4./3.)
      AZ=((A-2.*Z)/A)**2
      RMOB=A*(8.367+31.4506*AZ)-(0.783*Z+17.0354*A)
      RMPow=A23*(25.8357-44.2355*AZ)*((1.-0.62025/A23)**2)
      RMK=0.779*(Z*(Z-1.)/A13)*(1.-1.5849/A23+1.2273/A+1.5772/A43)
      RMEX=-0.4328*(Z43/A13)*(1.-0.57811/A13-0.14518/A23+0.49597/A)
      CAMERO=RMOB+RMPow+RMK+RMEX
      RETURN
      END
*****
*                               SUBROUTINE CFUN                               *
*****
      SUBROUTINE CFUN
      COMMON/CFUMAS/CF /TR2CFU/REC /EDEFF/Ed
      COMMON/QBOCFU/NSUMN,NSUMP /AN/AN /MPARIN/MPARIN
      COMMON/INIQBO/Z,CKA,CKB,RPA,RPB,RALA,RALB
      AP=1.
      IF(MPARIN.eq.3) AP=4.
      Z2=Z-FLOAT(NSUMP)+1.+(MPARIN-1)
      A2=AN-FLOAT(NSUMN+NSUMP)+2.+AP
      Z1=Z
      A1=AN
      CALL NRT_COEFF(Z1,Z2,A1,A2,ANRT,BNRT,GNRT)
      EDkeV=Ed
* NRT
      TT=REC*1000.
      If(TT.lt.EDkeV) then
          CF=0.0
          Return
          Endif
      If(TT.lt.2.*EDkeV) TT=2.*EDkeV
      CF=(0.8/(2.*EDkeV))*TT/
      + (1.+ANRT*TT+BNRT*(TT**0.75)+GNRT*(TT**0.1666666666))
      RETURN
      END
*****
*                               SUBROUTINE CHECK1                               *
*****
      SUBROUTINE CHECK1(G,T1,W1,IGEN,M1)
* limitation on orbital momenta according to Bunakov
      COMMON/PARTIC/WP,PX,PY,PZ,P,T,E,X,Y,Z,R,JIN,M
      COMMON/ACTSCI/PIN1,PIN2,PIN3,WPX,RK3,RK4,GAMMA,SK2,VC2,VCX,
*VCY,VCZ,MPX
      COMMON/SCIMEM/WPM,PXM,PYM,PZM,PM,TM,EM,XM,YM,ZM,RM,JINM,MM
      COMMON/IMOM/IMOM
      IF(IMOM.EQ.0)RETURN
C
      IF(G)1,1,2
      1 RK=RK4-(GAMMA-1.)*SK2/VC2

```

```

      GOTO 3
      2 RK=RK3+(GAMMA-1.)*SK2/VC2
      3 CONTINUE
      4 PX5=G*PIN1+RK*VCX
        PY5=G*PIN2+RK*VCY
        PZ5=G*PIN3+RK*VCZ
        P5=SQRT(PX5*PX5+PY5*PY5+PZ5*PZ5)
        T5=T1
        RORM=ORBIT(PX5,PY5,PZ5,X,Y,Z)
        CALL QUES(RORM,T5,W1,JIN,M1,IGEN)
        RETURN
C
      END
*****
*                SUBROUTINE CHESEP                *
*****
      SUBROUTINE CHESEP
      COMMON/INTTR1/PWX,PWY,PWZ,TW,NPREN,NPREP,NPREA
      COMMON/EVAMAS/NEVAN,NEVAP,NEVAD,NEVAT,NEVAHE,NEVAAL
      COMMON/INFSEP/KSEP(100,4),INFSEP,JSEPM
        DO 100 J=1,JSEPM
          IF(KSEP(J,1).NE.
+ (NPREN+NEVAN+NEVAD+2*NEVAT+NEVAHE+2*(NEVAAL+NPREA))) GOTO 100
          IF(KSEP(J,2).NE.
+ (NPREP+NEVAP+NEVAD+NEVAT+2*NEVAHE+2*(NEVAAL+NPREA))) GOTO 100
          KSEP(J,4)=KSEP(J,4)+1
100    CONTINUE
      RETURN
      END
*****
*                SUBROUTINE CHOPAR                *
*****
      SUBROUTINE CHOPAR(JZ,SXX)
      COMMON/DAINT/PF(33,4),RO1(33),RZON(33),FIG
      COMMON/PARTIC/WP,PX,PY,PZ,P,T,E,X,Y,Z,R,JIN,M
      COMMON/PARTNR/PPX,PPY,PPZ,PP,MX
      COMMON/TYPACT/L,L7 /QPARX/QPROT,QNEUT,QPROT2,QNEUT2
      COMMON/BOND1/QBON(200,200,6) /TFERMI/TF(34,4)
      COMMON/RNUCL/RNUCL /XPARAM/XPARAM,FIALPH
      COMMON/FICAP/FICAP,MZONA
      COMMON/URAND1/IYG
C
C Types of inetractions: L = 1  N-P  or  P-N
C                          L = 2  N-N  or  P-P
C                          L = 3  Elastic scattering NUCELON-ALPHA
C                          L = 4  Elastic scattering ALPHA-NUCLEON
C                          L = 5  Decay of ALPHA-PARTICLE in N-A interaction
C                          L = 6  NUCLEON-T  or  NUCLEON-HE-3
C                          L = 7  Decay of ALPHA-PARTICLE in A-N interaction
C
      MX = 0
      L = 0
      L7 = 0
          QNEUTX=QNEUT
          QPROTX=QPROT
      IF(JZ.GE.MZONA) QNEUTX=QNEUT2
      IF(JZ.GE.MZONA) QPROTX=QPROT2
C
      IF(M.EQ.3) GOTO 300

```

```

C
  CALL CSPPPN(T,SPP,SPN)
  CALL CSPANA(T,SPA,1)
C "+QBON" because FLM coefficients are shifted on Q
  TT = T - QBON(1,1,6) - TF(JZ,M)          + QBON(1,1,6)
  IF(TT.LT.0.0) TT = 0.0
  CSCAPT = 0.1 *
  # (-1.011E-06*(TT**3) + 0.0001748*TT*TT - 0.01128*TT+0.275742)
  CSCAPT = CSCAPT/( RNUCL * RO1(JZ) )
  IF(CSCAPT.LT.0.0) CSCAPT =0.0
  CSCAPT = CSCAPT*FICAP
C
  GOTO(4,5),M
C NEUTRON
  4 QPAR1=QNEUTX
  QPAR2=QPROTX
  GOTO 6
C PROTON
  5 QPAR1=QPROTX
  QPAR2=QNEUTX
  6 SPP=SPP*QPAR1
  SPN=SPN*QPAR2
C + CSCAPT due to introduction of D,HE3 in calculstions
  STOT=SPN+SPP
  IF(JZ.GE.MZONA) STOT=SPN+SPP+SPA+CSCAPT
  SXX = STOT
  YY=STOT * RANDOM(0)
  IF(YY-SPP)10,10,20
C INTERACTION WITH THE SAME TYPE
  10 MX=M
  L=2
  RETURN
  20 IF(YY-(SPN+SPP))100,100,200
  100 L=1
  IF(M-1)30,30,40
C INTERACTION NEUTRON-----PROTON
  30 MX=M+1
  RETURN
C INTERACTION PROTON-----NEUTRON
  40 MX=M-1
  RETURN
  200 IF(YY-(SPN+SPP+SPA))110,110,210
C INTERACTION NUCLEON-----ALPHA
  110 MX = 3
C DEFINE TYPE OF INTERACTION (ELASTIC-NONELASTIC)
  CALL CSPANA(T,SEL,2)
  If(SPA.lt.SEL) SPA = SEL
  YY=SPA * RANDOM(0)
  IF(YY-SEL)103,103,105
C ELASTIC INTERACTION N-A
  103 L=3
  RETURN
C DECAY OF ALPHA
C NO DECAY DUE TO PAULI
  105 L=3
  RETURN
C INTERACTION NUCLEON-----T,HE3
  210 MX = 4
  L = 6

```

```

        RETURN
C
C PROJECTILE IS ALPHA-PARTICLE
300 T4 = T/4.
        FI = FIALPH
        FIALPH = 1.
        CALL CSPANA(T4,STOT,1)
        CALL CSPANA(T4,SEL,2)
                If(STOT.lt.SEL) STOT = SEL
        FIALPH = FI
        SXX = STOT
        YY=STOT * RANDOM(0)
        IF(YY-SEL)1004,1004,1005
C ELASTIC INTERACTION A-N
1004 L=4
        GOTO 1007
C DECAY OF ALPHA-PARTICLE
1005 L=7
        L7 = 1
C
C DEFINE PARTNER
1007 YY = (QPROTX+QNEUTX) * RANDOM(0)
        IF(YY-QPROTX)1000,1000,2000
1000 MX=2
C INTERACTION ALPHA-----PROTON
        RETURN
2000 MX=1
C INTERACTION ALPHA-----NEUTRON
        RETURN
        END
*****
*                SUBROUTINE COULCH                *
*****
        SUBROUTINE COULCH(VP,VA,IPAR,AEFF,ZEFF,
+ P11P,RL11P,RM11P,RN11P,ECOP,P11A,RL11A,RM11A,RN11A,ECOA)
C Calculate Coulomb potential for protons and neutrons for inverse
C reaction cross-sections according to Chatterjee (see Block data also)
        IPAR=0
        ECO2=ECOP*ECOP
        B=-2.*P11P*ECOP+RL11P-RN11P/ECO2
        C=P11P*ECO2+RM11P+2.*RN11P/ECOP
C Discriminant of square equation
        D=B*B-4.*P11P*C
        IF(D.LT.0.) GOTO 80
        SQD=SQRT(D)
        ES1=0.5*(-B+SQD)/P11P
        ES2=0.5*(-B-SQD)/P11P
        IF(P11P)10,20,30
10        VP=AMIN1(ES1,ES2)
        GOTO 40
20        WRITE(8,21)P11P
21        FORMAT(1X,'ERROR: SUBROUTINE COULCH P11P=',E12.5)
        STOP
30        VP=AMAX1(ES1,ES2)
C the same for alpha-particles
40        ECO2=ECO*A*ECO
        B=-2.*P11A*ECO+RL11A-RN11A/ECO2
        C=P11A*ECO2+RM11A+2.*RN11A/ECO
C Discriminant of square equation

```

```

        D=B*B-4.*P11A*C
        IF(D.LT.0.) GOTO 80
        SQD=SQRT(D)
        ES1=0.5*(-B+SQD)/P11A
        ES2=0.5*(-B-SQD)/P11A
        IF(P11A)50,60,70
50      VA=AMIN1(ES1,ES2)
        GOTO 75
60      WRITE(8,61)P11A
61      FORMAT(1X,'ERROR:  SUBROUTINE COULCH  P11A=',E12.5)
        STOP
70      VA=AMAX1(ES1,ES2)
75      RETURN
80      WRITE(8,1080)ZEFF,AEFF
1080    FORMAT(1X,'FOR ZEFF=',F6.1,' AEFF=',F6.1,' BLANN SHARP CUT',
+ 'OFF CR SECT IS TAKEN')
        IPAR=1
        RETURN
        END
*****
*              SUBROUTINE CROZON                      *
*****
        SUBROUTINE CROZON(J1,J2,WM,P1,T,M)
        COMMON/TFERMI/TF(34,4)
        T=T+TF(J2,M)-TF(J1,M)
        P1=SQRT(T*(T+2.*WM))
        RETURN
        END
*****
*              FUNCTION CSCHAT                        *
*****
        FUNCTION CSCHAT(T0,MPARIN)
C Inverse cross-sections according to Chatterjee A., Murthy K.H.N.,
C Gupta S.K. Optical reaction cross sections for light projectiles
C Report IAEA,INDC(IND)- 27/GJ, 1980.
        COMMON/INIQBO/Z,CKA,CKB,RPA,RPB,RALA,RALB
        COMMON/AN/AN
        COMMON/DATREN/RL0N,RL1N,RM0N,RM1N,RN0N,RN1N,RN2N
        COMMON/DATREP/POP,P1P,P2P,RL0P,RL1P,RM0P,RM1P,RN0P,RN1P,RN2P
        GOTO(1,2,3),MPARIN
C NEUTRONS
1      AN13=AN**0.333333333
        AN23=AN13*AN13
        RL11N=RL0N/AN13+RL1N
        RM11N=RM0N*AN13+RM1N*AN23
        RN11N=RN0N*AN23*AN23+RN1N*AN23+RN2N
        CSCHAT=0.001*(RL11N*T0+RM11N+RN11N/T0)
        RETURN
C PROTONS
2      AP=AN
        ECOP=1.44*Z/(1.5*(AP**0.333333333))
        EC2=ECOP*ECOP
        AM=AP**RM1P
        P11P=POP+P1P/ECOP+P2P/EC2
        RL11P=RL0P*AP+RL1P
        RM11P=RM0P*AM
        RN11P=AM*(RN0P+RN1P*ECOP+RN2P*EC2)
C      EKSI=AMAX1(T0,ECOP)  CE%σ-AC T0 BCEf,,A > ECOP
        EKSI=T0

```

```

      CS=P11P*((T0-EKSI)**2)+RL11P*T0+RM11P+RN11P*(2.-T0/EKSI)/EKSI
      CSCHAT=0.001*CS
      RETURN
C NO CALCULATIONS FOR ALPHA INCIDENT
3      CSCHAT=0.0
      RETURN
      END
*****
*              SUBROUTINE CSPANA              *
*****
      SUBROUTINE CSPANA(T,SPA,ITYPE)
* Nucleon-alpha interaction cross-sections (fm**2)
* Data are correct only for T < 1 GeV
C ITYPE=1 total, =2 elastic
      COMMON/XPARAM/XPARAM,FI
      GOTO(1,2),ITYPE
C Total
1      IF(T-1.125)30,30,10
      10 IF(T-20.) 40,40,20
      20 IF(T-190.)50,50,60
C
      30 SPA=6754.8*(T**2) -1608.5*T + 778.94
      SPA=0.1*FI*SPA
      RETURN
C
      40 SPA=7467.2/(T**1.6089) -51.109*T + 1773.7
      SPA=0.1*FI*SPA
      RETURN
C
      50 SPA=5230.0/(T**0.43473) + 1.2270*T -658.81
      SPA=0.1*FI*SPA
      RETURN
C
      60 SPA= 3425.3/T + 0.073484* T + 74.410
      SPA=0.1*FI*SPA
      RETURN
C
C Elastic
2      IF(T-1.125)300,300,100
      100 IF(T-20.) 400,400,200
      200 IF(T-190.)500,500,600
C
      300 SPA=6754.8*(T**2) -1608.5*T + 778.94
      SPA=0.1*FI*SPA
      RETURN
C
      400 SPA=7466.4/(T**1.6338) -53.939*T + 1815.2
      SPA=0.1*FI*SPA
      RETURN
C
      500 SPA=10182.0/(T**0.76746) + 0.68190*T -282.56
      SPA=0.1*FI*SPA
      RETURN
C
      600 SPA= 4833.8/T + 0.036414* T -2.9546
      SPA=0.1*FI*SPA
      RETURN
      END
*****

```

```

*                               SUBROUTINE CSPPPN                               *
*****
      SUBROUTINE CSPPPN(T,SPP,SPN)
* Nucleon-nucleon interaction cross-sections (fm**2)
      IF(T-40.)30,30,10
      10 IF(T-310.)40,40,20
      20 IF(T-400.)50,50,60
C
      30 SPN=-505.74/T**2+906.92/T+0.69466
      SPP=-117.42/T**2+308.85/T+0.53107
      RETURN
C
      40 SPN=23938./T**2+180.2/T+2.7147
      SPP=9307.4/T**2-1.1148/T+2.2429
      RETURN
C
      50 SPN=23938./T**2+180.2/T+2.7147
      SPP=88.737/T+.005337*T+.35475
      RETURN
C
      60 SPN=3.45
      SPP=88.737/T+.005337*T+.35475
      RETURN
      END
*****
*                               SUBROUTINE DEFINE_ED                           *
*****
      SUBROUTINE DEFINE_ED
C Effective threshold damage energy Ed (eV)
C Data are from NJOY, except global value (NJOY: 25 eV)
      COMMON/INIQBO/Z,CKA,CKB,RPA,RPB,RALA,RALB /EDEFF/Ed
      Ed=40.
      IZ=ifix(Z+0.0001)
      If (IZ.eq. 4) Ed=31.
      If (IZ.eq. 6) Ed=31.
      If (IZ.eq.12) Ed=25.
      If (IZ.eq.13) Ed=27.
      If (IZ.eq.14) Ed=25.
      If (IZ.eq.20) Ed=40.
      If (IZ.ge.22.and.IZ.le.29) Ed=40.
      If (IZ.eq.40) Ed=40.
      If (IZ.eq.41) Ed=40.
      If (IZ.eq.42) Ed=60.
      If (IZ.eq.47) Ed=60.
      If (IZ.eq.73) Ed=90.
      If (IZ.eq.74) Ed=90.
      If (IZ.eq.79) Ed=30.
      If (IZ.eq.82) Ed=25.
C --> keV
      Ed=Ed/1000.
      Return
      End
*****
*                               SUBROUTINE DENS                               *
*****
      SUBROUTINE DENS
* Level density calculation (idea of M.Blann)
      DOUBLE PRECISION POW,SQ11,EE,PT,UCLA
      COMMON/LAB10/POW(6,10000) /LAB3/SIG(6,2000)

```

```

COMMON/LAB4/UCLA(6,2000) /INCR/ED
COMMON/DATINI/RA,T0,W0
COMMON/INIQBO/Z,CKA,CKB,RPA,RPB,RALA,RALB
COMMON/AN/AN /BOND1/QBON(200,200,6)
COMMON/MPARIN/MMM /JMAX1/TENED,JMAX
COMMON/XPARAM/XPARAM,FIALPH
DIMENSION RD(6)
  IF(MMM.le.2) MPARIN=MMM
  IF(MMM.eq.3) MPARIN=6
ED=0.5
C
C          1-N, 2-P, 3-D, 4-T, 5-HE3, 6-A
C
DO 6 I=1,2000
DO 6 K=1,6
6  UCLA(K,I)=0.
    ZEFF=Z
    AEFF=AN
    XMAX= T0+QBON(1,1,MPARIN)
    If(QBON(1,1,6).lt.0.0) XMAX= T0+QBON(1,1,MPARIN)-QBON(1,1,6)
    IMAX=INT(XMAX/ED+1.)
    IF(IMAX.GT.2000)Print 30000
    IF(IMAX.GT.2000)IMAX=2000
    PLD=1./XPARAM
    M3 = 6
C Inverse reaction cross-sections
  CALL SIGICH(ZEFF,AEFF)
  AMASS=AEFF
C This value corresponds to 150 MeV energy for total equilibrium spectra
  QJMAX=FLOAT(150)/ED
  JMAX=INT(QJMAX)
  IF(JMAX.GT.2000)JMAX=2000
  TENED=10.*ED
  RR=AMASS/PLD
  SOR=SQRT(RR*100.)
C
C Level density parameters for particles channels POW(I)
  RD(1)=(AMASS-1.)/PLD
  RD(2)=(AMASS-1.)/PLD
  RD(3)=(AMASS-2.)/PLD
  RD(4)=(AMASS-3.)/PLD
  RD(5)=(AMASS-3.)/PLD
  RD(6)=(AMASS-4.)/PLD
C
DO 7050 L=1,M3
DO 7050 IB=1,10000
  BJ=DFLOAT(IB)/10.-.05
  SQ=2.*SQRT(RD(L)*BJ)-SOR
  SQ11=SQ
7050 POW(L,IB)=(1./(1.+BJ**1.25))*DEXP(SQ11)
C Energy to join Fermi gas and constant temperature
  EX=2.
  TEN=10.*EX+0.05
  IT=INT(TEN)
  IF=IT-1
DO 7047 L=1,M3
  TEMP=SQRT(EX/RD(L))
  D=EXP((EX)/TEMP)
  CQ1=POW(L,IT)/D

```



```

DO 7048 IB=1,IF
EE=0.10*DFLOAT(IB)-0.05
POW(L,IB)=CQ1*DEXP((EE)/TEMP)
7048 CONTINUE
7047 CONTINUE
      Print *,'Level density calculated... '
DO 4000 KJ=1,M3
PRINT *,KJ
DO 1000 I=1,IMAX
EMAX=FLOAT(I-1)*ED
M=INT(EMAX/ED+1.0001)
IF(M-JMAX)415,415,410
410 M=JMAX
415 IF(M-1)430,420,420
430 Print *,'M < 1'
      Goto 1000
420 PT=0.0
      BI=10.*EMAX+0.05
      IB=INT(BI)
      If(IB.gt.10000) IB = 10000
      IF(IB.LE.0) GO TO 1000
DO 435 L=1,M
IF(IB.LT.1)GO TO 435
PT=PT+POW(KJ,IB)*SIG(KJ,L)
BI=BI-TENED
IB=BI
435 CONTINUE
      UCLA(KJ,I) = PT
1000 Continue
4000 Continue
      Return
30000 Format(//1x,60('Ä')/1x,5x,'ATTENTION! IMAX is REDEFINED'
# /1x,60('Ä'))
      End
*****
*              SUBROUTINE DISTPA              *
*****
      SUBROUTINE DISTPA(JZ)
      COMMON/DAINT/PF(33,4),RO1(33),RZON(33),FIG
      COMMON/PARTIC/WP,PX,PY,PZ,P,T,E,X,Y,Z,R,JIN,M
      COMMON/PARTNR/PPX,PPY,PPZ,PP,MX
      COMMON/DATCHO/RMP
      COMMON/TYPACT/L,L7
      COMMON/URAND1/IYG
      COMMON/k1996/k1996
      COMMON/XPARAM/XPARAM,FIALPH
C
C Types of interactions:  L = 1  N-P or P-N
C                        L = 2  N-N or P-P
C                        L = 3  Elastic NUCLEON-ALPHA
C                        L = 4  Elastic ALPHA-NUCLEON
C                        L = 5  Decay of ALPHA in N-A interaction
C                        L = 6  NUCLEON-T OR NUCLEON-HE-3
C                        L = 7  Decay of ALPHA in A-N interaction
C
C Temporarily: no averaging, L=5 is considered by SEL:
C For L=6 cross-sections are taken the same for all T or HE-3
      GOTO(1,2,3,4,5,106,7),L
1      CALL CSPPN(T,SPP,SY)

```

```

      GOTO 8
2     CALL CSPPPN(T,SYY,SPN)
      GOTO 8
3     CALL CSPANA(T,SYY,2)
      GOTO 8
4     T4 = T/4.
      FI = FIALPH
      FIALPH = 1.
      CALL CSPANA(T4,SYY,2)
      FIALPH = FI
      GOTO 8
5     CALL CSPANA(T,STOT,1)
      CALL CSPANA(T,SEL,2)
           SYY = STOT-SEL
           If(SYY.lt.0.0) SYY = 0.0
      GOTO 8
7     T4 = T/4.
      FI = FIALPH
      FIALPH = 1.
      CALL CSPANA(T4,STOT,1)
      CALL CSPANA(T4,SEL,2)
           SYY = STOT-SEL
           If(SYY.lt.0.0) SYY = 0.0
      FIALPH = FI
C
8     UU=RANDOM(0)
      IF(UU.ge.1.0) UU=0.99999
      RKSI = SYY * INT( 10.*UU + 1.0 )
106    PFM=PF(JZ,MX)
C
           VX = PX/WP
           VY = PY/WP
           VZ = PZ/WP
           V  = P /WP
      WPP=WM(MX)
      CALL WERO(PFM,PP,MX)
C
      KSS =0
9     SUM = 0.
      DO 900 II=1,15
C
      QCOS=1.-2.*RANDOM(0)
      FI=6.283185*RANDOM(0)
      QSIN=SQRT(ABS(1.-QCOS**2))
      CC=PP*QSIN
      PPX=CC*COS(FI)
      PPY=CC*SIN(FI)
      PPZ=PP*QCOS
      EP=SQRT(PP*PP+WPP*WPP)
      TRE=((E*SQRT(PP*PP+WPP*WPP)-PX*PPX-PY*PPY-PZ*PPZ)/WPP)-WP
           VXP = PPX/WPP
           VYP = PPY/WPP
           VZP = PPZ/WPP
           VV = SQRT((VXP-VX)**2 +(VYP-VY)**2 +(VZP-VZ)**2 )/V
C
C DEFINE CROSS-SECTION
C
      GOTO(10,20,30,40,50,60,70),L
10    CALL CSPPPN(TRE,SPP,SZZ)

```

```

      GOTO 800
20  CALL CSPPPN(TRE,SZZ,SPN)
      GOTO 800
30  CALL CSPANA(TRE,SZZ,2)
      GOTO 800
40  T4 = TRE/4.
      FI = FIALPH
      FIALPH = 1.
      CALL CSPANA(T4,SZZ,2)
      FIALPH = FI
      GOTO 800
50  CALL CSPANA(TRE,STOT,1)
      CALL CSPANA(TRE,SEL,2)
           SZZ = STOT-SEL
           If(SZZ.lt.0.0) SZZ = 0.0
      GOTO 800
60  RETURN
70  T4 = TRE/4.
      FI = FIALPH
      FIALPH = 1.
      CALL CSPANA(T4,STOT,1)
      CALL CSPANA(T4,SEL,2)
           SZZ = STOT-SEL
           If(SZZ.lt.0.0) SZZ = 0.0
      FIALPH = FI
C
800  SUM = SUM + SZZ * VV
C
           1 2 3 4 5 6 7
           If(SUM.ge.RKSI) GOTO(99,99,99,99,905,99,907),L
900  Continue
C
950  k1996 = k1996+1
           GOTO(99,99,99,99,905,99,907),L
99  RETURN
C-----L=5-----
C REDEFINITION OF PARTNER TYPE FOR ALPHA-DECAY (L=5)
905  PP=PP/4.
      PPX=PPX/4.
      PPY=PPY/4.
      PPZ=PPZ/4.
      TP = (PP**2)/(2.*WM(1))
      CALL CSPPPN(TP,SPP,SPN)
      YY=(SPN+SPP) * RANDOM(0)
      IF(YY-SPP)11,11,22
C INTERACTION WITH THE SAME TYPE
11  MX=M
      L=2
      RETURN
22  L=1
      IF(M-1)33,33,44
C INTERACTION NEUTRON----PROTON
33  MX=M+1
      RETURN
C INTERACTION PROTON----NEUTRON
44  MX=M-1
      RETURN
C-----L=7-----
C REDEFINITION OF TYPE OF INCIDENT PARTICLE FOR ALPHA-DECAY (L=7)
907  CALL MEMDEC(1)

```

```

        WP = WP/4.
        PX = PX/4.
        PY = PY/4.
        PZ = PZ/4.
        P  = P /4.
        T  = T /4.
        E  = E /4.
        CALL CSPPPN(T,SPP,SPN)
        YY=(SPN+SPP) * RANDOM(0)
        IF(YY-SPP)111,111,222
C INTERACTION WITH THE SAME TYPE
111  M=MX
      L=2
      RETURN
222  L=1
      IF(MX-1)333,333,444
C INTERACTION NEUTRON----PROTON
333  M=MX+1
      RETURN
C INTERACTION PROTON----NEUTRON
444  M=MX-1
      RETURN
      END
*****
* SUBROUTINE EVAPAR *
*****
      SUBROUTINE EVAPAR
      COMMON/DATEVA/GP,GD,GT,GHE,GAL,GAMP,GAMD,GAMT,GAMHE,GAMAL,CP,CD,
*CT,CHE,CAL,VP,VD,VT,VHE,VAL,QN,QP,QD,QT,QHE,QAL
      COMMON/EVATR2/WEIG,VX,VY,VZ
      COMMON/EVAMAS/NEVAN,NEVAP,NEVAD,NEVAT,NEVAHE,NEVAAL
      COMMON/TR1EVA/EXCIT,WMAI /URAND1/IYG
      COMMON/INTTR1/PWX,PWY,PWZ,TW,NPREN,NPREP,NPREA
      COMMON/SUM90/ER90,KER90
      COMMON/INFDIS/INFDIS,INFOUP(3)
      DIMENSION WIDTH(6),TAUX(6)
      WEIG=WMAI
              ER90=ER90+EXCIT
              KER90=KER90+1
1 CALL QBOND(EXCIT,WIDTH,TAUX,KEY)
      IF(KEY.EQ.0) RETURN
      CC=RANDOM(0)
      DO 2 KX = 1,6
      IF(CC.LE.WIDTH(KX)) GOTO 3
2 CONTINUE
      PRINT 1000,WIDTH,CC
      STOP
3 GOTO(11,22,33,44,55,66),KX
C N
11 NEVAN=NEVAN+1
      CALL FLIG(1,TAUX(1),E)
      WPAR=WM(1)
      WEIG = WEIG - WPAR
      EXCIT = TAUX(1) - E
      IF(INFOUP(1).EQ.1)CALL MEMEQU(E,1)
      GOTO 200
C P
22 NEVAP=NEVAP+1
      CALL FLIG(2,TAUX(2),E)

```

```

        WPAR=WM(2)
        WEIG = WEIG - WPAR
        EXCIT = TAUX(2) - E
        IF(INFOUP(2).EQ.1)CALL MEMEQU(E,2)
        GOTO 200
C D
    33 NEVAD=NEVAD+1
        CALL FLIG(3,TAUX(3),E)
        WPAR=WM(5)
        WEIG = WEIG - WPAR
        EXCIT = TAUX(3) - E
        GOTO 200
C T
    44 NEVAT=NEVAT+1
        CALL FLIG(4,TAUX(4),E)
        WPAR=WM(4)
        WEIG = WEIG - WPAR
        EXCIT = TAUX(4) - E
        GOTO 200
C HE3
    55 NEVAHE=NEVAHE+1
        CALL FLIG(5,TAUX(5),E)
        WPAR=WM(4)
        WEIG = WEIG - WPAR
        EXCIT = TAUX(5) - E
        GOTO 200
C A
    66 NEVAAL=NEVAAL+1
        CALL FLIG(6,TAUX(6),E)
        WPAR=WM(3)
        WEIG = WEIG - WPAR
        EXCIT = TAUX(6) - E
        IF(INFOUP(3).EQ.1)CALL MEMEQU(E,3)
    200 V=VELOC(WPAR,WEIG,E)
        CC=RANDOM(0)
        QCOS=1.-2.*CC
        QSIN=SQRT(ABS(1.-QCOS*QCOS))
        CC=RANDOM(0)
        FI=6.2831852*CC
        VX=VX+V*QSIN*COS(FI)
        VY=VY+V*QSIN*SIN(FI)
        VZ=VZ+V*QCOS
        GOTO 1
C
    1000 FORMAT(1X,'CONTROL SUBR EVAPAR: '/1X,6G12.5/1X,G12.5)
        END
*****
*                               FUNCTION FC                               *
*****
        FUNCTION FC(T,B)
C Written by Barashenkov, Polanski
        COMMON /FH/AMP,AMT,AP,AT,B0,R0
C      CMS ENERGY
        TC=T*AMT/(AMP+AMT)
        X=(TC-B)/1.2
        IF(X.GT.5) GO TO 1
        D=1.+EXP(X)
        FC=ALOG(D)/TC
        RETURN

```

```

1 FC=X/TC
  RETURN
  END
*****
*                FUNCTION FHS                *
*****
  FUNCTION FHS(IS,E,C)
C Written by Barashenkov, Polanski
C CALCULATION OF HIGH-ENERGY TOTAL (IS=2) AND
C INELASTIC (IS=1) CROSS-SECTIONS
C E - LAB. KINETIC ENERGY OF PROJECTILE(MEV)
  COMMON/FH/AM P,AMT,AP,AT,B0,R0
C SQUARED PROJECTILE CMS MOMENTUM
  PPC=AMT*AMT*E*(E+2.*AMP)/((AMP+AMT)**2+2.*AMT*E)
C DE BROGLE WAVE LENGTH
  AL=1.41*140./SQRT(PPC)
  EC=SQRT(PPC+AMP*AMP)-AMP
C COULOMB BARRIER
  B=B0/R0/(AP+AT+AL)
  FHS=31.416*1.21*(1.-B/EC)*(AP+AT+1.85*AP*AT/(AP+AT)
  *+AL-C)**2*IS
  RETURN
  END
*****
*                SUBROUTINE FLIG                *
*****
  SUBROUTINE FLIG(KJ,TAUX,E)
  DOUBLE PRECISION UCLA,WTOT,PT,POW
  COMMON/URAND1/IYG /MAIIPR/IPR
  COMMON/LAB10/POW(6,10000)
  COMMON/LAB3/SIG(6,2000)
  COMMON/LAB4/UCLA(6,2000)
  COMMON/INCR/ED
  COMMON/JMAX1/TENED,JMAX
  E=0.
  M=INT(TAUX/ED+1.)
  EMAX=FLOAT(M-1)*ED
  CC=RANDOM(0)
  WTOT = CC*UCLA(KJ,M)
  IF(M-JMAX)415,415,410
410 M=JMAX
415 IF(M-1)430,420,420
430 RETURN
C
420 PT=0.0
  BI=10.*EMAX+0.05
  IB=INT(BI)
  If(IB.gt.10000) IB = 10000
  IF(IB.LE.0) RETURN
C
DO 435 L=1,M
  IF(IB.LT.1)GO TO 435
  PT=PT+POW(KJ,IB)*SIG(KJ,L)
  IF(PT.GE.WTOT) GOTO 500
  BI=BI-TENED
  IB=BI
435 CONTINUE
  PRINT *,'BAD INTEGRAL: ',PT,' < ',WTOT,' CC=',CC
500 E=FLOAT(L)*ED - ED/2.

```

```

RETURN
END
*****
*                               SUBROUTINE GRAPH                               *
*****
SUBROUTINE GRAPH(Y,F,N3,IALOG)
* IALOG.ne.0 : logarithmic scale for function (Y)
COMMON/MAIIPR/IPR1
DIMENSION Y(N3),F(N3),F1(150)
INTEGER A1(40),B1,C1,D1,D2,D3,D4,D5,D6
DATA B1,C1,D1,D2,D5,D6/1H*,1H ,1H!,1H-,1HI,1H./
IF(N3.GT.150)STOP
N1=1
W=F(1)
DO 1 L=1,N3
IF(ABS(W).GT.ABS(F(L)))GOTO 1
W=F(L)
1 CONTINUE
IF(W.NE.0.)GOTO 70
WRITE(IPR1,41)
41 FORMAT(1X,' SUBR GRAPH: MAXIMAL FUNCTION VALUE IS EQUAL TO ZERO')
RETURN
70 IF(IALOG.NE.0)GOTO 199
WRITE(IPR1,60)
60 FORMAT(/3X,'Agrument      Function      ',4X,4('.....!'))
T=40./ABS(W)
DO 300 I=1,N3
300 F1(I)=F(I)
GOTO 7
199 WMIN=1.E+10
DO 200 I=1,N3
IF(F(I).NE.0..AND.F(I).LT.WMIN)WMIN=F(I)
200 CONTINUE
IMAX=-8
210 IF(W.LE.10.**IMAX)GOTO 220
IMAX=IMAX+1
GOTO 210
220 IMIN=IMAX
230 IF(WMIN.GE.10.**IMIN)GOTO 240
IMIN=IMIN-1
GOTO 230
240 R10=10.**IMIN
IF(IMIN.EQ.IMAX)GOTO 250
WW1=FLOAT(IMIN)
WW=FLOAT(IMAX-IMIN)
R20=10.**IMAX
WRITE(IPR1,62)R10,R20
62 FORMAT(1X,5X,'LOGARITHMICAL SCALE FOR FUNCTION'
1/3X,23X,E8.2,32X,E8.2)
GOTO 260
250 WW1=ALOG10(WMIN)
WW=ALOG10(WMAX)-ALOG10(WMIN)
260 DO 270 I=1,N3
FF=F(I)
IF(FF.EQ.0.)FF=R10
270 F1(I)=ALOG10(FF)-WW1
WRITE(IPR1,63)
63 FORMAT(/3X,'Agrument      Function      ',4X,4('.....'))
T=40./WW

```

```

7 CONTINUE
DO 3 I=1,N3
X=F1(I)
N=INT(X*T)
IF(I.EQ.N3)GOTO 105
IF(I.EQ.N1*10)GOTO 107
D4=C1
GOTO 108
105 D4=D6
GOTO 108
107 D4=D2
N1=N1+1
108 N2=1
DO 4 J1=1,40
IF(J1.EQ.20)GOTO 110
IF(J1.EQ.1.OR.J1.EQ.40)GOTO 24
D3=D4
GOTO 25
24 D3=D5
25 CONTINUE
GOTO 111
110 D3=D1
N2=N2+1
111 CONTINUE
IF(J1.EQ.N)GOTO 101
A1(J1)=D3
GOTO 102
101 A1(J1)=B1
102 CONTINUE
4 CONTINUE
WRITE(IPR1,61)Y(I),F(I),A1
61 FORMAT(G12.5,1X,1PE12.5,5X,40A1)
3 CONTINUE
RETURN
END
*****
* SUBROUTINE INIDAT *
*****
SUBROUTINE INIDAT(KZONESC)
COMMON/DATINI/RA,T0,W0 /DAINT/PF(33,4),RO1(33),RZON(33),FIG
COMMON/DATCHO/RMP /TFERMI/TF(34,4)
COMMON/DATEVA/GP,GD,GT,GHE,GAL,GAMP,GAMD,GAMT,GAMHE,GAMAL,CP,CD,
*CT,CHE,CAL,VP,VD,VT,VHE,VAL,QN,QP,QD,QT,QHE,QAL
COMMON/K/K /DATOUT/SGEOM,FOUT
COMMON/DATTR1/QNN,QPP /URAND1/IYG /DATPAU/BONCUT(3)
COMMON/EMEM/EMEM0(21),EMEM(21),RMEM(21,3),RMEM0(21,3),HMEM
COMMON/RNUCL/RNUCL/CSABS/CSABS,FIALP2
COMMON/EOUT/SPE(19,5,3),PI(19),EOUT1(5,3),EOUT2(5,3),MSPE
COMMON/TEMP2/BONNE/NREJ/REFR,NREJ/MM/RMASS
COMMON/QPARX/QPROT,QNEUT,QPROT2,QNEUT2 /BOND1/QBON(200,200,6)
COMMON/INIQBO/Z,CKA,CKB,RPA,RPB,RALA,RALB
COMMON/ALIBLI/ALINPK(6),BLINPK(6),ALINPC(6),BLINPC(6),
*ALINAK(6),BLINAK(6),ALINAC(6),BLINAC(6)
COMMON/DOSTRO/RKPD(6),RKAD(6),CPD(6),CAD(6),ZD(6)
COMMON/QNNN/QNNN /MAIPR/IPR /AN/AN /INF/INFBIG,INFS0
COMMON/EMEM91/EMEMT(21),RMEMT(21),HMEMT
COMMON/SPEFUL/ANGLIM(9,2,3),ANGSUM(21,9,3),ANGCEN(9,3),DCEN,MANG
COMMON/XPARAM/XPARAM,FIALPH /MPARIN/MPARIN
DIMENSION A1(10),A2(33),A(33)

```



```

C
C Number of zones (K)
C Values to approximate Woods-Saxon distribution
C 1.0 corresponds to the center of the nucleus
C 10 zones
  DATA A1/ 0.9, 0.8, 0.5, 0.3, 0.2, 0.1, 0.075, 0.05, 0.025, 0.01/
C 33 zones
  DATA A2/
* 0.98, 0.95, 0.90, 0.85, 0.80, 0.75, 0.70, 0.60, 0.50, 0.40,
* 0.30, 0.20, 0.10, 0.08, 0.06, 0.04, 0.02, 0.01, 0.008, 0.006,
* 0.004, 0.002, 0.001, 8.e-4, 6.e-4, 4.e-4, 2.e-4, 1.e-4, 8.e-5,
* 6.e-5, 4.e-5, 2.e-5, 1.e-5/
                                If(KZONESC.eq.0) KZONESC=1
                                If(KZONESC.lt.1.or.KZONESC.gt.2) goto 2000
C
C KZONESC =1 : 10 zones; = 2 : 33 zones
  If(KZONESC.eq.1) then
    K=10
    Do i=1,K
      A(i)=A1(i)
    Enddo

                                else

    K=33
    Do i=1,K
      A(i)=A2(i)
    Enddo

                                endif

  AM=AN
C QPROT2,QNEUT2 are for zones with alpha-particles
  QPROT=Z/AN
  QNEUT=(AN-Z)/AN
  QPROT2=(Z-2.*FIALPH*AN)/(AN-3.*FIALPH*AN)
  QNEUT2=(AN-Z-2.*FIALPH*AN)/(AN-3.*FIALPH*AN)
C Recalculation FIALPH
  FIALP2=FIALPH
  FIALPH=FIALPH*AN/(AN-3.*FIALPH*AN)
  ONE=QPROT2+QNEUT2+FIALPH
  print *,'ONE=',ONE
  RMASS=1./(1.+AM)
C Effective nucleus radius
  RNUCL=1.25*(AM**0.3333333333)
C Nuclear density
  DATA AA/0.545/,RO/0.17/
  R=1.07*(AM**0.3333333333)
  X1=(3.*(3.1415926**2))**0.333333333
  PARTFM=0.5*(20.7214+20.74998)*(X1**2)
  PARPFM=197.3285*X1
C
  RMP=0.5*(938.2796+939.5731)
  PRINT 69
  IF(INFBIG.GT.0)WRITE(IPR,69)
C
C PF(I,M), TF(I,M):
C M = 1 neutron
C M = 2 proton
C M = 3 alpha-particle
C M = 4 He-3, triton
  DO 1 I=1,K
    RO1(I)=A(I)*RO

```

```

      ROPRO=RO1(I)*QPROT
      RONEU=RO1(I)*QNEUT
      RZON(I)=R+AA*ALOG((1.-A(I))/A(I))
      PF(I,2)=PARPFM*(ROPRO**0.333333333)
      TF(I,2)=PARTFM*(ROPRO**0.666666666)
      PF(I,1)=PARPFM*(RONEU**0.333333333)
      TF(I,1)=PARTFM*(RONEU**0.666666666)
      TFEFF=QPROT*TF(I,2)+QNEUT*TF(I,1)
      PFEFF=SQRT(2.*RMP*TFEFF)
      TF(I,3) = 4.* TFEFF
      PF(I,3) = SQRT(2.*WM(3)*TF(I,3))
      TF(I,4) = 3.* TFEFF
      PF(I,4) = SQRT(2.*WM(4)*TF(I,4))
      PRINT 70,I,RZON(I),RO1(I),
*     PF(I,2),PF(I,1),PF(I,3),TF(I,2),TF(I,1),TF(I,3),PFeff,TFeff
      IF(INFBIG.GT.0)WRITE(IPR,70)I,RZON(I),RO1(I),
*     PF(I,2),PF(I,1),PF(I,3),TF(I,2),TF(I,1),TF(I,3),PFeff,TFeff
C TF and PF for neutrons and protons
      PF(I,1)=PFEFF
      TF(I,1)=TFEFF
      PF(I,2)=PFEFF
      TF(I,2)=TFEFF
      1 CONTINUE
      69 FORMAT(1X,'ZONE RADIUS DENS ',
*     ' PF(P) PF(N) PF(A) TF(P) TF(N) TF(A) PF(Eff) TF(Eff)')
      70 FORMAT(1X,1X,I2,1X, F7.2, F7.4, 2F6.1, F7.1, 3F6.1, 2F8.2)
C Number of division for free particle path (not used)
      FIG=3.
      FOUT=FIG
C Woods-Saxon nucleus radius
      RA=RZON(K)
C Mass of incident particle
      W0=939.5731
      IF(MPARIN.EQ.2)W0=938.2796
      IF(MPARIN.EQ.3)W0=4.0026033*931.4812
C
C For Dostrovsky inverse cross-section ( Barashenkov, Toneev Book,1972 p.413)
C Dostrovsky coeff = ALINAK * Z + BLINAK
      DO 555 I=2,6
      ZZ=ZD(I)-ZD(I-1)
      ALINPK(I)=(RKPD(I)-RKPD(I-1))/ZZ
      BLINPK(I)=-ALINPK(I)*ZD(I-1)+RKPD(I-1)
      ALINPC(I)=(CPD(I)-CPD(I-1))/ZZ
      BLINPC(I)=-ALINPC(I)*ZD(I-1)+CPD(I-1)
      ALINAK(I)=(RKAD(I)-RKAD(I-1))/ZZ
      BLINAK(I)=-ALINAK(I)*ZD(I-1)+RKAD(I-1)
      ALINAC(I)=(CAD(I)-CAD(I-1))/ZZ
555      BLINAC(I)=-ALINAC(I)*ZD(I-1)+CAD(I-1)
C See also BLOCK DATA
C
C Geometrical cross-section
      SGEOM=(3.1415926E-02)*((RA+4.552/SQRT(T0))**2)
      QN=QBON(1,1,1)
      QP=QBON(1,1,2)
      TF(K+1,1)=-QN
      TF(K+1,2)=-QP
      TF(K+1,3)=-QBON(1,1,6)
      TF(K+1,4)=-0.5*( QBON(1,1,4)+QBON(1,1,5) )
C Redefinition of this value for neutron and proton

```

```

TF(K+1,1)=QNEUT*TF(K+1,1)+QPROT*TF(K+1,2)
TF(K+1,2)=TF(K+1,1)
C
  QNN=QN
  QPP=QP
  QNNN=QN
  IF(MPARIN.EQ.2)QNNN=QP
  IF(MPARIN.EQ.3)QNNN=QBON(1,1,6)
C
C Coulomb potential for protons and alphas
C      VP=0.1*Z+0.8
C      VP=1.44*Z/RNUCL
C best value      VP=1.0 *Z/RNUCL
CC Zr (N,P) reaction
CC      VP=( Z-FLOAT(MPARIN-2) )*1.15/( 1.6 + 1.21*( AN**.3333+1.))
CC      VP=0.1*Z-0.2
CC      VAL=0.21*Z+2.5
CC      PRINT 600,VP,VAL
C
C Cut-off parameter BONCUT(1)-neutrons, (2)-protons, (3)-alpha
BONCUT(1)=-TF(K+1,1)+BONNE
BONCUT(2)=-TF(K+1,2)+VP+BONNE
BONCUT(3)=-TF(K+1,3)+VAL+BONNE
PRINT 1999,QN,QP,BONCUT(1),BONCUT(2),BONCUT(3),TF(K+1,1),BONNE,VP
  IF(QN.GT.-TF(K+1,1))BONCUT(1)=QN+BONNE
  IF(QP.GT.-TF(K+1,2))BONCUT(2)=QP+VP+BONNE
PRINT 1999,QN,QP,BONCUT(1),BONCUT(2),BONCUT(3),TF(K+1,1),BONNE,VP
1999 FORMAT(1X,' QN=',F6.2,' QP=',F6.2,' BONCUT(1)=',F6.2,' (2)=',
  *F6.2,' (3)=',F6.2,' TF(max)=',F6.2,' BONNE=',F6.2,' VP=',F6.2)
C
C=====
C Arrays and auxilarily for calculation energy spectra
C EMEM: evaporation spectrum, EMEM0: non-equilibrium spectrum
C EMEM=EMEM0. EEMEMT: recoil spectrum
EMEM0(1)=0.
RMEM0(1,1)=0.
RMEM0(1,2)=0.
RMEM0(1,3)=0.
  QBMIN = QBON(1,1,MPARIN)
  IF(MPARIN.eq.3) QBMIN =QBON(1,1,6)
  If(QBMIN.gt.QBON(1,1,1)) QBMIN = QBON(1,1,1)
  If(QBMIN.gt.QBON(1,1,2)) QBMIN = QBON(1,1,2)
  If(QBMIN.gt.QBON(1,1,6)) QBMIN = QBON(1,1,6)
  HMEM=( T0+QBON(1,1,MPARIN)-QBMIN )/20.
  IF(MPARIN.eq.3) HMEM=( T0+QBON(1,1,6)-QBMIN )/20.
EMEM(1)=0.
RMEM(1,1)=0.
RMEM(1,2)=0.
RMEM(1,3)=0.
  HMEMT=(9.*T0/AN)+0.2
  IF(MPARIN.eq.3) HMEMT=0.3*T0 ! rather arbitrary
  HMEMT=HMEMT/20.
  EEMEMT(1)=0.
  RMEMT(1)=0.
DO 567 NU=2,21
EMEM0(NU)=EMEM0(NU-1)+HMEM
EMEM(NU)=EMEM(NU-1)+HMEM
EEMEMT(NU)=EEMEMT(NU-1)+HMEMT

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```

RMEMO (NU,1)=0.
RMEMO (NU,2)=0.
RMEMO (NU,3)=0.
    RMEM (NU,1)=0.
    RMEM (NU,2)=0.
    RMEM (NU,3)=0.
567     RMEMT (NU)=0.
        EMEMT (21)=(9.*T0/AN)+3.0
C
C Arrays for calculation total angular distribution
QPI=3.1415926/18.
QAN=0.
PI(1)=1.
DO 597 IQAN =1,19
DO 597 IQAN2=1,5
DO 597 IQAN3=1,3
597 SPE(IQAN,IQAN2,IQAN3)=0.
    DO 598 IQAN=2,19
    QAN=QAN+QPI
598     PI(IQAN)=COS(QAN)
C
C Arrays for calculation of inclusive particle spectra
C ANGZEN is array for angles (9)
C DCEN is the angular bin for angles  ANGZEN +/- DCEN
    DCEN = 4.
    QPI=3.1415926/180.
    DO 1014 MP = 1,3
DO 1012 ICEN=1,9
    QAN1= ANGZEN(ICEN,MP) - DCEN
    QAN2= ANGZEN(ICEN,MP) + DCEN
    IF(QAN1.LT.0.0) QAN1 =0.0
    IF(QAN2.GT.180.0) QAN2 =180.0
    ANGLIM(ICEN,1,MP) = COS(QAN1*QPI)
    ANGLIM(ICEN,2,MP) = COS(QAN2*QPI)
    DO 1011 NU=1,21
1011     ANGSUM(NU,ICEN,MP) = 0.0
1012     CONTINUE
1014     CONTINUE
C=====
600 FORMAT(1X,10X,'VP=',F6.1,' VAL=',F6.1)
C REFR is the maximal number of reflections for current MC history
REFR=100.
PRINT 731,TF(K+1,1)
IF(INFBIG.GT.0)WRITE(IPR,731)TF(K+1,1)
731 FORMAT(1X,' Average binding energy ',E12.5)
C
C Define effective threshold damage energy
CALL DEFINE_ED(Z)
C
RETURN
2000 Print 2001,KZONESC
Write(IPR,2001)KZONESC
2001 Format(' Parameter KZONESC =',i5,' is not valid')
STOP
END
*****
*                SUBROUTINE INIPAR                *
*****
SUBROUTINE INIPAR

```

```

COMMON/PARTIC/WP,PX,PY,PZ,P,T,E,X,Y,Z,R,JIN,M
COMMON/K/K /DATINI/RA,T0,W0 /MAIIPR/IPR /MPARIN/MPARIN
COMMON/URAND1/IYG
WP=W0
CC=RANDOM(0)
RK=RA*SQRT(CC)
Z=-RA*SQRT(1.-CC)
UU=6.2831852*RANDOM(0)
X=RK*COS(UU)
Y=RK*SIN(UU)
R=RA
T=T0
JIN=K
PX=0.
PY=0.
P=SQRT(T**2+2.*WP*T)
PZ=P
M=MPARIN
CALL TRANS(K+1,K,ITR9)
IF(ITR9.NE.0) GOTO 10
E=T+WP
RETURN
10 WRITE(IPR,20)
20 FORMAT(1X,'ERROR IN INIPAR (REFLECTION AT THE ENTRANCE ',
1'IN NUCLEUS)')
STOP
END
*****
* SUBROUTINE INSEP *
*****
SUBROUTINE INSEP
COMMON/INFSEP/KSEP(100,4),INFSEP,JSEPM
COMMON/MAIIPR/IPR /IWRI/IWRI
C JSEPM is maximal number of reactions required
C If INFSEP=1 and input contains 0 0 0, no calculations
I=0
77 I=I+1
IF(I.GT.100)GOTO 3000
READ *,IN,IP,IA
KSEP(I,1)=IABS(IN)
KSEP(I,2)=IABS(IP)
KSEP(I,3)=IABS(IA)
JSEPM=I
IF((IABS(IN)+IABS(IP)+IABS(IA)).EQ.0) INFSEP=0
IF(INFSEP.EQ.0) RETURN
IF(IN.LT.0.OR.IP.LT.0.OR.IA.LT.0) RETURN
GOTO 77
3000 WRITE(IPR,4000)
IF(IWRI.NE.0)WRITE(IWRI,4000)
4000 FORMAT(1X,' SUBR INSEP. NUMBER OF REACTIONS REQUIRED > 100')
STOP
END
*****
* SUBROUTINE INSEP2 *
*****
SUBROUTINE INSEP2
COMMON/INFSEP/KSEP(100,4),INFSEP,JSEPM
COMMON/SEPSEP/RSEP2(100,2),JSEPM2
COMMON/MAIIPR/IPR

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```

COMMON/IWRI/IWRI
C JSEPM is maximal number of reactions required
C If INFSEP=2 and input contains 0 0 0, no calculations
      I=0
77      I=I+1
      IF(I.GT.100)GOTO 3000
      READ *,ZZZ,AAA
      RSEP2(I,1)=ABS(ZZZ)
      RSEP2(I,2)=ABS(AAA)
      JSEPM2=I
      IF((ABS(ZZZ)+ABS(AAA)).EQ.0.) INFSEP=0
      IF(INFSEP.EQ.0) RETURN
      IF(ZZZ.LT.0..OR.AAA.LT.0.) RETURN
      GOTO 77
3000   WRITE(IPR,4000)
      IF(IWRI.NE.0)WRITE(IWRI,4000)
4000   FORMAT(1X,'SUBR INSEP2. NUMBER OF REACTIONS REQUIRED > 100')
      STOP
      END
*****
*               SUBROUTINE INSEP3                               *
*****
      SUBROUTINE INSEP3(MM,ZZ,AA)
      COMMON/INFSEP/KSEP(100,4),INFSEP,JSEPM
      COMMON/SEPSEP/RSEP2(100,2),JSEPM2
      COMMON/MAIIPR/IPR /IWRI/IWRI
      MPARIN=MM
      Z=ZZ
      AN=AA
      ZCOMP=Z+FLOAT(MPARIN)-1.
      ACOMP=AN+1.
      IF(MPARIN.eq.3) ZCOMP=Z+2.
      IF(MPARIN.eq.3) ACOMP=AN+4.
      DO 10 I=1,JSEPM2
      TOT=ACOMP-RSEP2(I,2)
      ZI=ZCOMP-RSEP2(I,1)
      RNI=TOT-ZI
      IN=RNI+0.01
      IP=ZI+0.01
      IA=0
      KSEP(I,1)=IN
      KSEP(I,2)=IP
10      KSEP(I,3)=IA
      JSEPM=JSEPM2
      RETURN
      END
*****
*               SUBROUTINE INTPOP                               *
*****
      SUBROUTINE INTPOP(IKS,INT9)
      COMMON/DAINT/PF(33,4),RO1(33),RZON(33),FIG
      COMMON/K/K /NDIM/NPAR
      COMMON/INTTR1/PWX,PWY,PWZ,TW,NPREN,NPREP,NPREA
      COMMON/PARTIC/WP,PX,PY,PZ,P,T,E,X,Y,Z,R,JIN,M
      COMMON/PARTNR/PPX,PPY,PPZ,PP,MX
      COMMON/TYPACT/L,L7 /QSUM/QSUM /BOND1/QBON(200,200,6)
      COMMON/URAND1/IYG /INFDIS/INFDIS,INFOUP(3)
      COMMON/JACT/JACT /MAIIPR/IPR
      INT9=0

```

```

      J1=JIN
C
      CC=RANDOM(0)
C
      X1=ALOG(CC)
10  CONTINUE
      J3=J1-1
      IF(J3)12,12,14
12  RZJ0=0.
      GOTO 16
14  RZJ0=RZON(J3)
16  CONTINUE
      RZONX=RZON(J1)
      CALL ZONWAY(RZONX,RZJ0,J1,J3,J2,SLINE)
20  CONTINUE
      IF(J1.GT.K)GOTO 1985
      CALL CHOPAR(J1,SXX)
          IF(MX.EQ.0 .OR. L.EQ.0) GOTO 1995
      PATH=1./(RO1(J1)*SXX)
CCCCC  DSL=PATH/FIG
      DSL=PATH
      IF(SLINE-DSL)30,30,40
30  D1=SLINE
      GOTO 50
40  D1=DSL
50  X1=X1+D1/PATH
      HH=D1/P
          X=X+HH*PX
          Y=Y+HH*PY
          Z=Z+HH*PZ
      R=SQRT(X*X+Y*Y+Z*Z)
      SLINE=SLINE-D1
      IF(X1)60,52,150
52  IF(SLINE)200,53,150
53  DELTA=0.001
      GOTO 200
60  CONTINUE
      IF(ABS(SLINE)-0.0001)70,70,20
70  IF(J1-J2)80,80,140
80  J2=J1+1
      IF(J2-K)140,140,90
90  CONTINUE
      CALL TRANS(J1,J2,ITR9)
          IF(ITR9.NE.0) GOTO 250
      IF(J1-K)10,10,95
95  PWX=PWX+PX
      PWY=PWY+PY
      PWZ=PWZ+PZ
      TW=TW+T
      IF(M.NE.3) QSUM=QBON(NPREN+2*NPREA+1,NPREP+2*NPREA+1,M)+QSUM
      IF(M.EQ.3) QSUM=QBON(NPREN+2*NPREA+1,NPREP+2*NPREA+1,6)+QSUM
C
          IF(INFDIS.EQ.1.AND.JACT.NE.0)CALL MEMPRE(M,PX,PY,PZ,T)
C
      IF(M-2)101,102,103
101 NPREN=NPREN+1
      GOTO 111
102 NPREP=NPREP+1
      GOTO 111

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```

103 NPREA=NPREA+1
C
111 CONTINUE
    IF(NPAR)112,112,114
112 IKS=-1
    RETURN
114 IKS=0
    RETURN
140 CONTINUE
    CALL TRANS(J1,J2,ITR9)
        IF(ITR9.NE.0) GOTO 250
145     E=T+WP
    GOTO 10
150 DELTA=PATH*X1
200 HH=DELTA/P
        X=X-HH*PX
        Y=Y-HH*PY
        Z=Z-HH*PZ
        R=SQRT(X**2+Y**2+Z**2)
    IKS=1
    JIN=J1
    CALL DISTPA(J1)
    RETURN
250     INT9=1
    RETURN
C
C
1985 PRINT 1986,J1,K
    WRITE(IPR,1986)J1,K
1986 FORMAT(1X,' INTPOP  FALSE  J1=',I4,' K=',I4)
    STOP
1995 PRINT 1996,M,MX,L
    WRITE(IPR,1996)M,MX,L
1996 FORMAT(1X,' ERROR IN CHOPAR: M=',I5,' MX=',I5,' L=',I5)
    STOP
    END
*****
*           SUBROUTINE LEGEN                               *
*****
    SUBROUTINE LEGEN(X,P)
    DIMENSION P(30)
    P(1)=1.
    P(2)=X
    DO 1 M=1,7
    RM=FLOAT(M)
1   P(M+2)=((2.*RM+1.)*X*P(M+1)-RM*P(M))/(RM+1.)
    RETURN
    END
*****
*           SUBROUTINE LIBGEN                               *
*****
    SUBROUTINE LIBGEN
    COMMON/MPARIN/MPARIN /QBOCFU/NSUMN,NSUMP /AN/AN
    COMMON/INIQBO/Z,CKA,CKB,RPA,RPB,RALA,RALB
    COMMON/LIB91/WINLIB(100,250),INFLIB
    A1=1.+AN-FLOAT(NSUMN+NSUMP)+2.
    Z1=FLOAT(MPARIN-1)+Z-FLOAT(NSUMP)+1.
    IF(MPARIN.EQ.3) A1=4.+AN-FLOAT(NSUMN+NSUMP)+2.
    IF(MPARIN.EQ.3) Z1=2.+Z-FLOAT(NSUMP)+1.

```



```

      IAA=A1+0.01
      IZZ=Z1+0.01
      IF(IAA.GT.250.OR.IZZ.GT.100) GOTO 1000
      WINLIB(IZZ,IAA)=WINLIB(IZZ,IAA)+1.
      RETURN
1000  WRITE(12,2000)IAA , IZZ
      WRITE(1,2000)IAA , IZZ
      PRINT 2000,IAA , IZZ
2000  FORMAT(1X,' SUBR. LIBGEN : IAA=',I6,' IZZ=',I6,' EXCEED LIMIT')
      STOP
      END
*****
*                SUBROUTINE LIBOUT                *
*****
      SUBROUTINE LIBOUT(CSNON,RRR)
      REAL*8 ITYP(3),ICS(4)
      COMMON/MAIIPR/IPR /IWRI/IWRI /MPARIN/MPARIN
      COMMON/DATINI/RA,T0,W0 /AN/AN
      COMMON/INIQBO/Z,CKA,CKB,RPA,RPB,RALA,RALB
      COMMON/KHIST/KHIST /LIB91/WINLIB(100,250),INFLIB
      COMMON/INF/INFBIG,INFS0
      DIMENSION CSNON(4),LA(8),CC(8)
C B=BARASH,G=GEOMETRY,O=OPTICAL,C=CHATTERJEE
      DATA ICS/'B','G','O','C'/
      DATA ITYP/' NEUTRON',' PROTON',' ALPHA'/
C Output unit
      M=12
      ITZ=Z+0.01
      ITA=AN+0.01
      IPZ=MPARIN-1
      IPA=1
      IF(MPARIN.eq.3) IPZ=2
      IF(MPARIN.eq.3) IPA=4
C
      REASUM=RRR
C Define nonelastic cross-section
      ICSN=INFS0
      CRSNON=1000.*CSNON(ICSN)
      CRSTMP=CRSNON/REASUM
C
C Form file
      WRITE(M,1000)
1000  FORMAT('1',79('*'))
      KHISTN=REASUM+0.001
      IZSUP=ITZ+IPZ
      IASUP=ITA+IPA
      ISUMAL=0
      DO 50 LLLZ=1,IZSUP
      ISUMZ=0
      DO 20 MMMA=1,IASUP
      IF(WINLIB(LLLZ,MMMA).GE.1.E-04)ISUMZ=1
      IF(ISUMZ.EQ.1)GOTO 25
20    CONTINUE
25    IF(ISUMZ.EQ.1) ISUMAL=ISUMAL+1
50    CONTINUE
C Header
      WRITE(M,1001)ITZ,ITA, T0,ITYP(MPARIN),CRSNON,ICS(ICSN),
%                ISUMAL,KHISTN
1001  FORMAT(I3,I4,F8.1,' MEV',A8,F9.1,A1,' (' ,I2,'Z)',

```

```

%      3X,' DISCA',I7)
DO 500 I=1,IZSUP
IZ=IZSUP-I+1
ISUMZ=0
DO 200 JJ=1,IASUP
IF(WINLIB(IZ,JJ).GE.1.E-04)ISUMZ=ISUMZ+1
200 CONTINUE
IF(ISUMZ.EQ.0) GOTO 500
WRITE(M,1500)IZ,ISUMZ
1500 FORMAT(I3,'      (' ,I3,'A)')
      JJJ=0
DO 300 JA=1,IASUP
JM=IASUP-JA+1
WW=WINLIB(IZ,JM) * CRSTMP
IF(WW.LT.1.E-04) GOTO 300
JJJ=JJJ+1
IF(JJJ.GT.8) GOTO 7000
LA(JJJ)=JM
CC(JJJ)=WW
IF(JJJ.NE.8) GOTO 300
      WRITE(M,2000)(LA(J11),J11=1,8)
      WRITE(M,2001)(CC(J11),J11=1,8)
2000 FORMAT(4X,I3,7(7X,I3))
2001 FORMAT(8E10.3)
DO 299 LL=1,8
LA(LL)=-10
299 CC(LL)=-10.
      JJJ=0
300 CONTINUE
      IF(JJJ.NE.0) WRITE(M,2000)(LA(J11),J11=1,JJJ)
      IF(JJJ.NE.0) WRITE(M,2001)(CC(J11),J11=1,JJJ)
500 CONTINUE
C
RETURN
7000 WRITE(M,7001)
7001 FORMAT(1X,' ERROR IN SUBR LIBOUT ')
STOP
END
*****
* SUBROUTINE LYMASS *
*****
SUBROUTINE LYMASS(ZEE,AMASS,NZ,NA,MC,MP,AP,AT,ZP,ZT,QVAL)
* taken from Blann code ALICE
DIMENSION EM(10),XK(10),Y(2),F(2),XMS(24,11), EMP(10)
DIMENSION XQ(30)
COMMON/LYML/BE(11,24,4),SYMB(11,24),PAIR(11,24),SYMBP(11,24)
COMMON/SF/M3,KPLT
DATA BLANK,FOR,RINP/4H ,4H MSL,4H INP/
DO 1 I=1,11
DO 1 K=1,24
SYMBP(I,K)=BLANK
SYMB(I,K)=BLANK
PAIR(I,K)=0.
DO 1 L=1,4
BE(I,K,L)=0.
1 CONTINUE
DEL=0.
IF(MP.EQ.0.)DEL=2.
IF(MP.EQ.3.)DEL=1.

```

```

C
C ABOVE STATEMENTS DEFINE PAIRING TREATMENT
  IBIND=0
  IF(MC.LT.10) GO TO 6
  IBIND = 1
  MC=MC-10
6 EM(1)=0.0
  EM(2)=2.0
  EM(3)=8.0
  EM(4)=14.0
  EM(5)=28.0
  EM(6)=50.0
  EM(7)=82.0
  EM(8)=126.0
  EM(9)=184.0
  EM(10)=258.0
  CAY1=1.15303
  CAY3=200.0
  CAY4=11.0
  CAY5=8.07144
  CAY6=7.28899
  GAMMA=1.7826
  A1=15.4941
  A2=17.9439
  A3=0.7053
  D=0.444
  C=5.8
  SMALC=0.325
  PVAL=0.
  DO 15 I=1,10
    EMP(I)=EM(I)**(5.0/3.0)
15 CONTINUE
  DO 20 I=1,9
    XK(I)=0.6*(EMP(I+1)-EMP(I))/(EM(I+1)-EM(I))
20 CONTINUE
  RZ=.863987/A3
  L=0
  Z=1.0
25 KZ=ZEE
  KA=AMASS
  IF(QVAL.EQ.0..AND.PVAL.EQ.0.)GO TO 30
  GO TO 35
30 NNZ=3
  NNA=1
  GO TO 90
35 NNZ=NNZ+2
  NNA=NNA+2
cccc  WRITE (6,36)
36 FORMAT (1H1,53X,'MASS OPTIONS'//)
  IF (MC.EQ.1.AND.MP.NE.0) MC=0
cccc  IF(IBIND.EQ.1)WRITE(6,86)
86 FORMAT(20X,' EXPERIMENTAL MASSES ARE USED WHERE TABUL'
1,'ATED;LIQUID DROP VALUES OTHERWISE.')
cccc  IF(MC.EQ.0) WRITE(6,70)
cccc  IF(MC.EQ.1) WRITE(6,65)
cccc  IF (MC.EQ.2) WRITE (6,70)
50 Continue
cccc  IF(MP.EQ.0)WRITE(6,75)
cccc  IF(MP.EQ.1)WRITE(6,80)

```

```

cccc  IF(MP.EQ.3)WRITE(6,81)
      81 FORMAT(' NORMAL PAIRING SHIFT WITH ODD-EVEN REFERENCE POINT')
      65 FORMAT(40X,'LIQUID DROP WITHOUT SHELL CORRECTION TERM')
      70 FORMAT(41X,'LIQUID DROP WITH SHELL CORRECTION TERM')
      75 FORMAT(21X,'WITHOUT PAIRING, I.E. LEVEL DENSITY PAIRING ',
      1 'SHIFT ABSORBED IN BINDING ENERGIES')
      80 FORMAT(10X,'WITH PAIRING, LEVEL DENSITY PAIRING SHIFT',
      1 ' CALC. FROM MSL FORMULA AND APPLIED IN BACKSHIFTED',
      2 ' CONVENTION')
cccc  IF (MP.EQ.2) WRITE(6,85)
      85 FORMAT (20X,'MSL SHELL CORRECTION TERM INCLUDED IN LEVEL ',
      1 'DENSITY GROUND STATE SHIFT')
      90 DO 215 JZ=1,NNZ
          DO 215 JA=1,NNA
          IF(QVAL.EQ.0..AND.PVAL.EQ.0.)GO TO 95
          GO TO 115
      95 IF(JZ-2)100,105,110
100  Z=ZEE
      A=AMASS
      IA=A
      IZ=Z
      N=IA-IZ
      UN=AMASS-ZEE
      GO TO 125
105  Z=ZT
      A=AT
      IA=A
      IZ=Z
      N=IA-IZ
      UN=AT-ZT
      GO TO 125
110  Z=ZP
      A=AP
      IZ=Z
      IA=A
      N=IA-IZ
      UN=AP-ZP
      GO TO 125
115  IA=KA+2-JA-JZ
      IZ=KZ+1-JZ
      N=IA-IZ
120  Z=IZ
      UN=N
      A=IA
125  A3RT=A**(1.0/3.0)
      A2RT=SQRT(A)
      A3RT2=A3RT**2.0
      ZSQ=Z**2.0
      SYM=((UN-Z)/A)**2
      ACOR=1.0-GAMMA*SYM
      PARMAS=CAY5*UN+CAY6*Z
      VOLNUC=-1.0*A1*ACOR*A
      SUFNUC=A2*ACOR*A3RT2
      COULMB=A3*ZSQ/A3RT
      FUZSUR=-1.0*CAY1*ZSQ/A
      ODDEV=-1.0*(1.0+2.0*(N/2)-UN+2.*(IZ/2)-Z)/SQRT(A)*CAY4
      PAIR(JZ,JA)=-ODDEV
      SYMBP(JZ,JA)=FOR
      IF(MP.EQ.0)ODDEV=0.

```

```

      IF(MP.EQ.0)GO TO 11
10  PAIR(JZ,JA)=(2.0*(N/2)-UN+2.0*(IZ/2)-Z+DEL)/SQRT(A)*CAY4
      SYMBP(JZ,JA) = FOR
11  CONTINUE
      IF(SYM.GT.0.4)WTERM=0.
130 WTERM=0.
      WOTNUC=PARMAS+COULMB+FUZSUR+ODDEV+WTERM
      SMASS=WOTNUC+VOLNUC+SUFNUC
      XMS(JA,JZ)=SMASS
      XQ(JZ)=SMASS
135 CONTINUE
      C2=(SUFNUC+WTERM)/(A**(2.0/3.0))
      X=COULMB/(2.0*(SUFNUC+WTERM))
140 BARR=0.0
145 Y(1)=UN
      Y(2)=Z
      DO 165 J=1,2
      DO 150 I=1,9
      IF (Y(J)-EM(I+1)) 160,160,150
150 CONTINUE
155 STOP
160 F(J)=XK(I)*(Y(J)-EM(I))-0.6*(Y(J)**(5./3.))-EMP(I))
165 CONTINUE
      S=(2.0/A)**(2.0/3.0)*(F(1)+F(2))-SMALC*A**(1./3.)
      EE=2.*C2*D**2*(1.0-X)
      FF=.42591771*C2*D**3*(1.+2.*X)/A3RT
      SSHELL=C*S
      V=SSHELL/EE
      EPS=1.5*FF/EE
      IF(EE*(1.-3.*V).LE.0.0) GO TO 170
      QCALC=0.0
      THETA=0.0
      SHLL=SSHELL
      GO TO 210
170 TO=1.0
175 DO 180 IPQ=1,10
      T=TO-(1.-EPS*TO-V*(3.-2.*TO**2)*EXP(-TO**2))/(-EPS+V*(10.*TO-4.
1  *TO**3)*EXP(-TO**2))
      IF (T.LE.0.0) GO TO 190
      IF (ABS(T-TO) .LT.0.0001) GO TO 185
      TO=T
180 CONTINUE
      GO TO 200
185 IF (2.*EE*(1.-2.*EPS*T-V*(3.-12.*T**2+4.*T**4)*EXP(-T**2))
1  .GT.0.0) GO TO 205
190 DO 195 I=1,20
      TO=FLOAT(I)/10.
      GL=EE*(1.-EPS*TO-V*(3.-2.*TO**2)*EXP(-TO**2))
      IF (GL.GE.0.0) GO TO 175
195 CONTINUE
200 CONTINUE
      GO TO 215
205 THETA=T
      ALPHA0=D*SQRT(5.)/A**(1./3.)
      ALPHA=ALPHA0*THETA
      SIGMA=ALPHA*(1.+ALPHA/14.)
      QCALC=.004*Z*(RZ*A3RT)**2*(EXP(2.*SIGMA)-EXP(-SIGMA))
      SHLL=EE*T**2-FF*T**3+SSHELL*(1.-2.*T**2)*EXP(-T**2)
210 IF(MC.NE.1.OR.MP.NE.0) GO TO 211

```

```

PAIR(JZ,JA)=PAIR(JZ,JA)-SHLL
SHLL = 0.
211 CMASS=SMASS+SHLL
XMS(JA,JZ)=CMASS
IF(MP.EQ.2) PAIR(JZ,JA)=PAIR(JZ,JA)-SHLL
XQ(JZ)=CMASS
215 CONTINUE
IF(QVAL.EQ.0..AND.PVAL.EQ.0.)GO TO 220
GO TO 240
220 IF(ZP-20.)225,225,230
225 IF(AP.EQ.01..AND.ZP.EQ.01.)XQ(3)=7.29
IF(AP.EQ.01..AND.ZP.EQ.00.)XQ(3)=8.07
IF(AP.EQ.02..AND.ZP.EQ.01.)XQ(3)=13.14
IF(AP.EQ.03..AND.ZP.EQ.01.)XQ(3)=14.95
IF(AP.EQ.03..AND.ZP.EQ.02.)XQ(3)=14.93
IF(AP.EQ.04..AND.ZP.EQ.02.)XQ(3)=2.43
IF(AP.EQ.06..AND.ZP.EQ.03.)XQ(3)=14.09
IF(AP.EQ.07..AND.ZP.EQ.03.)XQ(3)=14.91
IF(AP.EQ.09..AND.ZP.EQ.04.)XQ(3)=11.35
IF(AP.EQ.10..AND.ZP.EQ.05.)XQ(3)=12.05
IF(AP.EQ.11..AND.ZP.EQ.05.)XQ(3)=8.67
IF(AP.EQ.12..AND.ZP.EQ.06.)XQ(3)=0.
IF(AP.EQ.13..AND.ZP.EQ.06.)XQ(3)=3.13
IF(AP.EQ.14..AND.ZP.EQ.07.)XQ(3)=2.86
IF(AP.EQ.15..AND.ZP.EQ.07.)XQ(3)=0.10
IF(AP.EQ.16..AND.ZP.EQ.08.)XQ(3)=-4.74
IF(AP.EQ.17..AND.ZP.EQ.08.)XQ(3)=-.81
IF(AP.EQ.18..AND.ZP.EQ.08.)XQ(3)=-.78
IF(AP.EQ.19..AND.ZP.EQ.09.)XQ(3)=-1.49
IF(AP.EQ.20..AND.ZP.EQ.10.)XQ(3)=-7.04
IF(AP.EQ.21..AND.ZP.EQ.10.)XQ(3)=-5.73
IF(AP.EQ.22..AND.ZP.EQ.10.)XQ(3)=-8.03
IF(AP.EQ.23..AND.ZP.EQ.11.)XQ(3)=-9.53
IF(AP.EQ.24..AND.ZP.EQ.12.)XQ(3)=-13.93
IF(AP.EQ.25..AND.ZP.EQ.12.)XQ(3)=-13.19
IF(AP.EQ.26..AND.ZP.EQ.12.)XQ(3)=-16.21
IF(AP.EQ.27..AND.ZP.EQ.13.)XQ(3)=-17.2
IF(AP.EQ.28..AND.ZP.EQ.14.)XQ(3)=-21.49
IF(AP.EQ.29..AND.ZP.EQ.14.)XQ(3)=-21.89
IF(AP.EQ.30..AND.ZP.EQ.14.)XQ(3)=-24.44
IF(AP.EQ.31..AND.ZP.EQ.15.)XQ(3)=-24.44
IF(AP.EQ.32..AND.ZP.EQ.16.)XQ(3)=-26.01
IF(AP.EQ.33..AND.ZP.EQ.16.)XQ(3)=-26.58
IF(AP.EQ.34..AND.ZP.EQ.16.)XQ(3)=-29.93
IF(AP.EQ.36..AND.ZP.EQ.16.)XQ(3)=-30.66
IF(AP.EQ.35..AND.ZP.EQ.17.)XQ(3)=-29.01
IF(AP.EQ.37..AND.ZP.EQ.17.)XQ(3)=-31.77
IF(AP.EQ.36..AND.ZP.EQ.18.)XQ(3)=-30.23
IF(AP.EQ.38..AND.ZP.EQ.18.)XQ(3)=-34.72
IF(AP.EQ.40..AND.ZP.EQ.18.)XQ(3)=-35.04
IF(AP.EQ.39..AND.ZP.EQ.19.)XQ(3)=-33.80
IF(AP.EQ.40..AND.ZP.EQ.19.)XQ(3)=-33.53
IF(AP.EQ.41..AND.ZP.EQ.19.)XQ(3)=-35.55
IF(AP.EQ.40..AND.ZP.EQ.20.)XQ(3)=-34.85
IF(AP.EQ.42..AND.ZP.EQ.20.)XQ(3)=-38.54
IF(AP.EQ.43..AND.ZP.EQ.20.)XQ(3)=-38.40
IF(AP.EQ.44..AND.ZP.EQ.20.)XQ(3)=-41.46
IF(AP.EQ.46..AND.ZP.EQ.20.)XQ(3)=-43.14
IF(AP.EQ.48..AND.ZP.EQ.20.)XQ(3)=-44.22

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```

230 PVAL=XQ(2)+XQ(3)-XQ(1)
cccc WRITE(6,235)PVAL
235 FORMAT(/41X,' QVAL FROM MYERS SWIATECKI MASS FORMULA = ',F8.3)
GO TO 25
240 DO 245 JZ=1,NZ
DO 245 JA=1,NA
SYMB(JZ,JA) = FOR
BE(JZ,JA,1)=8.07+XMS(JA+1,JZ)-XMS(JA,JZ)
BE(JZ,JA,2)=7.29+XMS(JA,JZ+1)-XMS(JA,JZ)
BE(JZ,JA,4)=13.3+XMS(JA+1,JZ+1)-XMS(JA,JZ)
245 BE(JZ,JA,3)=2.42+XMS(JA+2,JZ+2)-XMS(JA,JZ)
IF(IBIND.EQ.1) CALL BINDEN(ZEE,AMASS,NZ,NA,AP,AT,ZP,ZT,
1 QVAL,M3,MP)
cccc IF(QVAL.EQ.0.)WRITE(6,235)PVAL
IF(QVAL.EQ.0.)QVAL=PVAL
IF(MC.NE.2) GO TO 260
250 DO 255 IZ=1,NNZ
DO 255 IA=1,NNA
READ(5,270)BE1,BE2,BE3,BE4,PDEL
IF(BE1.EQ.0.) GO TO 400
BE(IZ,IA,1)=BE1
BE(IZ,IA,2)=BE2
BE(IZ,IA,3)=BE3
BE(IZ,IA,4)=BE4
SYMB(IZ,IA)=RINP
400 IF(PDEL.EQ.0.) GO TO 255
PAIR(IZ,IA)=PDEL
SYMBP(IZ,IA)=RINP
255 CONTINUE
cccc WRITE (6,275)
260 Continue
cccc WRITE(6,280)
DO 265 IZ=1,NNZ
MZ=ZEE+1-IZ
DO 265 IA=1,NNA
MA=AMASS+2-IA-IZ
cccc WRITE(6,285)MZ,MA,(BE(IZ,IA,K),K=1,4),SYMB(IZ,IA),
cccc 1 PAIR(IZ,IA),SYMBP(IZ,IA)
IF(MP.LE.0)PAIR(IZ,IA)=0.
PAIR(IZ,IA)=10.*PAIR(IZ,IA)
265 CONTINUE
cccc WRITE (6,268)
268 FORMAT (1H1)
RETURN
270 FORMAT(5F10.5)
275 FORMAT (20X,'SOME BINDING ENERGIES OR LEVEL DENSITY GROUND ',
* 'STATE SHIFTS PROVIDED BY USER')
280 FORMAT (/30X,'BINDING ENERGIES AND LEVEL DENSITY GROUND ',
* 'STATE SHIFTS USED'//22X,' IZ = Z-INDEX OF NUCLEUS,',
* ' IA = A-INDEX OF NUCLEUS IN PROGRAM ISOTOPE TABLE'/32X,
* 'MSL = CALCULATED BY MYERS SWIATECKI LYSEKILL MASS FORMULA'/
* 32X,'TAB = TAKEN FROM 1971 MASS TABLE'/32X,'INP = PROVIDED',
* ' BY USER'/32X,'ABE = ABSORBED IN BINDING ENERGY'//
* 10X,' IZ IA NEUTRON PROTON ALPHA ',
* 'DEUTERON SOURCE GS SHIFT SOURCE'//)
285 FORMAT(10X,2I4,2X,4(F10.5,2X),3X,A4,3X,F10.5,3X,A4)
END
*****
* SUBROUTINE MASDAT *

```

```

*****
* Only nucleon and alpha projectile is assumed
  SUBROUTINE MASDAT
  COMMON/MASTR1/W(21,21)
  COMMON/AN/AN
  COMMON/MPARIN/MPARIN
    AM=AN
    If(MPARIN.eq.3) AM=AN+3.
  DO 2 I=1,21
  DO 1 J=I,21
  W(I,J)=(AM-FLOAT(I-1)-FLOAT(J-2))*931.5016
  W(J,I)=W(I,J)
  1 CONTINUE
  2 CONTINUE
  RETURN
  END
*****
* SUBROUTINE MASS *
*****
  SUBROUTINE MASS(MZ,N,EXCES,ERRR,IRET)
* taken from Blann code ALICE
C FINDS MASS EXCESS (EXCES, IN MEV) AND ERROR (ERRR) FROM 1971
C WAPSTRA GOVE MASS TABLE UP TO 199PT, FROM 1977(?) TABLE UP TO 256E
C ERRR=500. MEANS MASS IS FROM SYSTEMATICS
C ERRR=+0. MEANS STABLE NUCLIDE
C PIONS IN MASS TABLE HAVE HAD Z ELECTRONS ADDED TO BE CONSISTENT
C WITH REST OF THE ATOMIC MASS TABLE
  DATA NT/ 1755/
  NZNO=MZ*1000+N
  NL=((MZ/10)*2-4)*100
  IF(NL.LE.0) NL=1
  DO 11 J=NL,NT
  IF(IZATAB(J).EQ.NZNO) GO TO 12
  11 CONTINUE
  IRET=IRET+1
  RETURN
  12 EXCES=ZAMASS(J)
  ERRR=ERRMAS(J)
  RETURN
  END
  FUNCTION IZATAB(J)
C TABLE OF ZA (1000*Z + A)
  DIMENSION ITABLE(1800),
  1 I1(54),I1A(46),I2(54),I2A(46),I3(54),I3A(46),I4(54),I4A(46),
  2 I5(54),I5A(46),I6(54),I6A(46),I7(54),I7A(46),I8(54),I8A(46),
  3 I9(54),I9A(46),I10(54),I10A(46),I11(54),I11A(46),
  4 I12(54),I12A(46),I13(54),I13A(46),I14(54),I14A(46),
  5 I15(54),I15A(46),I16(54),I16A(46),I17(54),I17A(46),
  6 I18(54),I18A(46)
  EQUIVALENCE (I1(1),ITABLE(1)),(I2(1),ITABLE(101)),
  1(I3(1),ITABLE(201)),(I4(1),ITABLE(301)),(I5(1),ITABLE(401)),
  2(I6(1),ITABLE(501)),(I7(1),ITABLE(601)),(I8(1),ITABLE(701)),
  3(I9(1),ITABLE(801)),(I10(1),ITABLE(901)),(I11(1),ITABLE(1001)),
  4(I12(1),ITABLE(1101)),(I13(1),ITABLE(1201)),(I14(1),ITABLE(1301)),
  5(I15(1),ITABLE(1401)),(I16(1),ITABLE(1501)),(I17(1),ITABLE(1601)),
  6(I18(1),ITABLE(1701))
  EQUIVALENCE (I1A(1),ITABLE(55)),(I2A(1),ITABLE(155)),
  1 (I3A(1),ITABLE(255)),(I4A(1),ITABLE(355)),
  2 (I5A(1),ITABLE(455)),(I6A(1),ITABLE(555)),

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3 (I7A (1),ITABLE(655 )),(I8A (1),ITABLE( 755)),
4 (I9A (1),ITABLE(855 )),(I10A(1),ITABLE( 955)),
5 (I11A(1),ITABLE(1055)),(I12A(1),ITABLE(1155)),
6 (I13A(1),ITABLE(1255)),(I14A(1),ITABLE(1355)),
7 (I15A(1),ITABLE(1455)),(I16A(1),ITABLE(1555)),
8 (I17A(1),ITABLE(1655)),(I18A(1),ITABLE(1755))
DATA I1/
1 -999, 0, 999, 1, 4, 1000, 1001, 1002, 1004,
2 2001, 2002, 2003, 2004, 2006, 3002, 3003, 3004, 3005,
3 3006, 3007, 3008, 4001, 4002, 4003, 4004, 4005, 4006,
4 4007, 4008, 5002, 5003, 5004, 5005, 5006, 5007, 5008,
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DATA I1A/
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DATA I2A/
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6 20023/
DATA I3/
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DATA I3A/
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DATA I4/
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DATA I4A/
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DATA I5/

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DATA I5A/

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DATA I6/

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DATA I6A/

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DATA I7/

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DATA I7A/

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DATA I8/

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DATA I8A/

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DATA I9/
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DATA I9A/
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6 96143/
DATA I18/
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DATA I18A/
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2    0,    0,    0,    0,    0,    0,    0,    0,    0,
3    0,    0,    0,    0,    0,    0,    0,    0,    0,
4    0,    0,    0,    0,    0,    0,    0,    0,    0,
5    0,    0,    0,    0,    0,    0,    0,    0,    0,
6    0/
IZATAB=ITABLE(J)
RETURN
END
FUNCTION ZAMASS(J)

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C
C
C

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MASS EXCESS IN MEV.

DIMENSION AMASS(1800),
1 A1 (54),A2 (54),A3 (54),A4 (54),A5 (54),A6 (54),A7 (54),
2 A8 (54),A9 (54),A10(54),A11(54),A12(54),A13(54),A14(54),
3 A15(54),A16(54),A17(54),A18(54),
4 A1A(46),A2A(46),A3A(46),A4A(46),A5A(46),A6A(46),A7A(46),
5 A8A(46),A9A(46),A10A(46),A11A(46),A12A(46),A13A(46),
6 A14A(46),A15A(46),A16A(46),A17A(46),A18A(46)
EQUIVALENCE (A1(1),AMASS (1)),(A2(1),AMASS (101)),
1(A3 (1),AMASS (201)),(A4 (1),AMASS (301)),(A5 (1),AMASS (401)),
2(A6 (1),AMASS (501)),(A7 (1),AMASS (601)),(A8 (1),AMASS (701)),
3(A9 (1),AMASS (801)),(A10(1),AMASS (901)),(A11(1),AMASS (1001)),
4(A12(1),AMASS (1101)),(A13(1),AMASS (1201)),(A14(1),AMASS (1301)),
5(A15(1),AMASS (1401)),(A16(1),AMASS (1501)),(A17(1),AMASS (1601)),
6(A18(1),AMASS (1701))
EQUIVALENCE (A1A(1),AMASS (55)),(A2A(1),AMASS (155)),
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2 ( A5A(1),AMASS (455)),( A6A(1),AMASS (555)),
3 ( A7A(1),AMASS (655)),( A8A(1),AMASS (755)),
4 ( A9A(1),AMASS (855)),(A10A(1),AMASS (955)),
5 (A11A(1),AMASS (1055)),(A12A(1),AMASS (1155)),
6 (A13A(1),AMASS (1255)),(A14A(1),AMASS (1355)),
7 (A15A(1),AMASS (1455)),(A16A(1),AMASS (1555)),
8 (A17A(1),AMASS (1655)),(A18A(1),AMASS (1755))
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3 17.59730, 31.61300, 11.68000, 14.08750, 14.90859, 20.94750,
4 24.95540, 34.10000, 41.70000, 34.92304, 18.37500, 15.77029,
5 4.94180, 11.34840, 12.60810, 20.17700, 24.94999, 27.94000,
6 22.92230, 12.41569, 12.05230, 8.66795, 13.37040, 16.56200,

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7 24.60000, 29.70000, 35.10000, 28.91200, 15.70270, 10.65019,
8 0.00000, 3.12527, 3.01995, 9.87350, 13.69299, 17.56000,
9 40.23163, 25.44999, 17.34400, 5.34570, 2.86382, .10180/
DATA A1A/
1 5.68350, 7.87100, 13.27400, 16.35000, 50.59094, 32.97922,
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3 3.33230, 3.80000, 34.32074, 17.66000, 10.69300, 1.95180,
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5 42.65895, 24.66971, 16.47999, 5.31900, 1.75210, -7.04170,
6 -5.73120, -8.02510, -5.15000, -5.94800, 25.57849, 12.97999,
7 6.84000, -2.18300, -5.18290, -9.52900, -8.41670, -9.35600,
8 -6.85300, -5.98000, 32.71106, 17.74000/
DATA A2/
1 10.91100, -.39900, -5.47240, -13.93130, -13.19149, -16.21339,
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3-12.20880, -17.19500, -16.84880, -18.21300, -15.89000, -15.56000,
4 23.93176, 10.76000, 3.82400, -7.14300, -12.38539, -21.49110,
5-21.89329, -24.43130, -22.94790, -24.09100, 10.57867, .21000,
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1-24.43840, -29.01300, -29.52180, -31.76150, -29.80000, -29.80200,
2-27.54000, 11.18168, -2.15889, -9.40000, -18.37900, -23.04939,
3-30.23049, -30.94740, -34.71440, -33.24000, -35.03919, -33.06610,
4-34.42000, -31.98000, -32.76000, -29.72700, -29.73200, -1.69218,
5-11.25000, -17.31700, -24.79840, -28.79200, -33.80529, -33.53410,
6-35.55830, -35.02140, -36.58200, -35.80500, -36.61100, -35.42600,
7-35.70400, 4.74011, -6.44739, -13.14400, -22.02299, -27.28300,
8-34.84570, -35.13710, -38.53810, -38.39900/
DATA A3/
1-41.46359, -40.80630, -43.13800, -42.34300, -44.22200, -41.29200,
2-39.57800, -20.52099, -28.64100, -32.10700, -36.17900, -37.81400,
3-41.06309, -41.75840, -44.32890, -44.49500, -46.55200, -44.54500,
4-15.80000, -25.12100, -29.34100, -37.54800, -39.00070, -44.12579,
5-44.92919, -48.48559, -48.55729, -51.43359, -49.73900, -49.47000,
6-23.85400, -31.90000, -37.07140, -42.00480, -44.47020, -47.95610,
7-49.21670, -52.19740, -51.43690, -51.86100, -49.93000, -19.47600,
8-31.24000, -34.62500, -42.81600, -45.38800, -50.25500, -51.44600,
9-55.41500, -55.28380, -56.93230, -55.12100, -55.26600, -31.01700/
DATA A3A/
1-37.72000, -42.62460, -48.24000, -50.70500, -54.68650, -55.55700,
2-57.71000, -56.90870, -57.62000, -56.06000, -26.75500, -35.79100,
3-40.23200, -48.33390, -50.94200, -56.25170, -57.47840, -60.60940,
4-60.18380, -62.15510, -60.67000, -61.43500, -59.03000, -37.03100,
5-44.06400, -48.00200, -54.01240, -56.04120, -59.34700, -59.84720,
6-62.23570, -61.65560, -62.92000, -61.53000, -61.86300, -60.11000,
7-29.63200, -40.71200, -45.35000, -53.90800, -56.10400, -60.23500,
8-61.16260, -64.47920, -64.22700, -66.75190/
DATA A4/
1-65.52150, -67.10930, -65.13390, -66.06000, -63.20000, -51.66800,
2-56.36300, -58.35200, -61.98180, -62.80500, -65.58740, -65.43180,
3-67.26480, -66.25980, -67.30200, -69.42000, -65.94000, -48.43700,
4-54.19300, -56.58000, -61.11500, -62.22200, -66.00640, -65.91410,
5-68.89450, -67.87670, -70.00430, -68.41620, -69.55970, -67.33200,
6-68.13100, -56.72000, -58.93400, -62.65500, -63.71900, -66.87600,
7-67.08500, -69.32300, -68.90600, -70.13810, -68.58760, -69.74000,
8-67.92000, -68.54000, -56.36000, -61.61700, -62.45000, -66.69800,

9-67.09750,-70.55950,-69.90300,-72.58070,-71.29320,-73.42240/
 DATA A4A/
 1-71.84100,-73.21230,-71.16000,-71.78000,-69.39000,-63.13000,
 2-64.33800,-67.89400,-68.23000,-70.95400,-70.85870,-73.02970,
 3-72.28620,-73.91700,-72.76000,-73.69000,-71.76000,-72.59000,
 4-62.89000,-67.63000,-68.21400,-72.21300,-72.16490,-75.25460,
 5-74.60140,-77.02680,-75.93390,-77.75700,-76.38700,-77.58700,
 6-75.44000,-75.92000,-63.51000,-65.21000,-69.15500,-70.15000,
 7-73.23690,-73.45300,-76.07410,-75.88530,-77.97400,-77.50300,
 8-79.01800,-77.73000,-78.67000,-75.96000/
 DATA A5/
 1-74.20000,-62.11000,-64.05000,-69.15000,-70.23700,-74.14700,
 2-74.44300,-77.89600,-77.68000,-80.59100,-79.98700,-82.43320,
 3-81.47260,-83.26130,-80.70000,-79.70000,-76.56000,-74.89000,
 4-71.50000,-70.92000,-72.10000,-75.42000,-76.19400,-78.94900,
 5-79.75300,-82.15960,-82.73830,-84.59260,-82.60400,-81.71000,
 6-79.30000,-78.00000,-75.02000,-73.05000,-71.62000,-75.59000,
 7-76.69900,-80.63980,-81.09600,-84.50940,-84.86610,-87.90760,
 8-86.19600,-85.92790,-83.68400,-82.92000,-79.95000,-78.74000,
 9-75.54000,-72.20000,-73.69000,-77.83600,-79.23600,-82.98400/
 DATA A5A/
 1-84.28900,-87.68560,-86.47390,-86.34900,-84.83400,-84.25400,
 2-82.26000,-81.23600,-78.63000,-76.83000,-72.94000,-77.94000,
 3-79.48400,-83.61000,-84.85100,-88.76260,-87.89350,-88.45690,
 4-87.14370,-87.26310,-85.66600,-85.42600,-82.93390,-81.27300,
 5-78.36000,-77.09000,-72.90000,-74.28000,-76.41000,-80.98000,
 6-82.65200,-86.63200,-86.45300,-87.20710,-86.36430,-86.78850,
 7-85.60900,-85.60500,-83.51000,-82.86000,-80.19000,-79.40000,
 8-76.20000,-76.20000,-71.81000,-75.01000/
 DATA A6/
 1-80.16500,-82.18800,-86.80840,-86.80900,-88.40990,-87.71339,
 2-88.79590,-87.54020,-88.11090,-85.95600,-86.18510,-83.50400,
 3-83.60000,-80.50000,-80.19000,-76.59000,-78.86000,-83.62300,
 4-84.15000,-86.01200,-85.86000,-87.19500,-86.52000,-87.32800,
 5-85.85000,-86.32500,-84.60000,-84.90000,-82.79000,-82.53000,
 6-79.82000,-77.42000,-82.56900,-83.45000,-86.07300,-86.04000,
 7-88.22300,-87.62020,-89.22190,-87.95570,-89.10020,-87.25300,
 8-88.09400,-85.93000,-86.32300,-83.71000,-83.71000,-78.45000,
 9-79.63000,-82.55000,-83.16600,-85.56800,-85.59200,-87.40200/
 DATA A6A/
 1-86.77800,-88.01600,-86.94400,-87.84700,-86.36200,-86.86000,
 2-85.03000,-85.11000,-82.94000,-77.75000,-81.37000,-82.16300,
 3-85.19000,-85.41200,-87.92700,-87.46300,-89.41100,-88.41300,
 4-89.90200,-88.37300,-89.52600,-87.60600,-88.34000,-86.02000,
 5-86.28000,-76.13000,-77.89000,-81.01000,-82.36700,-84.78000,
 6-85.31100,-87.07800,-86.92800,-88.40800,-87.60500,-88.72150,
 7-87.45550,-88.22400,-86.58000,-87.03500,-85.01000,-84.91000,
 8-82.42000,-75.48000,-79.47000,-80.38000/
 DATA A7/
 1-84.01000,-84.28000,-87.13020,-86.99100,-89.24800,-88.53900,
 2-90.34640,-89.25160,-90.57690,-89.04490,-90.01420,-88.09000,
 3-88.71500,-86.40800,-86.70400,-84.21000,-69.67000,-73.78000,
 4-75.51000,-79.18000,-80.39000,-83.50000,-84.10000,-86.52000,
 5-86.42000,-88.42600,-87.98900,-89.34200,-88.58400,-89.54100,
 6-88.24800,-88.92900,-87.45000,-87.71400,-85.49000,-85.82000,
 7-83.24000,-83.42000,-80.83000,-65.88000,-70.91000,-72.58000,
 8-77.09000,-78.20000,-82.00000,-82.72000,-85.82400,-85.91800,
 9-88.64800,-88.31700,-90.56500,-90.02700,-91.52180,-90.39260/
 DATA A7A/

1-91.64830,-90.06160,-91.09430,-89.20270,-89.93560,-87.80900,
2-88.22900,-85.89000,-86.01300,-83.51000,-83.40000,-63.18000,
3-65.69000,-70.10000,-72.20000,-76.02000,-77.62000,-81.02000,
4-81.85000,-84.41900,-84.87000,-86.99700,-87.02000,-88.64000,
5-87.95300,-89.48300,-88.41400,-89.58990,-88.32560,-89.21910,
6-87.61420,-88.26200,-86.33900,-86.70800,-84.70000,-84.59100,
7-82.35000,-82.09000,-79.59000,-79.00000,-60.05000,-65.29000,
8-67.42000,-72.12000,-73.62000,-77.65000/

DATA A8/

1-78.52000,-82.17000,-82.46000,-85.46000,-85.15000,-87.65000,
2-87.18900,-89.40200,-88.59000,-90.30380,-89.16200,-90.51410,
3-89.02730,-90.06490,-88.28900,-88.98890,-87.00400,-87.34540,
4-85.19100,-85.19300,-82.90000,-82.57000,-77.78000,-71.32000,
5-73.47000,-76.96000,-78.16000,-80.84000,-81.55000,-83.99000,
6-84.10000,-86.22000,-86.16000,-87.96000,-87.35400,-88.87930,
7-87.91400,-88.98140,-87.73510,-88.50300,-86.88800,-87.44320,
8-85.69800,-85.86000,-83.97000,-83.77600,-79.42000,-76.81000,
9-73.66000,-73.66000,-74.77000,-78.25000,-79.00000,-81.90000/

DATA A8A/

1-82.43000,-85.06000,-85.29000,-87.45000,-87.14000,-89.16500,
2-88.31700,-89.86010,-88.69400,-89.88010,-88.41400,-89.27840,
3-87.66000,-88.12300,-86.50200,-86.42300,-82.21300,-80.07000,
4-75.98000,-73.24000,-81.09000,-81.55000,-84.07000,-84.16000,
5-86.22700,-85.95300,-87.59000,-86.85700,-88.05900,-87.17900,
6-88.08700,-86.90600,-87.65900,-86.35600,-86.56100,-82.87000,
7-80.78000,-77.54000,-74.87000,-71.07000,-79.57000,-82.36000,
8-82.73000,-85.25000,-85.15000,-87.29700/

DATA A9/

1-86.71900,-88.45100,-87.57200,-88.96500,-87.86800,-88.90400,
2-87.73400,-88.27400,-84.92600,-83.24100,-79.97000,-77.77000,
3-74.01000,-71.80000,-77.73000,-78.45000,-81.15000,-81.60000,
4-83.76000,-83.74000,-85.67000,-85.25500,-86.83000,-86.03000,
5-87.23000,-86.48000,-87.18600,-84.27600,-82.96900,-79.97000,
6-78.21040,-74.90000,-72.91000,-69.44000,-79.46000,-82.34000,
7-82.37000,-84.75000,-84.53000,-86.46200,-86.03000,-87.53600,
8-86.91100,-88.04200,-85.39900,-84.48700,-81.59300,-80.40300,
9-77.11000,-75.74000,-72.23000,-70.68000,-78.55000,-80.95000/

DATA A9A/

1-81.26000,-83.28000,-83.09900,-84.79900,-84.65400,-85.98000,
2-83.75200,-83.03800,-80.71900,-79.59900,-76.82000,-75.43000,
3-72.48000,-71.38000,-68.66000,-78.80000,-79.28000,-81.80000,
4-82.00000,-84.18000,-84.17500,-85.91600,-83.97000,-83.71600,
5-81.40400,-80.89800,-78.12900,-77.38100,-74.37700,-73.66200,
6-70.89900,-70.12600,-77.50000,-78.28000,-80.45000,-81.10000,
7-82.90100,-81.34000,-81.23400,-79.42100,-79.02300,-76.85200,
8-76.04600,-73.53000,-73.36500,-71.35000/

DATA A10/

1-70.74000,-68.45000,-76.05000,-79.05000,-79.42200,-81.90400,
2-80.59600,-80.94700,-79.24800,-79.31700,-77.11800,-77.03390,
3-74.55300,-74.74900,-72.54400,-72.45100,-70.19300,-69.35900,
4-74.42000,-75.57700,-77.87600,-77.07500,-77.48600,-76.21700,
5-76.36000,-74.71900,-74.62900,-72.86300,-73.34700,-71.71300,
6-71.81800,-70.07200,-69.46100,-67.25000,-65.92000,-63.53000,
7-71.88000,-72.88000,-75.88000,-75.15800,-76.20700,-75.07200,
8-75.72800,-74.16500,-74.69100,-73.10600,-73.69100,-72.06500,
9-72.52400,-70.82100,-70.68000,-68.55300,-67.93400,-65.49400/

DATA A10A/

1-64.29000,-67.78000,-70.56000,-70.59000,-71.37500,-71.06000,
2-71.55700,-70.87100,-71.31000,-70.29000,-71.22000,-70.22000,

3-70.75700,-69.44000,-69.50300,-67.81300,-67.44500,-65.69000,
4-64.67000,-62.59000,-67.79000,-67.48000,-69.10000,-68.55200,
5-70.05700,-69.09000,-70.35600,-69.12100,-70.49100,-69.39400,
6-70.38400,-69.13800,-69.64800,-68.02700,-68.15100,-66.35100,
7-65.93400,-63.57700,-62.56300,-61.58000,-62.00000,-63.50000,
8-63.67000,-64.83200,-64.59800,-65.82000/

DATA A11/

1-65.39000,-66.89000,-66.40700,-67.44000,-66.72800,-67.21000,
2-65.98100,-66.34200,-64.95500,-64.87300,-63.04400,-62.29800,
3-60.20000,-58.75000,-56.39000,-57.90000,-58.20000,-60.43000,
4-60.25000,-62.40000,-62.01000,-63.69000,-62.99000,-64.91000,
5-64.34000,-65.93000,-65.16100,-66.29900,-65.13400,-65.91800,
6-64.50100,-64.90400,-63.26800,-62.96800,-60.89900,-60.09100,
7-57.70000,-56.48000,-53.42000,-50.90000,-51.93000,-53.90000,
8-54.49000,-56.31000,-56.69000,-58.19000,-58.31000,-60.14000,
9-60.13000,-61.64000,-61.60000,-62.71700,-61.95600,-62.93600/

DATA A11A/

1-61.86900,-62.52100,-61.27000,-61.25100,-59.77300,-59.19000,
2-57.36900,-56.21500,-53.87000,-52.28000,-49.34000,-47.30000,
3-50.01000,-50.42000,-53.07000,-53.21000,-55.31000,-55.14000,
4-57.33900,-57.14000,-59.30000,-59.02000,-60.86000,-60.18400,
5-61.60900,-60.56600,-61.54900,-60.34400,-60.74100,-59.28300,
6-59.23900,-57.53500,-56.93390,-54.68100,-53.48500,-50.97500,
7-49.47000,-42.69000,-43.93000,-46.31000,-47.11000,-48.94000,
8-49.53000,-51.64000,-52.20000,-54.22000/

DATA A12/

1-54.46000,-56.18000,-56.11000,-57.50000,-57.19000,-58.07400,
2-57.30100,-57.89000,-56.74000,-56.84500,-55.56200,-55.14900,
3-53.37000,-52.37100,-50.17000,-49.10000,-46.47000,-39.05000,
4-42.18000,-42.74000,-45.23000,-45.54000,-48.20000,-48.62000,
5-51.06000,-51.08000,-53.41000,-53.20000,-55.19000,-54.70000,
6-56.10000,-55.29000,-56.34000,-55.25000,-55.76000,-54.54200,
7-54.55900,-52.86800,-52.42200,-50.45000,-49.76600,-47.38900,
8-45.90000,-43.21900,-41.52000,-42.46000,-44.88000,-45.61000,
9-47.80000,-48.19000,-50.10000,-50.10000,-51.59000,-51.34000/

DATA A12A/

1-52.35000,-51.76000,-52.34000,-51.46000,-51.71000,-50.51000,
2-50.33100,-48.84000,-48.41200,-46.40300,-45.25900,-42.63700,
3-41.38000,-38.58000,-37.78000,-40.61000,-41.40000,-43.99000,
4-44.30000,-46.60000,-46.59000,-48.54000,-48.35000,-49.86000,
5-49.34000,-50.46000,-49.71000,-50.42000,-49.23000,-49.65000,
6-48.22500,-48.20800,-46.32700,-45.66700,-43.34500,-42.47500,
7-39.87000,-38.63400,-35.44000,-33.70000,-34.99000,-37.50000,
8-38.40000,-40.69000,-41.24000,-43.15000/

DATA A13/

1-43.46000,-45.04000,-44.96000,-46.11000,-45.76000,-46.54000,
2-45.86000,-46.43000,-45.34800,-45.77100,-44.06000,-43.77400,
3-41.88100,-41.18100,-38.98300,-37.94200,-35.49000,-34.46000,
4-29.60000,-32.60000,-33.49000,-36.14000,-36.75000,-39.06000,
5-39.34000,-41.36000,-41.41000,-42.96000,-42.74000,-43.96000,
6-43.40000,-44.25000,-43.37000,-44.15800,-42.75900,-42.95800,
7-41.18400,-41.10100,-38.95200,-38.67400,-36.36200,-35.85000,
8-33.36700,-32.39700,-29.85000,-25.23000,-26.62000,-29.30000,
9-30.37000,-32.74000,-33.58000,-35.59000,-35.96000,-37.64000/

DATA A13A/

1-37.86000,-39.10000,-38.95000,-39.97000,-39.44000,-40.26000,
2-39.12700,-39.68000,-38.26800,-38.45000,-36.62000,-36.67200,
3-34.79900,-34.49900,-32.49400,-31.85100,-29.46000,-28.41000,
4-25.51000,-20.84000,-24.00000,-24.97000,-27.85000,-28.68000,

5-31.07000,-31.65000,-33.68000,-33.85000,-35.59000,-35.48000,
6-36.94000,-36.46000,-37.50000,-36.78000,-37.72800,-36.55000,
7-37.29300,-35.67200,-36.25600,-34.43800,-34.73390,-32.78600,
8-32.63500,-30.41400,-29.90600,-27.40600/

DATA A14/

1-26.60000,-23.74000,-21.19000,-22.41000,-24.75000,-25.63000,
2-27.64000,-28.18000,-30.01000,-30.22000,-31.73000,-31.69000,
3-32.87000,-32.49000,-33.41000,-32.87600,-33.87000,-32.76800,
4-33.36000,-32.25600,-32.57200,-31.16200,-31.15000,-29.59100,
5-29.10400,-27.30000,-26.40000,-23.86000,-22.98000,-20.20000,
6-12.65000,-15.93000,-16.80000,-19.86000,-20.79000,-23.21000,
7-23.69000,-26.04000,-26.14000,-28.35000,-28.06000,-29.88000,
8-29.21000,-30.96000,-30.48000,-31.97400,-31.02000,-32.20600,
9-31.05600,-31.84600,-30.73500,-30.96400,-29.55700,-29.51400/

DATA A14A/

1-27.67200,-27.36500,-25.27700,-24.70300,-22.29900,-20.95500,
2-15.83000,-16.90000,-19.11000,-19.86000,-21.93000,-22.29000,
3-24.02000,-24.16000,-25.67000,-25.59000,-27.02000,-26.81000,
4-27.85000,-27.35000,-28.33900,-27.50000,-28.08000,-27.06000,
5-27.18500,-25.98800,-25.76900,-24.35300,-23.83700,-22.26900,
6-21.04100,-16.76800,-13.65000,-9.25100,-11.74000,-14.33900,
7-14.94000,-17.51000,-17.86000,-20.22000,-20.23000,-22.29000,
8-22.07000,-23.81000,-23.55000,-25.15000/

DATA A15/

1-24.63000,-25.90000,-25.98000,-26.16000,-25.32700,-25.94200,
2-24.79400,-25.11700,-23.77700,-23.79500,-22.46300,-21.79500,
3-17.62400,-14.73800,-10.49190,-7.56200,-3.14000,-.18500,
4 -9.87000,-10.85000,-15.05000,-13.67000,-15.56400,-15.98000,
5-17.68000,-17.76000,-19.41000,-19.30000,-20.61000,-20.46000,
6-21.41000,-21.04000,-21.60000,-20.82000,-21.07000,-20.03390,
7-20.05800,-18.87900,-18.26800,-14.80100,-11.86500,-8.13500,
8 -5.24300,-1.20900,1.71000,5.97000,-8.31000,-10.81000,
9-11.06000,-13.21000,-13.23000,-15.07000,-15.05000,-16.74000/

DATA A15A/

1-16.41000,-17.78000,-17.36000,-18.25000,-17.57600,-18.19000,
2-17.15000,-17.47500,-16.37300,-15.96300,-12.44400,-10.38100,
3 -6.63390,-4.47900,-.54000,1.76900,5.96000,8.35460,
4 -4.05000,-6.03000,-6.67000,-8.47000,-8.67000,-10.52000,
5-10.52000,-11.97000,-11.97000,-12.96000,-12.73000,-13.31000,
6-12.64000,-12.88800,-11.97600,-11.63500,-8.62500,-6.58900,
7 -3.38900,-1.26200,2.23700,4.38200,8.99000,10.53000,
8 14.20000,-3.74000,-3.95000,-5.88000/

DATA A16/

1 -6.00000,-7.77000,-7.60000,-8.97000,-8.69000,-9.56000,
2 -8.94000,-9.60800,-8.76100,-8.66600,-5.70600,-4.32800,
3 -1.17900,.24500,3.64900,5.21200,8.83070,10.59900,
4 14.38000,16.37000,3.16000,1.23000,.87000,-1.04000,
5 -1.18000,-2.65000,-2.77000,-3.76000,-3.64000,-4.22000,
6 -3.69000,-3.55600,-.96500,.30900,2.97500,4.30700,
7 7.05000,8.61700,11.47000,13.26500,16.33800,18.38230,
8 21.71000,23.79000,27.46000,29.58000,6.28000,5.98000,
9 3.96000,3.70000,1.93000,1.97000,.61000,.78000/

DATA A16A/

1 -.11000,.29000,.09000,2.53100,3.28500,5.88100,
2 6.66400,9.37700,10.26300,12.95700,14.32100,17.23480,
3 18.81300,21.98730,23.66570,27.18500,28.94100,32.72000,
4 34.56000,9.12000,8.86000,7.40000,7.18000,6.17000,
5 6.14000,5.95000,7.98000,8.70100,10.83700,11.56000,
6 13.74700,14.51800,16.61700,17.82500,20.21900,21.62600,

7 24.30100, 25.85000, 28.89500, 30.72000, 33.76000, 35.91000,
8 39.15000, 12.24000, 10.87000, 10.87000/

DATA A17/

1 10.39000, 12.14100, 12.36200, 14.47000, 14.66300, 16.93400,
2 17.19700, 19.25600, 19.99300, 22.30300, 23.18900, 25.80630,
3 26.75800, 29.58090, 30.86130, 33.81220, 35.44720, 38.73230,
4 40.61200, 44.15000, 21.95900, 22.33900, 23.79800, 24.32000,
5 26.02900, 26.83200, 28.87000, 29.88700, 32.16550, 33.42310,
6 35.93400, 37.48710, 40.34900, 42.32000, 45.54000, 47.64000,
7 51.27000, 27.18600, 28.88000, 29.22100, 31.20100, 31.60700,
8 33.78000, 34.59700, 36.91470, 38.14260, 40.91640, 42.44200,
9 45.38870, 47.30700, 50.57220, 52.71200, 33.75800, 35.23200/

DATA A17A/

1 35.62600, 37.29000, 38.01000, 39.95100, 41.03950, 43.42600,
2 44.86930, 47.45260, 49.30640, 52.21000, 54.31000, 57.52000,
3 38.36200, 40.04200, 40.34200, 42.16000, 42.88900, 45.08700,
4 46.16080, 48.58510, 50.12280, 52.95300, 54.71500, 57.75250,
5 59.80300, 63.15700, 65.29000, 44.46000, 44.65000, 46.02000,
6 46.64000, 48.41700, 49.38900, 51.44300, 52.93220, 55.46270,
7 57.17010, 59.87860, 61.89730, 64.92000, 67.13000, 70.49000,
8 47.89000, 49.17000, 49.39800, 51.09000/

DATA A18/

1 51.71200, 53.69600, 54.80150, 57.17740, 58.44960, 61.00130,
2 62.61600, 65.53000, 67.38900, 70.74800, 72.98600, 54.28000,
3 54.28000, 55.71000, 56.10000, 57.80000, 58.68500, 60.64600,
4 61.81100, 64.02000, 65.48400, 67.99000, 69.84800, 72.95000,
5 72.25000, 78.53000, 58.03000, 59.19000, 59.33200, 60.91000,
6 61.46500, 63.37700, 64.09620, 66.15000, 67.24300, 69.72160,
7 71.16980, 74.13000, 70.03100, 79.29900, 81.34200, 64.80000,
8 65.97000, 66.38000, 67.93000, 68.55000, 70.22000, 71.11600,
9 73.17000, 74.50300, 77.15000, 79.01240, 81.99200, 84.08000/

DATA A18A/

1 87.26000, 0.00000, 0.00000, 0.00000, 0.00000, 0.00000,
2 0.00000, 0.00000, 0.00000, 0.00000, 0.00000, 0.00000,
3 0.00000, 0.00000, 0.00000, 0.00000, 0.00000, 0.00000,
4 0.00000, 0.00000, 0.00000, 0.00000, 0.00000, 0.00000,
5 0.00000, 0.00000, 0.00000, 0.00000, 0.00000, 0.00000,
6 0.00000, 0.00000, 0.00000, 0.00000, 0.00000, 0.00000,
7 0.00000, 0.00000, 0.00000, 0.00000, 0.00000, 0.00000,
8 0.00000, 0.00000, 0.00000, 0.00000/

ZAMASS=AMASS(J)

RETURN

END

FUNCTION ERRMAS(J)

C
C
C

MASS EXCESS ERROR IN MEV.

DIMENSION ERR(1800),

1 E1 (54),E2 (54),E3 (54),E4 (54),E5 (54),E6 (54),E7 (54),
2 E8 (54),E9 (54),E10(54),E11(54),E12(54),E13(54),E14(54),
3 E15(54),E16(54),E17(54),E18(54),
4 E1A(46),E2A(46),E3A(46),E4A(46),E5A(46),E6A(46),E7A(46),
5 E8A(46),E9A(46),E10A(46),E11A(46),E12A(46),E13A(46),E14A(46),
6 E15A(46),E16A(46),E17A(46),E18A(46)

EQUIVALENCE (E1(1),ERR(1)),(E2(1),ERR(101)),

1(E3 (1),ERR(201)),(E4 (1),ERR(301)),(E5 (1),ERR(401)),
1(E6 (1),ERR(501)),(E7 (1),ERR(601)),(E8 (1),ERR(701)),
1(E9 (1),ERR(801)),(E10(1),ERR(901)),(E11(1),ERR(1001)),
1(E12(1),ERR(1101)),(E13(1),ERR(1201)),(E14(1),ERR(1301)),

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1(E15(1),ERR(1401)),(E16(1),ERR(1501)),(E17(1),ERR(1601)),
1(E18(1),ERR(1701))
EQUIVALENCE (E1A(1),ERR(55)),(E2A(1),ERR(155)),
1(E3A (1),ERR( 255)),(E4A (1),ERR( 355)),(E5A (1),ERR( 455)),
1(E6A (1),ERR( 555)),(E7A (1),ERR( 655)),(E8A (1),ERR( 755)),
1(E9A (1),ERR( 855)),(E10A(1),ERR( 955)),(E11A(1),ERR(1055)),
1(E12A(1),ERR(1155)),(E13A(1),ERR(1255)),(E14A(1),ERR(1355)),
1(E15A(1),ERR(1455)),(E16A(1),ERR(1555)),(E17A(1),ERR(1655)),
1(E18A(1),ERR(1755))
DATA E1/
1 13.0, 13.0, 13.0, .1, 500.0, -.1, -.2, -.2, 800.0,
2 -.2, -.3, 50.0, 3.6, 16.0, 50.0, .7, -.8, 1.0,
3 2.0, 500.0, 600.0, 500.0, 5.0, .8, .5, -.6, .7,
4 6.0, 500.0, 100.0, 1.3, .9, -.4, -.3, 1.3, 4.0,
5 500.0, 500.0, 40.0, 5.0, 1.8, 1.1, 0.0, -.2, -.3,
6 .9, 16.0, 500.0, 500.0, 500.0, 5.0, .9, -.1, -.4/
DATA E1A/
1 2.2, 15.0, 30.0, 500.0, 500.0, 500.0, 10.0, .3, 1.0,
2 -.2, -.9, -.3, 2.5, 8.0, 500.0, 500.0, 14.0, .5,
3 .9, -.7, .7, 7.0, 30.0, 170.0, 500.0, 500.0, 50.0,
4 5.0, 1.1, -.4, -1.0, -.5, 2.8, 10.0, 500.0, 70.0,
5 40.0, 9.0, .7, -1.5, 1.5, 9.0, 30.0, 700.0, 500.0,
6 210.0/
DATA E2/
1 16.0, 3.0, 2.7, -1.0, -1.2, -1.0, 1.4, 2.3, 500.0,
2 80.0, 7.0, 1.4, 1.1, -.9, 1.1, 5.0, 40.0, 500.0,
3 500.0, 500.0, 10.0, 3.0, 1.9, -.8, -1.0, -1.1, 1.4,
4 7.0, 500.0, 100.0, 8.0, 8.0, 2.8, -.9, .8, 2.4,
5 200.0, 75.0, 500.0, 500.0, 50.0, 3.0, 11.0, -.7, -1.4,
6 -1.6, .5, -1.5, 30.0, 30.0, 500.0, 500.0, 12.0, 2.9/
DATA E2A/
1 1.9, -.4, 1.0, -.4, 4.0, 18.0, 500.0, 500.0, 500.0,
2 500.0, 3.0, 1.8, -1.1, .8, -.9, 5.0, -.7, 1.3,
3 40.0, 70.0, 500.0, 60.0, 70.0, 500.0, 500.0, 21.0, 1.7,
4 8.0, -.8, -.9, -1.1, 1.7, 10.0, 40.0, 11.0, 16.0,
5 9.0, 500.0, 500.0, 25.0, 16.0, 5.0, -.9, 1.0, -2.2,
6 -2.2/
DATA E3/
1 -2.4, 2.4, -4.0, 4.0, -5.0, 6.0, 9.0, 7.0, 5.0,
2 3.2, 2.8, 6.0, -2.1, 2.2, 2.4, 6.0, 5.0, 16.0,
3 500.0, 6.0, 15.0, 6.0, 3.2, -1.7, -1.6, -1.5, -1.5,
4 -2.6, 5.0, 10.0, 500.0, 500.0, 2.8, 2.2, 3.7, 1.8,
5 -2.9, -1.6, 1.9, 25.0, 100.0, 500.0, 500.0, 28.0, 18.0,
6 10.0, -1.9, 1.8, -2.2, -2.2, -2.3, 6.0, 30.0, 500.0/
DATA E2A/
1 150.0, 3.2, 5.0, 4.0, 2.4, 4.0, -2.6, 2.6, 50.0,
2 110.0, 500.0, 500.0, 17.0, 13.0, 15.0, -2.7, 2.7, -2.5,
3 -2.5, -2.6, 3.7, 30.0, 70.0, 500.0, 500.0, 5.0, 3.3,
4 3.0, 2.6, 3.5, -2.9, 3.0, 18.0, 40.0, 19.0, 500.0,
5 25.0, 500.0, 80.0, 11.0, 7.0, -3.1, 3.0, -3.0, -3.1,
6 -3.2/
DATA E4/
1 3.3, -3.8, 5.0, 30.0, 300.0, 4.0, 11.0, 5.0, 3.8,
2 5.0, -3.3, 3.4, -3.6, 3.7, 8.0, 60.0, 70.0, 500.0,
3 18.0, 200.0, 10.0, 4.0, -3.4, 3.5, -3.6, 3.6, -3.5,
4 3.7, -3.2, 15.0, 7.0, 500.0, 30.0, 15.0, 5.0, 4.0,
5 5.0, -2.9, 3.0, -2.6, 2.8, 40.0, 50.0, 200.0, 500.0,
6 14.0, 50.0, 13.0, 3.8, -1.7, 2.4, -1.7, -1.7, -1.6/
DATA E4A/

```

1 12.0, 1.9, 40.0, 100.0, 210.0, 50.0, 20.0, 7.0, 7.0,
2 15.0, 3.3, -2.4, 2.4, 9.0, 100.0, 50.0, 200.0, 200.0,
3 500.0, 500.0, 18.0, -5.0, 2.6, -2.3, -2.2, -2.2, 6.0,
4 -2.6, 5.0, -6.0, 32.0, 70.0, 500.0, 500.0, 20.0, 500.0,
5 3.6, 4.0, -3.3, 3.1, -5.0, 7.0, 7.0, 50.0, 100.0,
6 400.0/
DATA E5/
1 500.0, 500.0, 500.0, 500.0, 30.0, -5.0, 9.0, -6.0, 100.0,
2 -5.0, -4.0, -3.2, 3.6, -3.9, 9.0, 100.0, 33.0, 90.0,
3 500.0, 50.0, 500.0, 100.0, 27.0, 32.0, 4.0, -3.2, 3.1,
4 -2.6, 15.0, 13.0, 90.0, 150.0, 500.0, 500.0, 500.0, 500.0,
5 30.0, -3.6, 6.0, -2.4, -2.4, -2.4, 4.0, 3.8, 12.0,
6 70.0, 70.0, 230.0, 500.0, 500.0, 30.0, 12.0, 10.0, 7.0/
DATA E5A/
1 5.0, -3.2, 3.3, 6.0, 20.0, 20.0, 200.0, 20.0, 500.0,
2 500.0, 500.0, 500.0, 21.0, 200.0, 4.0, -3.2, -3.1, -2.9,
3 3.7, -3.2, 4.0, -4.0, 16.0, 20.0, 500.0, 500.0, 500.0,
4 500.0, 500.0, 100.0, 6.0, 7.0, 8.0, -3.2, 3.1, 2.3,
5 5.0, 16.0, 100.0, 500.0, 500.0, 500.0, 500.0, 500.0, 500.0,
6 320.0/
DATA E6/
1 7.0, 29.0, -3.0, 4.0, -2.5, -2.2, -2.2, -2.1, -2.2,
2 6.0, -3.2, 19.0, 500.0, 500.0, 500.0, 500.0, 140.0, 14.0,
3 6.0, 11.0, 50.0, 9.0, 200.0, 4.0, 60.0, 25.0, 500.0,
4 100.0, 500.0, 200.0, 500.0, 500.0, 11.0, 11.0, -5.0, 100.0,
5 -4.0, -3.3, -3.3, -2.7, -2.9, 6.0, -5.0, 7.0, 11.0,
6 300.0, 610.0, 500.0, 11.0, 100.0, 11.0, 20.0, 20.0, 18.0/
DATA E6A/
1 7.0, -4.0, 4.0, 6.0, 11.0, 40.0, 600.0, 500.0, 100.0,
2 500.0, 500.0, 28.0, 500.0, 23.0, -9.0, 27.0, -10.0, -5.0,
3 -5.0, 4.0, -8.0, 4.0, -13.0, 50.0, 50.0, 100.0, 500.0,
4 400.0, 22.0, 60.0, 32.0, 21.0, 12.0, -4.0, 4.0, -3.8,
5 3.8, 4.0, 50.0, 20.0, 500.0, 100.0, 500.0, 420.0, 500.0,
6 500.0/
DATA E7/
1 500.0, 100.0, -3.9, 6.0, -3.7, 5.0, -3.1, -3.0, -2.8,
2 -2.7, -2.6, 10.0, -3.0, 14.0, 20.0, 300.0, 500.0, 500.0,
3 500.0, 500.0, 30.0, 150.0, 80.0, 8.0, 50.0, 29.0, 9.0,
4 -9.0, 7.0, -8.0, 8.0, 10.0, 300.0, 38.0, 600.0, 40.0,
5 800.0, 50.0, 500.0, 500.0, 500.0, 500.0, 500.0, 500.0, 500.0,
6 500.0, 17.0, 16.0, -8.0, 12.0, -6.0, -6.0, -3.3, -2.2/
DATA E7A/
1 -2.2, -2.2, -2.2, -3.1, -3.2, 6.0, -4.0, 6.0, 11.0,
2 500.0, 210.0, 500.0, 500.0, 500.0, 500.0, 500.0, 500.0, 500.0,
3 50.0, 32.0, 50.0, 21.0, 40.0, 40.0, 6.0, 20.0, 7.0,
4 2.2, 2.4, -2.6, 2.7, 4.0, 150.0, 7.0, 150.0, 30.0,
5 500.0, 500.0, 500.0, 500.0, 500.0, 500.0, 500.0, 500.0, 500.0,
6 500.0/
DATA E8/
1 500.0, 500.0, 200.0, 110.0, 50.0, 500.0, 20.0, -13.0, 500.0,
2 -3.3, -2.9, -2.8, -2.9, -2.9, 5.0, -3.2, 8.0, -3.7,
3 6.0, 21.0, 110.0, 500.0, 500.0, 500.0, 500.0, 500.0, 500.0,
4 110.0, 500.0, 400.0, 500.0, 500.0, 40.0, 100.0, 10.0, 3.1,
5 6.0, -3.5, 3.7, 6.0, 10.0, 3.2, 15.0, 50.0, 60.0,
6 22.0, 100.0, 500.0, 500.0, 500.0, 500.0, 500.0, 420.0, 500.0/
DATA E8A/
1 500.0, 500.0, 100.0, -140.0, 40.0, -7.0, 5.0, -1.8, -5.0,
2 -1.8, -3.1, -3.1, 8.0, -5.0, 11.0, -5.0, 21.0, 500.0,
3 220.0, 500.0, 500.0, 500.0, 40.0, 500.0, 21.0, 25.0, 500.0,

4 10.0, 7.0, 23.0, -8.0, 7.0, 8.0, 8.0, 7.0, 500.0,
 5 100.0, 100.0, 500.0, 500.0, 500.0, 500.0, 500.0, 500.0, 500.0,
 6 -10.0/
 DATA E9/
 1 18.0, -9.0, 8.0, -7.0, -7.0, -7.0, -7.0, -7.0, 7.0,
 2 15.0, 100.0, 100.0, 500.0, 500.0, 500.0, 500.0, 500.0, 500.0,
 3 40.0, 50.0, 500.0, 26.0, 120.0, 70.0, 500.0, -12.0, -12.0,
 4 12.0, 32.0, 13.0, 0.0, 500.0, 500.0, 500.0, 500.0, 500.0,
 5 500.0, 500.0, 500.0, -31.0, 500.0, -15.0, 19.0, -11.0, 11.0,
 6 -11.0, 12.0, 11.0, 100.0, 120.0, 500.0, 500.0, 500.0, 500.0/
 DATA E9A/
 1 500.0, 500.0, 18.0, 28.0, 12.0, -11.0, 11.0, 11.0, 11.0,
 2 15.0, 100.0, 200.0, 500.0, 200.0, 500.0, 500.0, 500.0, 500.0,
 3 500.0, 40.0, 18.0, -11.0, -11.0, -11.0, -11.0, -11.0, 11.0,
 4 -11.0, 15.0, -11.0, 14.0, 32.0, 500.0, 400.0, 40.0, 100.0,
 5 15.0, 40.0, 13.0, 25.0, 11.0, 15.0, 11.0, 80.0, 15.0,
 6 200.0/
 DATA E10/
 1 100.0, 500.0, 500.0, 120.0, 31.0, -11.0, 11.0, 20.0, -11.0,
 2 -11.0, -11.0, -11.0, 11.0, -11.0, 11.0, -12.0, 12.0, 17.0,
 3 200.0, 32.0, 19.0, 22.0, 14.0, 32.0, 500.0, 21.0, -11.0,
 4 11.0, -11.0, 13.0, 11.0, 14.0, 19.0, 120.0, 50.0, 500.0,
 5 500.0, 500.0, 500.0, 29.0, 12.0, 12.0, 21.0, 15.0, -12.0,
 6 11.0, -12.0, -11.0, -11.0, -11.0, -11.0, 12.0, -12.0, 15.0/
 DATA E10A/
 1 120.0, 500.0, 500.0, 300.0, 19.0, 22.0, 14.0, 32.0, 500.0,
 2 500.0, 20.0, 500.0, 12.0, 13.0, -11.0, 11.0, -12.0, 70.0,
 3 50.0, 100.0, 500.0, 500.0, 500.0, 29.0, 15.0, 15.0, 29.0,
 4 19.0, -16.0, 14.0, -13.0, 11.0, -11.0, 11.0, -11.0, -11.0,
 5 -11.0, 11.0, 12.0, 500.0, 500.0, 500.0, 300.0, 20.0, 23.0,
 6 500.0/
 DATA E11/
 1 500.0, 500.0, 14.0, 500.0, 32.0, 40.0, 32.0, 11.0, 11.0,
 2 -10.0, 10.0, 23.0, 100.0, 100.0, 300.0, 500.0, 500.0, 500.0,
 3 500.0, 500.0, 40.0, 500.0, 500.0, 500.0, 500.0, 500.0, 18.0,
 4 -16.0, 12.0, -13.0, 11.0, -10.0, -10.0, -10.0, 10.0, -11.0,
 5 11.0, 16.0, 300.0, 500.0, 500.0, 500.0, 500.0, 500.0, 500.0,
 6 500.0, 500.0, 500.0, 500.0, 100.0, 100.0, 23.0, 24.0, 32.0/
 DATA E11A/
 1 16.0, 28.0, 60.0, -11.0, 11.0, 11.0, 15.0, 32.0, 40.0,
 2 50.0, 70.0, 500.0, 500.0, 500.0, 500.0, 500.0, 500.0, 500.0,
 3 500.0, 500.0, 500.0, 500.0, 500.0, 38.0, 26.0, 20.0, -16.0,
 4 16.0, -11.0, -11.0, -11.0, -11.0, -11.0, 11.0, -12.0, 14.0,
 5 500.0, 500.0, 500.0, 500.0, 500.0, 500.0, 500.0, 500.0, 500.0,
 6 500.0/
 DATA E12/
 1 500.0, 500.0, 500.0, 70.0, 80.0, 34.0, 23.0, 500.0, 500.0,
 2 32.0, 13.0, 11.0, 11.0, 11.0, 50.0, 40.0, 100.0, 500.0,
 3 500.0, 500.0, 500.0, 500.0, 500.0, 500.0, 500.0, 500.0, 500.0,
 4 500.0, 500.0, 200.0, 500.0, 500.0, 500.0, 500.0, 31.0, 14.0,
 5 12.0, 11.0, 11.0, 11.0, 11.0, 12.0, 200.0, 30.0, 500.0,
 6 500.0, 500.0, 500.0, 500.0, 500.0, 500.0, 500.0, 500.0, 500.0/
 DATA E12A/
 1 500.0, 500.0, 500.0, 200.0, 12.0, 100.0, 19.0, -25.0, -12.0,
 2 12.0, 16.0, 32.0, 100.0, 60.0, 500.0, 500.0, 500.0, 500.0,
 3 500.0, 500.0, 500.0, 500.0, 500.0, 500.0, 500.0, 500.0, 500.0,
 4 100.0, 500.0, -200.0, 16.0, -12.0, -12.0, -12.0, 13.0, -13.0,
 5 13.0, 13.0, 200.0, 500.0, 500.0, 500.0, 500.0, 500.0, 500.0,
 6 500.0/

DATA E13/
1 500.0, 500.0, 500.0, 500.0, 210.0, 500.0, 200.0, 500.0, 24.0,
2 15.0, 500.0, -13.0, 13.0, -13.0, 13.0, 24.0, 200.0, 500.0,
3 500.0, 500.0, 500.0, 500.0, 500.0, 500.0, 500.0, 500.0, 500.0,
4 500.0, 500.0, 500.0, 500.0, 500.0, 500.0, -22.0, 13.0, -13.0,
5 -13.0, -13.0, -13.0, -13.0, 13.0, -14.0, 21.0, 20.0, 500.0,
6 500.0, 500.0, 500.0, 500.0, 500.0, 500.0, 500.0, 500.0, 500.0/
DATA E13A/
1 500.0, 500.0, 500.0, 500.0, 190.0, 500.0, 24.0, 500.0, 16.0,
2 500.0, 150.0, -14.0, 14.0, -20.0, 20.0, 28.0, 60.0, 200.0,
3 300.0, 500.0, 500.0, 500.0, 500.0, 500.0, 500.0, 500.0, 500.0,
4 500.0, 500.0, 500.0, 500.0, 500.0, 500.0, 500.0, 19.0, 500.0,
5 -24.0, 20.0, -14.0, 20.0, -19.0, -13.0, -13.0, 11.0, -21.0,
6 26.0/
DATA E14/
1 500.0, 110.0, 500.0, 500.0, 500.0, 500.0, 500.0, 500.0, 500.0,
2 500.0, 500.0, 500.0, 500.0, 500.0, 500.0, 26.0, 50.0, 17.0,
3 500.0, 16.0, 6.0, 9.0, 6.0, 6.0, 6.0, 50.0, 100.0,
4 200.0, 500.0, 300.0, 500.0, 500.0, 500.0, 500.0, 500.0, 500.0,
5 500.0, 500.0, 500.0, 500.0, 500.0, 500.0, 500.0, 80.0, 70.0,
6 500.0, 500.0, 26.0, 50.0, 10.0, 21.0, 6.0, 6.0, 6.0/
DATA E14A/
1 6.0, 6.0, 6.0, 6.0, 8.0, 21.0, 500.0, 500.0, 500.0,
2 500.0, 500.0, 500.0, 500.0, 310.0, 210.0, 500.0, 500.0, 500.0,
3 210.0, 500.0, 500.0, 80.0, 220.0, 10.0, 16.0, 18.0, 6.0,
4 6.0, 5.0, 5.0, 6.0, 6.0, 15.0, 13.0, 500.0, 500.0,
5 500.0, 500.0, 500.0, 500.0, 500.0, 500.0, 500.0, 500.0, 500.0,
6 500.0/
DATA E15/
1 500.0, 500.0, 90.0, 500.0, 35.0, 11.0, 10.0, 6.0, 6.0,
2 5.0, 5.0, 5.0, 5.0, 5.0, 3.8, 6.0, 500.0, 3.3,
3 500.0, 500.0, 500.0, 500.0, 500.0, 310.0, 210.0, 500.0, 500.0,
4 500.0, 500.0, 500.0, 500.0, 500.0, 50.0, 500.0, 9.0, 12.0,
5 8.0, 5.0, 5.0, 5.0, 6.0, 6.0, 11.0, 12.0, 100.0,
6 500.0, 500.0, 500.0, 500.0, 500.0, 500.0, 500.0, 500.0, 500.0/
DATA E15A/
1 500.0, 500.0, 90.0, 500.0, 35.0, 11.0, 11.0, 6.0, 7.0,
2 5.0, 5.0, 5.0, 7.0, 5.0, 3.7, 6.0, 500.0, 3.3,
3 500.0, 500.0, 310.0, 210.0, 500.0, 500.0, 500.0, 500.0, 500.0,
4 500.0, 500.0, 50.0, 500.0, 9.0, 12.0, 11.0, 6.0, 13.0,
5 6.0, 7.0, 6.0, 12.0, 13.0, 80.0, 500.0, 500.0, 500.0,
6 500.0/
DATA E16/
1 500.0, 500.0, 500.0, 500.0, 500.0, 500.0, 35.0, 12.0, 11.0,
2 7.0, 11.0, 11.0, 10.0, 11.0, 8.0, 5.0, 3.7, 6.0,
3 500.0, 3.3, 310.0, 210.0, 500.0, 500.0, 500.0, 500.0, 500.0,
4 500.0, 500.0, 50.0, 500.0, 11.0, 13.0, 13.0, 14.0, 14.0,
5 6.0, 9.0, 8.0, 12.0, 21.0, 3.7, 500.0, 500.0, 339.0,
6 100.0, 500.0, 500.0, 500.0, 500.0, 500.0, 500.0, 500.0, 90.0/
DATA E16A/
1 500.0, 35.0, 13.0, 12.0, 11.0, 13.0, 14.0, 14.0, 15.0,
2 9.0, 9.0, 3.7, 6.0, 3.6, 3.3, 20.0, 5.0, 500.0,
3 500.0, 500.0, 500.0, 500.0, 500.0, 500.0, 500.0, 50.0, 500.0,
4 15.0, 16.0, 16.0, 17.0, 18.0, 7.0, 11.0, 8.0, 12.0,
5 3.8, 3.1, 5.0, 150.0, 500.0, 100.0, 500.0, 500.0, 500.0,
6 90.0/
DATA E17/
1 500.0, 36.0, 16.0, 24.0, 23.0, 14.0, 16.0, 17.0, 18.0,
2 11.0, 6.0, 3.7, 6.0, 3.4, 2.9, 3.0, 2.3, 2.4,

```

3  4.0, 500.0, 35.0, 19.0, 20.0, 21.0, 12.0, 10.0, 9.0,
4 13.0, 3.7, 3.1, 12.0, 2.4, 5.0, 100.0, 200.0, 50.0,
5 300.0, 34.0, 500.0, 21.0, 11.0, 6.0, 50.0, 6.0, 3.3,
6  2.4, 2.4, 2.3, 2.5, 2.2, 2.2, 5.0, 29.0, 24.0/
  DATA E17A/
1 13.0, 500.0, 500.0, 9.0, 2.6, 10.0, 2.3, 2.3, 3.0,
2 60.0, 100.0, 500.0, 23.0, 23.0, 8.0, 60.0, 6.0, 6.0,
3  2.4, 2.4, 2.3, 2.3, 2.3, 3.5, 5.0, 30.0, 50.0,
4 500.0, 500.0, 500.0, 500.0, 32.0, 5.0, 20.0, 2.3, 2.7,
5  3.2, 3.1, 3.6, 50.0, 500.0, 500.0, 500.0, 500.0, 39.0,
6 500.0/
  DATA E18/
1  6.0, 6.0, 2.4, 2.6, 2.3, 2.9, 3.4, 5.0, 6.0,
2  8.0, 12.0, 500.0, 500.0, 500.0, 500.0, 500.0, 6.0, 21.0,
3  2.9, 500.0, 6.0, 500.0, 3.5, 5.0, 500.0, 500.0, 500.0,
4 500.0, 33.0, 500.0, 6.0, 6.0, 3.1, 500.0, 31.0, 3.0,
5  3.5, 5.0, 6.0, 10.0, 12.0, 500.0, 500.0, 500.0, 500.0,
6 31.0, 500.0, 7.0, 500.0, 8.0, 500.0, 3.5, 6.0, 500.0/
  DATA E18A/
1 500.0, 0.0, 0.0, 0.0, 0.0, 0.0, 0.0, 0.0, 0.0,
2  0.0, 0.0, 0.0, 0.0, 0.0, 0.0, 0.0, 0.0, 0.0,
3  0.0, 0.0, 0.0, 0.0, 0.0, 0.0, 0.0, 0.0, 0.0,
4  0.0, 0.0, 0.0, 0.0, 0.0, 0.0, 0.0, 0.0, 0.0,
5  0.0, 0.0, 0.0, 0.0, 0.0, 0.0, 0.0, 0.0, 0.0,
6  0.0/
  ERRMAS=ERR(J)
  RETURN
  END

```

```

*****
*                               SUBROUTINE MASSIV                               *
*****
  SUBROUTINE MASSIV(IM9)
  COMMON/MASOUT/WDIS(990),KPREN(990),KPREP(990),KEQD(990),KEQT(990)
  *,KEQHE(990),KEQAL(990),KSUMN(990),KSUMP(990),KREACT(990),
  * KPREA(990),KN
  COMMON/INTTR1/PWX,PWY,PWZ,TW,NPREN,NPREP,NPREA
  COMMON/EVAMAS/NEVAN,NEVAP,NEVAD,NEVAT,NEVAHE,NEVAAL
  COMMON/CFUMAS/CF /INF/INFBIG,INFSO
  COMMON/INFSEP/KSEP(100,4),INFSEP,JSEPM
  IM9=0
  IF(INFBIG.EQ.0)GOTO 200
  I=1
10 IF(KPREN(I).EQ.NPREN)GOTO 18
11 IF(I-KN)12,100,100
12 I=I+1
  GOTO 10
18 IF(KSUMN(I).EQ.(NPREN+NEVAN))GOTO 20
  GOTO 11
20 IF(KPREP(I).EQ.NPREP)GOTO 27
  GOTO 11
27 IF(KPREA(I).EQ.NPREA)GOTO 28
  GOTO 11
28 IF(KSUMP(I).EQ.(NPREP+NEVAP))GOTO 30
  GOTO 11
30 IF(KEQAL(I).EQ.(NEVAAL+NPREA))GOTO 40
  GOTO 11
40 IF(KEQD(I).EQ.NEVAD)GOTO 50
  GOTO 11
50 IF(KEQT(I).EQ.NEVAT)GOTO 60

```



```

        GOTO 11
    60 IF(KEQHE(I).EQ.NEVAHE)GOTO 70
        GOTO 11
    70 KREACT(I)=KREACT(I)+1
        WDIS(I)=WDIS(I)+CF
        IF(INFSEP.NE.0)CALL CHESEP
        RETURN
C
    100 KN=KN+1
        IF(KN.GT.990)GOTO 101
        KPREN(KN)=NPREN
        KPREP(KN)=NPREP
        KPREA(KN)=NPREA
        KEQD(KN)=NEVAD
        KEQT(KN)=NEVAT
        KEQHE(KN)=NEVAHE
        KEQAL(KN)=NEVAAL + NPREA
        KSUMN(KN)=NEVAN+NPREN
        KSUMP(KN)=NEVAP+NPREP
        KREACT(KN)=1
        WDIS(KN)=CF
        IF(INFSEP.NE.0)CALL CHESEP
        RETURN
C
    200 KN=1
        KPREN(KN)=NPREN+KPREN(KN)
        KPREP(KN)=NPREP+KPREP(KN)
        KPREA(KN)=NPREA+KPREA(KN)
        KEQD(KN)=NEVAD+KEQD(KN)
        KEQT(KN)=NEVAT+KEQT(KN)
        KEQHE(KN)=NEVAHE+KEQHE(KN)
        KEQAL(KN)=NEVAAL+KEQAL(KN) + NPREA
        KSUMN(KN)=NEVAN+NPREN+KSUMN(KN)
        KSUMP(KN)=NEVAP+NPREP+KSUMP(KN)
        KREACT(KN)=1+KREACT(KN)
        WDIS(KN)=CF+WDIS(KN)
        IF(INFSEP.NE.0)CALL CHESEP
        RETURN
C
    101 PRINT 102,KN
    102 FORMAT(1X,' SUBROUTINE MASSIV. KN =',i5,' EXCEEDS LIMIT')
        KN=KN-1
                IM9=1
        RETURN
        END
*****
*                SUBROUTINE MEMDEC                *
*****
        SUBROUTINE MEMDEC(I)
        COMMON/PARTIC/WP,PX,PY,PZ,P,T,E,X,Y,Z,R,JIN,M
        COMMON/PARTL7/WP1,PX1,PY1,PZ1,P1,T1,E1,X1,Y1,Z1,R1,JIN1,M1
        GOTO(1,2),I
1         WP1  =WP
           PX1  =PX
           PY1  =PY
           PZ1  =PZ
           P1   =P
           T1   =T
           E1   =E

```

```

X1  =X
Y1  =Y
Z1  =Z
R1  =R
JIN1 =JIN
M1  =M
RETURN
2   IF(M1.ne.3) goto 3
    WP  =WP1
    PX  =PX1
    PY  =PY1
    PZ  =PZ1
    P    =P1
    T    =T1
    E    =E1
    X    =X1
    Y    =Y1
    Z    =Z1
    R    =R1
    JIN  =JIN1
    M    =M1
    M1   =0
    RETURN
3   Write(6,4)M1
    Write(8,4)M1
4   Format(1x,'ERROR IN MEMDEC      M1=',i3)
    Stop
    END
*****
*           SUBROUTINE MEMEQU                               *
*****
      SUBROUTINE MEMEQU(E,MP)
C Evaporation
C Store characteristics of particles emitted from nucleus
COMMON/EMEM/EMEM0(21),EMEM(21),RMEM(21,3),RMEM0(21,3),HMEM
COMMON/EOUT/SPE(19,5,3),PI(19),EOUT1(5,3),EOUT2(5,3),MSPE
COMMON/IX190/IX191,IX192,IX193
COMMON/DATINI/RA,T0,W0 /MAIIPR/IPR
COMMON/SPEFUL/ANGLIM(9,2,3),ANGSUM(21,9,3),ANGCEN(9,3),DCEN,MANG
COMMON/TR1TR2/VX,VY,VZ /URAND1/IYG
C Transition to LCS
WP=WM(MP)
PP=SQRT( E *(E +2.*WP) )
CC=RANDOM(0)
  QCOS=1.-2.*CC
  QSIN=SQRT(ABS(1.-QCOS*QCOS))
  CC=RANDOM(0)
  FI=6.2831852*CC
PWX=PP*QSIN*COS(FI)
PWY=PP*QSIN*SIN(FI)
PWZ=PP*QCOS
  PWX=PWX+WP*VX
  PWY=PWY+WP*VY
  PWZ=PWZ+WP*VZ
QCOS=PWZ/SQRT(PWX*PWX+PWY*PWY+PWZ*PWZ)
C
  TW=E
  DO 1 NU=1,21
  IF(TW.LE.EMEM(NU))GOTO 2

```

```

1      CONTINUE
      IX191=IX191+1
      WRITE(IPR,87)TW
87     FORMAT(1X,' CONTROL MEMEQ ( ENERGY )', ' TW=',E14.5)
      IF (IX191.GT.10000)STOP
      RETURN
C
2      RMEM(NU,MP)=RMEM(NU,MP)+1.
C
      DO 7 ICEN=1,MANG
      IF(QCOS.LE.ANGLIM(ICEN,1,MP).AND.QCOS.GE.ANGLIM(ICEN,2,MP))
*     ANGSUM(NU,ICEN,MP) = ANGSUM(NU,ICEN,MP) + 1.
7      CONTINUE
C
C Total angular distribution for given TW interval
      DO 1000 L=1,MSPE
      IF(TW.GE.EOUT1(L,MP).AND.TW.LE.EOUT2(L,MP))GOTO 10
      GOTO 1000
10     DO 93 NANG=1,18
      IF(QCOS.GE.PI(NANG+1))GOTO 97
93     CONTINUE
      IX192=IX192+1
      WRITE(IPR,96)QCOS
96     FORMAT(1X,' CONTROL MEMEQ (ANGULAR) ', 'QCOS=',E14.5)
      IF (IX192.GT.10000)STOP
      RETURN
97     SPE(NANG,L,MP)=SPE(NANG,L,MP)+1.
1000  CONTINUE
      RETURN
      END
*****
*           SUBROUTINE MEMIN                               *
*****
      SUBROUTINE MEMIN
      COMMON/NDIM/N /SCIMEM/WP,PX,PY,PZ,P,T,E,X,Y,Z,R,JIN,M
      COMMON/MEMORY/U(11,20),MU(2,20) /MAIIPR/IPR
      N=N+1
      IF(N.GT.20)GOTO 10
      U(1,N)=WP
      U(2,N)=PX
      U(3,N)=PY
      U(4,N)=PZ
      U(5,N)=P
      U(6,N)=T
      U(7,N)=E
      U(8,N)=X
      U(9,N)=Y
      U(10,N)=Z
      U(11,N)=R
      MU(1,N)=JIN
      MU(2,N)=M
      RETURN
10    PRINT 20,N
      WRITE(IPR,20)N
20    FORMAT(1X,' SUBR MEMIN. ARRAYS LIMIT EXCEEDED. N=',I4)
      STOP
      END
*****
*           SUBROUTINE MEMOUT                               *
*****

```

```

*****
SUBROUTINE MEMOUT
COMMON/NDIM/N /MEMORY/U(11,20),MU(2,20)
COMMON/PARTIC/WP,PX,PY,PZ,P,T,E,X,Y,Z,R,JIN,M
WP=U(1,N)
PX=U(2,N)
PY=U(3,N)
PZ=U(4,N)
P=U(5,N)
T=U(6,N)
E=U(7,N)
X=U(8,N)
Y=U(9,N)
Z=U(10,N)
R=U(11,N)
JIN=MU(1,N)
M=MU(2,N)
N=N-1
RETURN
END
*****
* SUBROUTINE MEMPRE *
*****
SUBROUTINE MEMPRE(M,P1,P2,P3,T)
C Pre-equilibrium (cascade)
C Store characteristics of particles emitted from nucleus
COMMON/EMEM/EMEM0(21),EMEM(21),RMEM(21,3),RMEM0(21,3),HMEM
COMMON/EOUT/SPE(19,5,3),PI(19),EOUT1(5,3),EOUT2(5,3),MSPE
COMMON/IX190/IX191,IX192,IX193 /DATINI/RA,T0,W0
COMMON/MAIIPR/IPR /INFDIS/INFDIS,INFOUP(3)
COMMON/SPEFUL/ANGLIM(9,2,3),ANGSUM(21,9,3),ANGCEN(9,3),DCEN,MANG
MP=M
IF(INFOUP(MP).NE.1)RETURN
PWX=P1
PWY=P2
PWZ=P3
TW=T
QCOS=PWZ/SQRT(PWX*PWX+PWY*PWY+PWZ*PWZ)
DO 1 NU=1,21
IF(TW.LE.EMEM0(NU))GOTO 2
1 CONTINUE
IX191=IX191+1
C IF(IX191.GT.1000)STOP
WRITE(IPR,87)TW
87 FORMAT(1X,'CONTROL MEMPRE ( ENERGY )', ' TW=',E14.5)
RETURN
2 RMEM0(NU,MP)=RMEM0(NU,MP)+1.
C
DO 7 ICEN=1,MANG
IF(QCOS.LE.ANGLIM(ICEN,1,MP).AND.QCOS.GE.ANGLIM(ICEN,2,MP))
* ANGSUM(NU,ICEN,MP) = ANGSUM(NU,ICEN,MP) + 1.
7 CONTINUE
C
C Total angular distribution for interval TW
DO 1000 L=1,MSPE
IF(TW.GE.EOUT1(L,MP) .AND. TW.LE.EOUT2(L,MP)) GOTO 10
GOTO 1000
10 DO 93 NANG=1,18
IF(QCOS.GE.PI(NANG+1))GOTO 97

```

```

93 CONTINUE
    IX192=IX192+1
C    IF (IX192.GT.10) STOP
    WRITE (IPR,96) QCOS
96  FORMAT (1X, 'CONTROL MEMPRE (ANGULAR) ', 'QCOS=', E14.5)
    RETURN
97  SPE (NANG, L, MP) = SPE (NANG, L, MP) + 1.
1000 CONTINUE
    RETURN
    END
*****
*          SUBROUTINE MODEL          *
*****
    SUBROUTINE MODEL (IXX)
    COMMON /NPROL/ NPROL
    COMMON /JACT/ JACT
    CALL ZERO2
    CALL INIPAR
1   CALL INTPOP (IKS, INT9)
        IF (INT9.NE.0) GOTO 10
    IF (IKS) 4, 2, 3
2   CALL MEMOUT
    GOTO 1
3   CALL ACTIN (IKS)
    IF (IKS) 4, 2, 1
4   IF (JACT) 6, 5, 6
5   NPROL=NPROL+1

        IXX=2
        RETURN

6   CALL TREAT1
    CALL EVAPAR
    CALL TREAT2
    CALL CFUN
    CALL MASSIV (IM9)
        IF (IM9.NE.0) GOTO 20
        IXX=2
        RETURN

10  IXX=1
    RETURN

20  IXX=3
    RETURN

    END
*****
*          SUBROUTINE NADRAW          *
*****
    SUBROUTINE NADRAW (T, QCOS, FI)
    COMMON /URAND1/ IYG
    CC=RANDOM (0)
    FI=6.2831852*CC
    CC=RANDOM (0)
    DSDOM=-0.238*ALOG (T)+1.91
10  CC=RANDOM (0)
    CC1=RANDOM (0)
    TETA=CC*180.
    CALL OSTROU (T, TETA, DSDO)
    DSDO=DSDO*SIN (TETA*3.1415926/180.)
    IF ( DSDO - DSDOM*CC1 ) 10, 20, 20
20  QCOS=COS (TETA*3.1415926/180.)
    RETURN

```

```

      END
*****
*                SUBROUTINE NPDRAW                *
*****
      SUBROUTINE NPDRAW(QCOS,FI)
      COMMON/FIGA1B/T1(16),BA1(16),BB1(16),BB2(9),BB3(8)
      COMMON/ACTA1B/TREST /A1BNPD/S(4),PAR1
      COMMON/URAND1/IYG
      CALL A1B1B2
      CC=RANDOM(0)
      DO 10 I=1,4
      IF(CC.LE.S(I))GOTO 20
10  CONTINUE
      PRINT 12,CC,(S(I),I=1,4)
      WRITE(1,12)CC,(S(I),I=1,4)
      WRITE(8,12)CC,(S(I),I=1,4)
      WRITE(12,12)CC,(S(I),I=1,4)
12  FORMAT(1X,'CONTROL NPDRAW'/1X,5G15.8)
      I=4
20  CC=RANDOM(0)
      FI=6.2831852*CC
      CC=RANDOM(0)
      GOTO(30,40,50,60),I
30  QCOS=1.-CC
      RETURN
40  QCOS=ABS(1.-CC)**0.25
      RETURN
50  QCOS=-CC
      RETURN
60  QCOS=-(ABS(CC)**PAR1)
      RETURN
      END
*****
*                SUBROUTINE NRT_COEFF            *
*****
      Subroutine NRT_COEFF(Z1,Z2,A1,A2,ANRT,BNRT,GNRT)
      PI=3.1415926
      A0=0.52918E-08      ! Bohr radius, cm
      EL=4.8E-10         ! electron charge
C Classical NRT, Nucl.Eng.Des., 1975 :
C      RK0=0.1337*(Z1**(1./6.))*SQRT(Z1/A1)
C Robinson
      RK0=0.0793*(Z1**0.6666666)*SQRT(Z2)*((A1+A2)**1.5)/      (
#      (A1**1.5)*SQRT(A2)*((Z1**0.666666666+Z2**0.666666666)**0.75) )
      AA=A0*( (9.*Pi*Pi/128.))**0.333333333 )/
#      SQRT(Z1**0.6666666+Z2**0.6666666)
      E0=Z1*Z2*(EL**2)*(A1+A2)/(AA*A2)
      E0=E0/1.6E-06      ! erg ---> MeV
      E0=1000.*E0       !      ---> keV
      EE=1./E0
      ANRT=RK0*EE
      BNRT=0.40244*RK0*(EE**0.75)
      GNRT=3.4008*RK0*(EE**0.166666666)
      RETURN
      END
*****
*                SUBROUTINE OPEN_OUTPUT_FILES    *
*****
      SUBROUTINE OPEN_OUTPUT_FILES(NAMRD)

```

```

CHARACTER NAMRD*8
CHARACTER*12 NAM1,NAM7N,NAM7P,NAM7A,NAM8,NAM10,NAM12,NAM14
      Nam1 =Namrd//'.sho'
      Nam7n=Namrd//'.nnn'
      Nam7p=Namrd//'.ppp'
      Nam7a=Namrd//'.aaa'
      Nam8 =Namrd//'.ful'
      Nam10=Namrd//'.mlt'
      Nam12=Namrd//'.lib'
      Nam14=Namrd//'.alp'
open(1,file=Nam1)
open(71,file=Nam7n)
open(72,file=Nam7p)
open(73,file=Nam7a)
open(8,file=Nam8)
open(10,file=Nam10)
open(12,file=Nam12)
open(14,file=Nam14)
      open(33,file='d2sdedo.7r')
Return
End
*****
*
*          SUBROUTINE OPTIONS
*
*****
      SUBROUTINE OPTIONS(IPR,BONNE,IWRI,INFKAL)
      COMMON/K1996/K1996 /I1988/I1988 /I1990/I1990
      COMMON/R1R2/E1E2(200),IR1R2
      COMMON/IMOM/IMOM /ICHEN/ICHEN /URAND1/IYG
      COMMON/INFGAS/INFGAS
*
* IPR is the number of unit for general output file
      IPR=8
*
      I1988=0
      I1990=0
          IR1R2=1
C
C IMOM:limitation on orbital momenta (according to Bunakov et al)
C   : 0 - no, 1=yes
      IMOM=1
C ICHEN =0 is not used now
      ICHEN=1
      BONNE=0.01
      IWRI=1
C IYG for URAND pseudo random number generator
      IYG=1995
C INFGAS: calculation of total production cross-section for
C   particles with 0 < Z < 4: 0-no, 1=yes
      INFGAS = 1
C
C INFKAL: calculation of angular distributions for pre-equilibrium
C   particles for recoil spectra calculation (primary particle
C   energy T0 < 60 MeV)
C   = 0 - INC model
C   = 1 - old Kalbach, Mann approximation (not tested)
      INFKAL = 0
      IF(IPR.NE.IWRI)GOTO 1788
      PRINT 1789,IWRI
      WRITE(IPR,1789)IWRI

```

```

      STOP
1788  continue
*
* See Subr DISTPA
      K1996=0
*
      Return
1789  FORMAT(1X,' Bad unit:  IWRI=IPR=',I5)
      End
*****
*                FUNCTION ORBIT                *
*****
      FUNCTION ORBIT(PX,PY,PZ,X,Y,Z)
      RI=Y*PZ-Z*PY
      RJ=Z*PX-X*PZ
      RK=X*PY-Y*PX
      ORBIT=SQRT(RI*RI+RJ*RJ+RK*RK)
      RETURN
      END
*****
*                SUBROUTINE OSTROU                *
*****
* Data are correct only for T < 300 MeV
      SUBROUTINE OSTROU(T,TETA,DSDO)
* TETA in degrees
      C = 1.44465E-06 * (TETA**3) + 1.07744E-04*(TETA**2) -
      c 8.87089E-02 * TETA + 6.74152
      IF(30.GT.TETA) RK = (0.12/30.)*TETA
      IF(30.LE.TETA .AND. TETA.LE.165. )
      c RK = -1.45194E-10*(TETA**5) + 6.68681E-08 *(TETA**4) -
      c 1.05389E-05*(TETA**3) + 6.10544E-04*(TETA**2) -
      c 3.87393E-03 *TETA - 7.76363E-02
      IF(TETA.GT.165. )
      c RK = -1.45194E-10*(165.**5) + 6.68681E-08 *(165.**4) -
      c 1.05389E-05*(165.**3) + 6.10544E-04*(165.**2) -
      c 3.87393E-03 *165. - 7.76363E-02
      SQRTT = SQRT(T)
      DSDO = C * EXP(-RK*SQRTT)
      RETURN
      END
*****
*                SUBROUTINE OUTPUT                *
*****
      SUBROUTINE OUTPUT
      REAL*8 INFGEN
      COMMON/MASOUT/WDIS(990),KPREN(990),KPREP(990),KEQD(990),KEQT(990)
      +,KEQHE(990),KEQAL(990),KSUMN(990),KSUMP(990),KREACT(990),
      + KPREA(990),KN /DATOUT/SGEOM,FOUT /DATINI/RA,T0,W0 /KHIST/KHIST
      COMMON/NPROL/NPROL /DATPAU/BONCUT(3) /IMOM/IMOM /R001/R001
      COMMON/R003/R003 /R005/R005 /NREJ/REFR,NREJ /R1R2/E1E2(200),IR1R2
      COMMON/CSABS/CSABS,FIALP2 /XPARAM/XPARAM,FIALPH /ICHEN/ICHEN
      COMMON/TEMP2/BONNE /EVA/PARALP,PARPRO /I1988/I1988
      COMMON/MAIIPR/IPR /INFDIS/INFDIS,INFOUP(3) /INF/INFBIG,INFSO
      COMMON/MPARIN/MPARIN /AN/AN /IDOPCS/IDOPCS
      COMMON/INIQBO/Z,CKA,CKB,RPA,RPB,RALA,RALB /INFGEN/INFGEN(9)
      COMMON/IWRI/IWRI /AUXIL/ICOU1,ICOU2 /INF000/INFGAS
      COMMON/INF001/INFKAL /INF002/INFDOS /I1990/I1990 /INF003/INFDEN
      COMMON/INF004/KHIST0 /INFBON/IBOND /BOND1/QBON(200,200,6)
      COMMON/INF005/INFDM /SUM90/ER90,KER90 /INFSEP/KSEP(100,4),INFSEP,

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+JSEPM /LIB91/WINLIB(100,250),INFLIB /FICAP/FICAP,MZONA
COMMON/EDEFF/Ed
REAL*8 ITYP(3),ICS(4),ITYP1(3)
DIMENSION DREACT(990),M1(990),M5(990),MREACT(990)
DIMENSION CSNON(4),CSDNON(4),CSN(4),CSP(4),CSA(4)
DIMENSION CSD(4),CST(4),CSH(4)
      DATA ITYP/' NEUTRON',' PROTON',' ALPHA'/
      DATA ITYP1/'NEUTRON ','PROTON ',' ALPHA '/
      DATA ICS/' BARASH ','GEOMETRY',' OPTIC ','CHAT-JEE'/
C KPREA(i) is sum of non-equilibrium alpha-particles
C KEQAL(i) is sum of non-eq and evaporated alphas
      DO 111 I=1,KN
111  M5(I)=1
          X=FLOAT(KHIST)
          SGX=SGEOM/X
          SELA=SGX*FLOAT(NPROL)
          WRITE(IPR,499)(INFGEN(I),I=1,9)
          WRITE(IPR,500)Z,AN,ITYP(MPARIN),T0
          IF(KHIST0.NE.KHIST)WRITE(IPR,503)KHIST0
          WRITE(IPR,501)KHIST,SGEOM,SELA
          XPARA9=1./XPARAM
          IF(INFBIG.EQ.0)WRITE(IPR,131)XPARA9,ED*1000.
          IF(INFBIG.EQ.0)GOTO 200
          WRITE(IPR,444)R001
          WRITE(IPR,555)R003
          WRITE(IPR,888)R005
          WRITE(IPR,889)NREJ,REFR
          RCOU3=(FLOAT(ICOU2)/FLOAT(ICOU1))*100.
          WRITE(IPR,8890)RCOU3
          WRITE(IPR,439)PARALP,PARPRO
          IF(IMOM.EQ.1)WRITE(IPR,333)
          IF(ICHEN.EQ.2)WRITE(IPR,334)
          WRITE(IPR,887)I1988
          WRITE(IPR,8888)I1990
          XPAR22=1./XPARAM
          WRITE(IPR,10)FOUT,BONCUT(1),BONCUT(2),BONCUT(3),XPAR22,BONNE,KN
          WRITE(IPR,101)FIALP2,FICAP,MZONA
200      R=1.
          REASUM=0.
          DISSUM=0.
          DO 11 I=3,4
          CSNON(I)=0.
11      CSDNON(I)=0.
          DO 12 I=1,KN
          REASUM=REASUM+FLOAT(KREACT(I))
12      DISSUM=DISSUM+WDIS(I)
*      print *,'!!!!!!!',nprol,reamsum
          if(MPARIN.le.2) CALL BARASH(0.,MPARIN,AN,T0,CSNONB)
          if(MPARIN.eq.3) CSNONB=SIGION(2, 4., 2., AN, Z,T0)
          CSNON(1)=0.001*CSNONB
          CSNON(2)=SGX*REASUM
          IF(IDOPCS.EQ.1)CSNON(3)=CSABS
          IF(T0.LE.50.)CSNON(4)=CSCHAT(T0,MPARIN)
          IF(T0.LT.14.)CSNON(1)=CSNON(4)
          RR=DISSUM/REASUM
          CSNON(1)=CSNON(1)*RR
          CSNON(2)=CSNON(2)*RR
          IF(IDOPCS.EQ.1)CSNON(3)=CSNON(3)*RR
          IF(T0.LE.50.)CSNON(4)=CSNON(4)*RR

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C
      IF(INFGAS.EQ.0)GOTO 844
C Particle production
      CSNSUM=0.
      CSPSUM=0.
      CSASUM=0.
      CSDSUM=0.
      CSTSUM=0.
      CSHSUM=0.
      CSPRE=0.
      CSPREN=0.
      CSPREP=0.
      CSPREA=0.
      CSEQUN=0.
      CSEQUP=0.
      DO 848 I=1,KN
      RRR=FLOAT(KREACT(I))
      IF(INFBIG.EQ.0)RRR=1.
      CSNSUM=CSNSUM+FLOAT(KSUMN(I))*RRR
      CSPSUM=CSPSUM+FLOAT(KSUMP(I))*RRR
      CSASUM=CSASUM+FLOAT(KEQAL(I))*RRR
      CSPRE=CSPRE+(FLOAT(KPREN(I))+FLOAT(KPREP(I)))*RRR
      CSPREN=CSPREN+FLOAT(KPREN(I))*RRR
      CSPREP=CSPREP+FLOAT(KPREP(I))*RRR
      CSPREA=CSPREA+FLOAT(KPREA(I))*RRR
      CSEQUN=CSEQUN+FLOAT(KSUMN(I)-KPREN(I))*RRR
      CSEQUP=CSEQUP+FLOAT(KSUMP(I)-KPREP(I))*RRR
      CSDSUM=CSDSUM+FLOAT(KEQD(I))*RRR
      CSTSUM=CSTSUM+FLOAT(KEQT(I))*RRR
848      CSHSUM=CSHSUM+FLOAT(KEQHE(I))*RRR
C
C Non-equilibrium alpha-particle and triton production cross-section
C by F.Denisov, Mekhedov
C Multiplicity of cascade (non-equilibrium) nucleons RR0
C Note ! Denisov, Mekhedov contribuution is not added to the total
C alpha-production (see CSAFD=0.0 below) Turn it on in case of necessity.
C
C Multiplicity of cascade (non-equilibrium) nucleons RR0
      RR0=CSPRE/REASUM
C ----- alpha-particles -----
C RM0,CL0 are parameters
      RM0=0.06
C      CL0=0.12
C Fe56
      CL0=0.12*0.1*22.65
      VAL=0.21*Z+2.5
      EPSD=QBON(1,1,6)+VAL
      RMD=RM0*EPSD
C Number of alpha-clusters in nucleus
      CLD=CL0*(AN/4.)
C Knock-out probability for alpha-cluster
      WMD=(RR0/AN)**RMD
      CSAFD=CSNON(1)*CLD*WMD
* No contribution from Denisov, Mekhedov to total a-production
      CSAFD=0.0
C ----- tritons -----
C RM0,CL0 are parameters
      RM0T=0.06
C Fe56

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      CLOT=0.12*0.2*5.96*0.35
      VT=0.1*Z+0.8
      EPSDT=QBON(1,1,4)+VT
      RMDT=RM0T*EPSDT
C Number of t-clusters in nucleus
      CLDT=CLOT*(AN/3.)
C Knock-out probability for triton-cluster
      WMDT=(RR0/AN)**RMDT
      CSTFD=CSNON(1)*CLDT*WMDT
C ----- He-3 -----
C RM0,CL0 are parameters
      RM0H=0.06
C Fe56
      CLOH=0.12*0.2*2.625*1.687
      VH=0.21*Z
      EPSDH=QBON(1,1,5)+VH
      RMDH=RM0H*EPSDH
C Number of He3-clusters in nucleus
      CLDH=CLOH*(AN/3.)
C Knock-out probability for He3-cluster
      WMDH=(RR0/AN)**RMDH
      CSHFD=CSNON(1)*CLDH*WMDH
C
C
      RR1=CSNSUM/REASUM
      RR2=CSPSUM/REASUM
      RR3=CSASUM/REASUM
      RR33=CSPREA/REASUM
      RR4=CSDSUM/REASUM
      RR5=CSTSUM/REASUM
      RR6=CSHSUM/REASUM
      DO 850 I=1,4
      CSN(I)=CSNON(I)*RR1
      CSP(I)=CSNON(I)*RR2
      CSA(I)=CSNON(I)*RR3
      CSD(I)=CSNON(I)*RR4
      CST(I)=CSNON(I)*RR5
850      CSH(I)=CSNON(I)*RR6
C
      IF(INFDM.EQ.0)GOTO 35
      CSPREA = CSNON(1)*RR33
      SUMD=CSA(1)+CSAFD
      SUMDT=CST(1)+CSTFD
      SUMDH=CSH(1)+CSHFD
      WRITE(10,101)FIALP2,FICAP,MZONA
      WRITE(10,851)RR0,RR0,CL0,CLD,CSAFD,CSA(1),SUMD,EPST,QBON(1,1,6)
+ ,VAL,CSPREA,CSA(1),SUMD,RR0,RR0T,CL0T,CLDT,CSTFD,CST(1),SUMDT,
+ EPSDT,QBON(1,1,4),VT,RR0,RR0H,CL0H,CLDH,CSHFD,CSH(1),SUMDH,
+ EPSDH,QBON(1,1,5),VH
C Auxiliary printing
      YY1=CSPREA*1000.
      YY2=CSA(1)*1000.
      YY3=SUMD*1000.
      WRITE(14,852)T0,YY1,YY2,YY3,Z,AN
C
      DO 34 I=1,4
      CST(I)=CST(I)+CSTFD
      CSH(I)=CSH(I)+CSHFD
34      CSA(I)=CSA(I)+CSAFD

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C
C Write average excitation energy of residuals and particle multiplicity
35   ER90=ER90/FLOAT(KER90)
      RR900=RR1+RR2
      RR901=CSPREN/REASUM
      RR902=CSPREP/REASUM
      RR903=RR901+RR902
      RR904=CSEQUN/REASUM
      RR905=CSEQUP/REASUM
      RR906=RR904+RR905
      WRITE(10,19900)Z,AN,T0,ER90
      WRITE(10,19901)RR1,RR2,RR900,RR901,RR902,RR903,
+     RR904,RR905,RR906,RR33,RR3
      WRITE(10,19902)

C
C Calculation of relative multiplicity for non-equilibrium particles
      IOUT90=1
      IF(IOUT90.EQ.1.AND.INFBIG.NE.0)CALL OUTTMP

C
C Calculation of cross-section for selected reactions
      IF(INFSEP.NE.0) CALL OUTSEP(CSNON,REASUM)

C
C Formation of library
      IF(INFLIB.NE.0) CALL LIBOUT(CSNON,REASUM)

C
      IF(IWRI.NE.0.AND.INFDOS.EQ.1)WRITE(IWRI,1110)
      IF(IWRI.NE.0)WRITE(IWRI,1120)INFDEN,IMOM,IBOND,XPARA9,INFDM
      IF(IWRI.NE.0.AND.INFKAL.EQ.1)WRITE(IWRI,1100)
      IF(IWRI.NE.0)WRITE(IWRI,3100)T0,ITYP1(MPARIN),
+     (CSNON(I),I=1,4),Z,AN,RR,(CSDNON(I),I=1,4),
+     (CSN(I),I=1,4),(CSP(I),I=1,4),(CSA(I),I=1,4),
+     (CSD(I),I=1,4),(CST(I),I=1,4),(CSH(I),I=1,4)
      IF(INFDOS.EQ.1)WRITE(IPR,1110)
      WRITE(IPR,1120)INFDEN,IMOM,IBOND,XPARA9,INFDM
      IF(INFKAL.EQ.1)WRITE(IPR,1200)
      WRITE(IPR,5100)R,(CSNON(I),I=1,4),RR,(CSDNON(I),I=1,4),
+     (CSN(I),I=1,4),(CSP(I),I=1,4),(CSA(I),I=1,4),
+     (CSD(I),I=1,4),(CST(I),I=1,4),(CSH(I),I=1,4)
      GOTO 855
844  IF(IWRI.NE.0.AND.INFDOS.EQ.1)WRITE(IWRI,1110)
      IF(IWRI.NE.0)WRITE(IWRI,1120)INFDEN,IMOM,IBOND,XPARA9,INFDM
      IF(IWRI.NE.0.AND.INFKAL.EQ.1)WRITE(IWRI,1100)
      IF(IWRI.NE.0)WRITE(IWRI,310)T0,
+     R,(CSNON(I),I=1,4),Z,AN,RR,(CSDNON(I),I=1,4)
      IF(INFDOS.EQ.1)WRITE(IPR,1110)
      WRITE(IPR,1120)INFDEN,IMOM,IBOND,XPARA9,INFDM
      IF(INFKAL.EQ.1)WRITE(IPR,1200)
      WRITE(IPR,510)R,(CSNON(I),I=1,4),RR,(CSDNON(I),I=1,4)

C
855  IF(INFBIG.LT.2.AND.INFDIS.NE.1)RETURN

C
      IF(T0.LT.14..AND.INFS0.EQ.1)INFS0=4
      IF(T0.GT.50..AND.INFS0.EQ.4)INFS0=1
      IF(INFS0.LT.1.AND.INFS0.GT.4)INFS0=1
      SGX0=CSNON(INFS0)/REASUM

C
      IF(INFBIG.NE.3) GOTO 105

C
      WRITE(IPR,20)ICS(INFS0)

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DO 3 I=1,KN
  SREACT=SGX0*FLOAT(KREACT(I))
  SDISP=SGX0*WDIS(I)
3  WRITE(IPR,30)KPREN(I),KPREP(I),KSUMN(I),KSUMP(I),KEQAL(I),
+ KEQD(I),KEQT(I),KEQHE(I),SREACT,SDISP
  GOTO 107
C
105  IF(INFBIG.NE.2) GOTO 120
C
107  M8=0
  DO 70 I=1,KN
    KEY=0
    IF(M5(I).NE.1)GOTO 70
  DO 60 J=1,KN
    IF(J.EQ.I)GOTO 60
  IF(M5(J).NE.1)GOTO 60
    IF(KSUMN(I).NE.KSUMN(J))GOTO 60
    IF(KSUMP(I).NE.KSUMP(J))GOTO 60
    IF(KEQAL(I).NE.KEQAL(J))GOTO 60
    IF(KEQD(I).NE.KEQD(J))GOTO 60
    IF(KEQT(I).NE.KEQT(J))GOTO 60
    IF(KEQHE(I).NE.KEQHE(J))GOTO 60
  IF(KEY.NE.0)GOTO 56
  KEY=1
  M8=M8+1
  M1(M8)=I
  MREACT(M8)=KREACT(I)
  DREACT(M8)=WDIS(I)
56  MREACT(M8)=MREACT(M8)+KREACT(J)
  DREACT(M8)=DREACT(M8)+WDIS(J)
  M5(J)=-1
60  M5(I)=-1
C
70  IF(M8.EQ.0)GOTO 120
  WRITE(IPR,23)ICS(INFS0)
  DO 81 M9=1,M8
    M10=M1(M9)
    SREACT=SGX0*FLOAT(MREACT(M9))
    SDISP=SGX0*DREACT(M9)
81  WRITE(IPR,32)KSUMN(M10),KSUMP(M10),KEQAL(M10),
+ KEQD(M10),KEQT(M10),KEQHE(M10),SREACT,SDISP
C
120  IF(INFDIS.NE.1) RETURN
C Particle spectra printing
  WRITE(IPR,777)
  IF(INFOUP(1).EQ.1) CALL PRISPE(SGX0,1)
  IF(INFOUP(2).EQ.1) CALL PRISPE(SGX0,2)
  IF(INFOUP(3).EQ.1) CALL PRISPE(SGX0,3)
C Recoil spectrum printing
  CALL PRIREC(SGX0)
  RETURN
C
C
C
10  FORMAT(1X,'Divisions of free path ',F5.1/1X,'Cut off energy ',
+ '(neutrons)=' ,F7.2/1X,'Cut off energy (protons)=' ,F7.2/
+ 1X,'Cut off energy (alphas)=' ,F7.2/1X,'Level density parameter',
+ ' A /',E12.5/1X,'BONNE=' ,F8.4/1X,' Number of reaction types ',I4)
20  FORMAT(1X,' Excitation functions for all reactions ( CSnon - ',

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+A8,' ) :'/
+1X,' N(PRE) P(PRE) N(TOT) P(TOT) ALFA DEUT TRIT HE3 ',
+' CE-EH^E CE-.CM.'/1X,78('-'))
23 FORMAT(/1X,'Lumped cross-sections ( CSnon - ',A8,' ) :'/
+1X,70('-')/1X,' N(TOT) P(TOT) ALFA DEUT ',
+'TRIT HE3 CR.SECT DISPL.CR.S.'/1X,70('-'))
30 FORMAT(1X,8(I4,3X),E10.4,1X,E10.4)
32 FORMAT(1X,6(I4,3X),E10.4,1X,E10.4)
40 FORMAT(1X,'Elastic cross-section=',E10.4,' Elastic displacement',
+' cross-section is not calculated'/1X,'Reaction cross-section ',
+'( by SGEOM )= ',E10.4/1X,'Total displacement cross-section ',
+'for reactions ( by SGEOM )= ',1X,E10.4)
41 FORMAT(1X,'Reaction cross-section ( OPTIC )=',1X,E10.4/
+1X,'Total displacement cross-section for reactions ( OPTIC )=',
+1X,E10.4)
101 FORMAT(/1X,'Relative number of alpha-clusters ',F8.4/1X,
+'Probability of pick-up of t or He-3 ',F8.4/1X,'Alpha-parti',
+'cles exist beginning from ',i2,' zone')
131 FORMAT(1X,'Level density parameter = A/',F4.1,3X,'Ed =',f5.1,
+' eV')
310 FORMAT(1X,F8.2,5X,F3.1,3X,4(2X,E10.4)/1X,2F4.0,1X,E10.4,4(2X,
+E10.4)/' ',70('-'))
333 FORMAT(1X,20X,'Limitation on orbital momenta is applied')
334 FORMAT(1X,20X,' Correction for relative velocity')
439 FORMAT(1X,'NORMALIZATION OF DOSTROVSKY CROSS-SECTIONS (EVAPAR) ',
+'FOR ALPHAS AND PROTONS :'/1X,' PARALP=',F7.2,' PARPRO=',F7.2)
444 FORMAT(1X,' LIMITATION RULE WAS APPLIED ',E12.5,' TIMES')
499 FORMAT(1X,9A8)
500 FORMAT(1X,5X,'Nucleus',2F6.1/1X,'Incident particle:',A8,2X,
+'with energy =',F6.1,' MeV')
501 FORMAT(1X,'Events ',I8/1X,'Geometry cross-section=',F7.3,' b',
+1X,'Elastic cross-section=',F7.3,' b')
503 FORMAT(1X,'KHIST',I6,' can not be treated: arrays of C-blocks ',
+'MASOUT are overfilled')
510 FORMAT(' ',70('-')/1X,'CR.SECT.',3X,'[BARNs]',5X,'BARASH ',
+' GEOMETRY ', ' OPTIC(SCR) ', ' CHATTERJEE'/1X,' CSNON ',5X,F3.1
+,3X,4(2X,E10.4)/1X,' CSDNON ',1X,E10.4,4(2X,E10.4)/' ',70('-'))
555 FORMAT(1X,' REFLECTION TOOK PLACE ',E12.5,' TIMES')
667 FORMAT(1X,10(E10.3))
777 FORMAT(///' GRAPHS '///' Energy distributions : Energy(i-1) ',
+'to E(i) -- Function(i)'' Angular distributions: Angle(i) ',
+'to Angle(i+1) -- Function(i)')
851 FORMAT(/1X,' Alpha-particles :'/1X,'RR0=',F6.1,' M0=',F5.3,' N0=',
+F5.3,' CLD=',F5.1,' CSD=',F5.3,' CSA=',F5.3,' SUM=',F5.3/1X,
+' EPSD =',F7.1,' QBON(1,1,6)=',F7.1,' VAL=',F7.1/1X,F9.5,
+' Production cross-sect for non-eq alphas [b] ',
+'(CSnon-Barashenkov)'/1X,F9.5,' Total product cross-secti',
+'on for alphas without Denisov-Mekhedov correction (CSnon-B)'
+/1X,F9.5,' Total product cross-section for a-particles ',
+' + D-M correction (CSnon-B)''/1X,' Tritons :'/1X,'RR0=',
+F6.1,' M0=',F5.3,' N0=',F5.3,' CLD=',F5.1,' CSD=',F5.3,' CST=',
+F5.3,' SUM=',F5.3/1X,' EPSD =',F7.1,' QBON(1,1,4)=',F7.1,' VT =',
+F7.1/1X,' He-3 :'/1X,'RR0=',F6.1,' M0=',F5.3,' N0=',
+F5.3,' CLD=',F5.1,' CSD=',F5.3,' CSH=',F5.3,' SUM=',F5.3/1X,
+' EPSD =',F7.1,' QBON(1,1,5)=',F7.1,' VH =',F7.1)
852 FORMAT(1X,f8.2,3G12.5,2F6.1,' T0, Alpha(mbarn):Pre, Pre+',
+'Eq, Pre+Eq+Denisov')
887 FORMAT(1X,' DIMENSION FOR AT WAS EXCEEDED ',I8,' TIMES')
888 FORMAT(1X,' PAULI PRINCIPLE WAS APPLIED ',E12.5,' TIMES')

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889 FORMAT(1X,' REJECTED EVENTS ',I7,',MAXIMAL NUMBER OF',
+ ' REFLECTIONS',F7.1)
1100 FORMAT(1X,' Angular distributions have been calculated by ',
* 'Kalbach, Mann formulas')
1110 FORMAT(1X,' Coulomb potential for inverse reactions: VP=0.1*',
+ 'Z+0.8, VA=2.*VP')
1120 FORMAT(1X,'INF DEN=',I3,' IMOM=',I3,' IBOND=',I3,' XPARDE =',F5.1,
+ ' INFDM=',I3)
1200 FORMAT(1X,70('#')/1X,' Angular distributions have been calcul',
+ 'ated by Kalbach, Mann formulas'/1X,70('#'))
3100 FORMAT(1X,F8.2,1X,A8,2X,4(2X,E10.4)/1X,2F4.0,1X,E10.4,4(2X,E10.4)
+ /1X,' NEUTRON PRODUCTION',4(2X,E10.4)/1X,' PROTON PRODUCTION',
+ 4(2X,E10.4)/1X,' ALPHA PRODUCTION',4(2X,E10.4)
+ /1X,' H-2 PRODUCTION',4(2X,E10.4)/1X,' H-3 PRODUCTION',
+ 4(2X,E10.4)/1X,' HE-3 PRODUCTION',4(2X,E10.4)/' ',70('-'))
5100 FORMAT(' ',70('-')/1X,'CR.SECT.',3X,'[BARNS]',5X,'BARASH ',
+ ' GEOMETRY ', ' OPTIC(SCR) ', ' CHATTERJEE'/1X,' CSNON ',5X,
+ F3.1,3X,4(2X,E10.4)/1X,' CSDNON ',1X,E10.4,4(2X,E10.4)
+ /1X,' NEUTRON PRODUCTION',4(2X,E10.4)/1X,' PROTON PRODUCTION',
+ 4(2X,E10.4)/1X,' ALPHA PRODUCTION',4(2X,E10.4)/1X,' H-',
+ '2 PRODUCTION',4(2X,E10.4)/1X,' H-3 PRODUCTION',4(2X,E10.4)
+ /1X,' HE-3 PRODUCTION',4(2X,E10.4)/' ',70('-'))
8890 FORMAT(1X,' PROBABILITY TO OVERLOAD ENERGY ( > 500 )',F6.0,' %')
8888 FORMAT(1X,' CURRENT CHARGE WAS LOWER THAN ',
+ 'PERMISSIBLE ',I8,' TIMES')
C T(X) is the sum for nucleons in X-process
19900 FORMAT(1X,65('-')/' Task'/1X,'Z= ',F6.1,' A= ',F6.1,' T0= ',
+ F6.1/' Average energy of excitation after cascade stage =',
+ f9.3,' MeV'/)
19901 FORMAT(1X,'Particle multiplicity:'/1X,
+ ' N(SUM) P(SUM) T(SUM) N(PRE) P(PRE) T(PRE) ',
+ 'N(EQU) P(EQU) T(EQU) A(PRE) A(SUM without D-M)'
+ /1X,11F7.3)
19902 FORMAT(/34('='),'end',34('='))
END
*****
* SUBROUTINE OUTSEP *
*****
SUBROUTINE OUTSEP(CSNON,RRR)
REAL*8 ICS(4)
COMMON/MAIIPR/IPR /IWRI/IWRI /INFSEP/KSEP(100,4),INFSEP,JSEPM
COMMON/MPARIN/MPARIN /DATINI/RAAAAA,T0,W0
COMMON/SEPSEP/RSEP2(100,2),JSEPM2 /INF/INFBIG,INFS0
DIMENSION CSNON(4)
DATA ICS/' BARASH ', 'GEOMETRY', ' OPTIC ', 'CHAT-JEE'/
DATA RN,RP,RA/1HN,1HP,1HA/
REASUM=RRR
C Define CSnon
ICSN=INFS0
WRITE(IPR,900)ICS(ICSN)
IF(IWRI.NE.0)WRITE(IWRI,900)ICS(ICSN)
RI=RN
IF(MPARIN.EQ.2)RI=RP
IF(MPARIN.EQ.3)RI=RA
C Cross-section in mb
DO 100 J=1,JSEPM
CS=1000.*FLOAT(KSEP(J,4))*CSNON(ICSN)/REASUM
IF(INFSEP.EQ.1)
CWRITE(IPR,1000)RI,KSEP(J,1),KSEP(J,2),KSEP(J,3),CS

```

```

      IF(IWRI.NE.0.AND.INFSEP.EQ.1)
CWRITE(IWRI,1000)RI,KSEP(J,1),KSEP(J,2),KSEP(J,3),CS
      IF(INFSEP.EQ.2)
CWRITE(IPR,2000)RI,KSEP(J,1),KSEP(J,2),KSEP(J,3),CS,RSEP2(J,1),
C          RSEP2(J,2)
      IF(IWRI.NE.0.AND.INFSEP.EQ.2)
CWRITE(IWRI,2000)RI,KSEP(J,1),KSEP(J,2),KSEP(J,3),CS,RSEP2(J,1),
C          RSEP2(J,2)
100  CONTINUE
900  FORMAT(1X,'Cross-section for selected reactions (CSnon:',A8,')')
1000 FORMAT(1X,'( ',A1,',',I2,'n',I2,'p',I2,'a )',G12.5,' mb')
2000 FORMAT(1X,'( ',A1,',',I2,'n',I2,'p',I2,'a )',G12.5,' mb',
C ' Residual ',F6.1,F7.1)
      RETURN
      END
*****
*          SUBROUTINE OUTTMP          *
*****
      SUBROUTINE OUTTMP
C Relative multiplicity of pre-equilibrium (cascade) particles
      REAL*8 R1(2)
      COMMON/MASOUT/WDIS(990),KPREN(990),KPREP(990),KEQD(990),KEQT(990)
*,KEQHE(990),KEQAL(990),KSUMN(990),KSUMP(990),KREACT(990),
* KPREA(990),KN /MAIIPR/IPR /IWRI/IWRI
      DIMENSION TOT(4)
      DATA R1/'NEUTRONS',' PROTONS'/
      IF(IWRI.NE.0)WRITE(IWRI,1000)
      WRITE(IPR,1000)
          DO 18 I0=1,4
18          TOT(I0)=0.
      DO 400 J1=1,2
50          DO 100 I=1,KN
              RRR=FLOAT(KREACT(I))
              GOTO(81,82),J1
81              SUMX=FLOAT(KSUMN(I))
              PREX=FLOAT(KPREN(I))
              GOTO 90
82              SUMX=FLOAT(KSUMP(I))
              PREX=FLOAT(KPREP(I))
90          TOT(1)=TOT(1)+SUMX*RRR
              IF(PREX.EQ.0)GOTO 100
              TOT(2)=TOT(2)+RRR*PREX
              IF(PREX.GE.2.)TOT(3)=TOT(3)+RRR*(PREX-1.)
              IF(PREX.GE.3.)TOT(4)=TOT(4)+RRR*(PREX-2.)
100          CONTINUE
              PRETOT=100.*TOT(2)/TOT(1)
              PREGE2=100.*TOT(3)/TOT(1)
              PREGE3=100.*TOT(4)/TOT(1)
              IF(IWRI.NE.0)WRITE(IWRI,2000)R1(J1),PRETOT,PREGE2,PREGE3
400          WRITE(IPR,2000)R1(J1),PRETOT,PREGE2,PREGE3
1000         FORMAT(1X,'Multiplicity of precompound particles of this type ',
* 'to'/1X,16X,'all partiles of this type in %'/1X,8X,
* 7X,'TOTAL',14X,'>2',14X,'>3')
2000         FORMAT(1X,A8,3G16.2)
      RETURN
      END
*****
*          SUBROUTINE PAULI          *
*****

```



```

SUBROUTINE PAULI(TB1,TP1,IKS)
COMMON/PARTIC/WP,PX,PY,PZ,P,T,E,X,Y,Z,R,JIN,M
COMMON/SCIMEM/WPM,PXM,PYM,PZM,PM,TM,EM,XM,YM,ZM,RM,JINM,MM
COMMON/NDIM/NPAR /MEMORY/U(11,20),MU(2,20)
COMMON/ACTSCI/PIN1,PIN2,PIN3,WPX,RK3,RK4,GAMMA,SK2,VC2,VCX,
*VCY,VCZ,MPX /DATPAU/BONCUT(3) /TFERMI/TF(34,4)
COMMON/JACT/JACT /R005/R005 /TYPACT/L,L7
DIMENSION TT(2)
IF(TB1-TF(JIN,M))10,20,20
10 IKS=1
IF(L7.EQ.1) CALL MEMDEC(2)
IF(IGEN.EQ.1)RETURN
R005=R005+1.
RETURN
20 IF(TP1-TF(JIN,MPX))10,30,30
30 TT(1)=TF(JIN,M)+BONCUT(M)
TT(2)=TF(JIN,MPX)+BONCUT(MPX)
C
C
IF(TB1.GT.TT(1))GOTO 50
C TB1 < TT(1)
IF(M.EQ.2) CALL PROZR(TB1,TT(1),JIN,KEY,M)
IF(M.EQ.2.AND.KEY.EQ.1) GOTO 50
IF(TP1.GT.TT(2))GOTO 60
C TP1 < TT(2)
IF(MPX.EQ.2) CALL PROZR(TP1,TT(2),JIN,KEY,MPX)
IF(MPX.EQ.2.AND.KEY.EQ.1) GOTO 60
IGEN=2
CALL CHECK1(1.,TB1,WP,IGEN,M)
IF(IGEN.EQ.1)GOTO 10
IGEN=2
CALL CHECK1(-1.,TP1,WPX,IGEN,MPX)
IF(IGEN.EQ.1)GOTO 10
33 IF(NPAR.GT.0)GOTO 40
IKS=-1
JACT=1
RETURN
40 IKS=0
RETURN
50 IF(TP1.GT.TT(2))GOTO 70
C TP1 < TT(2)
IF(MPX.EQ.2) CALL PROZR(TP1,TT(2),JIN,KEY,MPX)
IF(MPX.EQ.2.AND.KEY.EQ.1) GOTO 70
IGEN=2
CALL CHECK1(-1.,TP1,WPX,IGEN,MPX)
IF(IGEN.EQ.1)GOTO 10
IGEN=2
CALL SCILSK(0,1.,TB1,WP,IGEN,M)
IF(IGEN.EQ.1)GOTO 10
IKS=3
JACT=1
RETURN
60 IGEN=2
CALL CHECK1(1.,TB1,WP,IGEN,M)
IF(IGEN.EQ.1)GOTO 10
IGEN=2
CALL SCILSK(0,-1.,TP1,WPX,IGEN,MPX)
IF(IGEN.EQ.1)GOTO 10
IKS=3

```

```

      JACT=1
      RETURN
70      IGEN=2
          CALL CHECK1(-1.,TP1,WPX,IGEN,MPX)
          IF(IGEN.EQ.1)GOTO 10
      IGEN=2
      CALL SCILSK(0,1.,TB1,WP,IGEN,M)
      IF(IGEN.EQ.1)GOTO 10
      IGEN=2
      CALL SCILSK(1,-1.,TP1,WPX,IGEN,MPX)
      IF(IGEN.EQ.1)GOTO 10
      CALL MEMIN
      IKS=3
      JACT=1
      RETURN
      END
*****
*              SUBROUTINE PICKUP                      *
*****
      SUBROUTINE PICKUP(IKS)
C Energy conservation
      COMMON/PARTIC/WP,PX,PY,PZ,P,T,E,X,Y,Z,R,JIN,M
      COMMON/PARTNR/PPX,PPY,PPZ,PP,MX
      COMMON/NDIM/NPAR
      COMMON/DATPAU/BONCUT(3)
      COMMON/TFERMI/TF(34,4)
      COMMON/JACT/JACT
      COMMON/R005/R005
      DIMENSION TT(2)
C
      T2 = (PP**2)/(2.*WM(MX))
C
C Alpha-particle characteristics
      WP1 = WM(3)
      M1 = 3
C Auxiliary values
      PX11 = PX + PPX
      PY11 = PY + PPY
      PZ11 = PZ + PPZ
      P11 = SQRT(PX11**2+PY11**2+PZ11**2)
      T1 = T + T2
      P1 = SQRT(T1**2+2.*WP1*T1)
      PX1 = PX11*(P1/P11)
      PY1 = PY11*(P1/P11)
      PZ1 = PZ11*(P1/P11)
      E1=T1+WP1
C
      TB1 = T1
      IF(TB1-TF(JIN,M1))10,20,20
10      IKS=1
      RETURN
20      TT(1)=TF(JIN,M1)+BONCUT(M1)
      IF(TB1.GT.TT(1))GOTO 50
C TB1 < TT(1)
      IF(NPAR.GT.0)GOTO 40
      IKS=-1
      JACT=1
      RETURN
40      IKS=0

```

```

RETURN
50 CONTINUE
C Prohibition on angular momentum
  IGEN=2
  RORM=ORBIT(PX1,PY1,PZ1,X,Y,Z)
  CALL QUES(RORM,T1,WP1,JIN,M1,IGEN)
  IF(IGEN.EQ.1)GOTO 10
C Creation of alpha-particle
  WP = WP1
  PX = PX1
  PY = PY1
  PZ = PZ1
  P = P1
  T = T1
  E = E1
  M = M1
  IKS=3
  JACT=1
  RETURN
  END
*****
*
SUBROUTINE PPDRAW
*
SUBROUTINE PPDRAW(QCOS,FI)
COMMON/URAND1/IYG
CC=RANDOM(0)
QCOS=1.-2.*CC
CC=RANDOM(0)
FI=6.2831852*CC
RETURN
END
*****
*
SUBROUTINE PRECAM
*
SUBROUTINE PRECAM
C Binding energy according to Cameron (Barashenkov, Tonnev, 1972,
C pp.418-419)
COMMON/AN/AN /BOND1/QBON(200,200,6)
COMMON/INIQBO/Z,CKA,CKB,RPA,RPB,RALA,RALB
COMMON/MPARIN/MPARIN /INFBON/IBOND
COMMON/DATCAM/CAMN(130),CAMP(130),MAXN,MAXP
COMMON/MAIIPR/IPR /MAX/MAXNEU,MAXPRO
REAL*8 RMAS(6),RAT,IP90(6)
DIMENSION ATO(200,200),RMA SM(6),NN(6),NP(6)
DATA RMAS/ 0.008 665 27, 0.007 825 22, 0.014 102 22,
c 0.016 049 71, 0.016 029 68, 0.002 603 3/
DATA RAT/931.5016/
C RMAS is mass defect in at. units
C
C RMAS: 1 2 3 4 5 6
C-----N-----P-----D-----T---HE-3---A--- particle
C J 1 2 3 4 5 6
C-----
C NN 1 0 1 2 1 2
C NP 0 1 1 1 2 2
C-----
DATA NN/ 1, 0, 1, 2, 1, 2/,NP/ 0, 3*1, 2*2/
DATA IP90/8H NEUTRON,8H PROTON,8HDEUTERON,8H TRITON,8H HE-3,
c8H ALPHA/

```

```

C
C MAXN/MAXP is the dimension of CAMN/CAMP array (see corresp BLOCK DATA),
C which is equal to maximal permissible number of neutrons/protons in
C target nucleus
C
C MAXNEU and MAXPRO are dimensions of QBON array
      MAXN=130
      MAXP=130
C L11N/L11P is minimal number of neutrons/protons in nucleus, for which
C corrections to Cameron formula are available
      L11N=1
      L11P=1
      IF(MAXN.LT.200.AND.MAXP.LT.200)GOTO 7
      WRITE(IPR,700)MAXN,MAXP
      STOP
7      IZNUCL=Z
      INNUCL=AN-Z
      IF(MPARIN.EQ.1)INNUCL=INNUCL+1
      IF(MPARIN.EQ.2)IZNUCL=IZNUCL+1
          IF(MPARIN.EQ.3)INNUCL=INNUCL+2
          IF(MPARIN.EQ.3)IZNUCL=IZNUCL+2
      IF(INNUCL.LE.MAXN)GOTO 10
      WRITE(IPR,800)INNUCL,MAXN
      STOP
10     IF(IZNUCL.LE.MAXP)GOTO 20
      WRITE(IPR,900)IZNUCL,MAXP
      STOP
C INNUCL-L11N is the number of neutrons emitted, +1 : array dimension
C ATO is more than this amount on 1,i.e. ATO(1,1) means 0 emitted
20     DO 80 I=L11N,INNUCL
          RN=FLOAT(I)
          DO 70 J=L11P,IZNUCL
              RZ=FLOAT(J)
              INN1=INNUCL-I+1
              IZN1=IZNUCL-J+1
              IF(INN1.LE.200.AND.IZN1.LE.200)GOTO 65
              WRITE(IPR,1000)INN1,IZN1
              STOP
65     ATO(INN1,IZN1)=CAMERO(RN,RZ)+CAMN(I)+CAMP(J)
70     CONTINUE
80     CONTINUE
          LMAXN=(INNUCL-L11N+1)-2
          LMAXP=(IZNUCL-L11P+1)-2
      MAXNEU=LMAXN
      MAXPRO=LMAXP
          IF(LMAXN.GT.5.AND.LMAXP.GT.5)GOTO 90
          WRITE(IPR,1100)LMAXN,LMAXP
          STOP
90     DO 92 I=1,6
92     RMASM(I)=RAT*RMAS(I)
          DO 200 IN=1,LMAXN
          DO 100 IZ=1,LMAXP
              AT1=ATO(IN,IZ)
          DO 95 NUCL=1,6
              AT2=ATO(IN+NN(NUCL),IZ+NP(NUCL))
95     QBON(IN,IZ,NUCL)=AT2+RMASM(NUCL)-AT1
100    CONTINUE
200    CONTINUE
      IF(IBOND.GT.0)RETURN

```

C TEST

```
      IF (IBOND.EQ.-3) RETURN
      WRITE(1,499)
      WRITE(6,499)
      WRITE(8,499)
      INM=MIN0(12,MAXNEU)
      IZM=MIN0(12,MAXPRO)
      DO 300 NUCL=1,6
        WRITE(1,500) IP90(NUCL)
        WRITE(6,500) IP90(NUCL)
        WRITE(8,500) IP90(NUCL)
      DO 300 IZ=1,IZM
        WRITE(1,600) IZ, (QBON(IN,IZ,NUCL),IN=1,INM)
        WRITE(6,600) IZ, (QBON(IN,IZ,NUCL),IN=1,INM)
300    WRITE(8,600) IZ, (QBON(IN,IZ,NUCL),IN=1,INM)
      STOP
499  FORMAT(1X,'TEST FOR BINDING ENERGIES' /
c    1X,'CAMERON FORMULAS FOR ALL NUCLIDES' / 1X,72(1H-))
500  FORMAT(/1X,A8/1X,'IZ  IN-----> NEUTRON NUMBER DECREASED')
600  FORMAT(1X,I2,12F6.1)
700  FORMAT(1X,'ERROR IN PRECAM: DIMENSION OF QBON, ATO, CAMN/CAMP',
c' ARE NOT CONSISTENT. CHANGE QBON AND ATO DIMENSIONS IN ALL CODE')
800  FORMAT(1X,'ERROR IN PRECAM: PERMISSIBLE AMOUNT IS EXCEEDED FOR:' /
c1X,5X,I5,' > ',I5/
c1X,'NEUTRONS IN TARGET NUCLEUS. ADD NEW CAMN AND CAMP DATA (SEE' /
c1X,'CORRESPONDING BLOCK DATA) AND CHANGE DIMENSION OF THESE ' /
c1X,'ARRAYS IN ALL CODE AND MAXN AND MAXP VALUES IN PRECAM (!)')
900  FORMAT(1X,'ERROR IN PRECAM: PERMISSIBLE AMOUNT IS EXCEEDED FOR:' /
c1X,5X,I5,' > ',I5/
c1X,'PROTONS IN TARGET NUCLEUS. ADD NEW CAMN AND CAMP DATA (SEE' /
c1X,'CORRESPONDING BLOCK DATA) AND CHANGE DIMENSION OF THESE ' /
c1X,'ARRAYS IN ALL CODE AND MAXN AND MAXP VALUES IN PRECAM (!)')
1000 FORMAT(1X,'ERROR IN PRECAM: DIMENSION OF ARRAY EXCEEDED ' / 1X,
c' ATO INNUCL-I+1=',I5,' > 200 ^ IZNUCL-J+1=',I5,' > 200')
1100 FORMAT(/1X,'***** SUBROUTINE PRECAM *****' / 1X,' TOO SMALL',
c' NUMBER OF CASCADES WILL BE SIMULATED ',I5,' AND ',I5//
c' CALL AUTHORS OF DISCA (AND LOOK IN THEIR EYES).') //)
      END
*****
*          SUBROUTINE PRELYM          *
*****
      SUBROUTINE PRELYM
C CALCULATION OF BINDING ENERGIES USING MASS TABLE AND MSL-FORMULA
C FOR NEUTRONS, PROTONS, DEUTERONS AND ALPHA-PARTICLES FOR RESIDUAL
C NUCLEI FORMED AFTER ESCAPE OF NOT MORE THAN 9 PROTONS AND 22 NEUTRONS.
C FOR OTHER NUCLEI THE CALCUALTION IS PERFORMD USING CAMERON FORMULA
C (SEE SUBR.PRECAM)
      COMMON/AN/AN /BOND1/QBON(200,200,6)
      COMMON/INIQBO/Z,CKA,CKB,RPA,RPB,RALA,RALB
      COMMON/MPARIN/MPARIN /MAIIPR/IPR
      COMMON/MAX/MAXNEU,MAXPRO /INFON/IBOND
      COMMON/LYM1/BE(11,24,4),SYMB(11,24),PAIR(11,24),SYMBP(11,24)
      COMMON/SF/M3,KPLT /LYM2/ILYM
      COMMON/LYM3/PAIRP(11,24),PAIRE(11,24),ILYM2
      REAL*8 IP90(6)
      DATA IP90/8H NEUTRON,8H PROTON,8HDEUTERON,8H TRITON,8H HE-3,
c8H ALPHA/
      NZ=MIN0(9,MAXPRO)
      NA=MIN0(22,MAXNEU)
```

```

      AT=AN
      ZT=Z
      AP=1.
      ZP=0.
      IF (MPARIN.EQ.2) ZP=1.
      IF (MPARIN.EQ.3) THEN
          ZP=2.
          AP=4.
      ENDIF

      ZEE=ZP+ZT
      AMASS=AP+AT
      MC=10
      MP=3
      QVAL=0.
      ILYM=0
      ILYM2=0
      KPLT=0
      M3=4
      CALL LYMASS(ZEE,AMASS,NZ,NA,MC,MP,AP,AT,ZP,ZT,QVAL)
C BE(11,24,K)   K=1-N, 2-P, 3-A, 4-D
      DO 200 NUCL=1,6
          IF (NUCL.EQ.1.OR.NUCL.EQ.2) KPART=NUCL
          IF (NUCL.EQ.3) KPART=4
          IF (NUCL.EQ.4.OR.NUCL.EQ.5) GOTO 200
          IF (NUCL.EQ.6) KPART=3
      DO 100 IZ=1,NZ
      DO 100 IN=1,NA
100         QBON(IN,IZ,NUCL)=BE(IZ,IN,KPART)
200         CONTINUE
          IF (IBOND.GT.0) RETURN
C TEST
      WRITE(1,499) NZ,NA
      WRITE(6,499) NZ,NA
      WRITE(8,499) NZ,NA
          INM=MIN0(12,MAXNEU)
          IZM=MIN0(12,MAXPRO)
      DO 300 NUCL=1,6
          WRITE(1,500) IP90(NUCL)
          WRITE(6,500) IP90(NUCL)
          WRITE(8,500) IP90(NUCL)
      DO 300 IZ=1,IZM
          WRITE(1,600) IZ, (QBON(IN,IZ,NUCL),IN=1,INM)
          WRITE(6,600) IZ, (QBON(IN,IZ,NUCL),IN=1,INM)
300         WRITE(8,600) IZ, (QBON(IN,IZ,NUCL),IN=1,INM)
          STOP
499         FORMAT(1X,'TEST FOR BINDING ENERGIES'/
c1X,'M.BLANN CALCULATION FOR NZ=',I4,' NA=',I4
c/1X,'OTHER NUCLIDES ARE OBTAINED BY CAMERON FORMULAS'
c/1X,72(1H-))
500         FORMAT(/1X,A8/1X,'IZ   IN-----> NEUTRON NUMBER DECREASED')
600         FORMAT(1X,I2,12F6.1)
          END
*****
*               SUBROUTINE PRIREC               *
*****
      SUBROUTINE PRIREC(SGX0)
* Printing of recoil spectra in separate file
      COMMON/EMEM91/EMEMT(21),RMEMT(21),HMEMT
      COMMON/INIQBO/Z,CKA,CKB,RPA,RPB,RALA,RALB

```

```

COMMON/AN/AN /DATINI/RA,T0,W0 /MAIIPR/IPR
DIMENSION EKE(21)
C --> mb
SGX1=SGX0*1000.
SUM = 0.0
EKE(1) = EMEMT(1)
DO 122 NU=2,21
122 EKE(NU)=( EMEMT(NU-1) + EMEMT(NU) ) / 2.
RMEMT(1)=RMEMT(1)*SGX1/HMEMT
DO 121 NU=2,21
RMEMT(NU)=RMEMT(NU)*SGX1/(EMEMT(NU)-EMEMT(NU-1))
121 SUM=SUM+RMEMT(NU)
SUM=SUM*HMEMT
WRITE(IPR,22200)
22200 FORMAT(/1X,'RECOIL SPECTRUM (LINEAR SCALE) ')
CALL GRAPH(EKE,RMEMT,21,0)
Write(33,2000)T0,SUM,Z,AN
2000 Format(f6.1,e12.5,t40,
c 'NEUTRON ENERGY AND SUM OF RECOIL SPECTRUM FOR TARGET ',2f6.1)
* Attention ! Last energy is not treated
MMAX = 21
Write(33,2010)MMAX
2010 Format(i7,t40,'NUMBER OF KE INTERVALS FOR SPECTRUM')
Write(33,2011)(EKE(I),I=1,MMAX)
2011 Format(10f7.3)
Write(33,2012)(RMEMT(I),I=1,MMAX)
2012 Format(1pe10.3,7e10.3)
RETURN
END
*****
* SUBROUTINE PRISPE *
*****
SUBROUTINE PRISPE(SGX0,MP)
COMMON/DATINI/RA,T0,W0
COMMON/EMEM/EMEM0(21),EMEM(21),RMEM(21,3),RMEM0(21,3),HMEM
COMMON/EOUT/SPE(19,5,3),PI(19),EOUT1(5,3),EOUT2(5,3),MSPE
COMMON/MAIIPR/IPR /MPARIN/MPARIN /AN/AN
COMMON/SPEFUL/ANGLIM(9,2,3),ANGSUM(21,9,3),ANGCEN(9,3),DCEN,MANG
REAL*8 ITYP(3)
DIMENSION ANGTMP(21), GR1(19), XSTE(150),YSTE(150),PRITMP(150,23)
C dimension of EOUT1,2(I,) = EMEAN
DIMENSION RTMP(21),EMEAN(5)
C IU is unit for printing (see open in main routine)
IU = 70 + MP
C PRITMP is array for histogram presentation
DATA ITYP/' NEUTRON',' PROTON',' ALPHA'/
DO 1 I=1,150
XSTE(I)=0.0
YSTE(I)=0.0
DO 1 J=1,23
1 PRITMP(I,J)=0.0
IF(MP.NE.3) WRITE(IPR,221)ITYP(MP)
IF(MP.EQ.3) WRITE(IPR,222)
C-----
C Energy distribution
SS1=0.
SSS=0.
C --> mb
SGX1=SGX0*1000.

```

```

DO 121 NU=1,21
  SSS=SSS+RMEM0 (NU,MP)
  RMEM0 (NU,MP)=RMEM0 (NU,MP)*SGX1/HMEM
  RMEM (NU,MP)=RMEM (NU,MP)*SGX1/HMEM
  SS1=SS1+RMEM0 (NU,MP)+RMEM (NU,MP)
121  CONTINUE
WRITE(IPR,220)
220  FORMAT(/1X,'NON-EQUILIBRIUM SPECTRUM DS/DE ----->')
      DO 700 NU=1,21
700    RTMP (NU) = RMEM0 (NU,MP)
        CALL GRAPH(EMEM0,RTMP,21,2)
        DO 1700 NU=1,21
          If(RTMP(NU).eq.0.0) RTMP(NU) = 1.E-13
1700    Continue
        SSS=SGX1*SSS
        WRITE(IPR,670)SSS
670    FORMAT(1X,'C`MMA ',G12.5)
C NSTE is the number of points obtained < 150
  CALL STEP93(EMEM0,RTMP,21,XSTE,YSTE,150,NSTE,1)
  DO 2 I=1,NSTE
    PRITMP(I,1) = XSTE(I)
  2    PRITMP(I,2) = YSTE(I)
      DO 701 NU=1,21
701    RTMP(NU) = RMEM(NU,MP)
WRITE(IPR,2210)
2210  FORMAT(/1X,'EQUILIBRIUM SPECTRUM DS/DE ----->')
      CALL GRAPH(EMEM,RTMP,21,2)
      DO 1701 NU=1,21
        If(RTMP(NU).eq.0.0) RTMP(NU) = 1.E-13
1701    Continue
      CALL STEP93(EMEM ,RTMP ,21,XSTE,YSTE,150,NSTE,1)
      DO 3 I=1,NSTE
  3    PRITMP(I,3) = YSTE(I)
      DO 987 NU=1,21
987    RMEM0 (NU,MP)=RMEM0 (NU,MP)+RMEM(NU,MP)
      DO 702 NU=1,21
702    RTMP(NU) = RMEM0 (NU,MP)
C
C Total spectrum
  IF(MP.NE.3) WRITE(IPR,22100)ITYP(MP)
22100  FORMAT(/1X,'TOTAL SPECTRUM - ',A8,' PRODUCTION')
  IF(MP.EQ.3) WRITE(IPR,22101)
22101  FORMAT(/1X,'TOTAL SPECTRUM - ALPHA PRODUCTION')
        CALL GRAPH(EMEM0,RTMP,21,2)
        DO 1702 NU=1,21
          If(RTMP(NU).eq.0.0) RTMP(NU) = 1.E-13
1702    Continue
        CALL STEP93(EMEM0,RTMP,21,XSTE,YSTE,150,NSTE,1)
        DO 4 I=1,NSTE
  4    PRITMP(I,4) = YSTE(I)
C
C-----
C Inclusive spectra :
  DO 1000 ICEN=1,MANG
  WRITE(IPR,888)ITYP(MP),ANGCEN(ICEN,MP),DCEN
    PI180=3.1415926/180.
    PPP0=DCEN
    QAN1 = ANGCEN(ICEN,MP)-DCEN
    IF(QAN1.LT.0.0) PPP0= ANGCEN(ICEN,MP)

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QAN1 = ANGCEN(ICEN,MP)+DCEN
IF(QAN1.GT.180.0) PPP0= 180.0-ANGCEN(ICEN,MP)
PPP0=PPP0+DCEN
      PPP= PPP0*(3.1415/180.)*2.*3.1415
      ANG=PI180*ANGCEN(ICEN,MP)
DO 322 NU=1,21
322  ANGTMP(NU)=0.0
DO 323 NU=1,21
      ANGTMP(NU)      =ANGSUM(NU,ICEN,MP)*SGX1/HMEM
323  ANGTMP(NU)      =ANGTMP(NU)      /((PPP*SIN(ANG) )
CALL GRAPH(EMEM0,ANGTMP,21,2)
      DO 1323 NU=1,21
      If(ANGTMP(NU).eq.0.0) ANGTMP(NU) = 1.E-13
1323  Continue
      CALL STEP93(EMEM0,ANGTMP,21,XSTE,YSTE,150,NSTE,1)
      DO 5 I=1,NSTE
5      PRITMP(I,4+ICEN) = YSTE(I)
1000  CONTINUE
C
      DO 2000 L=1,MSPE
C-----
C Total angular distribution
WRITE(IPR,777)EOUT1(L,MP),EOUT2(L,MP)
EOUEOU=1./(EOUT2(L,MP)-EOUT1(L,MP))
GR1(1)=0.
DO 97 NANG=2,19
97  GR1(NANG)=GR1(NANG-1)+10.
PI180=3.1415926/18.
      PPP=(3.1415/18.)*2.*3.1415
SPE(19,L,MP)=0.
ANG=0.
DO 99 NANG=1,18
ANG=ANG+PI180
ANG2=ANG - 5.*3.1415926/180.
99  SPE(NANG,L,MP)=SGX1*SPE(NANG,L,MP)*EOUEOU/(PPP*SIN(ANG2))
      DO 703 NANG=1,19
703  RTMP(NANG) = SPE(NANG,L,MP)
CALL GRAPH(GR1,RTMP,19,2)
      DO 1703 NU=1,21
      If(RTMP(NU).eq.0.0) RTMP(NU) = 1.E-13
1703  Continue
CALL STEP93(GR1 ,RTMP ,19,XSTE,YSTE,150,NSTE1,2)
DO 6 I=1,NSTE1
IF(L.EQ.1) PRITMP(I,13+L) = XSTE(I)
6  PRITMP(I,14+L) = YSTE(I)
2000 CONTINUE
C-----
      DO 49 I=1,5
49  EMEAN(I) = 0.5*(EOUT1(I,MP)+EOUT2(I,MP))
C
C PRITMP printing
WRITE(IU,7001)T0
7001  Format(1X,'" T0=',f7.1,' "')
WRITE(IU,7000)(ANGCEN(I,MP),I=1,9),(EMEAN(II),II=1,5)
7000  FORMAT(1X,5X,'"E"',6X,'"NEQ"',5X,'"EQ"',6X,'"TOT"',1X,
# 9(2X,'"','F5.1','ø'''), 2X,'" TETA "', 5(2X,'"','F6.1',''''))
DO 50 I=1,NSTE
IF(I.GT.20)WRITE(IU,5000)(PRITMP(I,NN),NN=1,19)
5000  FORMAT(1X,1PE10.2,18E10.2)

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      IF(I.EQ.1)WRITE(IU,5001)(PRITMP(I,NN),NN=1,19),ITYP(MP)
5001  FORMAT(1X,1PE10.2,18E10.2,'  EMITTED PARTICLE: ',A8)
      IF(I.EQ.2)WRITE(IU,5002)(PRITMP(I,NN),NN=1,19)
5002  FORMAT(1X,1PE10.2,18E10.2,'  "A": ENERGY FOR COLUMNS "B"- "M"  ')
      IF(I.EQ.3)WRITE(IU,5003)(PRITMP(I,NN),NN=1,19)
5003  FORMAT(1X,1PE10.2,18E10.2,'  "B":DS/DE(PRE), "C":(EQ), "D":(TOT)')
      IF(I.EQ.4)WRITE(IU,5004)(PRITMP(I,NN),NN=1,19)
5004  FORMAT(1X,1PE10.2,18E10.2,'  "E"- "M": D2S/DEXDO')
      IF(I.EQ.5)WRITE(IU,5005)(PRITMP(I,NN),NN=1,19),ANGCEN(1,MP)
5005  FORMAT(1X,1PE10.2,18E10.2,'  "E":',0PF6.1)
      IF(I.EQ.6)WRITE(IU,5006)(PRITMP(I,NN),NN=1,19),ANGCEN(2,MP)
5006  FORMAT(1X,1PE10.2,18E10.2,'  "F":',0PF6.1)
      IF(I.EQ.7)WRITE(IU,5007)(PRITMP(I,NN),NN=1,19),ANGCEN(3,MP)
5007  FORMAT(1X,1PE10.2,18E10.2,'  "G":',0PF6.1)
      IF(I.EQ.8)WRITE(IU,5008)(PRITMP(I,NN),NN=1,19),ANGCEN(4,MP)
5008  FORMAT(1X,1PE10.2,18E10.2,'  "H":',0PF6.1)
      IF(I.EQ.9)WRITE(IU,5009)(PRITMP(I,NN),NN=1,19),ANGCEN(5,MP)
5009  FORMAT(1X,1PE10.2,18E10.2,'  "I":',0PF6.1)
      IF(I.EQ.10)WRITE(IU,5010)(PRITMP(I,NN),NN=1,19),ANGCEN(6,MP)
5010  FORMAT(1X,1PE10.2,18E10.2,'  "J":',0PF6.1)
      IF(I.EQ.11)WRITE(IU,5011)(PRITMP(I,NN),NN=1,19),ANGCEN(7,MP)
5011  FORMAT(1X,1PE10.2,18E10.2,'  "K":',0PF6.1)
      IF(I.EQ.12)WRITE(IU,5012)(PRITMP(I,NN),NN=1,19),ANGCEN(8,MP)
5012  FORMAT(1X,1PE10.2,18E10.2,'  "L":',0PF6.1)
      IF(I.EQ.13)WRITE(IU,5013)(PRITMP(I,NN),NN=1,19),ANGCEN(9,MP)
5013  FORMAT(1X,1PE10.2,18E10.2,'  "M":',0PF6.1)
      IF(I.EQ.14)WRITE(IU,5014)(PRITMP(I,NN),NN=1,19)
5014  FORMAT(1X,1PE10.2,18E10.2,'  "N"- "S": D2S/DEXDO FOR E1-E2')
      IF(I.EQ.15)WRITE(IU,5015)(PRITMP(I,NN),NN=1,19)
5015  FORMAT(1X,1PE10.2,18E10.2,'  "N": ANGLES FOR COLUMNS "O"- "S"  ')
      IF(I.EQ.16)WRITE(IU,5016)(PRITMP(I,NN),NN=1,19),EOUT1(1,MP),
+
      EOUT2(1,MP)
5016  FORMAT(1X,1PE10.2,18E10.2,'  "O":',0PF7.1,'-',F7.1,'  EEV')
      IF(I.EQ.17)WRITE(IU,5017)(PRITMP(I,NN),NN=1,19),EOUT1(2,MP),
+
      EOUT2(2,MP)
5017  FORMAT(1X,1PE10.2,18E10.2,'  "P":',0PF7.1,'-',F7.1,'  MEV')
      IF(I.EQ.18)WRITE(IU,5018)(PRITMP(I,NN),NN=1,19),EOUT1(3,MP),
+
      EOUT2(3,MP)
5018  FORMAT(1X,1PE10.2,18E10.2,'  "Q":',0PF7.1,'-',F7.1,'  MEV')
      IF(I.EQ.19)WRITE(IU,5019)(PRITMP(I,NN),NN=1,19),EOUT1(4,MP),
+
      EOUT2(4,MP)
5019  FORMAT(1X,1PE10.2,18E10.2,'  "R":',0PF7.1,'-',F7.1,'  MEV')
      IF(I.EQ.20)WRITE(IU,5020)(PRITMP(I,NN),NN=1,19),EOUT1(5,MP),
+
      EOUT2(5,MP)
5020  FORMAT(1X,1PE10.2,18E10.2,'  "S":',0PF7.1,'-',F7.1,'  MEV')
50   CONTINUE
C
C*****
221  FORMAT(/72('=')/1X,10X,'EMISSION SPECTRA FOR ',A8,
+ 'S (MB/MEV...)' )
222  FORMAT(/72('=')/1X,10X,'EMISSION SPECTRA FOR ALPHA-PARTICLE',
+ 'S (MB/MEV...)' )
777  FORMAT(/1X,10X,'TOTAL ANGULAR DISTRIBUTION FOR ENERGY RANGE:'/1X,
+ 2X,'EOUT1=',F6.1,2X,'EOUT2=',F6.1)
888  FORMAT(/1X,A8,': ', 'INCLUSIVE SPECTRUM FOR ANGLE ',
+ F6.1,' +/- ',F6.1)
      RETURN
      END
*****

```

```

*                SUBROUTINE PROZR                *
*****
      SUBROUTINE PROZR(TP,TT,JIN,KEY,M)
C Sub-barrier proton penetration
      COMMON/DAINT/PF(33,4),RO1(33),RZON(33),FIG
      COMMON/TFERMI/TF(34,4) /RNUCL/RNUCL /K/KF
      COMMON/URAND1/IYG
      KEY=0
      T=TP-TF(JIN,M)+TF(KF+1,M)
      IF(T.LE.0.)RETURN
      B=TT-TF(JIN,M)+TF(KF+1,M)
      STB=SQRT(T/B)
      GAMMA = ( ACOS(STB)/STB ) - SQRT(1.-T/B)
      G = -2.*RNUCL/(4.5/SQRT(B))
      D=EXP(G*GAMMA)
      O=RANDOM(0)
      IF(O.LE.D) KEY=1
      RETURN
      END
*****
*                SUBROUTINE QBOND                *
*****
      SUBROUTINE QBOND(EXCIT,WIDTH,TAUX,KEY)
      DOUBLE PRECISION UCLA,RELX
      COMMON/BOND1/QBON(200,200,6)
      COMMON/EVAMAS/NEVAN,NEVAD,NEVAT,NEVAHE,NEVAAL
      COMMON/INTTR1/PWX,PWY,PWZ,TW,NPREN,NPREP,NPREA
      COMMON/INIQBO/Z,CKA,CKB,RPA,RPB,RALA,RALB
      COMMON/I1988/I1988 /QBOCFU/NSUMN,NSUMP
      COMMON/MAX/MAXNEU,MAXPRO /AN/AN
      COMMON/LAB4/UCLA(6,2000) /INCR/ED
      DIMENSION RELX(6),WIDTH(6),TAUX(6)
      KEY=0
      NSUMN=1+NPREN+NEVAN+NEVAD+2*NEVAT+NEVAHE+2*(NEVAAL+NPREA)
      NSUMP=1+NPREP+NEVAP+NEVAD+NEVAT+2*NEVAHE+2*(NEVAAL+NPREA)
      IF(NSUMN.GT.MAXNEU.OR.NSUMP.GT.MAXPRO)GOTO 100
C
C 1-N, 2-P, 3-D, 4-T, 5-HE3, 6-A
C QN =QBON( , ,1)  QP=QBON( , ,2)  QD=QBON( , ,3)
C QT =QBON( , ,4)  QHE=QBON( , ,5)  QAL=QBON( , ,6)
C
      DO 1 K = 1,6
      RELX(K) = 0.0
      TAUX(K) = EXCIT - QBON(NSUMN,NSUMP,K)
      IX =INT(TAUX(K)/ED+1.)
C to avoid overloading
      IF(IX.gt.2000) IX = 2000
      IF(IX.lt.1) goto 1
      RELX(K) = UCLA(K,IX)
1    CONTINUE
      DO 2 K=2,6
2    RELX(K) = RELX(K-1)+RELX(K)
      IF(RELX(6).eq.0.D+00) RETURN
      KEY = 1
C normalize on 1
      DO 3 K=1,6
C "+1.E-04" is to avoid cycling
3    WIDTH(K) = (RELX(K)/RELX(6)) + 1.D-04
      RETURN

```

```

100  I1988=I1988+1
      RETURN
      END
*****
*                SUBROUTINE QUES                *
*****
      SUBROUTINE QUES(RORM,T,W,JIN,M,IGEN)
      COMMON/TFERMI/TF(34,4) /RNUCL/RNUCL  COMMON/R001/R001
      COMMON/MASTR1/WN(21,21) /DATINI/RA,T0,W0
      COMMON/DAINT/PF(33,4),RO1(33),RZON(33),FIG
      COMMON/DATTR1/QNN,QPP /MPARIN/MPARIN/K/KF
C
      no check ?
      IF(M.EQ.3) goto 3
C Asymptotic energy must be lower than EMAX
      TA=T+TF(KF+1,M)-TF(JIN,M)
      IF(M.EQ.1.AND.MPARIN.EQ.1) EMAX = T0
      IF(M.EQ.1.AND.MPARIN.EQ.2) EMAX = T0 + QPP - QNN
      IF(M.EQ.2.AND.MPARIN.EQ.1) EMAX = T0 + QNN - QPP
      IF(M.EQ.2.AND.MPARIN.EQ.2) EMAX = T0
      IF(TA.LE.EMAX) GOTO 3
      IGEN=1
      RETURN
3
      TX=T-TF(JIN,M)+TF(JIN+1,M)
      IF(TX.LT.0.0) RETURN
      PX=SQRT(TX*(TX+2.*W))
      IF(RORM.GT.(PX*RZON(JIN))) IGEN=1
      IF(IGEN.EQ.1)R001=R001+1.
      RETURN
      END
*****
*                FUNCTION RANDOM                *
*****
      FUNCTION RANDOM(NO ARGUMENTS)
*
* random number generator
*
**** GNU Fortran pseudo random generator:
****
****
****      RANDOM=RAND(0)
**
**
** WATCOM Fortram pseudo random number generator
** generator is initialized in Subroutine OPTIONS
**
      Common/urand1/iyg
      RANDOM=URAND(iyg)
**
      Return
      End
*****
*                SUBROUTINE REGR1                *
*****
      SUBROUTINE REGR1(X1,X2,Y1,Y2,A,B)
      RR=X2-X1
      A=(Y2-Y1)/RR
      B=(Y1*X2-X1*Y2)/RR
      RETURN
      END

```

```

*****
*                               SUBROUTINE SCILSK                               *
*****
      SUBROUTINE SCILSK(I,G,T1,W1,IGEN,M1)
      COMMON/PARTIC/WP,PX,PY,PZ,P,T,E,X,Y,Z,R,JIN,M
      COMMON/ACTSCI/PIN1,PIN2,PIN3,WPX,RK3,RK4,GAMMA,SK2,VC2,VCX,
+VCY,VCZ,MPX
      COMMON/SCIMEM/WPM,PXM,PYM,PZM,PM,TM,EM,XM,YM,ZM,RM,JINM,MM
      COMMON/IMOM/IMOM
      IF(G)1,1,2
1   RK=RK4-(GAMMA-1.)*SK2/VC2
      GOTO 3
2   RK=RK3+(GAMMA-1.)*SK2/VC2
3   IF(I)4,4,50
4   PX5=G*PIN1+RK*VCX
      PY5=G*PIN2+RK*VCY
      PZ5=G*PIN3+RK*VCZ
      P5=SQRT(PX5*PX5+PY5*PY5+PZ5*PZ5)
      T5=T1
      IF(IMOM.EQ.0)GOTO 21
      RORM=ORBIT(PX5,PY5,PZ5,X,Y,Z)
      CALL QUES(RORM,T5,W1,JIN,M1,IGEN)
      IF(IGEN.EQ.1)RETURN
21  PX=PX5
      PY=PY5
      PZ=PZ5
      P=P5
      T=T5
      WP=W1
      E=T+W1
      M=M1
      RETURN
50  PX5=-PIN1+RK*VCX
      PY5=-PIN2+RK*VCY
      PZ5=-PIN3+RK*VCZ
      P5=SQRT(PX5*PX5+PY5*PY5+PZ5*PZ5)
      T5=T1
      IF(IMOM.EQ.0)GOTO 121
      RORM=ORBIT(PX5,PY5,PZ5,X,Y,Z)
      CALL QUES(RORM,T5,W1,JIN,MPX,IGEN)
      IF(IGEN.EQ.1)RETURN
121 PXM=PX5
      PYM=PY5
      PZM=PZ5
      PM=P5
      TM=T5
      WPM=W1
      EM=T1+W1
      XM=X
      YM=Y
      ZM=Z
      RM=R
      JINM=JIN
      MM=MPX
      RETURN
      END
*****
*                               SUBROUTINE SIGICH                               *
*****

```

```

SUBROUTINE SIGICH(ZEFF,AEFF)
COMMON/LAB3/SIG(6,2000)/DATREN/RL0N,RL1N,RM0N,RM1N,RN0N,RN1N,RN2N
COMMON/DATREP/POP,P1P,P2P,RL0P,RL1P,RM0P,RM1P,RN0P,RN1P,RN2P
COMMON/DATREA/POA,P1A,P2A,RL0A,RL1A,RM0A,RM1A,RN0A,RN1A,RN2A
COMMON/INCR/ED
* IPAR =0 Chatterjee compilation, =1 Blann inverse cross-section
* IPARR=0 minimum printing
  IPAR=0
  IPARR=0
C 1-N, 2-P, 3-D, 4-T, 5-HE3, 6-A
  2 IF(IPAR.EQ.1)WRITE(8,290)
  DO 6 I=1,2000
  DO 6 K=1,6
  6 SIG(K,I)=0.
C NEUTRON
  AN=AEFF-1.
  AN13=AN**0.333333333
  AN23=AN13*AN13
  RL11N=(RL0N/AN13+RL1N)
  RM11N=RM0N*AN13+RM1N*AN23
  RN11N=(RN0N*AN23*AN23+RN1N*AN23+RN2N)
C PROTON
  AP=AEFF-1.
  ZP=ZEFF-1.
  ECOP=1.44*ZP/(1.5*(AP**0.333333333))
  EC2=ECOP*ECOP
  AM=AP**RM1P
  P11P=POP+P1P/ECOP+P2P/EC2
  RL11P=RL0P*AP+RL1P
  RM11P=RM0P*AM
  RN11P=AM*(RN0P+RN1P*ECOP+RN2P*EC2)
C ALPHA
  AA=AEFF-4.
  ZA=ZEFF-2.
  ECOA=2.88*ZA/(1.5*(AA**0.333333333)+1.2)
  EC2=ECOA*ECOA
  AM=AA**RM1A
  P11A=POA+P1A/ECOA+P2A/EC2
  RL11A=RL0A*AA+RL1A
  RM11A=RM0A*AM
  RN11A=AM*(RN0A+RN1A*ECOA+RN2A*EC2)
  RP=1.21*((AEFF-1.)**.3333+1.)
  RD=1.21*((AEFF-2.)**.3333+1.260)
  RA=1.21*((AEFF-4.)**.3333+1.587)
  CONRP=31.42*RP*RP
  CONRA=31.42*RA*RA
  CONRD=31.42*RD*RD
  VD=(ZEFF-1.)*1.32/(RD+1.6)
C
  IF(IPAR.EQ.0) CALL COULCH(VP,VA,IPAR,AEFF,ZEFF,
+P11P,RL11P,RM11P,RN11P,ECOP,P11A,RL11A,RM11A,RN11A,ECOA)
  IF(IPAR.EQ.1)VP=(ZEFF-1.)*1.15/(RP+1.6)
  IF(IPAR.EQ.1)VA=(ZEFF-2.)*2.64/(RA+1.6)
  RMP=1.-1./AEFF
  RMD=3.-6./AEFF
  RMT=3.-9./AEFF
  RMH=3.-9./AEFF
  RMA=2.-8./AEFF
C •EPEHOPM^POBKA CE-EH% „<ÿ HE%TPOHOB •P^ •HEPf^^ < 1 M•B

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```

RCH=1.
IF(IPAR.EQ.0) RCH = ( RL11N+RM11N+RN11N ) /
+ ( 31.42*(RP+3.4/SQRT(1.+5))**2 )
DO 10 IK=1,2000
EI=FLOAT(IK)*ED-ED/2.
E1=EI
IF(E1.GT.50.)E1=50.
C N
IF(IPAR.EQ.1)SIG(1,IK)=31.42*(RP+3.4/SQRT(EI+5))**2
IF(IPAR.EQ.0.AND.EI.GE.1.)SIG(1,IK)=RL11N*E1+RM11N+RN11N/E1
IF(IPAR.EQ.0.AND.EI.LT.1.)SIG(1,IK)=
+ RCH * ( 31.42*(RP+3.4/SQRT(EI+5))**2 )
IF(SIG(1,IK).LT.0.)IPAR=1
IF(SIG(1,IK).LT.0.)GOTO 2
C D
IF(VD.GE.EI) GO TO 11
SIG(3,IK) = CONRD*(1.-VD/EI)
C P
11 IF(VP.GE.EI)GO TO 10
IF(IPAR.EQ.1)SIG(2,IK)=CONRP*(1.-VP/EI)
EKSI=AMAX1(E1,ECOP)
IF(IPAR.EQ.0)SIG(2,IK)=
+P11P*((E1-EKSI)**2)+RL11P*E1+RM11P+RN11P*(2.-E1/EKSI)/EKSI
IF(SIG(2,IK).LT.0.)IPAR=1
IF(SIG(2,IK).LT.0.)GOTO 2
C A
IF(VA.GE.EI) GO TO 10
IF(IPAR.EQ.1)SIG(6,IK)=CONRA*(1.-VA/EI)
EKSI=AMAX1(E1,EOA)
IF(IPAR.EQ.0)SIG(6,IK)=
+P11A*((E1-EKSI)**2)+RL11A*E1+RM11A+RN11A*(2.-E1/EKSI)/EKSI
IF(SIG(6,IK).LT.0.)IPAR=1
IF(SIG(6,IK).LT.0.)GOTO 2
10 CONTINUE
C D=T, HE3 = A
DO 20 IK=1,2000
SIG(4,IK)=SIG(3,IK)
20 SIG(5,IK)=SIG(6,IK)
IF(IPARR.eq.0) goto 151
DO 150 K=1,6
GO TO (201,202,203,204,205,206),K
201 WRITE(7,211) RCH
211 FORMAT(/,38X,'CHAT-BLANN NEUTRON INVERSE CROSS SECTIONS'
+, ' ( ',G12.5,' )'/)
GO TO 135
202 WRITE(7,222)
222 FORMAT(/,38X,'CHATTERJEE PROTON INVERSE CROSS SECTIONS'/)
GO TO 135
203 WRITE(7,233)
233 FORMAT(/,37X,'SHARP CUTOFF DEUTERON INVERSE CROSS SECTIONS'/)
GO TO 135
204 WRITE(7,244)
244 FORMAT(/,37X,'SHARP CUTOFF TRITON=D INVERSE CROSS SECTIONS'/)
GO TO 135
205 WRITE(7,255)
255 FORMAT(/,37X,'CHATTERJEE HE3=ALPHA INVERSE CROSS SECTIONS'/)
GO TO 135
206 WRITE(7,266)
266 FORMAT(/,39X,'CHATTERJEE ALPHA INVERSE CROSS SECTIONS'/)

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135 WRITE(7,145) (SIG(K,JE),JE=1,2000)
145 FORMAT ( 1H ,10F7.0)
150 CONTINUE
151 DO 200 K=1,2000
    EI=(FLOAT(K)*ED-ED/2.)*ED
    SIG(1,K)=SIG(1,K)*EI*RMP
    SIG(2,K)=SIG(2,K)*EI*RMP
    SIG(3,K)=SIG(3,K)*EI*RMD
    SIG(4,K)=SIG(4,K)*EI*RMT
    SIG(5,K)=SIG(5,K)*EI*RMH
200  SIG(6,K)=SIG(6,K)*EI*RMA
    RETURN
290 FORMAT(1X,'FOR Z TREATED BLANN SHARP CUTOFF APPROX. IS USED')
    END
*****
*                               FUNCTION SIGION                               *
*****
    FUNCTION SIGION(ISS,A1,Z1,A2,Z2,T)
C Written by Barashenkov, Polanski
C   FOR CALCULATION OF NUCLEUS-NUCLEUS TOTAL(ISS=1)
C   AND INELASTIC(ISS=2) CROSS SECTIONS
C   A1,Z1 - PROJECTILE MASS AND CHARGE NUMBERS (A1>1)
C   A2,Z2 - THE SAME FOR TARGET NUCLEUS(3<A2<240)
C   T - LAB. KINETIC ENERGY OF PROGECTALE (1 MEV/NUCLEON< T <1 TEV/NUCLEON)
COMMON /CX/CX(38)
COMMON /FH/AMP,AMT,AP,AT,B0,R0
IS=3-ISS
IF(IS.LE.0) RETURN
IF(A1.LT.1.0.OR.A1.GT.240.0.OR.A2.LT.3.0.OR.A2.GT.240.) GO TO 101
IF(ABS(Z1).LT.1.0) GO TO 101
IF(T.LT.1.0) GO TO 101
SIGION=0.
TP=T/A1
AP=A1**0.333333
AT=A2**0.333333
AMP=A1*930.63
AMT=A2*930.63
C   PARAMETER FOR CALCULATION OF NUCLEAR RADIUS
R0=1.4
IF(ABS(A1-4.) .LT. 0.1) R0=1.3
B0=1.44*Z1*Z2
I=1
    IF(IS.EQ.2) I=20
C   SELECTION OF PROJECTILE
C   HEAVY ION
    IF(A1.GT.4.1) N=I
C   ALFA,HELION,TRITON
    IF(A1.GT.2.1 .AND. A1.LT.4.1) N=I+6
C   DEUTERON
    IF(A1.LT.2.1) N=I+12
C   HIGH-ENERGY CROSS-SECTION
C   SELECTION OF PROJECTILE ENERGY
    IF(TP.LT.CX(N+1)) K=2
    IF(TP.LT.CX(N+4)) K=5
C   CROSS-SECTION PARAMETERS
C=CX(I)
    IF(TP.LT.CX(N+1)) C=CX(N+K)+CX(N+K+1)*LOG10(TP)
    CP=CX(N+5)+CX(N+6)
    IF(TP.LT.10.) GO TO 1

```



```

C      HIGH-ENERGY CROSS-SECTION
      SIGION=FHS(IS,T,C)
      RETURN
C      CALCULATION OF LOW-ENERGY CROSS-SECTION
C      NORMALIZATION OF HIGH-ENERGY CROSS-SECTION
1      SH10=FHS(IS,10.*A1,CP)
      R0=1.45
      IF(ABS(A1-4.).LT. 0.1) R0=1.4
C      RENORMALIZED COULOMB BARRIER
      B=B0/R0/(AP+AT)
C      LOW-ENERGY CROSS-SECTION
      SIGION=SH10*FC(T,B)/FC(10.*A1,B)
      IF(SIGION) 101,100,100
101   WRITE(6,1001)
1001  FORMAT(' ERROR IN INPUT OF PARAMETERS OF FUNCTION SIGION')
100   CONTINUE
      RETURN
      END
*****
*               SUBROUTINE STEP93               *
*****
C Histograms
      SUBROUTINE STEP93(E,CS,ND1,ERES,CSRES,ND2,JMAX,LL)
C If LL = 1 - energy distributions
C   LL = 2 - angular distributions
C ND2 must be < 150
      DIMENSION E(ND1),CS(ND1),ERES(ND2),CSRES(ND2)
      N = ND1
      N1 = N - 1
      ERES(1) = E(1)
      CSRES(1) = CS(1)
                                     J=2
      DO 300 I=1,N1
      GOTO(1,2),LL
1      ERES(J) = E(I)
      CSRES(J) = CS(I+1)
          ERES(J+1) = E(I+1)
          CSRES(J+1) = CS(I+1)
      GOTO 3
2      ERES(J) = E(I+1)
      CSRES(J) = CS(I)
          ERES(J+1) = E(I+1)
          CSRES(J+1) = CS(I+1)
3      J = J+2
      IF(J.GT.150)then
          PRINT 10000
          WRITE(8,10000)
          RETURN
      endif
300   CONTINUE
      GOTO(11,22),LL
11      ERES(J) = E(N)
      CSRES(J) = 1.0E-13
      JMAX=J
      RETURN
22      JMAX=J-2
      RETURN
10000  FORMAT(1X,' STEP93: Dimension of arrays exceeded. ','
c      No histograms ')

```

```

      END
*****
*                SUBROUTINE TRANS                *
*****
      SUBROUTINE TRANS(J1,J2,ITR9)
      COMMON/PARTIC/WP,PX,PY,PZ,P,T,E,X,Y,Z,R,JIN,M
      COMMON/R003/R003 /R008/R008 /NREJ/REFR,NREJ
      ITR9=0

      T7=T
      CALL CROZON(J1,J2,WP,P1,T7,M)
      QCOS=(PX*X+PY*Y+PZ*Z)/(P*R)
      QSIN=SQRT(ABS(1.-QCOS*QCOS))
      QSIN1=QSIN*P/P1
      IF(QSIN1-1.)20,10,10
C Reflection
      10 RK1=-2.*P*QCOS/R
      R003=R003+1.
      R008=R008+1.
      IF(R008.GT.REFR) THEN
          ITR9=1
          RETURN
      ENDIF

      GOTO 30
      20 J1=J2
      T=T7
          RK1=0.
      If(QCOS.ne.0.0)RK1=((P1*QCOS/ABS(QCOS))*SQRT(ABS(1.-QSIN1**2))-
      *P*QCOS)/R
      P=P1
      30    PX=PX+X*RK1
          PY=PY+Y*RK1
          PZ=PZ+Z*RK1
      RETURN
      END
*****
*                SUBROUTINE TREAT1                *
*****
      SUBROUTINE TREAT1
      COMMON/MASTR1/WN(21,21) /DATINI/RA,T0,W0
      COMMON/INTTR1/PWX,PWY,PWZ,TW,NPREN,NPREP,NPREA
      COMMON/TRLEVA/EXCIT,WMAI /TR1TR2/VAICX,VAICY,VAICZ
      COMMON/QSUM/QSUM /URAND1/IYG
      COMMON/QNNN/QNNN /MAIIPR/IPR /INF001/INFKAL
      N1 = NPREN + 2*NPREA + 1
      N2 = NPREP + 2*NPREA + 1
      IF(N1.GT.21.OR.N2.GT.21)GOTO 100
      WMAI=WN(N1,N2)
      PZ0=SQRT(T0*(T0+2.*W0))
C
      IF(INFKAL.EQ.1)CALL AUXANG
      EXCIT=QNNN-QSUM+
      *T0-TW-(PWX*PWX+PWY*PWY+(PWZ-PZ0)**2)/(2.*WMAI)
      VAICX=-PWX/WMAI
      VAICY=-PWY/WMAI
      VAICZ=(PZ0-PWZ)/WMAI
      RETURN
      100 WRITE(IPR,101)N1,N2
      101 FORMAT(1X,'ERROR IN SUBROUTINE TREAT1: '/1X,' N1 OR',
      +' N2 EXCEED MAXIMUM '/1X,' N1=',I5,' N2=',I5)

```

```

        STOP
        END
*****
*                SUBROUTINE TREAT2                *
*****
        SUBROUTINE TREAT2
        COMMON/TR1,TR2/V1,V2,V3 /EVATR2/W,VX,VY,VZ /MAI,IPR/IPR
        COMMON/TR2CFU/RECOIL /INFDIS/INFDIS,INFOUP(3)
        COMMON/EMEM91/EMEMT(21),RMEMT(21),HMEMT
        COMMON/LIB91/WINLIB(100,250),INFLIB
C
        IF(INFLIB.EQ.1) CALL LIBGEN
        RECOIL=W*0.5*((V1+VX)**2+(V2+VY)**2+(V3+VZ)**2)
        IF(INFDIS.EQ.0)RETURN
C Recoil spectrum
        DO 10 NU=1,21
        IF(RECOIL.LE.EMEMT(NU))GOTO 50
10 CONTINUE
        WRITE(IPR,20)RECOIL
20     FORMAT(1X,' CONTROL SUBR TREAT2. RECOIL=',G12.5)
        RETURN
50 RMEMT(NU)=RMEMT(NU)+1.
        RETURN
        END
*****
*                FUNCTION VELOC                *
*****
        FUNCTION VELOC(WPAR,W0,E)
        VELOC=SQRT(2.*WPAR*E/(W0*(W0+WPAR)))
        RETURN
        END
*****
*                SUBROUTINE WERO                *
*****
        SUBROUTINE WERO(PFM,PP,MX)
        COMMON/BOND1/QBON(200,200,6)
        COMMON/URAND1/IYG
        GOTO(1,1,3,4),MX
C
C NEUTRON, PROTON
1 IPOWER = 2
PFMAX = PFM**IPOWER
C
10 CC=RANDOM(0)
CC1=RANDOM(0)
GGG=PFM*CC
IF( (GGG**IPOWER) - PFMAX*CC1 )10,20,20
20 PP=GGG
RETURN
C
C ALPHA-PARTICLE
3 IPOWER = 8
PFMAX = PFM**IPOWER
100 CC=RANDOM(0)
CC1=RANDOM(0)
GGG=PFM*CC
IF( (GGG**IPOWER) - PFMAX*CC1 )100,200,200
200 PP=GGG
RETURN

```

```

C
C TRITON, HE-3
4      IPOWER = 6
      PFMAX = PFM**IPOWER
1000   CC=RANDOM(0)
      CCL=RANDOM(0)
      GGG=PFM*CC
      IF( (GGG**IPOWER) - PFMAX*CCL )1000,2000,2000
2000   PP=GGG
      RETURN
      END
*****
*                FUNCTION WM                *
*****
      FUNCTION WM(M)
C  1 - N
C  2 - P
C  3 - A
C  4 - T, HE3
C  5 - D
      WM=938.2796
      GOTO(1,2,3,4,5),M
1      WM=939.5731
      RETURN
2      WM=938.2796
      RETURN
3      WM=3726.
      RETURN
4      WM=2794.5
      RETURN
5      WM=1863.
      RETURN
      END
*****
*                SUBROUTINE ZERLIB          *
*****
      SUBROUTINE ZERLIB
      COMMON/LIB91/WINLIB(100,250),INFLIB
      DO 1 I=1,100
      DO 1 J=1,250
1      WINLIB(I,J)=0.
      RETURN
      END
*****
*                SUBROUTINE ZERO1          *
*****
      SUBROUTINE ZERO1
      COMMON/MASOUT/WDIS(990),K1(990),K2(990),K3(990),K4(990),
+K5(990),K6(990),K7(990),K8(990),K9(990),K10(990),KN
      COMMON/NPROL/NPROL /R001/R001 /R003/R003
      COMMON/R005/R005 /IX190/IX191,IX192,IX193
      COMMON/NREJ/REFR,NREJ /AUXIL/ICOUL,ICOUL2
      COMMON/SUM90/ER90,KER90
      COMMON/INFSEP/KSEP(100,4),INFSEP,JSEPM
      DO 10 I=1,990
      WDIS(I)=0.
      K1(I)=0
      K2(I)=0
      K3(I)=0

```

```

      K4(I)=0
      K5(I)=0
      K6(I)=0
      K7(I)=0
      K8(I)=0
      K9(I)=0
10   K10(I)=0
      KN=0
      NPROL=0
      R001=0.
      R003=0.
      R005=0.
      IX191=0
      IX192=0
      IX193=0
      NREJ=0
      ICOU1=0
      ICOU2=0
      ER90=0.
      KER90=0
      DO 100 I=1,100
100  KSEP(I,4)=0
      RETURN
      END
*****
*                SUBROUTINE ZERO2                *
*****
      SUBROUTINE ZERO2
      COMMON/INTTR1/PWX,PWY,PWZ,TW,NPREN,NPREP,NPREA
      COMMON/EVATR2/WEIG,VX,VY,VZ /EVAMAS/N1,N2,N3,N4,N5,N6
      COMMON/JACT/JACT /NDIM/NPAR /MEMORY/U(11,20),MU(2,20) /R008/R008
      COMMON/IZET/IZET /QSUM/QSUM /QBOCFU/NSN,NSP
      PWX=0.
      PWY=0.
      PWZ=0.
      TW=0.
      VX=0.
      VY=0.
      VZ=0.
      NPREN=0
      NPREP=0
      NPREA=0
      NSN=0
      NSP=0
      N1=0
      N2=0
      N3=0
      N4=0
      N5=0
      N6=0
      JACT=0
      DO 2 I=1,11
      DO 1 J=1,20
1   U(I,J)=0.
2  CONTINUE
      DO 3 I=1,20
      MU(1,I)=0
3  MU(2,I)=0
      NPAR=0

```

```

R008=0.
IZET=0
QSUM=0.
RETURN
END
*****
*                SUBROUTINE ZONWAY                *
*****
      SUBROUTINE ZONWAY(RZJ1,RZJ0,J1,J3,J2,SLINE)
      COMMON/PARTIC/WP,PX,PY,PZ,P,T,E,X,Y,Z,R,JIN,M
      IF(R-1.E-06)2,2,8
2     SLINE=RZJ1
      RETURN
8     QCOS=(PX*X+PY*Y+PZ*Z)/(R*P)
      IF(QCOS)10,20,20
10    D1=-1.
      J2=J3
      RRJ=RZJ0
      GOTO 30
20    D1=1.
      J2=J1
      RRJ=RZJ1
30    DD=(RRJ**2)-(1.-(QCOS**2))*(R**2)
      IF(DD)50,50,70
50    CONTINUE
      OOO=RRJ-RZJ1
      IF(OOO)20,60,20
60    CONTINUE
      SLINE=0.
      RETURN
70    CONTINUE
      SLINE=-R*QCOS+D1*SQRT(DD)
      RETURN
      END

```